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## Slot-die coating of electron transport layers for perovskite solar cells using water and butanol-based tin oxide dispersions†

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Lead halide perovskite photovoltaics have shown an impressive efficiency increase over the past decade. Making this technology industrially viable requires precise optimization of every single deposition step. Here we used slot-die coating, a promising scalable deposition technique to enable large scale deposition. We demonstrate the challenges in developing high-quality slot-die coated tin oxide (SnO<sub>2</sub>) films, suited as electron selective layers in perovskite solar cells. We studied the film quality of two commercially available colloidal SnO<sub>2</sub> dispersions by controlling pump rate, coating speed and temperature of the indium tin oxide substrates (ITO). The water-based dispersion was more difficult to control, but resulted in better perovskite solar cell performance than the butanol-based dispersion. Hysteresis in *J*–*V* curves from the water-based tin oxide dispersion was reduced by potassium fluoride addition. A maximum power conversion efficiency of 17.5% was achieved for MAPbI<sub>3</sub>-based solar cells by careful optimization of the deposition parameters.

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## Introduction

Lead halide-based perovskite materials are considered one of the most promising materials for developing next-generation solar cells due to their excellent optoelectronic properties.<sup>1,2</sup> Over the last decade, continuous advances in device engineering resulted in unprecedented improvements in their power conversion efficiency (PCE) from 3.8% to 26.1%.<sup>3–5</sup>

Due to this excellent performance, interest in the technologies that facilitate the transition from laboratory to industrial scale is growing. For instance, spin coating is a commonly used deposition method, but unsuited for industrial upscaling. Taking perovskite solar cells to an industrial level requires a lot of effort and optimization in upscaling technologies. Therefore, it is important to develop suitable printing methods for each layer of the perovskite solar cell.<sup>6,7</sup>

The perovskite solar cell device n–i–p stack consists of a glass substrate with a transparent conductive oxide (TCO),

electron transport layer (ETL), perovskite layer, p-type hole transport layer (HTL) and metal back contact electrode.<sup>8</sup> Carrier-selective ETL and HTL are crucial for extracting and transporting charges, while minimizing the interfacial charge recombination. In an n–i–p configured perovskite solar cell, the perovskite layer is deposited on top of the ETL layer.<sup>9</sup> Therefore, the quality and properties of the ETL layer directly affect the properties of the light absorbing perovskite layer. Thus, developing and optimizing the ETL layer has become a hot topic for research.

Initially, TiO<sub>2</sub> was widely used as the electron transport layer in perovskite solar cells, owing to its suitable optoelectronic properties. However, it has photocatalytic properties under UV-illumination and requires high temperature annealing of about 500 °C to achieve proper crystallinity, making this material less suitable for use in upscaling and commercialization of PSC.<sup>3,10–12</sup> To overcome these drawbacks, alternative n-type metal oxides have been studied, which should allow for low temperature processing, are low in cost and should improve stability.<sup>13–17</sup>

Among the various alternatives, SnO<sub>2</sub> stands out as a very suitable ETL and has gained major attention in recent years.<sup>8,18,19</sup> The highest power conversion efficiency for PSC with SnO<sub>2</sub> as ETL has reached more than 25%. The SnO<sub>2</sub>-based ETLs exhibit several qualities which are suitable for solar cells, such as wide bandgap (3.6 eV), good optical transmittance,

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high charge mobility and compatibility with low temperature processing, all of which make it a good choice as an ETL in PSC.<sup>20,21</sup>

Low temperature solution-processed  $\text{SnO}_2$  were first applied as an ETL applied in 2015 by Ke *et al.*<sup>22</sup> The  $\text{SnO}_2$  layer was prepared from  $\text{SnCl}_2 \cdot 2 \text{H}_2\text{O}$  by sol-gel method and yielded a power conversion efficiency (PCE) of 17.21%. After the first report research focused on improving the solution processing of  $\text{SnO}_2$  by tuning precursor composition. The relatively low stability and reliability of sol-gel processed  $\text{SnO}_2$  led to further research into alternative approaches. A major breakthrough was that Jiang *et al.* found that a commercial  $\text{SnO}_2$  colloidal solution could be used to form the ETL. Aqueous  $\text{SnO}_2$  colloidal solution with 3–4 nm sized  $\text{SnO}_2$  nanoparticles formed a dense, pinhole free  $\text{SnO}_2$  film after mild heating, with good transparency, pushing the PSC efficiency to a record value of 25.7%.<sup>23</sup> After this breakthrough, commercial water-based  $\text{SnO}_2$  has been widely used in solar cells with various modification strategies.<sup>24–26</sup>

