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Melting of aqueous NaCl solutions in porous materials: shifted phase transition distribution (SIDI) approach for determining NMR cryoporometry pore size distributions[†]

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Nuclear magnetic resonance cryoporometry (NMRC) and differential scanning calorimetry thermoporometry (DSC-TPM) are powerful methods for measuring mesopore size distributions. The methods are based on the fact that, according to the Gibbs–Thomson equation, the melting point depression of a liquid confined to a pore is inversely proportional to the pore size. However, aqueous salt solutions, which inherently exist in a broad range of biological porous materials as well as technological applications such as electrolytes, do not melt at a single temperature. This causes artefacts in the pore size distributions extracted by traditional Gibbs–Thomson analysis of NMRC and DSC-TPM data. Bulk aqueous NaCl solutions are known to have a broad distribution of melting points between the eutectic and pure water phase transition points (252–273 K). Here, we hypothesize that, when aqueous NaCl solution (saline) is confined to a small pore, the whole melting point distribution is shifted toward lower temperatures by the value predicted by the Gibbs–Thomson equation. We show that this so-called shifted phase transition distribution (SIDI) approach removes the artefacts arising from the traditional Gibbs–Thomson analysis and gives correct pore size distributions for saline saturated mesoporous silica gel and controlled pore materials analyzed by NMR cryoporometry. Furthermore, we demonstrate that the method can be used for determining pore sizes in collagen–chondroitin sulphate hydrogels resembling the composition of the extracellular matrix of articular cartilage. It is straightforward to apply the SIDI analysis for DSC-TPM data as well.

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1. Introduction

Mesoporous materials and their associated pore structures are of interest to several fields of science and technology. They have pores ranging from 2 to 50 nm in diameter and are of high interest with over 4000 publications related to the topic each year.^{1–3} Mesoporous materials have applications in areas such as catalysis,^{4,5} electronics,^{6–8} construction materials,^{9–11} medicine^{12–14} and energy storage.¹⁵ Due to an increasing use of mesoporous materials, there is a need for reliable

characterization methods capable of measuring their pore size distributions.

Gas adsorption and desorption^{16–18} as well as mercury intrusion porosimetry (MIP)^{19,20} are the most popular methods for measuring pore size distributions of mesoporous materials. However, neither method can be applied to wet samples. One alternative method is thermoporometry (TPM).²¹ TPM is a calorimetric method that utilizes differential scanning calorimetry (DSC) for the observation of solid–liquid phase transitions in pores which can be applied to wet samples.^{2,3,12,21–24} Another means for detecting the distribution of phase transitions is Nuclear Magnetic Resonance Cryoporometry (NMRC).^{25–27} DSC-TPM and NMRC methods are based on the fact that liquid confined in a small pore melt at a lower temperature than free liquid. The melting point depression ΔT is mathematically related to the pore size through the Gibbs–Thomson equation

$$\Delta T = T_0 - T = \frac{2\gamma_{\text{sl}} T_0}{\rho \Delta h r} = \frac{k}{r} = \frac{2k}{d}, \quad (1)$$

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in which T_0 is the melting point of bulk liquid, γ_{sl} is the surface tension at the solid–liquid interface, ρ is the density of the solid liquid, Δh is the specific enthalpy of melting, r is the pore radius and d is the pore diameter.^{25–27} The surface tension, density, enthalpy of melting, and melting point are liquid specific and required to be known *a priori* which is often impractical. In practice, the combined liquid Gibbs–Thomson coefficient k is determined using samples with known pore sizes saturated in the probe liquid of choice. The most common liquid is water.²⁸ However, other liquids such as benzene,²⁹ acetonitrile,³⁰ acetone,³¹ and cyclohexane³² have also been used. In DSC-TPM, melting point distribution of liquid is determined from the heat flows associated with the melting transitions when the temperature of initially frozen sample is raised.^{2,3,21} In NMRC, the amount of unfrozen solvent as a function of temperature is determined by quantitative spin echo or Carr–Purcell–Meiboom–Gill (CPMG)³³ NMR experiments, in which the signal of frozen solvent is filtered out based on its much shorter T_2 relaxation time.^{25–27,34}

Due to their versatility, DSC-TPM and NMRC have found lots of applications for measuring the pore size distributions in a range of hydrated solid porous media,^{9,10,28,35–40} gels^{14,24,31,41,42} and biological samples including wood,^{43–45} skin,²² articular cartilage¹² and collagen fibres.⁴⁶ However, despite the advantages of the methods for measuring wet samples, they have not been widely applied to biological samples because the use of a pure probe liquid is required. This limits their use because many biological samples need to be stored in a salt solution to prevent swelling. Bulk aqueous NaCl solution does not have a single freezing or melting temperature. Instead, it has a broad melting point distribution between the melting point of pure water (273 K) and eutectic phase transition temperature (252 K).⁴⁷ Therefore, it is not possible to assume that a single lowered melting point temperature is associated with a single pore size like in the traditional Gibbs–Thomson equation-based pore size analysis. It has been experimentally verified that replacing pure water by a salt solution shifts the pore size distribution obtained by NMRC towards smaller pore sizes.⁴⁸ Similar issue may be encountered in technological applications such as freezing and melting studies of aqueous electrolytes confined within mesopores.⁴⁹

