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# Aluminum-based ceramic/metal composites with tailored thermal expansion fabricated by spark plasma sintering

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We have devised a moderate temperature spark plasma sintering route for preparing aluminum matrix composites which possess tailored coefficients of thermal expansion (CTEs) in combination with tunable electrical and thermal conductivities. Due to its isotropic negative thermal expansion over a wide temperature range, cubic-phase  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$  ( $x = 0.0, 1.0$ ) is an ideal secondary phase for metal matrix composites with suitable CTEs. In this study, high-density  $\text{ZrW}_2\text{O}_8/\text{Al}$  and  $\text{ZrWMoO}_8/\text{Al}$  composites containing 30–70 vol% Al were fabricated using spark plasma sintering. X-ray diffraction analysis indicated that the composites were composed of a thermally-stable cubic phase at temperatures as high as 873 K for  $\text{ZrW}_2\text{O}_8$  and 773 K for  $\text{ZrWMoO}_8$ , without any orthorhombic high-pressure phase derived from the large thermal mismatch between the ceramic and metal during sintering. The thermal expansion curves of the  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites were consistent with the predictions made using the Rule-of-Mixtures. The CTEs could be controlled from negative to positive and even close to zero by simply varying the volume fraction of aluminum. Similarly, the thermal and electrical conductivity of the  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites increases with increasing Al content, which is thought to be mainly related to the contribution of the free electron conduction path of Al in the composites.

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## 1. Introduction

Aluminum matrix composites are widely used for industrial production because of aluminum's low density, easy processability, and good heat and electrical conductivity at room temperature and normal pressure. Another important aspect is that aluminum has a relatively high coefficient of thermal expansion of  $23.21 \times 10^{-6} \text{ K}^{-1}$ , which is significant compared to other metals or alloy materials (copper:  $16.6 \times 10^{-6} \text{ K}^{-1}$ , steel:  $11.5 \times 10^{-6} \text{ K}^{-1}$ , titanium:  $8.2 \times 10^{-6} \text{ K}^{-1}$ , silver:  $18.9 \times 10^{-6} \text{ K}^{-1}$ ). When Aluminum is used in combination with a thermal expansion inhibiting material, the property of having a large coefficient of thermal expansion allows for a wider adjustment of the desired coefficient of thermal expansion. At the same time, it preserves the excellent electrical and thermal conductivity of Al as much as possible. This flexibility improves the applicability of aluminum matrix composites in a variety of situations. It is, thus, anticipated that the addition of a material with a negative thermal expansion (NTE) to an aluminum matrix can help achieve precisely-matched thermal expansion

(positive, negative, or even zero) by adjusting the volume fractions of the different phases in such composites. These composites have potentially useful applications in heat sinks, thermoelectric modules, and other electronic devices.<sup>1–3</sup>

Cubic-phase  $\text{ZrW}_2\text{O}_8$  is a typical material with a negative thermal expansion, which demonstrates a large three-dimensional isotropic NTE coefficient ( $-8.8$  to  $-4.9 \times 10^{-6} \text{ K}^{-1}$ ) over a wide temperature range (0.3–1050 K).<sup>4–7</sup> These characteristics render it an ideal secondary phase for aluminum matrix composites with suitable thermal expansion coefficients. Near 443 K,  $\text{ZrW}_2\text{O}_8$  undergoes a reversible order–disorder phase transition from a low-temperature acentric cubic phase ( $\alpha\text{-ZrW}_2\text{O}_8$ :  $-8.8 \times 10^{-6} \text{ K}^{-1}$ ) to a high-temperature centric cubic phase ( $\beta\text{-ZrW}_2\text{O}_8$ :  $-4.9 \times 10^{-6} \text{ K}^{-1}$ ).<sup>6–8</sup> The abrupt change of NTE coefficient is a disadvantage in practical applications if the phase transition temperature of the materials is within the working temperature range. Numerous investigations have confirmed that the phase transition temperature of  $\text{ZrW}_2\text{O}_8$  can be adjusted through  $\text{Mo}^{6+}$  partially doping in  $\text{W}^{6+}$ , which it was reported that increasing the Mo content in  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$  leads to a lower phase transition temperature.<sup>9–13</sup> J. S. O. Evans *et al.*<sup>10</sup> reported that the  $\alpha$ – $\beta$  phase transition temperature shifted to below room temperature for  $\text{ZrWMoO}_8$  by conducting neutron powder diffraction experiments, indicating that  $\text{ZrWMoO}_8$  is also a very promising inhibitor of thermal expansion. However, due to its relatively modest thermal expansion coefficient above

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room temperature ( $-3.5 \times 10^{-6} \text{ K}^{-1}$ ), its applicability to composite materials is somewhat limited. Therefore, comparing the thermal expansion properties of composites by incorporating  $\text{ZrW}_2\text{O}_8$  and  $\text{ZrW}_2\text{MoO}_8$  separately as thermal expansion inhibitors with Al is crucial for practical applications.

In addition, low-temperature cubic phase  $\alpha\text{-ZrW}_2\text{O}_8$  transforms into an orthorhombic phase ( $\gamma\text{-ZrW}_2\text{O}_8$ ), when subjected to pressures above 0.2 GPa, with a dramatically low NTE coefficient, which decreases from  $-8.8$  to  $-1.0 \times 10^{-6} \text{ K}^{-1}$ .<sup>14–16</sup> It has been reported that  $\gamma\text{-ZrW}_2\text{O}_8$  was formed during  $\text{ZrW}_2\text{O}_8/\text{Al}$  composite sintering, wherein the cubic–orthorhombic phase transition strongly influenced the thermal properties of the composites, due to the different thermal expansion coefficients of the ceramic and metal matrix particles.<sup>1,17,18</sup> Similar phenomena were also observed in other metal matrix composites containing  $\text{ZrW}_2\text{O}_8$  particles such as  $\text{ZrW}_2\text{O}_8/\text{Cu}$ ,  $\text{ZrW}_2\text{O}_8/\text{Al-Si}$  composites.<sup>19–24</sup> The biggest disadvantage of  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites is their high sintering temperature, which causes  $\text{ZrW}_2\text{O}_8$  to decompose into  $\text{ZrO}_2$  and  $\text{WO}_3$  above 1050 K, whereas the melting point of aluminum is about 933 K.<sup>25</sup> Therefore, a low-temperature, low-pressure sintering method is needed for the fabrication of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites in order to suppress the  $\alpha$ – $\gamma$  phase transition.