Since most of the research has only been focused on spin coating technology for small area solar cell fabrication, which are not easily transferable to upscaling conditions. Galagan *et al.* demonstrated the feasibility of depositing  $\text{SnO}_2$  using slot-die coating.<sup>27</sup> Smith *et al.* developed  $\text{SnO}_2$ -nanoparticle deposition with two scalable techniques including slot die coating and achieved power conversion efficiency over 19%.<sup>28</sup> Bu *et al.* reported KOH treatment to  $\text{SnO}_2$  beneficial for obtaining high performance and hysteresis free device in flexible cells and modules-based slot-die coated  $\text{SnO}_2$  ETL.<sup>29</sup> Recently Richards *et al.* demonstrated the roll-to-roll (R2R) slot-die coating of the  $\text{SnO}_2$  ETL by applying the low flow limit to showcase prediction of the processing window for solvent-engineered  $\text{SnO}_2$ .<sup>30</sup> Besides slot-die coating, other scalable  $\text{SnO}_2$  deposition methods for perovskite modules, such as blade coating, screen printing and spray coating have been developed and several issues such as manufacturing costs, intrinsic stability, and reproducibility should be carefully studied.<sup>29,31–36</sup>

In this work, we exclusively discuss the challenges of the application of two types of commercially available colloidal  $\text{SnO}_2$  solutions in a benchtop slot die coater. High quality ETL layers are obtained by carefully controlling different parameters such as pump rate, coating speed and temperature, *etc.* To assess the ETL quality, we completed the fabrication of perovskite solar cells by depositing perovskite and hole transport layers using conventional spin coating and the gold contact by vacuum evaporation.

## Results and discussion

In the current study, we selected two commercially available  $\text{SnO}_2$  colloidal solutions from Alfa Aesar (15 wt% in water) and Avantama (2.5 wt% in 1-butanol). In the aqueous colloid solution the nanoparticles are stabilized by a negative charge and have a size of 3–4 nm.<sup>29</sup> In the butanol solution  $\text{SnO}_2$  nanoparticles (size 7 nm) are stabilized by organic ligands with

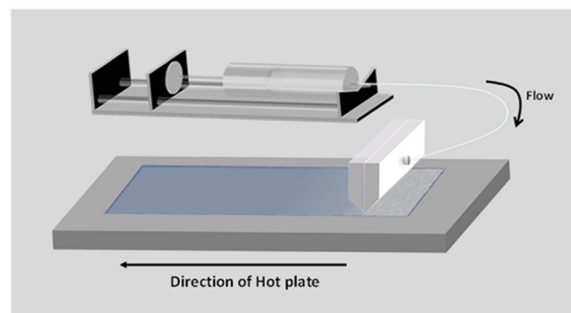


Fig. 1 Schematic representation of slot-die coating of  $\text{SnO}_2$  solution.

a phosphate group. From here onwards we refer to the water-based solution as W- $\text{SnO}_2$  and butanol based as B- $\text{SnO}_2$ .

To set appropriate operating parameters to obtain a high-quality  $\text{SnO}_2$  layer for perovskite solar cells, we have systematically controlled the pump rate, coating speed, coating temperature and coating gap. Fig. 1 shows the schematics of the slot-die coating process of  $\text{SnO}_2$  deposition. Slot-die coating is a non-contact deposition method where the solution is pumped through a syringe to the well-defined slit of the slot-die head unit at a defined pump rate. In the slot-die coater unit, die head is fixed and the substrate holder moves underneath at set speed.

The slot die-coater used in this work is placed inside a fume hood. All the film fabrication discussed are done at ambient atmosphere with around 40 to 50% relative humidity. We found that highly uniform  $\text{SnO}_2$  thin films can be deposited, when the deposition parameters are optimized carefully. Coating was started on a well cleaned ITO-coated glass substrate. Selecting a cleaned substrate for coating plays a crucial role in film formation. We noticed a considerable difference in the contact angle of W- $\text{SnO}_2$  on previously cleaned and freshly cleaned substrates (Fig. S1 in ESI†). It is advantageous if the surface is cleaned using deionized (DI) water just before the deposition to increase the wetting of  $\text{SnO}_2$  solution on ITO substrates. It is worth to note that we didn't apply any other prior treatments, such as UV-ozone, to improve the surface wetting of ITO before  $\text{SnO}_2$  deposition.

To deposit  $\text{SnO}_2$  films of appropriate thickness on ITO, we diluted W- $\text{SnO}_2$  with deionized water and B- $\text{SnO}_2$  with 1-butanol and adjusted deposition speed and pump rate. The concentration of the W- $\text{SnO}_2$  was fixed to 2 wt% and B- $\text{SnO}_2$  was fixed to 1.2 wt% to aim for a final film thickness of about 50 nm, which we confirmed from the SEM cross section. (Fig. S2 in ESI†).

Initial optimization stages with water-based W- $\text{SnO}_2$  were challenging due to low viscosity (0.890 cp) and high surface tension (72.8 mN m<sup>-1</sup>) of water, which promote excessive flow and droplet formation/contraction, respectively. We tried to mix water-based solution with isopropanol (IPA) and 1-butanol to increase the viscosity and decrease the surface tension. Since miscibility of butanol in water is very limited, we focused on the addition of IPA. We diluted the W- $\text{SnO}_2$  with 1 : 1 deionized water and IPA. IPA was added dropwise to the



diluted solution to avoid agglomeration of the nanocrystals. Due to the difficulty in producing reproducible film quality with such mixed solvent solutions, we decided to focus on diluting the stock solution with DI water alone.