Recently, there has been some efforts to evaluate how the phase transitions in salt solutions can be exploited in DSC-TPM. Burba *et al.* observed that confined aqueous NaCl solutions have dominant melting points that are lower than those of pure water confined within the same porous silica host, and the magnitude of the melting point depression increases with increasing salt concentration.⁵⁰ Furthermore, they developed an extended Gibbs–Thomson equation for the melting of the ice phase in dilute NaCl solutions in porous materials. Similarly, Malfait *et al.* introduced an extended version of Gibbs–Thomson equation for the melting of aqueous solutions of glycerol confined in porous material.⁵¹ These rigorous equations provide theoretical framework to understand the melting behaviour of the pore-confined solutions with different concentrations, however their use in practical applications is not straightforward. The depression of the

eutectic phase transition has previously been observed in several salt solutions in porous media. Meissner *et al.*⁵² showed that there is a systematic decrease in the eutectic phase transition temperature with decreasing pore size and increasing salt concentration for a series of aqueous salt systems in silica materials, indicating that the eutectic phase transition depression could be used for determining pore sizes by DSC-TPM. Majda *et al.*¹² exploited the eutectic melting point depression for determining the pore size distribution in bovine cartilage saturated in saline (0.9 wt% of NaCl in water) by DSC. The resulting pore size distributions included a single peak at the lower edge of detection, at about 6 nm, with a tail over a range of pore sizes up to 200 nm. However, also these methods rely on an assumption of a single phase transition temperature, which is not strictly correct for salty solutions, and therefore they may produce artefacts in pore size distributions, especially for the systems including several pore sizes. Furthermore, the amount of saline freezing/melting in the eutectic phase transition is only about 3% of the total amount of saline, and therefore the methods relying on the eutectic phase transitions are rather insensitive. Depression of both dominant and eutectic phase transition temperatures of NaCl solution in porous structure is explained by the larger fraction of pore volume occupied by salt hydrates.^{50,52} In pore-confined NaCl solutions, the Na⁺ ions strive to position along the pore walls.⁴⁹ In addition, during freezing, salts have a habit of crystallizing in form of hydrates, which makes them occupy larger space. This changes the surface to volume ratio of the pore wall which the solution experiences, leading to lowered melting points.

In this study, we propose a novel method for determining pore size distributions, which does not assume a single phase transition temperature of saline in a pore. Instead, we assume that, for saline confined to a pore, the whole melting point curve of bulk saline is shifted towards lower temperatures, and the shift is inversely proportional to pore size according to the Gibbs–Thomson equation. This is a reasonable assumption, because, as described above, both dominant and eutectic phase transition temperatures have been shown to be lowered in a small pore size.^{50,52} This so-called shifted phase transition distribution (SIDI) method is tested by studying melting of saline in mesoporous silica gels and control pore glasses as well as hydrogels mimicking extracellular matrix of articular cartilage using NMRC. We show that the method results in pore size distributions which are in good agreement with the known pore sizes, and the distributions do not include artificial peaks, which are present in the distributions obtained by assuming a single dominant or eutectic phase transition point in a pore. Furthermore, the sensitivity of the method is significantly higher than that of the method relying on the observation of depressed eutectic phase transition temperature. The SIDI method is applicable for analysing DSC-TPM data as well.

2. Materials and methods

2.1. Materials

Porous materials saturated with saline (0.9 wt% NaCl in H₂O) were investigated by NMRC. The porous materials included



three silica gels (SG, Merck, Darmstadt, Germany) with mean pore diameters of 4, 5, and 10 nm and particle sizes of 63–200 µm, and one controlled pore glass (CPG, CPG Inc, Lincoln Park, New Jersey) with mean pore diameter of 8.1 nm and particle sizes of 125–177 µm, respectively. The sizes were given by the manufacturers. The samples are referred to as SG 4 nm, SG 6 nm, SG 10 nm and CPG 8.1 nm, respectively. The samples were placed in a 5 mm NMR tube with a layer of bulk saline above the particles, which was partially inside the NMR detection region and used as an internal standard. For comparison, a bulk saline sample including 0.9 wt% NaCl in water without any porous material was also analysed.

Four hydrogel samples were prepared with varying collagen type II and chondroitin sulphate (CS) content in phosphate buffered saline (PBS): 20 mg g⁻¹ of collagen type II with 10 mg g⁻¹ of CS, and 40 mg g⁻¹ of collagen type II with 0, 10 mg g⁻¹ or 20 mg g⁻¹ of CS. Collagen solution (rat tail, ~6 mg mL⁻¹ in 0.01 M acetic acid, Merck KGaA, Darmstadt, Germany), 5 mL and 10 mL for final collagen concentrations of 20 mg g⁻¹ and 40 mg g⁻¹, respectively, was added to a sample tube together with 0.15 mL 10× PBS. Stock solution of CS (50–80 mg mL⁻¹ CS powder from bovine trachea, Merck KGaA, Darmstadt, Germany in double distilled water) corresponding to the desired final CS concentration was added to the collagen solution and the mixture was diluted with double distilled water to give a total volume of 6 and 11 mL, respectively. Samples were thoroughly mixed, and pH adjusted to basic (pH: 8–9) using 1 M sodium hydroxide (NaOH) and 0.5 M hydrochloric acid (HCl). Sample tubes were placed for 45–60 min in a water bath at 37 °C to solidify the mixture into a gel. If samples did not solidify during this time, the pH adjustment and incubation steps were repeated. The solid was removed from the sample tubes, transferred into a plastic cell culture dish, and dried at 40 °C in a laminar flow oven until the mass of each sample was reduced to 1.50 ± 0.03 g in order to achieve final collagen contractions higher than the concentration of the commercially obtained solution. Finally, these samples were also placed in 5 mm NMR tubes.