Spark plasma sintering (SPS) is a promising method for bonding various kinds of solid materials (*e.g.*, metal to metal, metal-to-ceramic, *etc.*). The mechanism of SPS involves the instantaneous generation of high-temperature spark plasma in the gap due to the discharge effect between the powder particles. Throughout the SPS process, the combined effects of spark discharge (leading to the generation of spark plasma and localized spark impact pressure), Joule heating, electrodiffusion, and plastic deformation contribute to fast and efficient sintering. Our group synthesized single-phase  $\text{ZrW}_2\text{O}_8$  ceramics and  $\text{ZrW}_2\text{O}_8/\text{SiO}_2$  and  $\text{ZrW}_2\text{O}_8/\text{Cu}$  composites at 873 K and 50 MPa by using SPS.<sup>26,27</sup> Since the melting point of aluminum is about 933 K, this coincides well with the synthesis temperature of  $\text{ZrW}_2\text{O}_8$  in our past work, which facilitates a better synergy between the two materials in the composite process. In this study, dense  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ) composites containing 30 to 70 vol% Al were fabricated using SPS. We investigated the effects of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$  as thermal expansion inhibitors on the thermal expansion properties of the composites and carried out a comparison of the thermal expansion curves with predictions made using the Rule-of-Mixtures. In addition, the thermal conductivity and electrical conductivity of the  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites were evaluated to explore the application prospects of the composites.

## 2. Experimental

### 2.1 Fabrication of $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$ ( $x = 0.0, 1.0$ ) composites

$\text{ZrW}_2\text{O}_8/\text{Al}$  composites and  $\text{ZrW}_2\text{MoO}_8/\text{Al}$  composites were fabricated by spark plasma sintering method. High-purity cubic-phase  $\text{ZrW}_2\text{O}_8$  and  $\text{ZrW}_2\text{MoO}_8$  powders were synthesized using a sol–gel-hydrothermal method.<sup>28</sup> First,  $\text{ZrOCl}_2 \cdot 8\text{H}_2\text{O}$  (Kishida Chemical, Japan, 99%) was dissolved in 4 mol  $\text{L}^{-1}$  acetic acid and 2-butanol in the air for 3 hours. At the same

time,  $\text{WCl}_6$  (High Purity Chemicals, Japan, 99.99%),  $\text{MoCl}_5$  (Sigma-Aldrich, USA, 95%), were separately dissolved in ethanol under Nitrogen atmosphere. After stirring for 3 hours, the tungsten and molybdenum solutions were poured into zirconium solution for 72 hours stirring. Subsequently, the mixed solution of tungsten, molybdenum and zirconium was heated in a silicone oil bath at around 360 K. The sol–gel precursors were obtained after the solution had been completely evaporated.

The second stage is referred to as the hydrothermal stage. The obtained sol–gel precursors were dissolved in 60 mL of distilled water and after addition to a 100 mL Teflon-lined Parr bomb, placed in a mantle heater at 453 K for 18 hours with continuous stirring. The sol–gel-hydrothermal precursors were finally centrifuged, washed with distilled  $\text{H}_2\text{O}$ , and dried in an oven at 333 K. The sol–gel-hydrothermal precursors were precalcined at 873 K for  $\text{ZrW}_2\text{O}_8$  in a drying oven (DX-41, Yamato Scientific, Tokyo, Japan). Aluminum powders (Kojundo Chemical, 99.99%, Tokyo, Japan) were mixed with  $\text{ZrW}_2\text{O}_8$  and  $\text{ZrW}_2\text{MoO}_8$  powders at various volume ratios (0 vol% Al, 30 vol% Al, 50 vol% Al, 70 vol% Al, 100 vol% Al). Ethanol was added to the mixed powders, and the mixture was kneaded for 30 min in an agate mortar. After kneading, the mixed powders were placed in a drying oven at 373 K for 3 h. The mixed powders were filled in graphite dies (10 mm in diameter and 20 mm in depth) separately and wrapped in carbon sheets. An SPS apparatus (SPS-515S; Fuji Electronic Industrial, Saitama, Japan), with a pulse duration of 3.3 ms and on/off pulse intervals of 12 : 2, was used to fabricate dense  $\text{ZrW}_2\text{O}_8/\text{Al}$  and  $\text{ZrW}_2\text{MoO}_8/\text{Al}$  composites. The composites were sintered at 873 K ( $\text{ZrW}_2\text{O}_8/\text{Al}$ ) and 773 K ( $\text{ZrW}_2\text{MoO}_8/\text{Al}$ ) for 10 min at a heating rate of 100  $\text{K min}^{-1}$  to obtain  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites. During SPS, the applied pressure was held constant at 90 MPa in an argon atmosphere, until the conclusion of the sintering process. The volume contraction between the two graphite punches, namely the Z-axis linear shrinkage value, was recorded every 30 s during SPS. The Z-axis linear shrinkage curve of Al 50 vol%  $\text{ZrW}_2\text{O}_8/\text{Al}$  composite and optical photos of  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites with different Al volume fractions are shown in Fig. 1.

### 2.2 Evaluation methods

Phase identification of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ) composites was carried out using powder X-ray diffraction (Rigaku, Ultima IV, Tokyo, Japan). XRD data were collected at a scan speed of  $6^\circ \text{ min}^{-1}$ , with the  $2\theta$  ranging from  $10^\circ$  to  $80^\circ$  under 40 kV/40 mA using  $\text{Cu-K}\alpha$  radiation ( $\lambda = 0.15406 \text{ nm}$ ) employing the continuum scanning method. The morphological composition of the samples was systematically evaluated using a field-emission scanning electron microscope (HITACHI, SU8230, Tokyo, Japan) equipped with an energy-dispersive X-ray (EDX) spectrometer. The applied voltage included an accelerating voltage of 3.0 kV, and the current parameters were set to an electron beam current of 10 100 nA. The coefficients of thermal expansion of the samples were measured with a thermodynamic analyzer (Shimadzu, TMA-60/60H, Kyoto, Japan). The data were collected at a heating rate of  $1 \text{ K min}^{-1}$  from 323 to

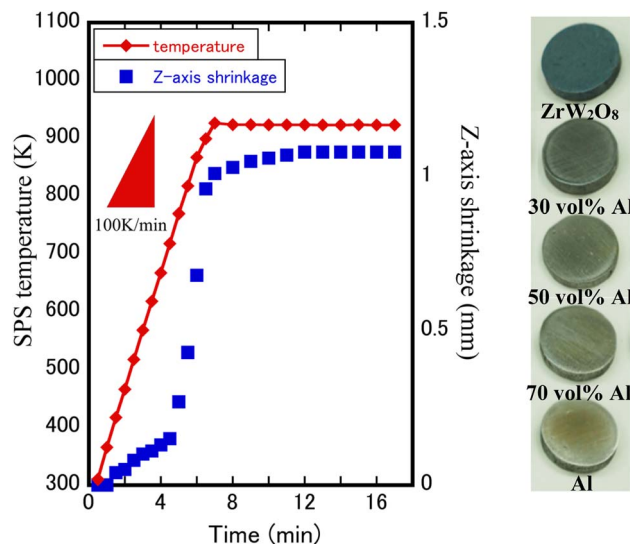


Fig. 1 Z-axis linear shrinkage curve of Al 50 vol% ZrW<sub>2</sub>O<sub>8</sub>/Al composite and optical photos of ZrW<sub>2</sub>O<sub>8</sub>/Al composites.