To obtain uniform, defect-free coatings in a slot-die coating process, the solution should be transferred *via* the slot-die head to the substrate in a steady state, where the fluid pressure must be balanced in its upstream (from the die head) and downstream (to the substrate). Coating defects such as meniscus break, spreading/leaking of solution and air bubble formation can originate from an unbalanced pressure.

Adjusting the pump rate together with the substrate coating speed, is the best way to control the fluid pressure. As the pump rate is increased, more fluid is forced into the coating bead per unit time, raising the pressure inside the coating bead. Increasing the substrate line speed helps to reduce the pressure of the fluid to some extent. A good balance between pump rate and coating speed must be carefully optimized to obtain high-quality films. To obtain high-quality, uniform, pinhole-free SnO<sub>2</sub> layers, we systematically varied the colloid concentration, pump rate, coating speed and the temperature of the hotplate holding the substrate.

Here in, we started controlling the pump rate while keeping all the other parameters constant. The pump rate was varied from 50  $\mu\text{L min}^{-1}$  to 300  $\mu\text{L min}^{-1}$  for W-SnO<sub>2</sub> and 100  $\mu\text{L min}^{-1}$  to 300  $\mu\text{L min}^{-1}$  for B-SnO<sub>2</sub>. The obtained film quality of W-SnO<sub>2</sub> changed drastically with different pump rates. Higher pump rates force more fluid to reach the substrate, which leads to an uncontrolled flow of solution on the substrate, resulting in an uneven film morphology with higher thickness. To make more uniform and reproducible film, we adopted a relatively low pump rate for coating.

On the other hand, B-SnO<sub>2</sub> film quality was not affected by the pump rate, see Fig. S3 (ESI<sup>†</sup>). This difference is attributed to the viscosity of the butanol (3.5 cp), which is higher than that of water (0.89 cp), and its surface tension, which is lower (21 mN m<sup>-1</sup> *vs.* 72 mN m<sup>-1</sup>). The combination of these parameters will promote uniform coating for butanol-based inks, while drop formation and contraction may occur for water-based inks. The optimized slot-die coating parameters for deposition of the two colloidal SnO<sub>2</sub> solutions are listed in Table 1. The optimum pump rate for W-SnO<sub>2</sub> was found to be 90  $\mu\text{L min}^{-1}$  with coating speed of 80 cm min<sup>-1</sup> and a substrate temperature of 80 °C.

Transmission measurements of SnO<sub>2</sub> films on ITO was performed (Fig. 2a) to understand the optical properties. Both B-SnO<sub>2</sub> and W-SnO<sub>2</sub> show excellent light transmittance in the visible region, which indicates good optical quality of the films. It is observed that the transmittance of the B-SnO<sub>2</sub> films in the

wavelength range from 350 nm to 450 nm higher than that of W-SnO<sub>2</sub>. Corresponding images of the slot-die coated SnO<sub>2</sub> films are shown in Fig. 2b.

Scanning electron microscopy (SEM) was used to study the surface morphology of the two kinds of SnO<sub>2</sub> film and compared with the bare ITO substrate. Both W-SnO<sub>2</sub> and B-SnO<sub>2</sub> films completely covered the ITO and the surface images confirmed uniform film formation as well. Lower magnification images are given in the electronic supplementary information (ESI<sup>†</sup> Fig. S3).

To study the formation of perovskite on the slot-die coated SnO<sub>2</sub> films, we spin coated MAPbI<sub>3</sub> perovskite on top of bare ITO substrates, as well as on W-SnO<sub>2</sub> and B-SnO<sub>2</sub>-coated substrates. The average grain size of perovskite crystals was 80–250 nm, which remained the same for both SnO<sub>2</sub> films. To deposit the perovskite layer by spin coating, usually prior UV-Ozone treatment is needed, which improves the wetting of the substrates with the perovskite precursor solution. To confirm this effect, contact angle measurements of perovskite precursor on both types of SnO<sub>2</sub> films were performed, where 20 min UV-Ozone treatment was applied before perovskite deposition. In the case of W-SnO<sub>2</sub>, this pretreatment improved the wetting of the perovskite precursor on W-SnO<sub>2</sub> the average contact angle of perovskite solution on W-SnO<sub>2</sub> was 40.29° without UV-ozone treatment, decreasing to 25.75° after 20 min UV-ozone treatment. On the other hand, the contact angle of perovskite solution on B-SnO<sub>2</sub> films did not change much with UV-ozone treatment (without 35.81°, with UV-ozone 32.98°), see ESI<sup>†</sup> Fig. S4.

The absorption spectra of the perovskite films on was very similar on all substrates investigated here (Fig. 4a), which indicates that the thickness of perovskite layer was same on each electrode, about 450 nm. In contrast, a clear effect of the substrate was found on the photoluminescence (PL) of the perovskite films. Fig. 4b shows the steady state PL spectra of MAPbI<sub>3</sub> films on ITO, ITO/W-SnO<sub>2</sub> and ITO/B-SnO<sub>2</sub> respectively. We observe that the added SnO<sub>2</sub> ETL layers lead to significant PL quenching. The PL quenching was less on B-SnO<sub>2</sub> (75% compared to bare ITO substrate), whereas it was stronger on W-SnO<sub>2</sub> (92%), which suggests better electron injection from perovskite into the W-SnO<sub>2</sub> ETL layer.

