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# Planar micro-supercapacitors toward high performance energy storage devices: design, application and prospects

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The burgeoning revolutions of portable and integrated electronic products have drastically stimulated the upgrade of traditional power supplies toward miniaturized scales. In this regard, planar micro-supercapacitors (PMSCs) are considered as candidates for energy storage devices owing to the unique two-dimensional structure, fast charge/discharge rate, high power density and long cycling lifetime. However, the manufacturing of PMSCs requires advanced techniques to provide rational designs on microelectrodes and reduce the size while maintaining high-resolution. The vacuum filtration and spray coating techniques have been used to design millimeter-scale electrodes with the assistance of an interdigital mask. The electrochemical strategy and other mask-free techniques can further reduce the size of the microelectrodes and meet the requirements of high-resolution PMSCs, including electrolytic and electrophoretic deposition, inkjet printing, laser scribing, plasma jet, nanoimprint lithography and 3D printing techniques. The precise design of PMSCs contributes to energy storage devices, sensors and filters. Furthermore, it is vital to design a microelectrode with superior structural integrity for the controllable manufacture of high precision and high performance PMSCs by considering the mechanism and key factors of microfabrication strategies.

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# 1. Introduction

The emerging miniaturized electronic components have become an integral part of the Internet of Things (IoTs), concomitantly leading to the renovation of traditional energy storage supplies to reduce the size without sacrificing the power and energy densities.<sup>1–3</sup> In particular, wearable electronics, biomedical sensors and renewable energy grids can facilitate the miniaturization and integration of energy storage systems.<sup>4,5</sup> Lithium-ion batteries (LIBs) and supercapacitors (SCs) are commonly used as the energy storage components in different fields depending on their intrinsically high energy and power densities, respectively. However, the limited lifetime and power density of LIBs may restrain their widespread application for on-chip electronics as well as be a bottleneck in micro-sized and integrated systems. Compared with LIBs, SCs can deliver long-term stability and meet the high-power requirements in automatic systems, intelligent grids and rail traffic.<sup>6–8</sup> However, the integration of traditional SCs in a miniaturized module is commonly restricted by their large space

occupancy and unsatisfactory integration capabilities. Therefore, it is expected that micro-sized energy storage devices with fertile energy and power densities will be designed and manufactured for the next generation of power supplies.

Recently, micro-supercapacitors (MSCs), especially planar micro-supercapacitors (PMSCs), have been considered as one of the candidates for traditional energy storage devices due to their unique two-dimensional structure, fast charge/discharge rate, high power density and long-term stability. The size of PMSCs can be reduced to several millimeters and even micrometers, and the corresponding planar configuration is evidently different from the conventional sandwich-like SCs.<sup>9–11</sup> The unique in-plane structure enables the integration of the monolithic device into the overall system with low space occupancy. The ion transport inside the PMSCs can be drastically accelerated owing to the interdigital structure of the planar microelectrodes.<sup>12–14</sup> The ion diffusion distance between the negative and positive electrodes can be shortened to several micrometers, which endows fast ionic diffusion kinetics for high-rate capability.<sup>15,16</sup> PMSCs can be assembled



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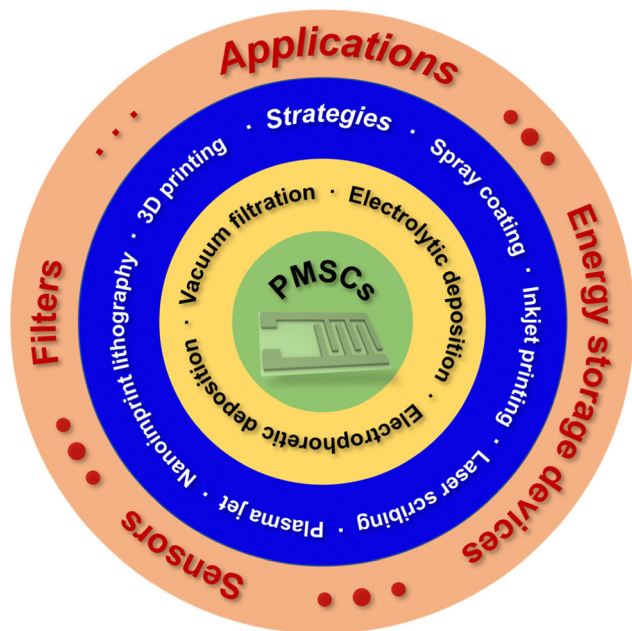


Fig. 1 Schematic diagram of the contents of this review, including strategies for constructing PMSCs and corresponding applications.

into micro-integrated systems over conventional energy storage components.<sup>17</sup> However, the technique of fabricating PMSCs remains a critical hurdle due to the complicated process. Recent reports have tended to reduce the electrode size and shorten the gap between adjacent electrodes, while retaining the high-resolution of the PMSCs simultaneously. The design strategies of MSCs have been extensively reviewed in relevant literature.<sup>18–20</sup> Researchers have focused on the recent progress in advanced techniques to demonstrate the practicality of diverse manufacturing strategies. The manufacturing strategies determine the size and precision of the microelectrodes based on the guidance of the interdigital mask. Hence, it is necessary to develop suitable design strategies for the desired PMSCs through in-depth analysis and comparison of different fabrication techniques.