2.2. NMRC measurements

¹H NMRC experiments were performed using a Bruker Avance III 500 MHz spectrometer equipped with a 10 mm BBO probe and liquid nitrogen evaporator for sample cooling. NMR signal intensity was acquired as a function of temperature using the CPMG pulse sequence.³³ In the analysis of the NMRC data, the intensity of the first CPMG echo was used. The CPMG was run with a 200 µs echo time and 5000 echoes for a total detection time of 1 second. The whole CPMG trace was collected to assure the quality of the experiments and to evaluate whether the echo time was suitable for filtering the solid signal. Relaxation delay was 3.5 s and 64 scans were acquired. The CPMG experiment time was 4 min 49 seconds. In the measurements of the silica gels and the controlled pore glass, the temperature was varied from 185 to 293 K by 1.15 K steps for a total of 95 steps, and in the measurements of the hydrogels, from 185 to 191.2 K by 1.8 K steps for total of 60 steps. Average heating rate was about 0.13 K min⁻¹. At the beginning of the experiment, the sample

was kept at 185 K for 3 h to ensure the sample reached equilibrium. The total experiment time of the whole temperature series was 17 h.

2.3. Data analysis

The data analysis included fitting of eqn (9) (the SID1 signal curve) with the experimental NMRC signal intensities measured as a function of temperature. Sums of least squares were minimized using Solver in Excel. The Excel files can be found from ESI.† In the fitting, the melting point distribution was assumed to be a sum of two or three Gaussian functions (eqn (12), $N = 2$ or 3), from which one corresponds to melting of bulk saline. The melting point distributions were converted into pore size distributions by using eqn (11). For comparison, NMRC signal intensities were also converted into pore size distributions by the standard Gibbs–Thomson analysis using eqn (8). An alternative Python based code for the SID1 analysis (sidiPackage) is given in the ESI.†

3. Results and discussion

3.1. Freezing and melting of bulk saline

The phase diagram of NaCl and water binary system is shown in Fig. 1a.^{53,54} According to the diagram, saline, 0.9 wt% of NaCl in water, starts to freeze when the sample is cooled below 272.8 K. A small portion of liquid turns into ice, and NaCl is squeezed out from the ice phase, increasing the NaCl concentration in the remaining liquid (brine) phase and therefore decreasing its freezing point. As illustrated in Fig. 1e, the relative amount of ice increases with decreasing temperature, and, at the same time, the NaCl concentration of the residual liquid brine increases. At the eutectic phase transition temperature (252 K), remaining high NaCl concentration (23 wt%) brine solidifies.

According to ref. 53 and 54, the freezing/melting temperature of brine as a function of NaCl mass fraction w_{NaCl} (wt%) is

$$T = b_1 w_{\text{NaCl}}^2 + b_2 w_{\text{NaCl}} + T_0, \quad (2)$$

where $b_1 = -0.0234$ K, $b_2 = -0.418$ and T_0 is the freezing/melting temperature of pure water without NaCl (273.15 K). Hence, the mass fraction of NaCl in the unfrozen liquid brine as a function of temperature is

$$w_{\text{NaCl}} = \frac{-b_2 - \sqrt{b_2^2 - 4b_1(T_0 - T)}}{2b_1}. \quad (3)$$

On the other hand, as all NaCl squeezes out from the ice phase during freezing, the mass fraction of NaCl in brine is

$$w_{\text{NaCl}}(T) = \frac{m_{\text{NaCl}}^{\text{tot}}}{m_1} \cdot 100\% = \frac{m_0}{m_1} w_{\text{NaCl}}^0 \cdot 100\%, \quad (4)$$

where $m_{\text{NaCl}}^{\text{tot}}$ is the total mass of NaCl in the sample, m_1 is the mass of the unfrozen liquid brine, m_0 is the total mass of saline, and w_{NaCl}^0 is the NaCl mass fraction in unfrozen saline (0.9 wt%). Consequently, according to eqn (3) and (4), the mass

