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## Current induced cooling in a metal/*n*-InAs structure

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This paper focuses on the specific features of an Ohmic contact on undoped *n*-InAs ( $n = 2 \times 10^{16} \text{ cm}^{-3}$ ) that could be used for temperature stabilization and/or temperature reduction in electronic devices, mainly operating in the 3–5  $\mu\text{m}$  mid-IR range. This feature has been demonstrated in a 100  $\mu\text{m}$  thick *n*-InAs slab with three unannealed Cr–Au–Ni–Au contacts formed *via* evaporation in vacuum. The *I*–*V* characteristics showed no deviation from Ohm's law in the temperature range 77–340 K, manifesting a contact resistance ranging from  $3.6 \times 10^{-5}$  to  $7.2 \times 10^{-5} \Omega \text{ cm}^2$  at room temperature. The 2D thermal radiation distribution and the temperature distribution over the *n*-InAs surface opposite the contact side surface was obtained *via* a pre-calibrated IR microscope operating at a wavelength of 3  $\mu\text{m}$ . The measurements revealed a current dependent temperature decline in the area adjacent to the negatively biased contact: at the applied power of 5 mW, cooling as strong as  $\Delta T \approx 1 \text{ K}$  occurred at an ambient temperature of 340 K. The results show potential for the fabrication of heterostructures with a “built-in” cooler that is monolithically integrated with another electronic device.

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### Introduction

Electrically driven solid state refrigeration has been known for more than a century, and Peltier coolers are now used in a variety of applications. Nevertheless, the demand for low-power on-chip devices for many applications<sup>1,2</sup> is one of the most significant demands of this decade, including coolers that are monolithically integrated into them. Therefore, the need for a compact and efficient miniature “heat pump” for electronic components strongly encourages the investigation of electrocaloric materials<sup>3</sup> and p–n structures, *e.g.* at a forward bias (FB). Previous research has reported opto-thermionic refrigeration,<sup>4</sup> thermophotonic heat pumping,<sup>5</sup> thermo-electro-photo cooling,<sup>6</sup> electroluminescent refrigeration,<sup>7</sup> and electroluminescent cooling,<sup>8</sup> all referring to electronic cooling in FB p–n heterostructures. An alternative to the above approach employs the negative luminescence (NL) phenomenon in narrow-gap semiconductors activated by the magnetoconcentration/galvanomagnetic effect or by a reverse biasing of p–n structures.<sup>9–12</sup> The corresponding heat engine ability has been referred to as a “radiative cooling effect due to negative luminescence”<sup>13</sup> or “photonic cooling through the control of the chemical potential of photons”<sup>14</sup> and has been

used in experiments with spatially separated NL devices and an object to be cooled.

All the above-mentioned semiconductor devices utilize metal/semiconductor (MS) junctions as a source of non-equilibrium charge carriers that enter or leave the semiconductor body. In most cases, these junctions, including the Me/*n*-InAs junction,<sup>15,16</sup> were considered as Ohmic electrical contacts—in other words, potential sources of Joule heat. This may not be fully true as an MS interface with certain parameters is capable of producing the cooling of a contact area at a negative bias on the metal.<sup>17</sup> However, to the best of our knowledge, there have been no attempts to test the potential cooling ability of the Me/*n*-InAs junction.

In this paper, we demonstrate that the current flow through the Ohmic contact at the Me/*n*-InAs junction leads to the cooling effect instead of Joule heating.

### Materials and methods

The sample consists of a *p*-InAsSb (3  $\mu\text{m}$  thick)/*n*-InAsSb (3  $\mu\text{m}$  thick) heterostructure (HS) grown using the LPE method onto an undoped *n*-InAs (100) substrate cut from a Czochralski ingot fabricated *via* GIREDMET.<sup>18</sup> Table 1 summarizes the parameters of the ingot (substrate mother) as declared by the manufacturer's certificate.