Herein, we discussed the basic configurations, energy storage mechanisms and fabrication techniques of PMSCs in comparison with conventional SCs. The rational design of microelectrodes plays a key role in the manufacture of high-resolution PMSCs. For vacuum filtration and spray coating techniques, the interdigital mask can be designed as a structured guidance for the fabrication of millimeter-scale electrodes. Further reduction in the size of the microelectrodes can be achieved by electrolytic and electrophoretic deposition, inkjet printing, laser scribing, plasma jet, nanoimprint lithography and 3D printing techniques. The well-designed PMSCs with high resolution and structural integrity can be used as energy storage devices, sensors and filters (Fig. 1).

## 2. Configuration and energy storage mechanism of PMSCs

The basic configuration of PMSCs consists of four coplanar parts, including a positive and a negative electrode, a gel or

solid-state electrolyte, and a substrate. Whether the current collector is needed depends on the electrical conductivity of the electrode materials.<sup>21,22</sup> Carbon-based materials generally deliver a decent metalloid electron conductivity of  $10^3$ – $10^7$  S m<sup>−1</sup>, enabling carbon-based electrodes to be an alternative to the current collector.<sup>23</sup> Meanwhile, metal oxides and hydroxides commonly suffer from inferior electric conductivities ( $10^{-1}$ – $10^{-5}$  S m<sup>−1</sup>). Therefore, the conductive substrate in PMSCs is necessary for a high charge-transfer efficiency.<sup>24</sup> In addition, electrode materials utilized in PMSCs are basically in accordance with conventional SCs, which can be divided into two types based on the charge storage mechanisms: (1) electric double layered capacitor (EDLC) type materials, relying on the mechanism of ion adsorption/desorption on the surface of electrodes; (2) pseudocapacitive materials, depending on the reversible faradaic redox reaction between the electrodes and electrolyte ions.<sup>25</sup> Basically, the specific capacitance of pseudocapacitive materials, such as metal oxides and hydroxides, is higher than that of EDLC type materials (such as the carbon-based materials) owing to the fast reversible faradaic redox reactions.<sup>26–28</sup> However, the universal drawback of PMSCs and SCs is the unsatisfactory energy density in comparison with batteries. Various approaches have been dedicated to tackling the issue according to the equation  $E = \frac{1}{2}CV^2$ . The energy density ( $E$ ) can be directly enhanced *via* improving the specific capacitance ( $C$ ) of electrode materials and expanding the potential window ( $V$ ). In this regard, pseudocapacitive materials may be employed to push the energy density towards a higher level due to the intrinsically superior capacitance. Besides, the potential window can be expanded by assembling an asymmetric device to match the operating voltage of pseudocapacitive materials and EDLC materials for an enhanced energy density.<sup>29–31</sup>

The electrolytes used in PMSCs are mainly divided into two types, namely gel polymers and ionic liquids. Conventional aqueous electrolytes, including KOH, H<sub>2</sub>SO<sub>4</sub> and Na<sub>2</sub>SO<sub>4</sub>, have a risk of leakage in planar devices as well as a limitation in potential window (below 1.23 V) due to water electrolysis.<sup>32</sup> Meanwhile, gel polymer electrolytes have been demonstrated to be excellent electrolytes for PMSCs. In general, poly (vinyl alcohol) (PVA) is used as the host polymer to mix with acid, alkali, and neutral-based electrolytes.<sup>33–35</sup> The solvent evaporation and poor thermal stability are the main disadvantages of gel polymer electrolytes. To this end, ionic liquids have garnered tremendous attention recently for their fair stability and high operating voltage (up to 3.7 V).<sup>36,37</sup> The superior stability arises from the combination of ionic liquids and the silica matrix in polycondensation processes. Therefore, the selection of an appropriate electrolyte is critical for optimizing the energy storage capabilities and ensuring long-term cycling stability of PMSCs.