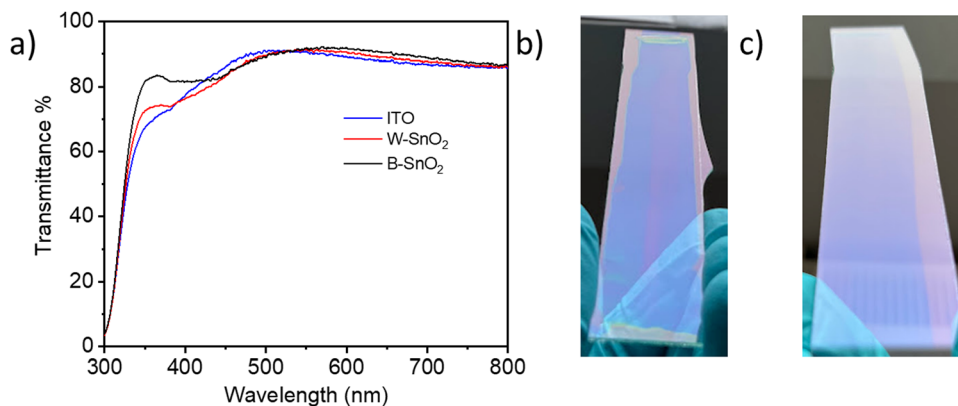
To investigate the functionality of both W-SnO<sub>2</sub> and B-SnO<sub>2</sub> as an ETL layer, perovskite solar cells were fabricated with standard methods. A schematic representation of the solar cell architecture is shown in Fig. 5a, where SnO<sub>2</sub> layer was made by slot-die coating, while the other layers were prepared by spin coating using standard methods (see details in the experimental section). The perovskite material used was MAPbI<sub>3</sub>, prepared using a one-step method with antisolvent treatment. The current density–voltage (*J*–*V*) characteristics of champion devices, recorded under 100 mW cm<sup>-2</sup> illumination are shown in Fig. 5b and the corresponding solar cell parameters are summarized in Table 2.

We systematically varied the pump rate of the colloidal SnO<sub>2</sub> solutions while keeping all other parameters constant. The pump rate was varied from 50  $\mu\text{L min}^{-1}$  to 300  $\mu\text{L min}^{-1}$  for

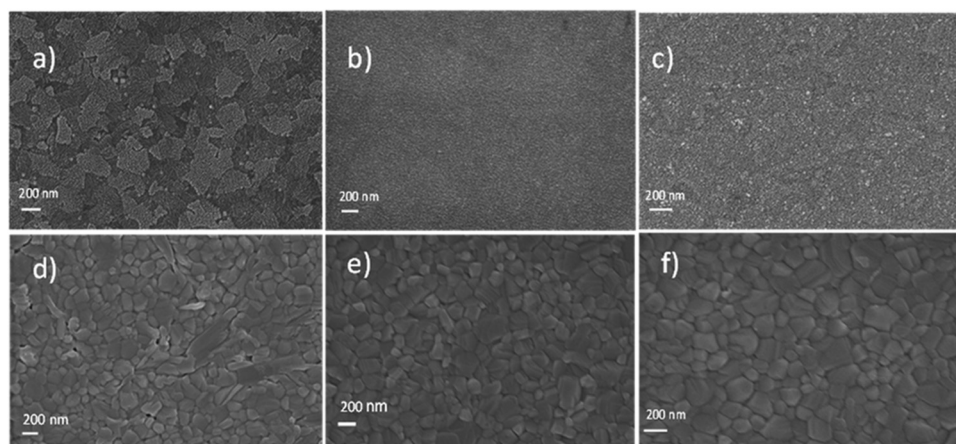
**Table 1** Optimized slot die coating parameters for W-SnO<sub>2</sub> and B-SnO<sub>2</sub>

|                    | Pump rate<br>( $\mu\text{L min}^{-1}$ ) | Coating speed<br>(cm min <sup>-1</sup> ) | Coating<br>temperature (°C) | Coating<br>gap ( $\mu\text{m}$ ) |
|--------------------|---|--|-----------------------------|----------------------------------|
| W-SnO <sub>2</sub> | 90                                      | 80                                       | 80                          | 88                               |
| B-SnO <sub>2</sub> | 200                                     | 80                                       | 60                          | 100                              |

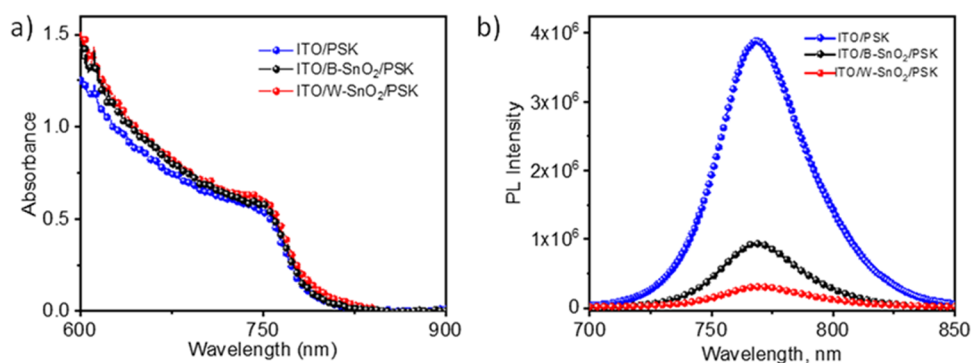




**Fig. 2** (a) Transmittance spectra of slot die coated  $\text{SnO}_2$  films on ITO-glass substrates. Photographic images of the corresponding films (14 cm  $\times$  3 cm): (b) W- $\text{SnO}_2$  (c) B- $\text{SnO}_2$ .