The transmission spectrum shown in Fig. 1 is typical for the undoped *n*-InAs, as it suggests a lack of significant free electron absorption at long wavelengths. Also shown in Fig. 1 is an IR microscope responsivity spectrum, *i.e.* the spectrum

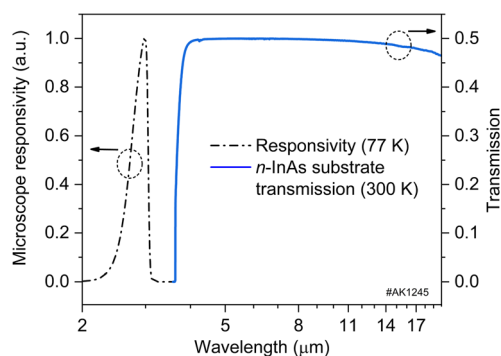
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**Table 1** *n*-InAs ingot parameters

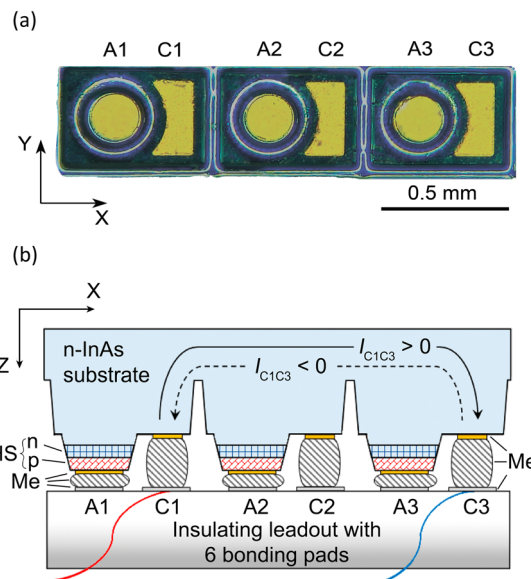
Parameter	Ratings	Units
Bulk resistance, 77 K	$(5.98\text{--}5.72) \times 10^{-3}$	$\Omega \text{ cm}$
Free electron concentration, 77 K	$(2.17\text{--}2.28) \times 10^{16}$	$\text{cm}^{-3}$
Dislocation density	$(1.6\text{--}3) \times 10^4$	$\text{cm}^{-2}$

of the cooled InAs detector developed at the Institute of Semiconductor Physics, the Siberian Branch of the Russian Academy of Sciences,<sup>19</sup> which provided  $128 \times 128$  px ( $2 \times 2$  mm) radiation intensity maps of the sample under study. As seen from the data in Fig. 1, the microscope sensitivity subsides at around  $3 \mu\text{m}$  so that the substrate transmission and microscope responsivity have poor overlapping. Therefore, we were able to measure the purely thermal radiation as well as the temperature distribution over the *n*-InAs surface without the concern of detecting some kind of electroluminescence that could potentially arise from radiative recombination near the Me/*n*-InAs interface. The 2D temperature distribution was estimated utilizing calibration curves that were experimentally derived using the same sample under study at  $T = 300\text{--}370$  K.

The sample was a “troika of diodes” (a  $1 \times 3$  linear array) with three  $30 \mu\text{m}$  high circular mesas ( $\varnothing_m = 190 \mu\text{m}$ ),  $\sim 50 \mu\text{m}$  deep separation grooves, three circular Cr–Au–Ni–Au based anodes (A1, A2 and A3) ( $\varnothing_A = 170 \mu\text{m}$ ) and three Cr–Au–Ni–Au cathodes (C1, C2 and C3) of nearly rectangular shape formed by evaporation in vacuum and a standard photolithography process and wet chemical etching so that the *n*-InAs (100) substrate surface was free of contacts as in previous reports.<sup>16,20</sup> No annealing was used while preparing the contacts. Fig. 2 shows the troika cross section schematic, where a  $7.1 \times 7.1$  mm AlN leadout with six bonding pads provided an electrical connection to the troika contacts. Further descriptions refer to the features of the sample biased through the  $C_i\text{--}C_j$  pairs of contacts ( $i, j = 1, 2$ , and  $3$ ; see the red and blue lines in Fig. 2 depicting the corresponding communication wires for the C1–C3 case). We denote the current flowing from left to right in Fig. 2 as the positive current  $I_{C_iC_j} > 0$  and



**Fig. 1** Spectral responsivity of the IR microscope/camera at 77 K (left scale) and the estimated optical transmission of a  $100 \mu\text{m}$ -thick *n*-InAs substrate (right scale).