To cater for the requirements of high mechanical stability and flexibility, substrates used in the PMSCs can be classified into two categories. The first category is rigid substrates, such as silicon wafers, which are promising candidates for on-chip electronics.<sup>27,38,39</sup> As the second category, flexible substrates





(polymer, paper, and textile cloth) have been incorporated into foldable and wearable devices.<sup>40–43</sup> To evaluate the electrochemical performance of PMSCs, conventional test parameters should be finely tuned based on the planar configuration. The measurement units need to be changed to the area and volume of PMSCs instead of the mass of active materials. Generally, the areal capacitance ( $C_a$ ,  $\text{mF cm}^{-2}$ ) and volumetric capacitance ( $C_v$ ,  $\text{mF cm}^{-3}$ ) can be calculated by eqn (1) and (2), while the areal energy density ( $E_a$ ,  $\text{mW h cm}^{-2}$ ) and power density ( $P_a$ ,  $\text{mW cm}^{-2}$ ) of PMSCs can be obtained *via* eqn (3) and (4). The volumetric energy density ( $E_v$ ,  $\text{mW h cm}^{-3}$ ) and power density ( $P_v$ ,  $\text{mW cm}^{-3}$ ) can be calculated through eqn (5) and (6), respectively.<sup>20,44,45</sup>

$$C_a = \frac{I\Delta t}{S\Delta V} \quad (1)$$

$$C_v = \frac{I\Delta t}{Sd\Delta V} \quad (2)$$

$$E_a = \frac{1}{2 \times 3600} C_a \Delta V^2 \quad (3)$$

$$P_a = \frac{3600 E_a}{\Delta t} \quad (4)$$

$$E_v = \frac{1}{2 \times 3600} C_v \Delta V^2 \quad (5)$$

$$P_v = \frac{3600 E_v}{\Delta t} \quad (6)$$

where  $I$  is the discharging current (mA),  $\Delta t$  is the discharging time (s),  $S$  is the area of the microdevice ( $\text{cm}^2$ ),  $\Delta V$  is the potential window (V), and  $d$  is the thickness of the active material (cm).

The areal mass loading of the active material determines the energy storage capability of PMSCs. The higher mass loading can contribute to the improved  $C_a$  on considering two devices with equal area. However, the device resistance ( $R$ ) may also increase with the mass loading, leading to a deteriorated time constant ( $\tau$ ) according to eqn (7).<sup>11,16,19</sup>

$$\tau = RC_a \quad (7)$$

The power performance of PMSCs is closely related to  $\tau$ . A high value of  $\tau$  can result in decreased power performance. Hence, it is crucial to explore materials with high conductivity for lowering the  $\tau$  to improve the power performance and enhance the energy capability of PMSCs.

### 3. Preparation strategies of PMSCs

The trend towards miniaturized and integrated electronics has greatly stimulated the development of techniques for designing PMSCs. A variety of approaches have been dedicated to the manufacture of micro-sized electrodes. The challenge is to reduce the adjacent distance of interdigital electrodes and ensure the device has a high resolution simultaneously.<sup>32,46</sup>

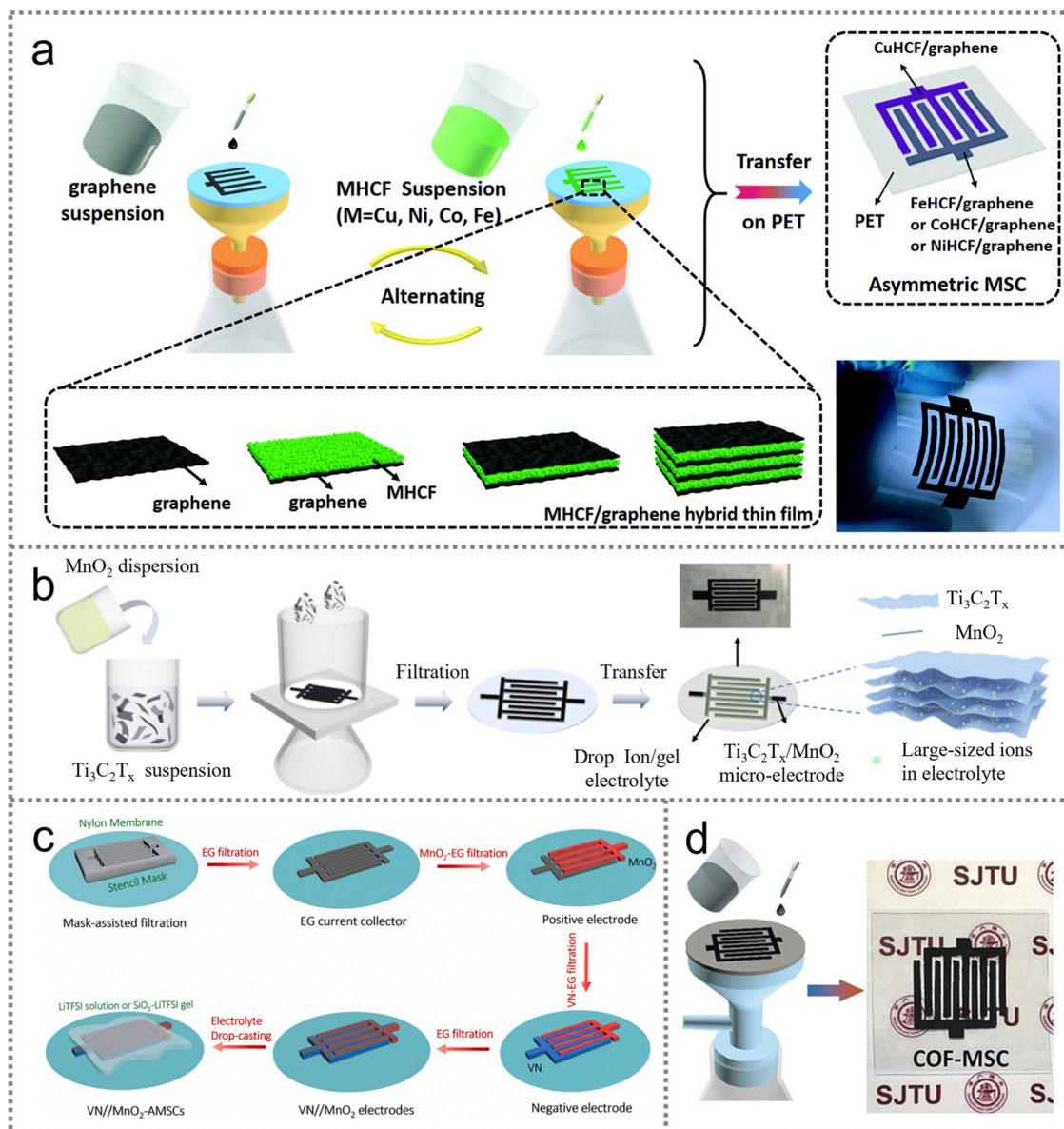
In this regard, the vacuum filtration and spray coating techniques can fabricate millimeter-sized electrodes with the assistance of masks, which are designed by laser cutting technology with a hollow interdigital structure. The electrochemical strategies can reduce the size of PMSCs to the micrometer-scale without using masks. The inkjet printing, laser scribing, plasma jet, nano-imprint lithography and 3D printing techniques can also be applied to design and manufacture miniaturized PMSCs. The working conditions of each technique determine their feasibility for large-scale fabrication and precise design of monolithic devices.