523 K and three replicate experiments were carried out. The theoretical CTEs of the composites were calculated using the Rule-of-Mixtures. The Rule of Mixtures (ROM) is a theoretical framework used to predict the properties of composite materials based on the volume fractions and properties of the individual components. ROM considers the matrix to be free of voids, in which each material is perfectly bonding to the matrix so that each component is distorted independently. Coefficients of thermal expansion are usually assumed to follow a linear ROM dependence on the volume fraction. The CTE values used were as follows:  $23 \times 10^{-6} \text{ K}^{-1}$  for Al,  $-8.8 \times 10^{-6} \text{ K}^{-1}$  for low-temperature cubic phase  $\alpha$ -ZrW<sub>2</sub>O<sub>8</sub>,  $-4.9 \times 10^{-6} \text{ K}^{-1}$  for high-temperature cubic phase  $\beta$ -ZrW<sub>2</sub>O<sub>8</sub>, and  $-3.5 \times 10^{-6} \text{ K}^{-1}$  for ZrW<sub>2</sub>MoO<sub>8</sub>.<sup>29</sup> The relative densities of the composites were measured by Archimedes' principle using distilled water. The specific Archimedes method steps are as follows: obtain post-sintered samples of ZrW<sub>2</sub>O<sub>8</sub>/Al and ZrW<sub>2</sub>MoO<sub>8</sub>/Al composite materials, ensuring that their surfaces are clean and free of impurities. Then, use a precision balance to weigh the mass of each sample and record the accurate mass values ( $m_1$ ). Subsequently, gently and uniformly immerse the samples in deionized water, ensuring that no bubbles adhere to the sample surfaces. Wait for stability and record the mass of the samples

when submerged in deionized water ( $m_2$ ). Calculate the relative density ( $\rho_r$ ) using the following formula:  $\rho_r = m_1 / [(m_1 - m_2) \times \rho_1]$ , where  $\rho_1$  is the density of deionized water at ambient temperature. The measured density of all specimens as well as the theoretical values have been listed in Table 1. The theoretical densities of the composites were calculated by using reference data (the density of Al is  $2.70 \text{ g cm}^{-3}$ ) based on the theoretical density of  $\alpha$ -ZrW<sub>2</sub>O<sub>8</sub> ( $\rho = 5.08 \text{ g cm}^{-3}$ ).<sup>6</sup> The measured density of all specimens exceeded 90% of the theoretical value, and that of the ZrW<sub>2-x</sub>Mo<sub>x</sub>O<sub>8</sub>/Al ( $x = 0.0, 1.0$ ) specimens were close to the estimated theoretical density. Furthermore, the relative density of the ceramic-metal composites was found to increase with the increase in metal content. The coefficients of thermal diffusion and the specific heat were measured by the conventional laser flash method using a thermal constant analyzer (ULVAC, TC7000, Kanagawa, Japan). The thermal conductivity coefficients were calculated from the experimental thermal diffusivity as well as the specific heat capacity and density values, which were measured by Archimedes' principle.

### 3. Results and discussion

#### 3.1 Fabrication of ZrW<sub>2-x</sub>Mo<sub>x</sub>O<sub>8</sub>/Al composites

Fig. 1 shows the Z-axis linear shrinkage curve of the Al 50 vol% ZrW<sub>2</sub>O<sub>8</sub>/Al composite at a sintering temperature of 873 K. In the temperature range of 300–370 K, a slight Z-axis shrinkage is observed, which may be due to the evaporation of H<sub>2</sub>O and CO<sub>3</sub><sup>2-</sup> on the surface of the pre-calcining powders. The remarkable shrinkage caused by the densification takes place at a temperature of 380 K and ends at a set temperature of 873 K. This indicates that Al and ZrW<sub>2</sub>O<sub>8</sub> fuse with each other and reach densification in this temperature interval, and the SEM images of ZrW<sub>2-x</sub>Mo<sub>x</sub>O<sub>8</sub>/Al composites shown in Fig. 3 can be observed in the mixed state of metal matrix and ceramic. The XRD patterns of ZrW<sub>2</sub>O<sub>8</sub>/Al and ZrW<sub>2</sub>MoO<sub>8</sub>/Al composites obtained after SPS sintering are shown in Fig. 2(a) and (b). All XRD patterns are similar, and the characteristic reflections of each phase were indexed to ZrW<sub>2</sub>O<sub>8</sub> and Al. The absence of some special (221, 310) reflections for  $x = 1.0$  samples is related to the occurrence of an order-disorder phase transformation, which shows variation in the space group from the low-temperature phase (space group:  $P2_13$ ) to the high-temperature phase (space group:  $Pa\bar{3}$ ). The fabrication stress during SPS and the thermal stress between ZrW<sub>2</sub>O<sub>8</sub> and Al was not high enough to

Table 1 Density and relative density values of ZrW<sub>2</sub>O<sub>8</sub>/Al and ZrW<sub>2</sub>MoO<sub>8</sub>/Al composites

Al volume fraction (vol%)	ZrW <sub>2</sub> O <sub>8</sub> /Al			ZrW <sub>2</sub> MoO <sub>8</sub> /Al		
	Density (g cm <sup>-3</sup> )	Theoretical density (g cm <sup>-3</sup> )	Relative density (%)	Density (g cm <sup>-3</sup> )	Theoretical density (g cm <sup>-3</sup> )	Relative density (%)
0	4.80	5.08	94.5	4.17	4.33	96.3
30	4.10	4.37	93.8	3.56	3.84	92.7
50	3.91	3.89	101	3.33	3.52	93.9
70	3.35	3.41	98.2	2.93	3.19	91.9
100	2.69	2.70	99.8	2.69	2.70	99.8