**Fig. 2** (a) Image of the diode troika from a surface with contacts: A1, A2 and A3 are anodes, C1, C2 and C3 are cathodes; (b) schematic of the troika chip where HS is the *n*-InAsSb/*p*-InAsSb heterostructure, Z is growth direction of the *p*- and *n*-epitaxial layers [100], X is the [011] direction, Me is multilayer Ohmic contacts, including solder, and  $I_{C_1C_3}$  is current flowing from left to right at a positive bias at C1 (solid arrow); current flowing from right to left at a positive bias at C3 is denoted by dashed arrow. Schematic is not to scale.

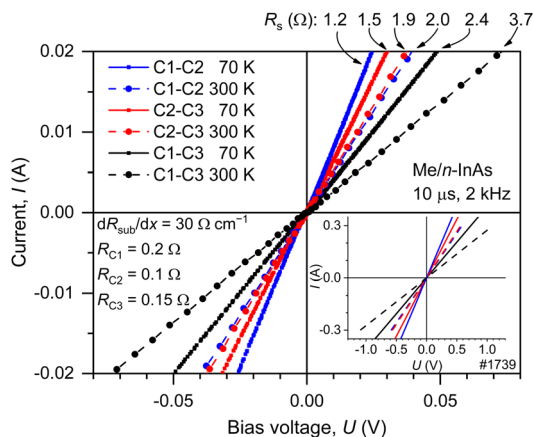
the current flowing from right to left as the negative one  $I_{C_iC_j} < 0$  so that  $I_{C_iC_j} = -I_{C_jC_i}$ . No bias was applied to the *p*–*n* junctions.

## Results

Measurements of  $I$ – $V$  characteristics at 77 and 300 K revealed no deviation from Ohm's law; substrate resistance at RT progressively increased with the inter-contact distance as  $dR_{\text{sub}}^{300\text{K}}/dx = 3 \Omega \text{ mm}^{-1}$ , amounting to  $R_{\text{sub}} = 1.7 \Omega$  to  $R_{\text{sub}} = 3.4 \Omega$  for the C1–C2 (C2–C3) and C1–C3 connections, respectively (see Fig. 3). Contact resistances were 10-fold smaller than the  $R_s$  and consisted of  $R_{C_1} = 0.2 \Omega$ ,  $R_{C_2} = 0.1 \Omega$  and  $R_{C_3} = 0.15 \Omega$  (contact resistances normalized to the unit area are  $7.2 \times 10^{-5}$ ,  $3.6 \times 10^{-5}$  and  $5.4 \times 10^{-5} \Omega \text{ cm}^2$ , respectively).

Shown in Fig. 4a is a  $\Delta X$  by  $\Delta Y$  false IR image of the troika at  $I_{C_1C_2} = -15$  mA, that is, the 2D distribution of  $\Delta L(x, y) = L(x, y) - L_0(x, y)$ , where  $L(x, y)$  is the radiation intensity of the activated troika,  $L_0(x, y)$  is the intensity without a bias and  $XY$  is the plane parallel to the (100) plane. As a rule, IR images contain bright areas at the edges of the sample where the radiation exhibits an enhanced extraction efficiency due to edge effects and shape imperfections. We will ignore these edge effects, and, thus, further considerations will deal with the emission from the *n*-InAs substrate surface only, so the areas of interest will not include the sample edges, as shown in Fig. 4b by the dashed rectangle with an area of  $\Delta X \Delta Y$ .