**Fig. 3** Scanning electron microscopy surface images of (a) ITO substrate (b) W- $\text{SnO}_2$  on ITO (c) B- $\text{SnO}_2$  on ITO. (d)–(f)  $\text{MAPbI}_3$  films deposited on (a)–(c) respectively.



**Fig. 4** (a) UV-Vis spectra of  $\text{MAPbI}_3$  perovskite films on ITO, ITO/B- $\text{SnO}_2$  and ITO/W- $\text{SnO}_2$ . (b) Steady-state photoluminescence spectra the same films.

W- $\text{SnO}_2$  and  $100 \mu\text{L min}^{-1}$  to  $300 \mu\text{L min}^{-1}$  for B- $\text{SnO}_2$ . The obtained film's quality of W- $\text{SnO}_2$  drastically changes when a low pump rate is adapted, as is evident from their solar cell performance (Fig. S5, ESI<sup>†</sup>). Higher pump rate forces more fluid to reach the substrate, which leads to an uncontrolled flow of

solution on the substrate resulted in an uneven film morphology with higher thickness. Decreasing the pump rate, to find an optimum balance between pump rate and coating speed resulted in a much more uniform film. The highest power conversion efficiency of W- $\text{SnO}_2$  based solar cell is 17.1% with a





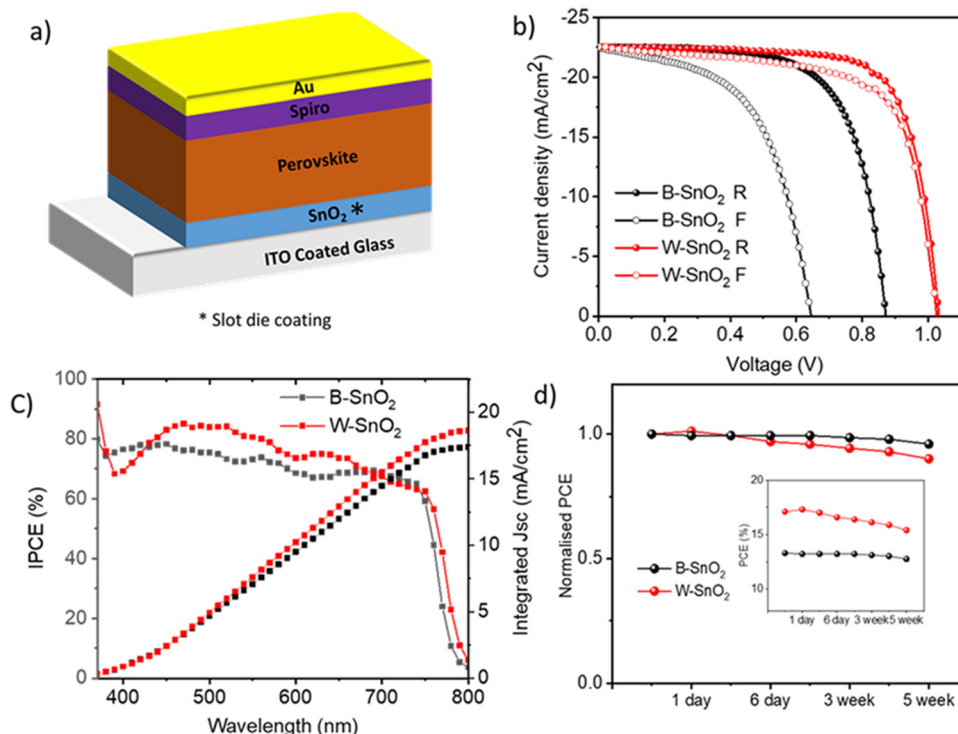


Fig. 5 (a) N-i-p solar cell architecture; (b) champion *JV* curves for devices with slot-die coated  $\text{SnO}_2$  as electron transport layers; (c) IPCE spectra (d) normalized storage stability (inset actual stability over several weeks).