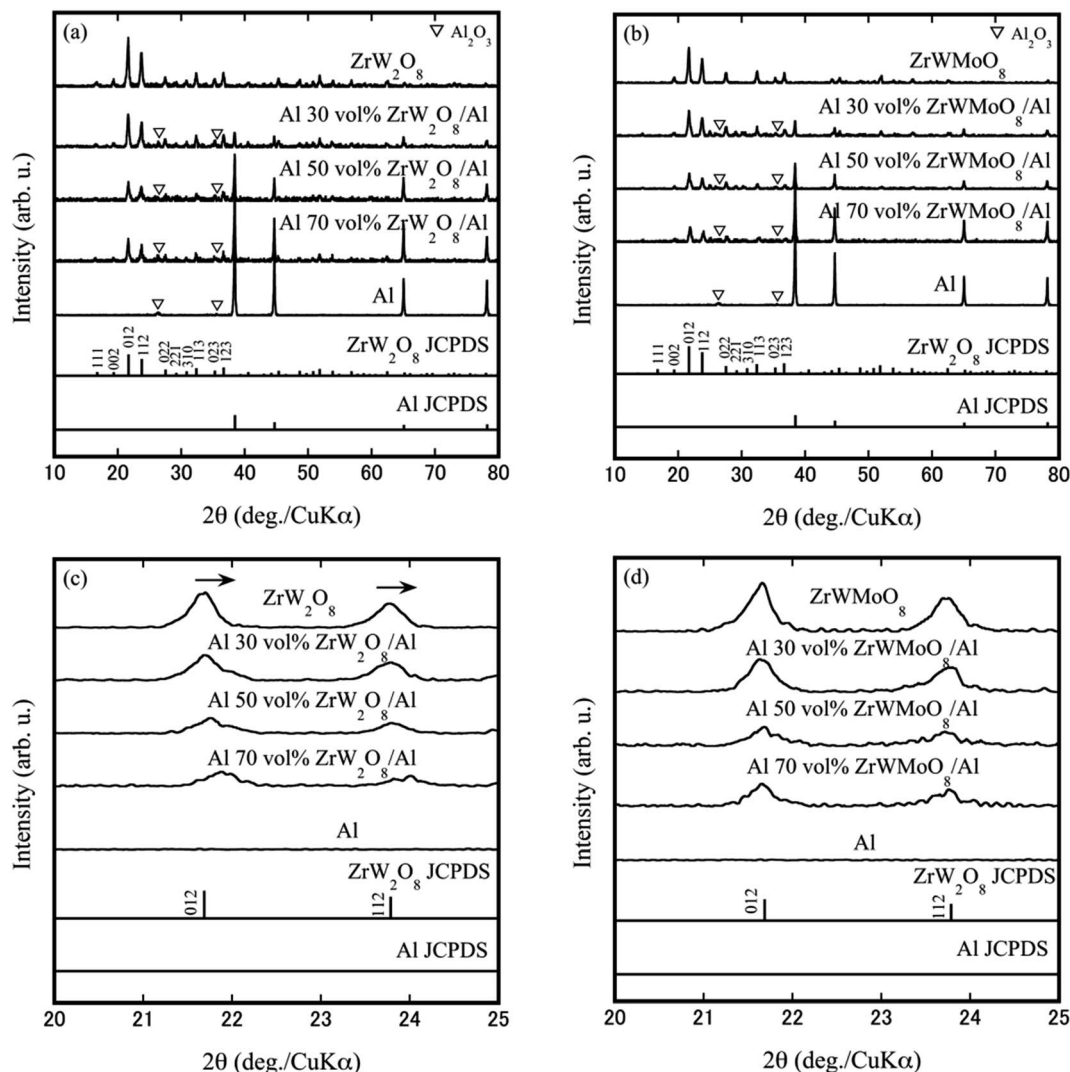


Fig. 2 XRD patterns of (a) and (c)  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites and (b) and (d)  $\text{ZrWMoO}_8/\text{Al}$  composites.

be able to induce cubic–orthorhombic phase transition, which suggests the successful fabrication of  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites without a high-pressure phase transition. However, some  $\text{Al}_2\text{O}_3$  characteristic reflections were observed due to the partial oxidation of aluminum. Fig. 2(c) and (d) correspond to the (012) and (112) reflections in Fig. 2(a) and (b), respectively. No clear reflection shift was observed in the XRD patterns of the  $\text{ZrWMoO}_8/\text{Al}$  specimens, whereas the reflections of  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens shifted to higher angles as the Al volume fraction. In addition, the full width at half maximum (FWHM) of  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens increased upon increasing the Al volume fraction. This may be due to the fact that at lower sintering temperatures,  $\text{ZrWMoO}_8$  has a relatively smaller compressive strain in the aluminum matrix than  $\text{ZrW}_2\text{O}_8$  grains, and this difference in compressive strain will be reflected in the thermal expansion results below. The crystallite size corresponding to the FWHM of certain reflections (012, 112) using the Scherrer formula was calculated. The crystallite size range for the  $\text{ZrW}_2\text{O}_8/\text{Al}$  sample is between 120 nm and 180 nm, while for the  $\text{ZrWMoO}_8/\text{Al}$

sample, it falls between 170 nm and 270 nm. A comparison reveals that the crystallites in the  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens are finer than those in the  $\text{ZrWMoO}_8/\text{Al}$  specimens.

Fig. 3(a)–(f) shows the backscattered electron images of the microstructure of the polished surface of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ). Different ceramic compositions resulted in different homogeneity of composites. Especially in the Al 70 vol%  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites, many 1  $\mu\text{m}$  to 10  $\mu\text{m}$  aggregates were observed in the  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimen, whereas in the  $\text{ZrWMoO}_8/\text{Al}$  specimen, the aggregates had sizes from 100 nm to 1  $\mu\text{m}$ , and the homogeneity of Al and  $\text{ZrWMoO}_8$  was improved. The dispersed particles were smaller in the  $\text{ZrWMoO}_8/\text{Al}$  specimens, and there was less particle agglomeration. As a result, because the specific surface area of  $\text{ZrW}_2\text{O}_8$  particles was larger than Al, the compressive stress generated from Al during cooling is expected to be larger than that in the  $\text{ZrWMoO}_8/\text{Al}$  specimens.