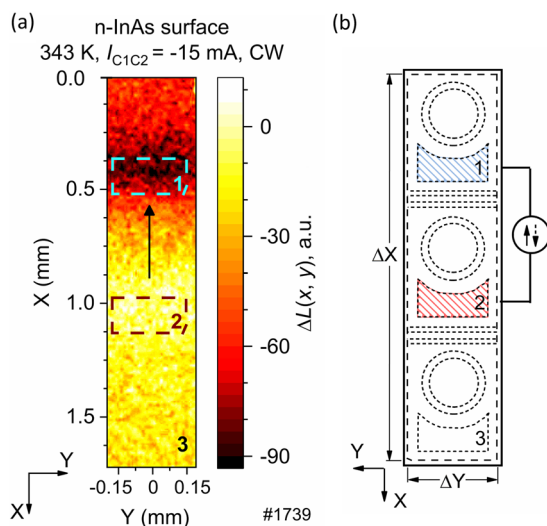




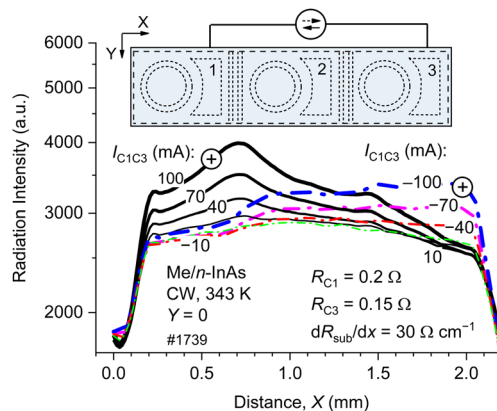
**Fig. 3**  $I$ - $V$  characteristics at 70 K (solid lines) and 300 K (dashed lines) for three connection types: C1-C2 (blue), C2-C3 (red) and C1-C3 (black). The insert shows  $I$ - $V$  characteristics at the bias up to  $\pm 1$  V.

As seen in Fig. 4a, the 2D radiation distribution is far from uniform; the IR map clearly indicates two distinguishable areas of low and high brightness above the C1 and C2 contact areas (see dashed small rectangles #1 and #2 in Fig. 4a). Very similar features to those shown in Fig. 4a were obtained for the chip activation using the contact combinations C2-C3 and C1-C3 pairs.

Shown in Fig. 5 is the IR radiation intensity distribution along the long side of the chip activated through the C1-C3 pair of contacts (raw data). The above distribution clearly reveals the heat dissipation bottlenecks, namely, two intensity steps at thin substrate regions located at  $x \sim 0.6$  mm and  $x \sim 1.2$  mm in Fig. 5. This result is not a surprise since these distribution steps naturally originate from the



**Fig. 4** (a) False IR image of the troika surface activated by current  $I_{C1C2} = -15$  mA (see vertical arrow indicating current direction) together with the areas above the anodes (dashed lines) and  $\Delta L(x, y)$  color scale on the right; (b) troika schematic (top n-InAs substrate view) with projections of mesas, separation grooves, contacts (all dashed lines) and the area for analysis  $\Delta X \Delta Y$  (dashed line).

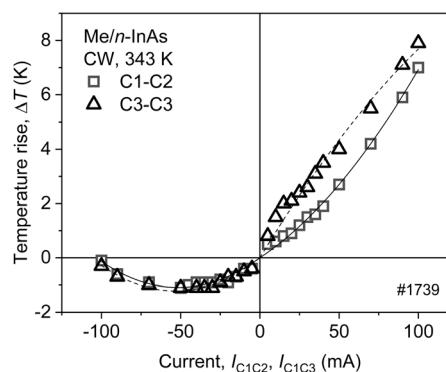


**Fig. 5** Thermal radiation intensity  $L(x, y)$  at the  $n$ -InAs surface vs. the distance along the symmetry axis  $X$  ( $Y = 0$ ) with two directions of current: from left to right (solid lines) and from right to left (dashed lines).

low lateral thermal conductivity in the regions of deep separation grooves. The surprise is that, at both polarities, the radiation peaked at the contact with the positive polarity and subsided at the negatively biased electrode (contact).