Table 2 Solar cell device data for perovskite solar cells with slot-die coated  $\text{SnO}_2$  ETL

|                     | $V_{\text{OC}}$ (V) | $J_{\text{SC}}$ ( $\text{mA cm}^{-2}$ ) | FF (%) | PCE (%) | Hysteresis index |
|---------------------|---------------------|---|--------|---------|------------------|
| W- $\text{SnO}_2$ R | 1.03                | −22.5                                   | 73.6   | 17.1    | 0.07             |
| W- $\text{SnO}_2$ F | 1.03                | −22.5                                   | 69.0   | 15.9    |                  |
| B- $\text{SnO}_2$ R | 0.872               | −22.5                                   | 67.5   | 13.3    | 0.37             |
| B- $\text{SnO}_2$ F | 0.645               | −22.4                                   | 55.2   | 8.0     |                  |

low hysteresis index of 0.07, whereas B- $\text{SnO}_2$  showed a maximum efficiency of 13.3% with a high hysteresis index of 0.37. The hysteresis index is defined here as follows:  $\text{HI} = 1 - \text{PCE}(\text{forward})/\text{PCE}(\text{reverse})$ . Hysteresis in PSC is generally attributed to ion movements in perovskite films and accumulations of ions at interfaces. We attribute the strong hysteresis for PSC with B- $\text{SnO}_2$  to a poor  $\text{SnO}_2$ /perovskite interface, which may be related to the ligands on the  $\text{SnO}_2$  nanoparticle or the porosity of the film.

We found a significance difference in photovoltaic performance for the two different  $\text{SnO}_2$  ETL in perovskite solar cells, see the device statistics in ESI† (ESI† Fig. S6). There is a remarkable difference in the open circuit potential ( $V_{\text{OC}}$ ), which is about 100–200 mV larger for W- $\text{SnO}_2$  devices. The most likely reason for this is that B- $\text{SnO}_2$  films are poorly hole blocking, because of porosity or pin-holes, as will be shown below in separate electrochemical experiments.

We compared the incident photon to current conversion efficiency (IPCE) of the devices, in which W- $\text{SnO}_2$  showed a maximum value of 85%, whereas B- $\text{SnO}_2$  showed 78% in the

wavelength 400–600 nm as shown in Fig. 5c. The integrated current density of W- $\text{SnO}_2$  ( $18.6 \text{ mA cm}^{-2}$ ) and B- $\text{SnO}_2$  ( $17.6 \text{ mA cm}^{-2}$ ) obtained from IPCE are lower when compared with the *JV* measurements, likely caused by the very low light intensity of monochromatic light used in the IPCE measurements, which give rise to photocurrents in the order of microamperes. This measurement is therefore sensitive to even small shunting effects in the devices.

The shelf life stability of the both types of cells were investigated over several weeks, see Fig. 5d. PCE of B- $\text{SnO}_2$  remained quite stable while the efficiency of W- $\text{SnO}_2$  started dropping to 80% of the initial value in 5 weeks.

To study the recombination mechanism in these solar cells,  $J_{\text{SC}}$  and  $V_{\text{OC}}$  at different intensities 10 to 100  $\text{mW cm}^{-2}$  were measured. Fig. 6a shows the  $J_{\text{SC}}$ , which is approximately linearly connected to the different light intensity and the slope of doubly logarithmic plot is 0.963 and 0.957 for W- $\text{SnO}_2$  and B- $\text{SnO}_2$  respectively. From Fig. 6b, the  $V_{\text{OC}}$  vs. light intensity studies showed an ideality factor of 1.92 (W- $\text{SnO}_2$ ) and 2.68 (B- $\text{SnO}_2$ ) for the corresponding solar cells.

A marked difference is also found in the  $V_{\text{OC}}$  transients. Upon switching on the light (1 sun) it takes more than 10 s to achieve a stable  $V_{\text{OC}}$  value. Notably, B- $\text{SnO}_2$  devices were significantly slower than W- $\text{SnO}_2$  (Fig. 6c). After switching off the light, part of the  $V_{\text{OC}}$  decays rapidly in the ms-regime, while another part decay very slowly in the second-regime (Fig. 6d). The slow response of  $V_{\text{OC}}$  to light changes is correlated to ionic motion to and from the charge-selective contacts upon charging/discharging the device. Specifically, we believe that a