To better understand the dispersion of Al and  $\text{ZrW}_2\text{O}_8$  particles and the composition of each component of the





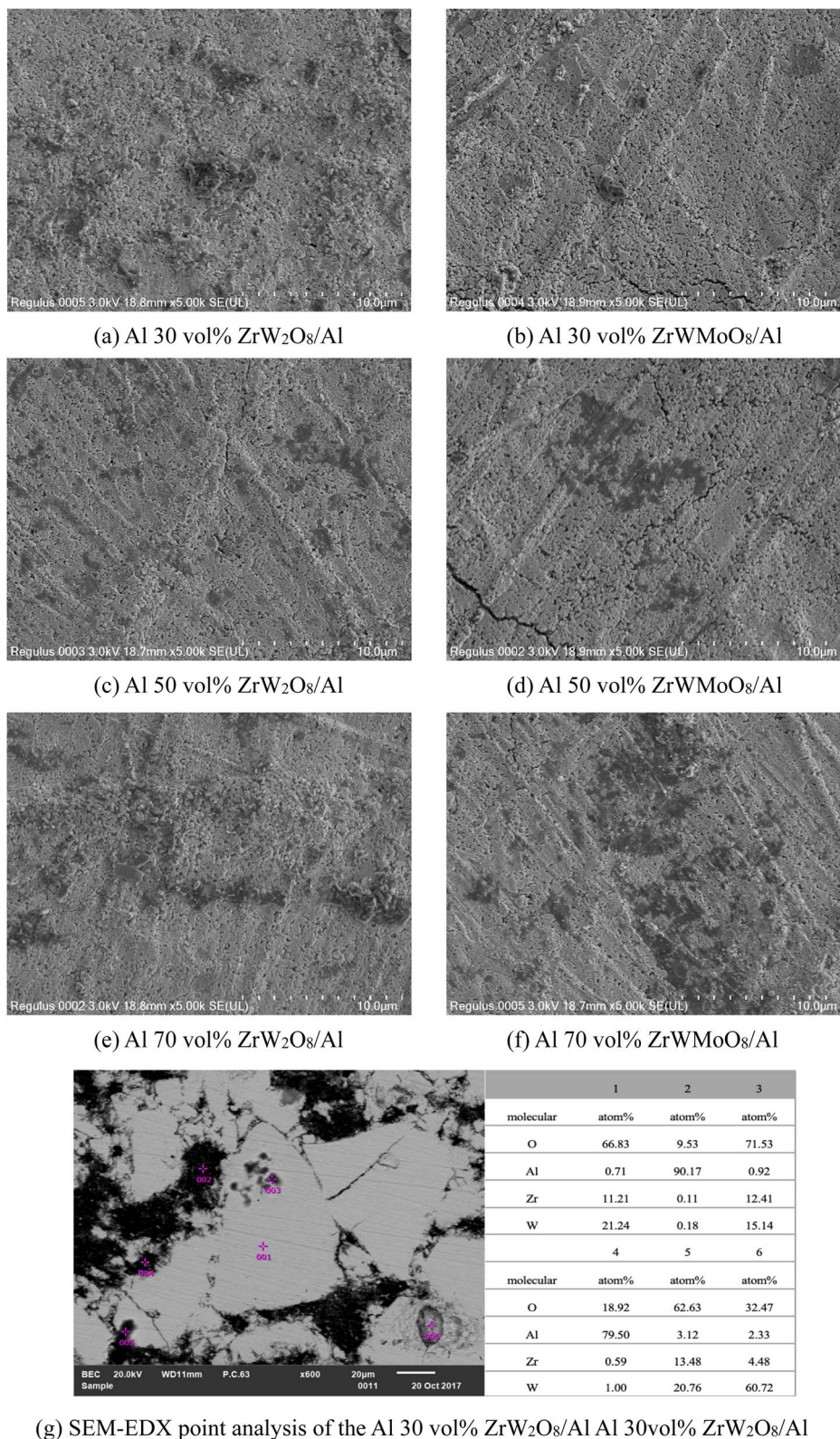


Fig. 3 (a–f) SEM images of the polished surface of ZrW<sub>2-x</sub>Mo<sub>x</sub>O<sub>8</sub>/Al ( $x = 0.0, 1.0$ ) composites; (g) SEM-EDX point analysis of the Al 30 vol% ZrW<sub>2</sub>O<sub>8</sub>/Al specimen.

composites, SEM-EDX point analysis was employed for investigating the elemental composition at six points of Al 30 vol% ZrW<sub>2</sub>O<sub>8</sub>/Al specimen (Fig. 3(g)). Point 1 seems to have ZrW<sub>2</sub>O<sub>8</sub>

as the main phase because the quantitative analysis shows that the ratio of Zr : W is about 1 : 2. Point 2 seems to have Al as the main phase, and the existence of oxygen may be related to the



oxidation of Al, but oxygen doesn't exist in a significant quantity. Al was highly oxidized at Point 4, which presumably lies near the tissue interface of Al and  $\text{ZrW}_2\text{O}_8$ . This is inevitable because the oxide-forming tendency of Al is low in comparison with other metals. The sparse black spots (Point 3 and Point 5) in the SEM image have a Zr:W ratio that deviates from 1:2. These spots may be due to impurities such as  $\text{Al}_2\text{O}_3$  that were introduced as contaminants at the time of powder production. The same applies to Point 6.

### 3.2 Thermal expansion properties of $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$ composites

The CTEs obtained from heating and cooling (three continuous repeat measurements) as a function of temperature are plotted in Fig. 4(a) and (b). For Al 50 vol%  $\text{ZrW}_2\text{O}_8/\text{Al}$  and Al 50 vol%  $\text{ZrWMoO}_8/\text{Al}$  specimens, the thermal expansion curves observed during the heating cycle increased

continuously upon increasing the temperature and showed the same trend during the cooling cycle; however, it can be observed that the thermal expansion of the  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimen during the first cycle was different from those observed during the second and third heating-cooling cycles, in which the sample could not shrink to its original length after one heating-cooling cycle. This may be related to the strain relaxation of  $\text{ZrW}_2\text{O}_8$ , in which the residual stresses resulted from the thermal mismatch between the matrix, and the ceramic distorted the sparse structure of  $\text{ZrW}_2\text{O}_8$ . Compared with the thermal expansion hysteresis behavior of  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites, in the  $\text{ZrWMoO}_8/\text{Al}$  specimens, the thermal expansion was relatively consistent after the second heating and cooling cycle, indicating that the thermal deformation of the  $\text{ZrWMoO}_8/\text{Al}$  composites was small. Another clear difference between  $\text{ZrW}_2\text{O}_8$  and  $\text{ZrWMoO}_8$  is the presence or absence of a phase transition around 410–420 K, in which a change in the slope of the thermal expansion curve near the