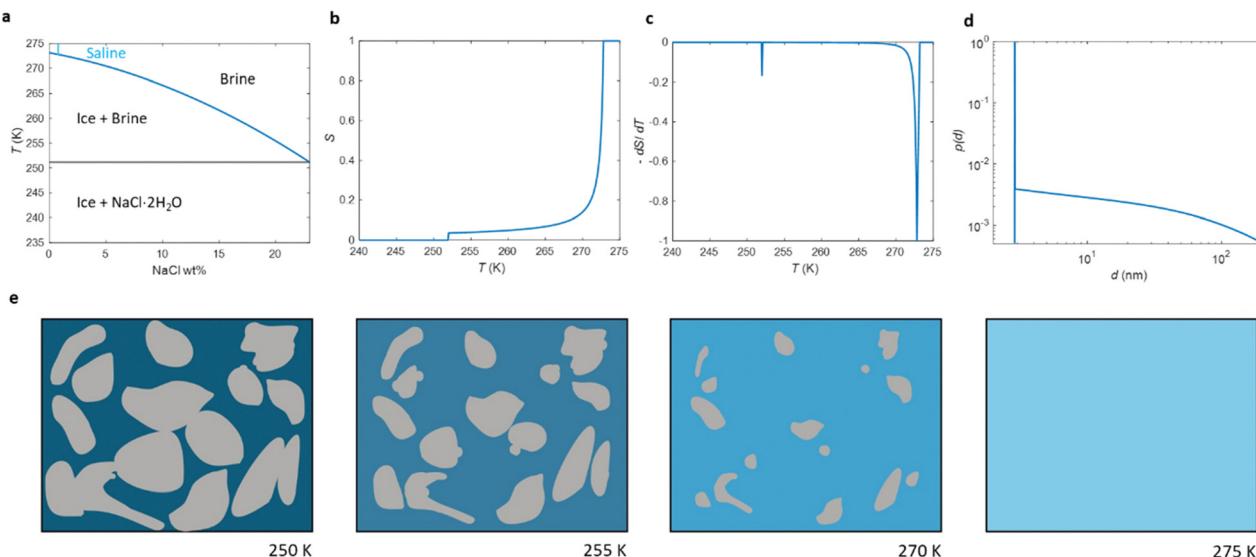


Fig. 1 (a) Phase diagram of NaCl and water binary system. The light blue vertical line represents the saline including 0.9 wt% NaCl. (b) Theoretical (eqn (7)) NMRC signal intensity of bulk saline as a function of temperature. The intensity is proportional to the amount of liquid water in unfrozen brine. (c) Negation of the derivative of the theoretical NMRC signal intensity as a function of temperature, which is equivalent to the heat curve observed in DSC-TPM. The peaks corresponding to the dominant and eutectic phase transition are visible around 272.8 and 252 K. The derivative is non-zero over the whole region in between of those temperatures. (d) Pore size distribution obtained by analyzing the theoretical bulk saline NMRC melting curves using the Gibbs–Thomson equation (eqn (1), $T_0 = 272.8$ K). Note the logarithmic scale on the vertical axis. The distribution includes an artificial peak around 3 nm due to eutectic melting point as well as non-zero values at higher pore sizes due to continuous melting of saline between the eutectic and dominant melting points. (e) Schematics of freezing and melting of saline. Light blue represents liquid saline/brine (saline refers to 0.9% NaCl solution, brine to higher salt concentration), gray ice and dark blue solidified brine. At 275 K, whole saline sample is in liquid state. Below 272.8 K, saline starts to freeze, and small ice crystals are visible at 270 K. During freezing, NaCl is squeezed out from ice, increasing NaCl concentration in liquid brine (illustrated by darker blue color). The amount of ice and size of ice crystals increases with decreasing temperature.⁴⁷ Below the eutectic phase transition point (252 K), remaining high NaCl concentration (about 23 wt%) brine is solidified.

of unfrozen liquid brine as a function of temperature is

$$m_l = \frac{2b_1 m_0 w_{\text{NaCl}}^0}{-b_2 - \sqrt{b_2^2 - 4b_1(T_0 - T)}}, \quad (5)$$

The mass of water in unfrozen liquid brine is

$$m_w = m_l - m_{\text{NaCl}} = m_l \left(1 - \frac{w_{\text{NaCl}}}{100\%}\right) = \left[\frac{2b_1}{-b_2 - \sqrt{b_2^2 - 4b_1(T_0 - T)}} - 0.01 \right] m_0 w_{\text{NaCl}}^0. \quad (6)$$

Signal intensity in the NMRC experiment after the Curie correction⁵⁵ is proportional to m_w . Consequently, relative NMRC signal intensity of bulk saline with respect to the maximum signal intensity above 272.8 K can be expressed as

$$S_b = \left[\frac{2b_1}{-b_2 - \sqrt{b_2^2 - 4b_1(T_0 - T)}} - 0.01 \right] m_0 w_{\text{NaCl}}^0, \quad (7)$$

when $252 \text{ K} \leq T \leq 272.8 \text{ K}$. Below the eutectic melting point (252 K), $S_b = 0$, and above the freezing point of saline (272.8 K), $S_b = 1$.

Relative NMRC signal as a function of temperature (eqn (7)) is plotted in Fig. 1b. At the lowest temperatures, signal is zero, as there is only $\text{NaCl}\cdot 2\text{H}_2\text{O}$ and ice. At the eutectic melting point (252 K), there is a sudden increase in the intensity from 0 to about 0.03, *i.e.* eutectic melting corresponds to about 3% of

the maximum amplitude. Thereafter, the signal increases slowly with increasing temperature. Before 272.8 K, there is a sharp increase in signal intensity due to dominant melting transition of saline.