#### 3.1 Mask-assisted strategies

**3.1.1 Vacuum filtration.** The vacuum filtration strategy has been commonly used to *in situ* fabricate microelectrodes within the interdigital pattern of the mask for PMSCs.<sup>47</sup> The solid product can be directly separated from the liquid suspension by the negative pressure and the thickness of the electrodes can be tuned by the addition of suspensions. The obtained interdigital electrodes should be then transferred onto a substrate, such as polyethylene terephthalate (PET) film. The vacuum filtration strategy showed promising applications in: (1) alternative filtration, (2) composite filtration, (3) asymmetric filtration, and (4) symmetric filtration. For instance, the mask-assisted vacuum filtration approach was reported to design a series of sandwich structured transition metal hexacyanoferrates (MHCF)/graphene ( $M = \text{Cu, Ni, Co, Fe}$ ) hybrid films with an interdigital pattern (Fig. 2(a)).<sup>48</sup> The MHCF and graphene suspension were alternatively filtered ten times through an interdigital-mask on the tetrafluoroethylene (PTFE) filter membrane. The active materials could be successively stacked and the average thickness of the film was about  $2 \mu\text{m}$ , demonstrating the flexibility of filtration processes. After the electrode was transferred to the PET film, the LiCl/PVA hydrogel electrolyte was dropped onto the interdigital area to assemble the PMSC device, which exhibited a high voltage of 1.8 V. Nanorod-structured materials can be introduced to the suspension for further vacuum filtration of composite materials. A  $\text{Ti}_3\text{C}_2\text{T}_x$ -based PMSC was fabricated with a modulated inter-space *via* the filtration of  $\text{MnO}_2$ -containing suspensions (Fig. 2(b)).<sup>49</sup> The electrolyte ions could intercalate into layers for an enhanced charge storage performance. The areal capacitance of the PMSC could reach  $24.7 \text{ mF cm}^{-2}$  at the 50 wt% feeding ratio of  $\text{MnO}_2$  to  $\text{Ti}_3\text{C}_2\text{T}_x$ , indicating that vacuum filtration is a viable route to fabricate composite electrodes.