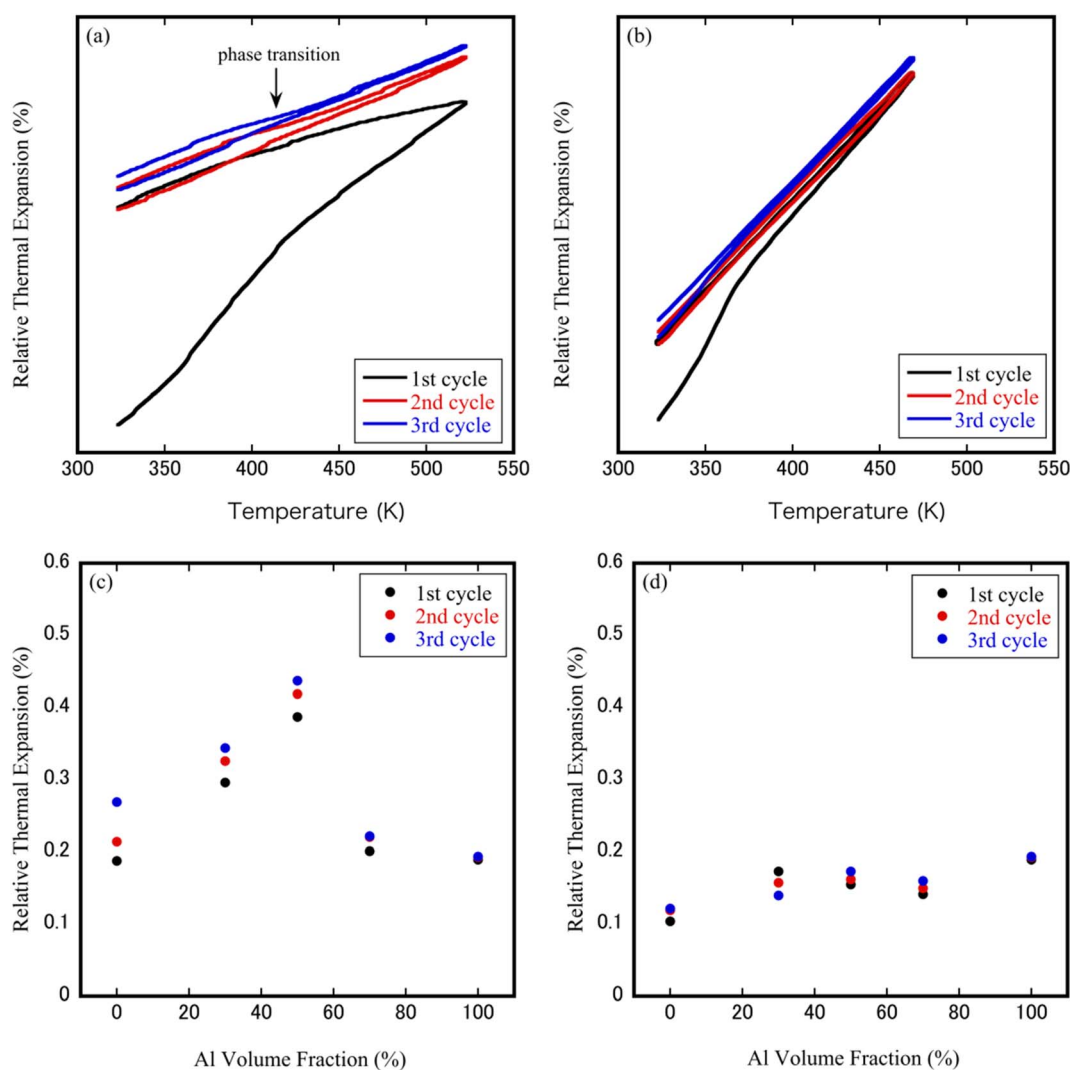


Fig. 4 TMA curves of (a) Al 50 vol%  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimen and (b) Al 50 vol%  $\text{ZrWMoO}_8/\text{Al}$  specimen subjected to three heating-cooling cycles; change in the CTEs after heating cycle as a function of the volume fraction of (c)  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens and (d)  $\text{ZrWMoO}_8/\text{Al}$  specimens for three cycles.

phase transition temperature was observed in  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens. In contrast, the thermal expansion curves were straight lines for  $\text{ZrWMoO}_8/\text{Al}$  composites; therefore, it is suggested that a mismatched thermal expansion during the thermal cycles of  $\text{ZrW}_2\text{O}_8/\text{Al}$  may be affected by the particles dispersed in aluminum and also by phase transitions. This result verifies the XRD reflections shift in Fig. 2(c) and (d).

Fig. 4(c) and (d) depicts the changes in the CTEs after the heating cycle relative to the volume fraction of Al. In  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens, a convex parabolic trend can be observed, with the maximum CTE reached at 50 vol% Al. The change in the CTEs of  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens was about 0.1 to 0.3%, whereas the CTE variation of the  $\text{ZrWMoO}_8/\text{Al}$  sample remains more or less constant. This difference in CTE seems to be related to the dispersion state of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$  with Al. In the  $\text{ZrW}_2\text{O}_8/\text{Al}$  specimens, because the  $\text{ZrW}_2\text{O}_8$  particles formed 100  $\mu\text{m}$  agglomerates, the stress from Al relieved the agglomeration and pores of  $\text{ZrW}_2\text{O}_8$ . The  $\text{ZrW}_2\text{O}_8$  particles subjected to stress from Al increased because the dispersed particle size was small in the  $\text{ZrWMoO}_8/\text{Al}$  specimens.

The thermal expansion behavior of the composites was further analyzed by comparing the experimental results with theoretical models. Several models have been proposed to estimate the CTEs of ceramic-metal composites.<sup>30–32</sup> Among them, the most widely used is the (ROM). ROM considers the matrix to be free of voids, in which each material is perfectly bonding to the matrix so that each component is distorted independently. CTEs are usually assumed to follow a linear ROM dependence on the volume fraction. Fig. 5(a) and (b) shows the thermal expansion of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ) composites with different Al volume fractions obtained from the third heating cycle and a comparison with the values predicted by the ROM model. In contrast to the measured curves of  $\text{ZrWMoO}_8/\text{Al}$  composites were consistent with the theoretical curves of the ROM model, the measured curves of  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites show a slight deviate from the theoretical curves of the ROM model, possibly due to the presence of nanoparticles, which led to residual stresses in the composites. Furthermore, the thermal expansion behavior of both composites confirmed that the CTEs changed from negative to near-zero to positive by