An alternative way for visualizing the melting point distribution is to plot the derivative of the NMRC signal, dS/dT , as a function of temperature, or alternatively $-dS/dT$, because the latter function is analogous to the heat flow graphs of endothermic melting transitions obtained in DSC TMP experiments. The theoretical $-dS/dT$ curve represented in Fig. 1c show a major phase transition around 272.8 K and a minor phase transition corresponding to eutectic melting point at 252 K. The derivative is non-zero over the whole region in between these points.

3.2. Melting of saline in porous materials

In conventional NMRC and DSC-TMP analysis, porous materials are saturated with a single component probe liquid, such as water,²⁸ acetonitrile³⁰ or cyclohexane,³² which freeze or melt in a single temperature. The freezing or melting point of the liquid in a small pore is lower than that of bulk liquid, and typically freezing occurs at lower temperatures than melting. This phenomenon of different freezing and melting temperatures of liquid in pores is called freezing-melting hysteresis. Hysteresis originates from the nucleation barriers and pore blocking effects which are present only during freezing.³⁵ Here, only the melting transitions are discussed.



According to the Gibbs–Thomson equation (eqn (1)), the melting point depression is inversely proportional to the pore size. The NMRC signal intensity, being proportional to the amount of unfrozen probe liquid, reveals the distribution of melting points in the sample. Consequently, the NMRC signal intensity can be converted into pore size distribution using the following equation:²⁶

$$p(r) = \frac{k}{r^2} \frac{dS}{dT}. \quad (8)$$

In DCS-TMP, heat flow graphs reveal the melting point distribution, and pore size distribution is calculated by an equation analogous to eqn (8).

Because binary liquids, such as aqueous solutions of NaCl, do not freeze or melt at a single temperature, conventional pore size distribution analysis by the Gibbs–Thomson equation results in artefacts. For example, when the theoretical NMRC signal curve of bulk saline shown in Fig. 1b is converted into pore size distribution by eqn (8) using $k = 30 \text{ K nm}$, which is a typical value determined for water,²⁶ the distributions shown in Fig. 1d include a sharp peak around $d = 3 \text{ nm}$ arising from the eutectic transition as well as a broad distribution of pores above that due to continuous melting of brine between the eutectic and dominant phase transition temperatures (252–272.8 K), although the bulk saline includes no pores. Therefore, different a kind of analysis is needed.

As explained in Introduction, according to ref. 12, 50 and 52 both eutectic and dominant phase transitions of binary solutions of water and salts are lowered, when the solutions are confined to a small pore, allowing, in principle, estimation of pore sizes by means of the Gibbs–Thomson equation. However, if the melting point depression of the dominant transition is used in the determination of pore size distribution, artificial peaks due to eutectic phase transition as well as the distribution of melting points in between the eutectic and dominant phase transition temperatures are observed, leading to a biased picture about the porous structures. In principle, determination of pore size distribution based on depression of eutectic phase transition would be less prone for artefacts, as the derivative of the signal above the eutectic phase transition point is small (see Fig. 1b and c). However, this approach suffers from low sensitivity, as the signal corresponding to the eutectic phase transition is only about 3% of the maximum signal.

Here, we propose an alternative way for extracting pore size distribution from NMRC signal and DSC-TMP heat flow graphs of binary solutions of water and salts confined to porous materials. As both eutectic and dominant melting point depressions are known to be inversely proportional to pore size, we hypothesize that, for saline confined to a small pore, the whole melting point curve (eqn (2)) is shifted towards lower temperatures by the amount indicated by the Gibbs–Thomson equation (eqn (1)), as illustrated in Fig. 2a. The proposed phase diagram has a close resemblance with the experimentally observed phase diagrams of $\text{H}_2\text{O}-\text{CaCl}_2$ binary solution in bulk and KSKG silica gel.⁵⁶ Consequently, the NMRC signal intensity

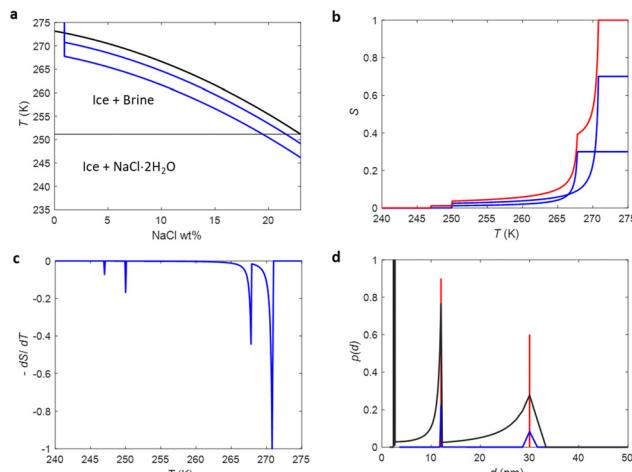


Fig. 2 (a) Phase diagram of NaCl and water binary system. The diagram is identical to Fig. 1a but complemented with the hypothesized concentration curves of saline confined to small pores with two different pore sizes, in which the concentration curves of bulk saline are shifted by 2 and 5 K (blue lines). (b) Theoretical NMRC signal of a saline saturated sample including the two different pore sizes ($d = 30$ and 12 nm , relative pore volumes 0.7 and 0.3, respectively), calculated by eqn (9). The signals of each component are represented by blue lines and their sum by red solid line. (c) Corresponding derivative plot. (d) Pore size distributions obtained by the conventional Gibbs–Thomson analysis (eqn (8)) using the dominant (272.8 K, black line) and eutectic (252 K, blue line) melting point depression as well as the SID analysis proposed in this article (red line). In the analysis, k was assumed to be 30 nm K .