Furthermore, the vacuum filtration strategy can be used to manufacture asymmetric electrodes with the assistance of pre-designed positive and negative masks. After the filtration of exfoliated graphene (EG) as the current collector, the porous VN and mesoporous  $\text{MnO}_2$  were successively filtrated as the negative and positive electrodes, respectively (Fig. 2(c)).<sup>50</sup> The VN|| $\text{MnO}_2$  based PMSC was assembled by using a novel “water-in-salt” gel of  $\text{SiO}_2$ -lithium bis(trifluoromethane sulfonyl)imide (LiTFSI) as the electrolyte. The device delivered a voltage window of 2.0 V due to the asymmetric configuration. Meanwhile, the porous VN and  $\text{MnO}_2$  can accelerate the electrolyte ion transportation in plane for enhanced diffusion kinetics.<sup>51,52</sup> Apart from this asymmetric configuration, the symmetric covalent organic framework (COF)-





**Fig. 2** Vacuum filtration of electrode material suspensions to construct PMSCs. (a) Schematic illustration of the fabrication process of nano-sandwiched MHCF/graphene ( $M = \text{Cu, Ni, Co, Fe}$ ) PMSCs on the PET substrate and the corresponding photograph. Reproduced with permission.<sup>48</sup> Copyright 2019, Royal Society of Chemistry. (b) Schematic illustrating the fabrication process of the  $\text{Ti}_3\text{C}_2\text{T}_x/\text{MnO}_2$ -based PMSCs. Reproduced with permission.<sup>49</sup> Copyright 2020, IOP. (c) Schematic preparation process of  $\text{VN}||\text{MnO}_2$ -AMSCs. Reproduced with permission.<sup>50</sup> Copyright 2018, Elsevier. (d) Mask-assisted construction process of COF-MSC and the corresponding optical photograph. Reproduced with permission.<sup>53</sup> Copyright 2019, Wiley-VCH.

based MSC was fabricated through a one-step mask-assisted vacuum filtration strategy (Fig. 2(d)).<sup>53</sup> The assembled MSC exhibited a thickness of 3  $\mu\text{m}$  and showed an excellent flexibility by using the PET substrate and LiCl/PVA gel electrolyte.

To sum up, vacuum filtration is a simple strategy to manufacture thickness-controlled PMSCs without time-consuming processes. However, the size of the electrode is critically determined by the pre-designed mask. The adjacent distance between interdigital electrodes is commonly several millimeters in width. The reduction of the size from millimeters to micrometers remains a great challenge owing to the possibility of crosslinking between interdigital electrodes during filtration processes.

Therefore, the vacuum filtration strategy is suitable for the fast and scalable fabrication of PMSCs, which have no specific requirements for micro-sized and high-resolution devices.

**3.1.2 Spray coating.** The spray coating strategy can be used to fabricate microelectrodes for PMSCs with the assistance of customized patterned masks. The active materials are homogeneously dispersed in the aqueous and organic solutions to form a viscous ink, which can be transferred onto the interdigital mask covered substrate by a blade or spray gun.<sup>54</sup> This strategy is simpler and more universal than vacuum filtration to achieve scalable fabrication of electrodes. The penetration of the active materials through the filter paper can be avoided due

to the elimination of the slow filtration process under negative pressure. For instance, an N-doped mesoporous carbon nanosphere-based PMSC was fabricated with the customized mask-assisted coating technique (Fig. 3(a)).<sup>55</sup> The planar microelectrodes were prepared by uniformly spreading the active material slurry on the PET substrate with a doctor blade. The electrode size was in accordance with the interdigital mask with a finger length of 7 mm and 1 mm width with the interspace of 0.5 mm. Besides, a spray gun was used to fabricate a series of polyaniline (PANI)-based PMSCs with the guidance of an interdigital mask (Fig. 3(b)).<sup>56</sup> The aniline was firstly mixed with carboxylic multi-walled carbon nanotube (C-MWCNT) conductive networks for further polymerization. The obtained PANI ink was coated onto the interdigital current collector with neat and clean edges.

An interdigital Au electrode can be designed by the thermal evaporation technique on a PET substrate to facilitate the electron transfer and improve the conductivity of the device. Then, the graphene oxide@polyaniline (GO@PANI) ink was drop cast on the interdigital Au current collector followed by *in situ* laser reduction for fabricating LRGO@PANI PMSC (Fig. 3(c)).<sup>57</sup> The assembled symmetric PMSC presented a 13 times higher areal capacitance of  $72 \text{ mF cm}^{-2}$  than that of the RGO-based device at the current density of  $35 \mu\text{A cm}^{-2}$ . As an effective strategy to improve the electrochemical performance, the asymmetric PMSCs can also be constructed by coating methods. The carbon foam (CF)-based asymmetric PMSC was designed to exhibit a wide potential window of 1.4 V by using CF-MnO as the positive and CF-Fe<sub>2</sub>O<sub>3</sub> as the