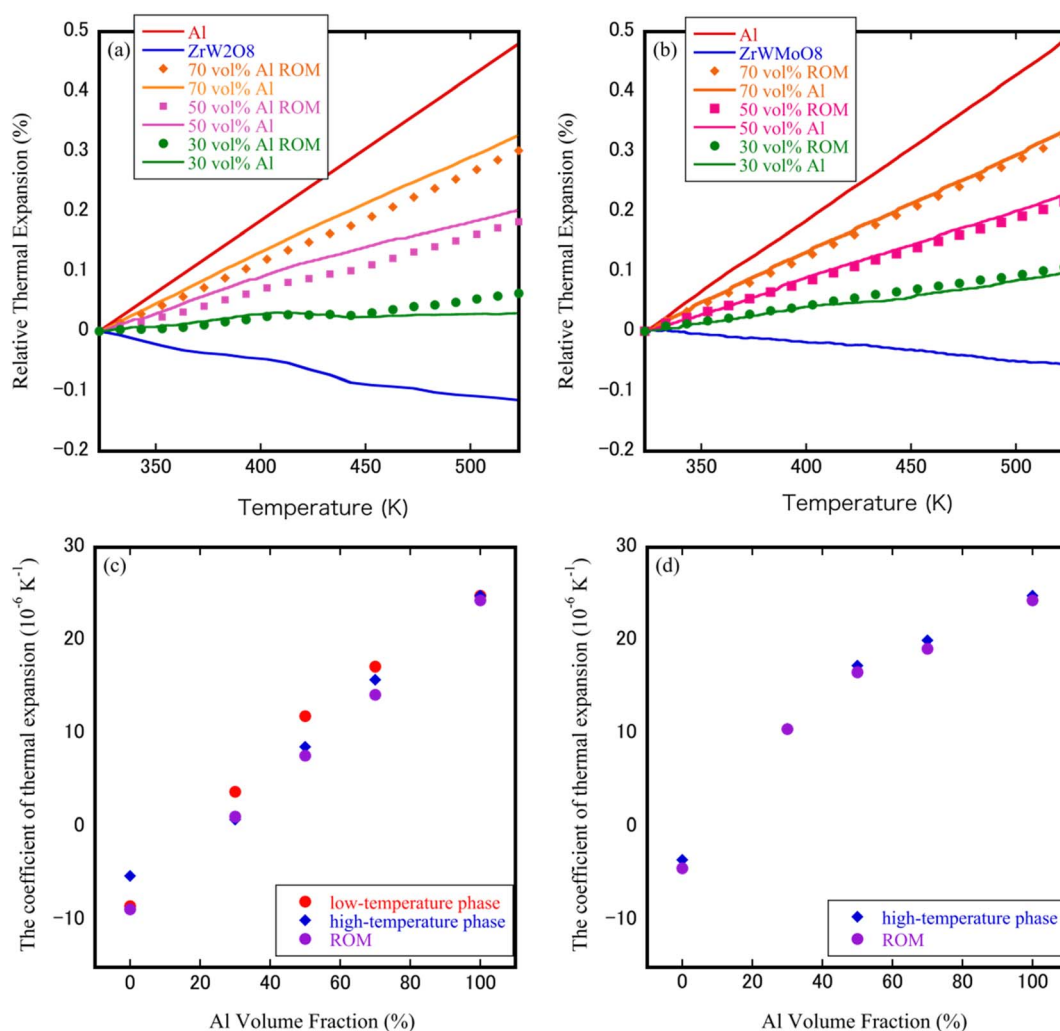


Fig. 5 TMA curves of (a)  $\text{ZrW}_2\text{O}_8/\text{Al}$  and (b)  $\text{ZrWMoO}_8/\text{Al}$  composites during the third heating cycle; CTEs of (c)  $\text{ZrW}_2\text{O}_8/\text{Al}$  and (d)  $\text{ZrWMoO}_8/\text{Al}$  composites.





changing the volume fraction of Al. For  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites, non-linear changes in the CTEs were observed around 420–440 K, which was associated with the order–disorder phase transition of  $\alpha\text{-ZrW}_2\text{O}_8$  to  $\beta\text{-ZrW}_2\text{O}_8$ .

The CTEs of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ) composites measured by thermo-mechanical analysis and estimated based on the ROM model are plotted in Fig. 5(c) and (d). The measured coefficients have values similar to the values reported for  $\text{ZrW}_2\text{O}_8$  powders in the literature ( $\alpha\text{-ZrW}_2\text{O}_8$ :  $-8.8 \times 10^{-6} \text{ K}^{-1}$ ;  $\beta\text{-ZrW}_2\text{O}_8$ :  $-4.9 \times 10^{-6} \text{ K}^{-1}$ ). Compared with the  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites, the  $\text{ZrWMoO}_8/\text{Al}$  composites had slightly higher CTEs because the absolute value of the negative CTEs value of  $\text{ZrWMoO}_8$  is smaller than that of  $\text{ZrW}_2\text{O}_8$ . Additionally, when the Al content rises, the value of the CTEs of  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites at the room temperature gradually increases, from  $-8.46 \times 10^{-6} \text{ K}^{-1}$  for  $\text{ZrW}_2\text{O}_8$  to  $3.37 \times 10^{-6} \text{ K}^{-1}$  for Al 30 vol% specimen,  $11.90 \times 10^{-6} \text{ K}^{-1}$  for Al 50 vol% specimen and rised to  $17.20 \times 10^{-6} \text{ K}^{-1}$  for Al 70 vol% specimen. The same phenomenon was observed in  $\text{ZrWMoO}_8/\text{Al}$  composites, where the CTEs increased from  $-3.49 \times 10^{-6} \text{ K}^{-1}$  for  $\text{ZrWMoO}_8$  to  $10.54 \times 10^{-6} \text{ K}^{-1}$  for Al 30 vol% specimen,  $17.29 \times 10^{-6} \text{ K}^{-1}$  for Al 50 vol% specimen, and  $20.00 \times 10^{-6} \text{ K}^{-1}$  for Al 70 vol% specimen. This indicates that  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ) composites with a tunable thermal expansion coefficient (negative, positive, or close to zero) could be produced by adjusting the volume fraction of Al. Thus, this result suggests that the CTEs can be controlled to some extent by using  $\text{ZrWMoO}_8$  as an inhibitor, as in the case of  $\text{ZrW}_2\text{O}_8$ . The two NTE ceramic materials as inhibitors have their own characteristics in controlling the thermal expansion properties, among which  $\text{ZrW}_2\text{O}_8$  has a larger NTE coefficient, which can maintain the original properties (such as electrical conductivity, thermal conductivity) of the composite matrix, to a greater extent while regulating the CTEs; on the other hand, the advantage of  $\text{ZrWMoO}_8$  is that it does not have the phase transition from the low-temperature phase to the high-temperature phase above room temperature, which avoids the drastic change of the CTEs during phase transition.