The difference in the Joule heat power dissipated at the two contacts with different resistance ( $R_{C1} = 0.2 \Omega$ ,  $R_{C3} = 0.15 \Omega$ ) could hardly be responsible for the lack of symmetry in the 1D distributions shown in Fig. 5, as the thermal generation is insensitive to the bias polarity. Moreover, the intensity behavior at a negatively biased contact at some contact pair connections contradicts the Joule heating law: the thermal emission intensity declines as the current increases. This contact feature, that is, the heat pump ability, is demonstrated in Fig. 6, where the maximum temperature rise with respect to ambient temperature value at a contact region is plotted against the current. As seen from Fig. 6, some regions above the contact appeared 1 K colder than the ambient temperature at a pumping current of  $\approx -50$  mA. This means that, under these conditions, the Joule heat power is smaller than the heat pump power and the Peltier process dominates.

The Seebeck effect, which is a mirror-like image of the Peltier process, has been observed using a noncontact IR



**Fig. 6** Maximum temperature rise  $\Delta T$  in the contact regions C1 ( $X = 0.35$ - $0.5$  mm) in the contact pair C1-C2 (squares) and C3 in the pair C1-C3 ( $X = 1.6$ - $1.75$  mm) vs. current.



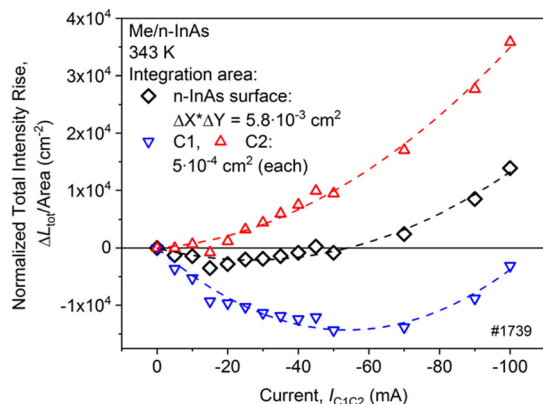


Fig. 7 Normalized total intensity rise vs. the current  $I_{C1C2}$  at three integration areas: above the contacts C1 and C2 (triangles) and above the (100)  $n$ -InAs surface (clubs).

sensing technique as described elsewhere.<sup>21</sup> In our study, a temperature gradient was formed by a 0.98  $\mu\text{m}$  diode laser emission ( $P = 0.1$  W,  $\tau = 0.5$  s) with a  $\sim 800$   $\mu\text{m}$  wide spot on the  $n$ -InAs substrate near one of the three mesa areas ( $A_{ij} = 1, 2, 3$ ). For example, a temperature difference of  $\Delta T_{A1A3} = T_{A1} - T_{A3} = 313 - 315 = -2$  K resulted in Seebeck voltage on the C1–C3 pair of contacts with a corresponding short circuit current of  $I_{C1C3} = -280$   $\mu\text{A}$ , while an alternative laser beam position ( $\Delta T_{A1A3} = 314.5 - 313 = 1.5$  K conditions) resulted in a sign change of the current induced by the Seebeck effect ( $I_{C1C3} = 280$   $\mu\text{A}$ ).