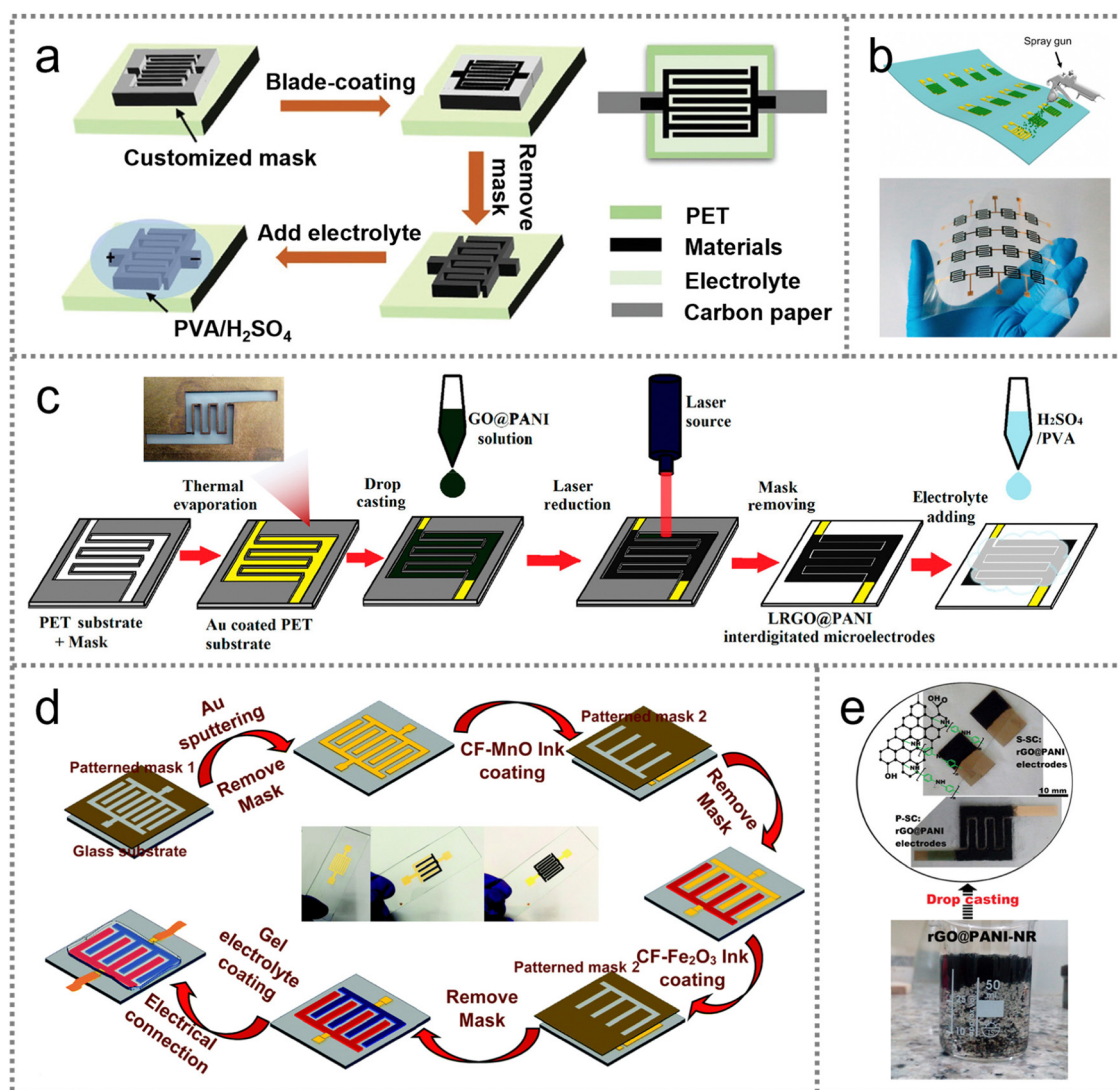


Fig. 3 Spray coating strategy for PMSC fabrication. (a) Schematic illustration of the mask-assisted preparation process of PMSCs and the corresponding configuration. Reproduced with permission.<sup>55</sup> Copyright 2019, Wiley-VCH. (b) Illustration of a spray coating method to construct PMSC arrays. Reproduced with permission.<sup>56</sup> Copyright 2021, Elsevier. (c) Schematic illustration of the fabrication process for LRGO@PANI-PMSC. Reproduced with permission.<sup>57</sup> Copyright 2020, American Chemical Society. (d) Schematic illustrating the procedure of solid-state PMSCs on a glass substrate. Reproduced with permission.<sup>58</sup> Copyright 2021, Royal Society of Chemistry. (e) Digital photographs of the rGO@PANI-NR nanocomposite for fabricating electrodes. Reproduced with permission.<sup>59</sup> Copyright 2021, American Chemical Society.





negative electrode on a glass substrate (Fig. 3(d)).<sup>58</sup> Three types of interdigital stainless-steel masks with different patterns assisted the coating of the Au current collector, positive electrode and negative electrode, respectively. The in-plane configuration of the PMSCs enabled fast ion transport and charge transfer for the superior rate capability. The RGO@PANI nanorod composite-derived PMSCs showed higher energy and power densities than those of sandwich structured SCs (Fig. 3(e)).<sup>59</sup>

Generally, the spray coating strategy can fabricate PMSCs on a large scale with simple procedures. The active materials can be directly coated on the substrates with the guidance of interdigital masks. However, the low homogeneity of the slurry has a negative effect on the uniformity of the microelectrodes. The weak adhesion between the electrodes and substrate hinders their long-term stability. Therefore, the exploration of homogenous slurries is expected to enhance the affinity with substrates for fabricating high-performance devices.