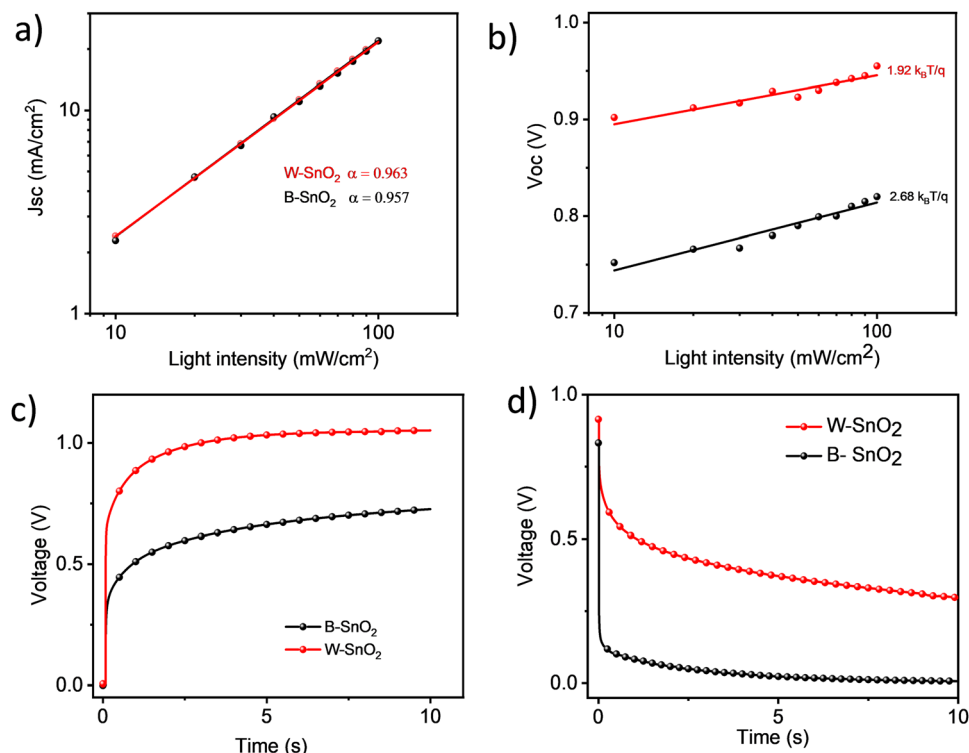


Fig. 6 (a)  $J_{SC}$  vs. light intensity; (b)  $V_{OC}$  vs. light intensity; (c)  $V_{OC}$  rise upon switching on light (1 sun); (d)  $V_{OC}$  decay.

build-up of ions at the perovskite/ $\text{SnO}_2$  interface is important to reach the high voltages in PSC with  $\text{SnO}_2$  contacts. Clearly, it will then have a significant effect whether or not there are ligands present at the  $\text{SnO}_2$  surface, as is the case for  $\text{SnO}_2$ -B.

To find out the reason for the difference in the solar cell performance for the two types of  $\text{SnO}_2$  ETL, we carried out further fundamental studies. Dynamic light scattering was used to analyze the colloidal  $\text{SnO}_2$  solutions (Fig. 7a). A significant difference in  $\text{SnO}_2$  particle size was found. The average particle size of W- $\text{SnO}_2$  is 4–7 nm, whereas B- $\text{SnO}_2$  shows 20–30 nm size, which is significantly larger than the reported size of 7 nm. Partially this may be ascribed to the organic ligands, but also some aggregation must be considered. Both aspects could lead to relatively porous  $\text{SnO}_2$  films upon deposition.

To measure the blocking behavior of both types of slot-die coated  $\text{SnO}_2$  films we carried out cyclic voltammetry (CV) by

observing the anodic current density obtained with ferri/ferrocyanide redox couple. Fig. 5b shows typical cyclic voltammogram of a bare ITO (blue) in comparison with W- $\text{SnO}_2$  (red) and B- $\text{SnO}_2$  (black). W- $\text{SnO}_2$ -coated ITO does not produce much anodic current density, confirming the film with excellent hole blocking behavior and supporting the scanning electron microscopy image of the corresponding film (Fig. 3b). In contrast, B- $\text{SnO}_2$  exhibits higher anodic current, which indicates it is not acting as hole blocking layer in solar cell, even though it appears to completely cover the ITO surface. To confirm the coverage of both  $\text{SnO}_2$  on ITO, we also carried out x-ray photoelectron spectroscopy (see ESI† Fig. S6), we could not find any Indium peak on the XPS spectra, which indicate the complete coverage of both types of  $\text{SnO}_2$  films on ITO; this result also supports the scanning electron microscopy images of both  $\text{SnO}_2$  films.

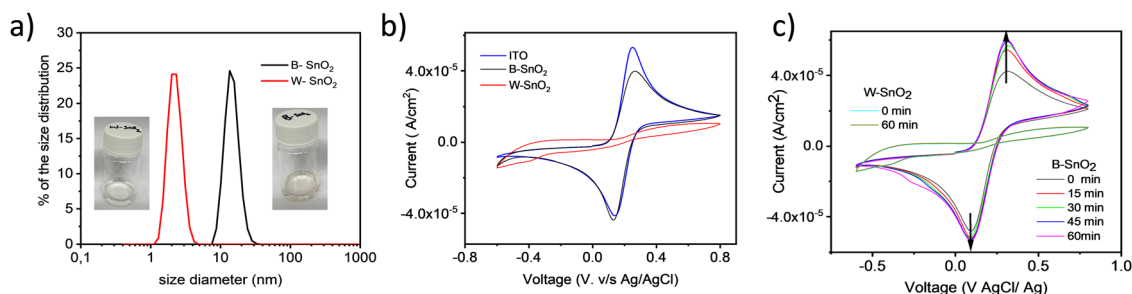


Fig. 7 (a) Dynamic light scattering of  $\text{SnO}_2$  particles (b) cyclic voltammograms of different  $\text{SnO}_2$  films on ITO in comparison with bare ITO (c) cyclic voltammogram of  $\text{SnO}_2$  films at different time intervals.