### 3.3 Thermal conductivity and electrical conductivity of $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$ composites

Fig. 6(a) and (b) shows the thermal conductivity and electrical conductivity coefficients of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ) composites at room temperature. It can be observed that the thermal and electrical conductivity curves of the  $\text{ZrW}_2\text{O}_8/\text{Al}$  and  $\text{ZrWMoO}_8/\text{Al}$  composites are basically the same. Furthermore, the thermal and electrical conductivity coefficients also show irregular non-linear curves with the variation of Al volume fraction, unlike the linear proportionality observed in the CTEs result. To the best of our knowledge, the electrical conductivity of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites is not inherently random; it is determined by the composition, arrangement, and interactions of the components. However, there can be some variability due to factors like the distribution and orientation of conductive particles, as well as the quality of the interface between the conductive (Al) and non-conductive ( $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$ ) phases. We believe that the close packing or dispersed arrangement of Al particles can influence the electron conduction within the composite material. Additionally, non-uniform distribution or different orientations of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$  ( $x = 0, 1$ ) ceramic particles and Al particles can result in uneven electrical conductivity in the  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites. Fig. 7 presents a schematic simulation of the internal electron conduction in  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites with varying aluminum volume fractions. When the Al volume fraction is low (0–30 vol%), the structure of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites is such that Al is isolated and dispersed in  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$ , and the free electron conduction path to Al is blocked by the  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$  insulator, resulting in limited connection and propagation of free electrons. In this case, the thermal conductivity is thought to be dominated by the phonon contributions of Al and  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$ , which contribute little to the thermal conductivity. As the Al volume fraction in the composite increases to 50 vol%, both phonons and electrons contribute to the rapid change in thermal conductivity, with the heat conduction shifting from phonon to

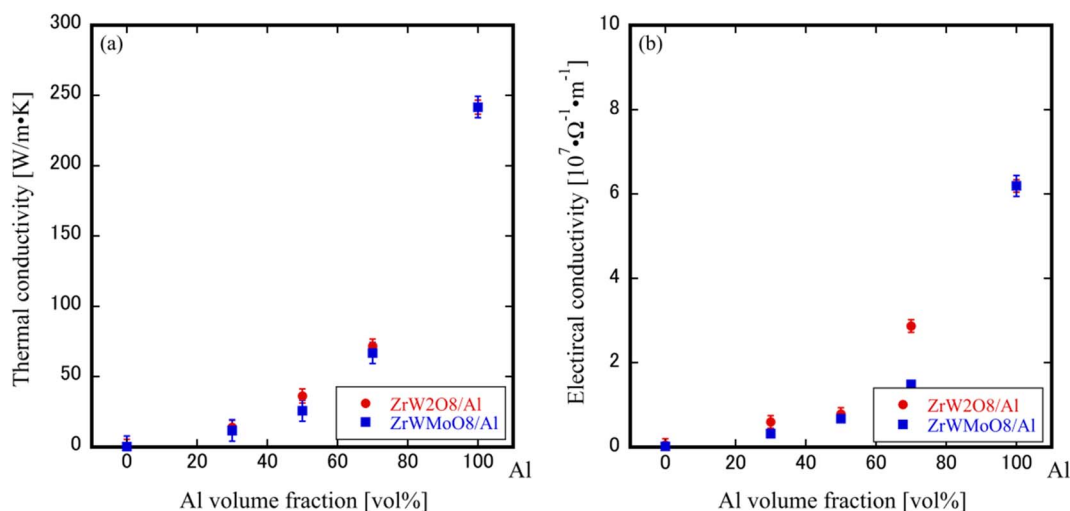


Fig. 6 (a) Thermal conductivity and (b) electrical conductivity of  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites at room temperature.



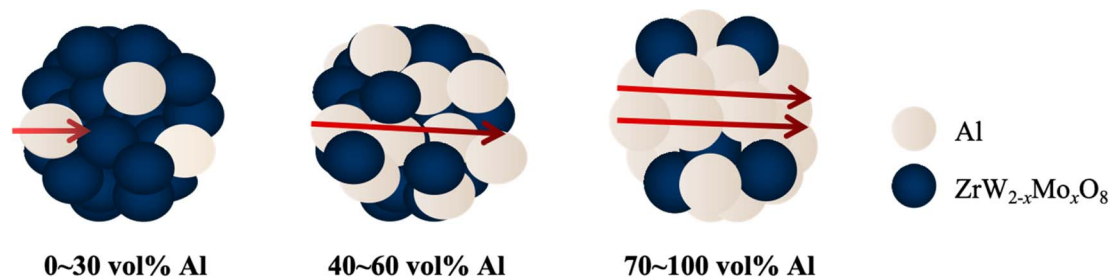


Fig. 7 Simulation diagram of internal electron conduction in  $\text{ZrW}_2\text{O}_8/\text{Al}$  composites with different Al volume fraction.

free electron contribution, and the electron conduction starting to proceed smoothly. The substantial increase in conductivity with the same Al volume fraction is more definitely attributed to the conduction path where the connection and propagation of free electrons occur. When the Al content is as high as 70 to 100 vol%,  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8$  is isolated and dispersed in Al, with the contribution of phonons to the thermal conductivity being minimal and the contribution of free electrons from Al being dominant in conduction. Therefore, when the Al content is high, the conduction paths of the electron conduction carriers are connected, and the propagation of the dominant conduction electrons is smooth, resulting in high values of thermal and electrical conductivity.

## 4. Conclusion

High-density cubic-phase  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  ( $x = 0.0, 1.0$ ) composites were successfully fabricated by spark plasma sintering, and their microstructure, thermal expansion properties and thermal (electrical) conductivity were characterized and analyzed. The main conclusions are as follows: the  $\text{ZrW}_2\text{O}_8/\text{Al}$  and  $\text{ZrWMoO}_8/\text{Al}$  composites prepared at z-axis 90 MPa pressure and sintering temperatures of 873 K and 773 K, respectively, did not induce the formation of the high-pressure phase  $\gamma\text{-ZrW}_{2-x}\text{Mo}_x\text{O}_8$ . The thermomechanical analysis results showed that the volume fraction of Al particles significantly affected the thermal expansion of the composites. The CTEs of the  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites could be controlled from near-zero to positive simply by changing the volume fraction of Al, and the experimental CTEs had similar values to those predicted by the ROM models. Moreover, the thermal conductivity and electrical conductivity of the  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites can be increased with the increase of Al content in order to formulate reasonable coefficients of thermal expansion, thermal conductivity and electrical conductivity by setting the volume fraction of Al. It means that  $\text{ZrW}_{2-x}\text{Mo}_x\text{O}_8/\text{Al}$  composites have potential applications in electronic devices such as heat sinks that require thermal expansion regulation.

## Conflicts of interest

The authors declare that there are no known competing financial interests or personal relationships which have appeared to affect the work reported herein.

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