### 3.2 Strategies without using masks

**3.2.1 Electrolytic and electrophoretic deposition.** Electrolytic deposition is a universal technique to deposit metal oxides and hydroxides onto the interdigital current collector for the fast fabrication of PMSCs. The electrolyte ions can be oxidized or reduced at the interface of the electrode/electrolyte under an electric field. The electrode materials can nucleate and adhere to the conductive substrate during prolonged periods of deposition time.<sup>60,61</sup> For instance, Mn/V oxide was electrodeposited on the coated multi-walled carbon nanotubes (MWCNTs) with the deposition potential of 1 V for 3600 s (Fig. 4(a)).<sup>62</sup> The evaporated Au film with a thickness of 100 nm was used as the current collector on the polyimide (PI) substrate. The thickness of the MWCNTs increased with the deposition time owing to the coating of mixed Mn/V oxide, which could provide pseudocapacitance to enhance the electrochemical performance of the symmetric PMSC. Besides, the electrolytic deposition technique could also be used to manufacture asymmetric devices. The zinc-ion hybrid MSC (ZIHMSC) was assembled with a capacitor-type  $\text{Ti}_3\text{C}_2\text{T}_x$  anode and a battery-type  $\text{V}_2\text{O}_5$  cathode (Fig. 4(b)).<sup>63</sup> The interdigital graphite paper was designed as the current collector to serve as the deposition platform for  $\text{V}_2\text{O}_5$  under a constant current density of  $20 \text{ mA cm}^{-2}$  for 0.5–1.5 h. The structure of the designed current collector determines the growth sites of active materials during the electrolytic deposition process, indicating the key role of conductive substrates in structural design of microelectrodes.

As an alternative strategy to electrolytic deposition, electrophoretic deposition has been deemed as another effective electrochemical method to construct interdigital electrodes. The charged nanosheets, nanoparticles, and nanorods can diffuse toward the current collector under the electric field force for further deposition. In Fig. 4(b), the charged  $\text{Ti}_3\text{C}_2\text{T}_x$  nanosheets were electrophoretically deposited onto the finger-structure graphite paper as the anode under the potential of 20 V. The interdigital current collector (ICC) also plays a significant role in guiding the electrophoretic deposition

process as the forementioned electrolytic deposition strategy (Fig. 4(c)).<sup>64</sup> The patterned Ni seed layer was deposited with Ni and Au to serve as the ICC for the fabrication of an interfacial enhanced active carbon symmetrical MSC (IE SMSC). The interdigital electrode presented a finger width of  $500 \mu\text{m}$  and interspace of  $300 \mu\text{m}$ , demonstrating the feasibility of the electrochemical strategy in the reduction of electrode size from millimeter to micrometer-scale in comparison to the mask-assisted techniques. In the case of charged nanoparticles, the asymmetric carbon||carbon/ $\text{TiO}_2$  PMSC was fabricated with the electrophoretic deposition method on a PI substrate (Fig. 4(d)).<sup>65</sup> The micro-scale interdigital pattern was designed *via* laser direct writing followed by air-plasma etching for the hydrophilic surface, which was conducive to the deposition of  $\text{TiO}_2$  nanoparticles on the substrate.

The electrochemical strategies exhibit simple procedures to obtain controllable thickness and reduced size of interdigital electrodes. However, the uncontrollable growth in the lateral direction can lead to the deteriorated resolution of the electrolytic deposited electrode owing to the decreased interspace. For the electrophoretic deposition strategy, the active materials are required to be electrically charged for directional migration to the conductive substrate under the electric field. Meanwhile, the fabricated electrodes may suffer from poor stability due to the weak adhesion between the deposited materials and conductive substrates.

**3.2.2 Inkjet printing.** Inkjet printing is a time-saving strategy to achieve the scalable fabrication of PMSCs without using customized masks. The length and width of the interdigital electrodes and distances between adjacent finger-structured electrodes are determined by the nozzles and program parameters of the inkjet printer.<sup>66–69</sup> In comparison with the mask-assisted and electrochemical strategies, the inkjet printing technique is more efficient to manufacture PMSCs due to the well-designed programs. The current collector, electrode, and electrolyte can be successively fabricated to obtain an all-printed solid-state PMSC, holding superior advantages in the high utilization of raw materials for scalable production (Fig. 5(a)).<sup>70</sup> However, the structural integrity is considered to be one of the major difficulties in manufacturing the all-printed device. To tackle this issue, a metallic current collector was obtained with a flash-light-sintering (FLS) processed mixture of Ni flakes, Ni nanoparticles, photo-reactive polymer binder, and polyvinylpyrrolidone (PVP). The graphene electrode was fabricated with a mixture of graphene nanoplatelets, conductive carbon black, multiwalled carbon nanotubes (MWCNTs), poly(acrylic acid), and ethylene glycol. The ionic liquid electrolyte was also printed with a mixture of 1-ethyl-3-methylimidazolium bis(trifluoromethylsulfonyl)imide (EMIM-TFSI), trimethylolpropane ethoxylate triacrylate, and 2-hydroxy-2-methylpropiophenone followed by solidification under ultraviolet (UV) radiation. Each component was expected to deliver high conductivity and strong adhesion to ensure the structural stability of the PMSC device. Apart from the programmable dispensing machine, an office inkjet printer can also be used to fabricate interdigital electrodes. For instance, sodium ascorbate-capped MXene (SA-MXene) based PMSC was printed and encapsulated by the PVA/ $\text{H}_2\text{SO}_4$  gel electrolyte without using current collectors