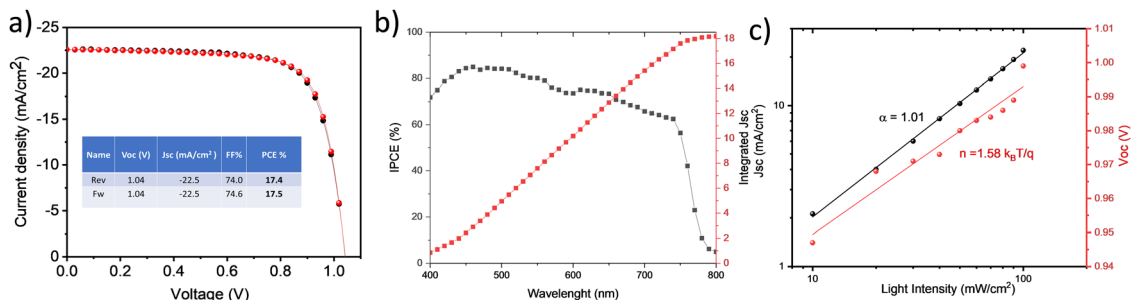


Fig. 8 (a) Champion JV curve of W-SnO<sub>2</sub> with KF (b) IPCE spectra of the best cell (c) J<sub>sc</sub> and V<sub>oc</sub> vs. light intensity curve.

Additional time-dependent cyclic voltammetry measurements displayed that for B-SnO<sub>2</sub> films the anodic current density values gradually increased over a time period of one hour, in contrast to W-SnO<sub>2</sub>, which did not show any change in current density. This could point to film instability and removal of B-SnO<sub>2</sub> particles over time. We noted a small scratch or a soft touch is enough to remove B-SnO<sub>2</sub> films from the substrate, this we confirmed by analyzing the XPS spectra before and after a mild touch on the film (see ESI† Fig. S7), whereas W-SnO<sub>2</sub> films are more rugged. This might also affect the cell performance, since there is a possibility of film dissolution or pinhole formation upon dropping the perovskite precursor in DMF: DMSO on to this substrate.

From here onwards, we will focus on improvement of the film quality and device performance of W-SnO<sub>2</sub>. From the literature it is clear that adding a small amount potassium fluoride (KF) helps to reduce the hysteresis effect and stability of the devices.<sup>37</sup> We added different amount of KF (3 mg to 8 mg) into corresponding stock solution to find out the optimum amount. 6 mg/1 ml SnO<sub>2</sub> solution was found to be the best one (see ESI† Fig. S8 and Table S1) and showed maximum efficiency of 17.5% with negligible or even no hysteresis effect. The KF-doped SnO<sub>2</sub> has enhanced electron mobility and deep conduction band. F<sup>-</sup> ion presented in the SnO<sub>2</sub>, can migrate in to perovskite film can reduce the non-radiative recombination and trap density. Fig. 8a shows the best J-V curve and corresponding incident photon to current conversion efficiency is showed in Fig. 8b.

J<sub>sc</sub> and V<sub>oc</sub> at different intensities 10 to 100 mW cm<sup>2</sup> were also measured (Fig. 8c), the observation is in good agreement with previous results. The statistical distribution of solar cell parameters is shown in ESI† Fig. S10. The electronic structure of B-SnO<sub>2</sub>, W-SnO<sub>2</sub> and WKF-SnO<sub>2</sub> was studied by ultraviolet photoelectron spectroscopy (UPS) measurements and optical bandgap. Fig. S11 (ESI†) represents the valence band energy (*E*<sub>VB</sub>) region (left) and secondary electron cut off region (*E*<sub>cutoff</sub>) region (right). The work function can be derived by subtracting the *E*<sub>cutoff</sub> from standard He I irradiation energy 21.22 eV. Valence band maxima is calculated by VBM = 21.22 - (*E*<sub>cutoff</sub> - *E*<sub>VB</sub>). The conduction band maximum (CBM) can be calculated from VBM and optical bandgap (*E*<sub>g</sub>). *E*<sub>g</sub> of each SnO<sub>2</sub> was estimated from Tauc plot based on UV-vis spectroscopy (see Fig. S12, ESI†). We have summarized all the results in

Table S2 in the ESI.† The energy band alignment of two different SnO<sub>2</sub> and KF modified SnO<sub>2</sub> are depicted in Fig. S13 (ESI†). The results indicate CBM of WKF-SnO<sub>2</sub> more favorable for an efficient charge extraction from perovskite.

Electrochemical impedance spectroscopy measurements were also performed to analyze the charge carrier recombination in the devices, corresponding Nyquist plots was investigated at applied voltage 0.80 V under dark in the frequency range from 1000 kHz to 0.1 Hz. The equivalent circuit and fitted parameters are shown in Fig. S14 (ESI†). It is found that WKF-SnO<sub>2</sub> shows much higher recombination resistance compared to W-SnO<sub>2</sub> indicating that the recombination was effectively suppressed in these devices.

## Conclusion

We successfully demonstrated thin film coating of two different commercially available SnO<sub>2</sub> by slot die coating. We systematically investigated the film quality by different parameters such as pump rate, coating speed and temperature. Although film formation ability and quality of B-SnO<sub>2</sub> found to be good when compared to W-SnO<sub>2</sub> even though the solar cell performance was not as expected. From cyclic voltammetry measurements it appears the B-SnO<sub>2</sub> layers are porous and do not serve well in its role as a blocking layer in the perovskite solar cell. To improve the film quality of W-SnO<sub>2</sub>, KF doping was introduced, which decreased the non-radiative recombination and lowered trap density in the solar cell.

## Conflicts of interest

There are no conflicts to declare.

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