The cooling ability of the Me/ $n$ -InAs junction could be also traced through an analysis of total radiation intensity measurements, presented in Fig. 7. The normalized total thermal emission intensity rise  $\Delta L_{\text{tot}}/\text{area}$  shown in Fig. 7 is understood as  $\Delta L_{\text{tot}} = L_{\text{tot}}(U \neq 0) - L_{\text{tot}}(U = 0) = \int \Delta L(x, y) dx dy$  normalized to the integration area and refers to 1) the area above the whole  $n$ -InAs substrate surface ( $\Delta X \Delta Y$  in Fig. 4b) and 2) the areas designated by the dashed rectangles in Fig. 4a, that is, to the areas above the contacts. As seen in Fig. 7, at currents of  $(-20 \div 0)$  mA, negligible heating is observed in the area above the positively biased contact C2. At the same time, a temperature reduction is seen at the negatively biased contact C1 area, since the corresponding intensity integral is less than zero. The cooling ability of the C1 contact area remains down to  $\sim -100$  mA, evidence both for the cooling ability saturation and the Joule heating enhancement. Note that at  $I = (-50 \div 0)$  mA, the integral thermal intensity is less than the ambient intensity, which means the sample surface is cooling as a whole.

## Discussion

At 343 K, InAs attains a nearly intrinsic conductivity which is essential for the start of at least two current induced effects: heat transfer by the current<sup>17</sup> and charge carrier exclusion.<sup>22</sup> In an  $n$ -type semiconductor, the conduction band bottom is above the Fermi level by a value of  $E_n$ . The average energy of carriers in the conduction band is assumed to be  $2kT$  for the

phonon scattering mechanism. Therefore, the energy ( $E_n + 2kT$ ) is taken from the lattice at the transition of an electron from the metal to the conduction band of the nondegenerate  $n$ -type semiconductor.<sup>17</sup> On the other hand, the reduction of the charge carrier concentration initiated by the exclusion in InAs is also followed by thermal emission suppression and is accompanied by negative luminescence.<sup>23</sup> The latter process is responsible for the sample temperature decay as well.<sup>13,14</sup>

The abovementioned effects may be responsible for the sample cooling in our experiments as these particular effects are usually accompanied by other sample properties, namely specific features of  $I$ - $V$  characteristics. As seen in Fig. 3, there are no grounds to consider any kind of barriers at the Me/ $n$ -InAs interface as the  $I$ - $V$  characteristics are linear.

The electron–phonon drag is closely related to the cooling effect explanation as it is a bulk effect that does not prove the existence of interface barriers.<sup>24</sup> However, in our case, the process is inverted so that it should be considered a phonon–electron drag process.

It is worth mentioning that the heat pump power of the Me/ $n$ -InAs structure in terms of the local temperature decrease  $\Delta T \approx 1$  K appeared comparable with those reported for electronic pump engines other than Peltier coolers.<sup>25</sup>

The spatial nonequilibrium temperature distribution was smooth, and the cooling area covered the neighboring  $p$ - $n$  junctions as well. Thus, the activation of current in the substrate (bias onto a  $C_i$ - $C_j$  contact pair) could be useful in precise photometric measurements for temperature stabilization of a diode operating in photovoltaic mode (*e.g.*, using the  $C_i$ - $A_i$  pair of contacts).

## Conclusions

The measurements of temperature in current activated Me/ $n$ -InAs structures revealed cooling of the sample near the contact that delivers electrons into  $n$ -InAs and heating of the opposite contact area. The surface temperature drop was as high as  $\Delta T \approx 1$  K at an ambient temperature of 343 K and a CW current of  $I = 50$  mA in spite of Joule heating. At currents higher than 50 mA, the above heat pump ability saturates. The results show a potential for the fabrication of heterostructures with a built-in cooler that is monolithically integrated with another electronic device, *e.g.*, an LED or photodiode.

## Author contributions

N. D. Il'inskaya: resources, writing – Review & Editing (equal), S. A. Karandashev: methodology, validation, writing – review & editing (equal), T. S. Lukhmyrina: data curation, formal analysis (equal), visualization, writing – review & editing (equal), B. A. Matveev: conceptualization, formal analysis (equal), writing/original draft preparation, M. A. Remennyi: project administration, supervision, writing – review & editing (equal), A. E. Chernyakov: investigation, software.



## Conflicts of interest

There are no conflicts to declare.

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