function of saline in a small pore has the same shape as bulk saline (eqn (7)), but it is shifted towards lower temperatures. In the general case, in which the sample includes pores with different sizes, NMRC signal is an integral of the NMRC signal distributions corresponding to the bulk saline (eqn (7)) shifted by the melting point depression ΔT indicated by the Gibbs–Thomson equation (eqn (1)) and weighted by the melting point distribution corresponding to the pore size distribution:

$$S = \int p_{\text{mp}}(\Delta T) S_b(T - \Delta T) d\Delta T. \quad (9)$$

This is called the SID signal curve. Here, the melting point distribution $p_{\text{mp}}(\Delta T)$ refers to the distribution of the dominant, highest temperature melting points, which are spread over a range of temperatures due to pore size distribution. Bulk saline corresponds to $\Delta T = 0$ (infinite pore size) in eqn (9). The melting point distribution can be determined by fitting eqn (9) with the measured NMRC signal amplitudes. Alternatively, derivatives of the signals, which are analogous to heat flow graphs in DSC-TMP experiments, can be used in the fittings:

$$\frac{dS}{dT} = \int p_{\text{mp}}(\Delta T) \frac{dS_b(T - \Delta T)}{dT} d\Delta T. \quad (10)$$

As the melting point distribution $p_{\text{mp}}(\Delta T)$ reflects the relative volume of pores associated with the melting point depression of ΔT , the melting point distribution can be converted into pore

size distribution by the following equation:

$$p(r) = \frac{k}{r^2} p_{\text{mp}}(\Delta T). \quad (11)$$

The shape of $p_{\text{mp}}(\Delta T)$ obtained by fit of eqn (9) or (10) is heavily affected by experimental noise. The stability of the fitting can be improved by using regulators and constraints including *a priori* knowledge or guesses about the shape of the melting point distribution. One option is to assume that the melting point distribution is a sum of N Gaussian functions:⁵⁷

$$p_{\text{mp}}(T) = \sum_{i=1}^N \frac{p_{\text{mp}}^i}{\sigma_i \sqrt{2\pi}} \exp\left[-\frac{(T - T_{ci})^2}{2\sigma_i^2}\right], \quad (12)$$

where p_{mp}^i is the integral, σ_i is the standard deviation, and T_{ci} is the mean melting temperature of component i .

Fig. 2b shows a theoretical NMRC signal curve of a sample including pores with two different sizes saturated by saline calculated by eqn (9). In the calculations, ΔT values associated with the bigger and smaller pores were assumed to be 2 and 5 K and relative pore volumes are 0.7 and 0.3, respectively. The curves corresponding to individual pores are drawn by blue lines and their sum by red line. Corresponding derivative curves, calculated by eqn (10), are shown in Fig. 2c. The derivative curves show two major peaks around 270 and 267 K associated with the depressed dominant phase transition temperatures in the big and small pores, respectively. Furthermore, there are two smaller peaks around 248 and 245 K related to the lowered eutectic phase transition points in the big and small pores, respectively. The pore size distribution calculated by converting the melting point distribution obtained by fitting eqn (9) with the signal intensity curve is shown in Fig. 2d (red curve; k was assumed to be 30 nm K).²⁶ It reveals that the sizes of the small and big pores are 12 and 30 nm, respectively. For comparison, pore size distributions obtained by the conventional Gibbs–Thomson analysis based on the dominant (black curve) and eutectic (blue curve) transition are shown in Fig. 2d as well. The former includes two artificial peaks associated with the eutectic phase transition around 2–3 nm, and the true peaks are also significantly broadened and partially overlapping due to broad dominant transition temperature range. The distribution corresponding to the eutectic phase transition does not include the artificial peaks. However, the true peaks are broadened, and sensitivity lowered as only about 3% of water molecules contribute signal. Consequently, this theoretical example demonstrates well the potential of the proposed SIDI method for improving the reliability and quality of the NMRC and DSC TMP pore size distributions.

3.3. Pore size distributions of mesoporous materials

To test how the SIDI analysis works in practice, three silica gel (SG) and one controlled pore glass (CPG) mesoporous materials saturated with saline were analysed by ^1H NMRC. NMRC signal curves of the porous materials measured as a function of temperature from 185 to 293 K are shown in Fig. 3a (solid lines). For the comparison, the signal curve of the bulk saline sample is shown as well. The experimental saline signal curve is qualitatively similar to the theoretical curve shown in Fig. 1b.

However, the experimental curve is smoothed both around the eutectic and dominant phase transition points, most probably due to experimental factors such as small temperature gradients in the sample and imperfect equilibrium due to the finite (8 min K⁻¹) temperature stabilization delays.

Above 270 K, the curves of the porous materials follow roughly the curve of the bulk saline, as this region is associated with the dominant melting transition of bulk saline on top and in between the 63–200 μm particles. The knees around 260–270 K arise from lowered dominant melting transitions of saline confined to mesopores. The knees shift to lower temperatures with decreasing nominal pore size in agreement with the Gibbs–Thomson equation. Signal intensities at the lowest temperature in the region of 200–240 K are also inversely proportional to the pore size, indicating that also the eutectic melting point shifts to lower temperatures with decreasing pore size.

Fits of the theoretical SIDI signal curve (eqn (9)) with the experimental data are shown by dotted lines in Fig. 3a. The experimental signal curve of the bulk saline was used as $S_b(T - \Delta T)$ in eqn (9), because the bulk saline and porous materials experiments were expected to have similar experimental imperfections due to the temperature gradients, heating rates *etc*. The melting point distribution $p_{\text{mp}}(T)$ was assumed to be a sum of three Gaussian functions ($N = 3$ in eqn (12)). One component is associated with the bulk transition above 270 K and another with the mesopore transition between 260 and 270 K. Furthermore, good fits require an additional low

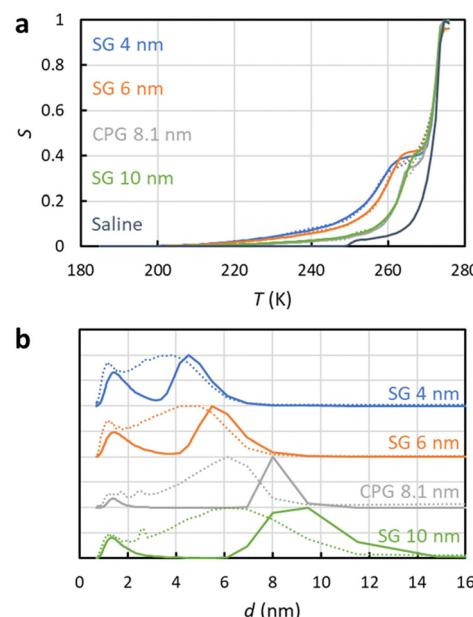


Fig. 3 (a) Experimental ^1H NMRC signal curves (solid lines) of the mesoporous silica gel (SG) and controlled pore glass (CPG) materials saturated with saline (0.9 wt% NaCl in water). For the comparison, corresponding curve of the bulk saline sample is shown as well. The dotted lines show the fits of eqn (9) with the experimental data (the SIDI approach). (b) Pore size distributions obtained by the SIDI (solid lines) and conventional (dotted lines) approaches.



temperature (230–245 K) transition component corresponding to smaller pores or non-frozen surface layer (see below).

The SIDI pore size distributions calculated by eqn (11) are shown in Fig. 3b (solid lines). The positions of the dominant peaks are in good agreement with the nominal pore sizes. The centres of the SG 6 nm and CPG 8.1 nm peaks are almost perfectly located on the nominal pore sizes. On the other hand, the centres of the SG 4 nm and SG 10 nm are shifted to slightly above and below the nominal pore size, respectively. This may reflect small inaccuracy of the method or nominal pore sizes given by manufacturers; in fact, our earlier NMC analysis of the same porous materials using acetonitrile as a probe liquid resulted in similar deviations from the nominal pore sizes.⁵⁸ The CPG 8.1 nm peak is narrower than the SG peaks because the CPG material is known to have narrower pore size distributions than the SG materials.⁵⁸

The pore size distributions also include a minor component below 2 nm, which has been observed also in the NMRC of silica materials using acetonitrile as a probe liquid.⁵⁹ It may arise from saline in micropores, or it may be an artefact arising from the non-frozen surface layer.⁵⁹

For comparison, pore size distributions obtained by the conventional Gibbs–Thomson analysis using eqn (8) are shown by dotted lines in Fig. 3b. As expected, the distributions are much broader than the SIDI distributions due to the artefacts caused by the broad melting point distribution of salty solutions. There is a broad major peak ranging from 1 nm to slightly above the nominal pore size, and the distribution extends much beyond that toward larger pore sizes due to the spread bulk transition. The mean pore size is much below the nominal pore size. There is a small bump around 2.6 nm associated with the eutectic phase transition point of the bulk saline on top and in between the particles in the pore size distributions of CPG 8.1 nm and SG 100 nm. Overall, the SIDI distributions are in much better agreement with the known pore size distributions of the materials than the distributions obtained by the conventional Gibbs–Thomson analysis.

3.4. Pore size distributions of collagen and chondroitin sulphate hydrogels

The SIDI analysis method was also tested for analysing pore sizes in hydrogels composed of varying concentrations of collagen type II and chondroitin sulphate. The collagen and chondroitin sulphate gels are models for the extracellular matrix (ECM) of articular cartilage, which is the tissue that covers the end of articulating joints. The ECM of cartilage is primarily composed of collagen type II, proteoglycans, and water (including NaCl). Collagen is a rope like protein responsible for forming the fibril network. The collagen–collagen covalent crosslinks create the collagen network. Proteoglycans are hydrophilic macromolecules composed of negatively charged glycosaminoglycans (GAGs) covalently bonded to a protein core. Chondroitin sulphate is the most common GAG in cartilage. Proteoglycans exist in the intrafibrillar space created by collagen–collagen crosslinks. Water exists within

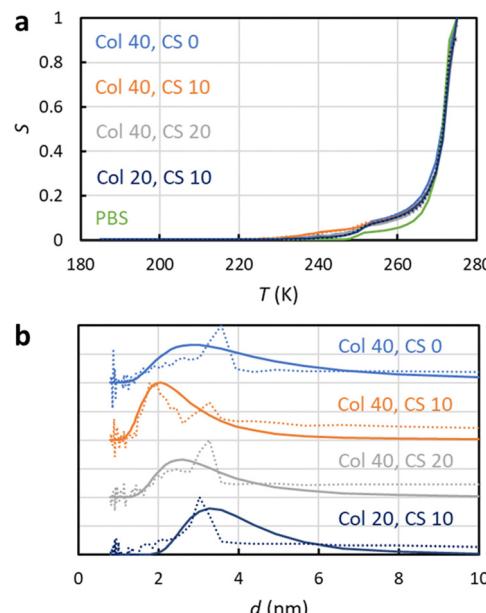


Fig. 4 (a) Experimental ^1H NMRC signal curves (solid lines) of collagen and chondroitin sulphate hydrogels. The amounts of collagen (Col) and chondroitin sulphate (CS) in the unit of mg g^{-1} are indicated in the figure. For the comparison, corresponding curve of the bulk phosphate buffered saline (PBS) sample is shown as well. The dotted lines show the fits of eqn (9) with the experimental data (the SIDI approach). (b) Pore size distributions obtained by the SIDI (solid lines) and conventional (dotted lines) approaches.

the matrix formed by the proteins and comprises about 60–80% of the tissue mass.^{60–62}

The pore size distribution of cartilage is difficult to determine as it must contain buffer solution, such as PBS, and the pore size may change under pressure and other mechanical stress. An additional constraint is that the pore size distributions in polymer gels are not well defined. To address these limitations, the effective pore size of cartilage has been measured using indirect methods such as estimating the pore size based on the transport of molecules with varying diameters^{63–67} and hydraulic permeability methods.⁶¹ The downside of these measurements is that they require the introduction of tracer molecules which interact with the sample or require the use of high pressures which may alter the structure of the sample. The cartilage ECM have been estimated to have pore sizes of 2–6 nm in the inter-GAG spacing^{62,68–72} and 10–100 nm in the inter-collagen fibril spacing.⁴⁶

NMRC signal curves of the hydrogel samples including 20–40 mg g^{-1} of collagen type II, 0–20 mg g^{-1} of chondroitin sulphate and PBS are shown Fig. 4a. The signal intensities are non-zero below the eutectic melting point of bulk PBS in the region of 230–250 K, and they are higher than the intensity of the bulk PBS sample in the region of 250–270 K due to the porosity of the gel. The pore size distributions extracted by the SIDI method include a peak ranging from about 2 to 6 nm, which is in a good agreement with the pore sizes of the inter-GAG spacing determined by the indirect methods. As the pore sizes are well above the 1 nm peak of the SG and CPG samples,



which may be an artefact arising from the non-frozen surface layer, we expect that the pore size distributions reflect true pore structures of the gels. The distributions obtained by the conventional approach include an artificial broad shoulder extending to about 40 nm due to the melting point distribution of the bulk PBS in the gels, again emphasizing the importance of the SIDI analysis.

4. Conclusions

A novel method for analysing NMR cryoporometry (NMRC) and differential scanning calorimetry (DSC) thermoporometry (TPM) data of porous materials saturated with water and NaCl binary solutions was introduced. The approach is based on the hypothesis that, in a small pore, the whole melting point distribution curve of bulk saline is shifted to lower temperatures by the value predicted by the Gibbs-Thomson equation. Theoretical analysis shows that the proposed shifted phase transition distribution (SIDI) approach removes artefacts existing in the pore size distributions obtained by the conventional Gibbs-Thomson analysis assuming a single phase transition temperature in a pore. The SIDI approach takes into account the eutectic phase transition at 252 K as well as a broad distribution of phase transitions between 252 and 273 K for bulk saline. The method was experimentally tested by measuring NMRC data of mesoporous silica gel and controlled pore glass materials saturated with saline. The SIDI pore size distributions were in good agreement with known pore size distributions of the materials, while the conventional Gibbs-Thomson analysis gave significantly biased pore size distributions. Furthermore, the method was applied for characterization of pore size distributions of hydrogels resembling the composition of articular cartilage, and the resulting pore sizes (2–6 nm) were in good agreement with the inter-GAG spacing determined by other methods. The SIDI method has a broad range of potential applications in the analysis of biological and technological electrolytes.

Author contributions

S. Mailhiot was responsible for conceptualization, methodology, validation, investigation, resources, and writing – original draft. K. Tolkkinen was responsible for conceptualization, methodology, validation, investigation, and writing – review and editing. H. Henschel, M. T. Nieminen and M. Hanni were responsible for planning and preparing the hydrogel sample, and writing – review and editing. J. Mares was responsible for making the Python SIDI analysis code, and writing – review and editing. V.-V. Telkki was responsible for conceptualization, supervision, resources, and writing – review and editing.

Conflicts of interest

There are no conflicts to declare.

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