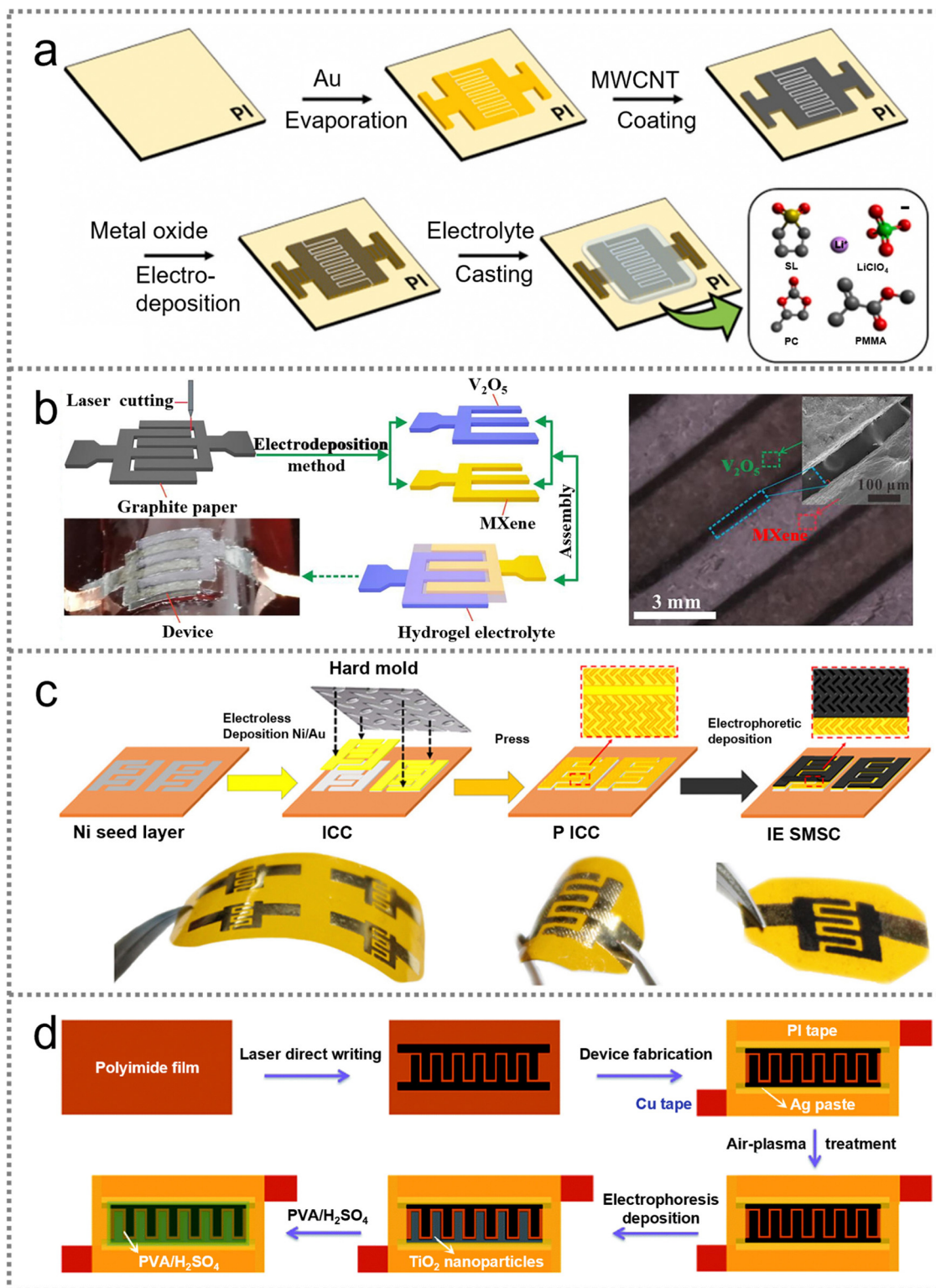


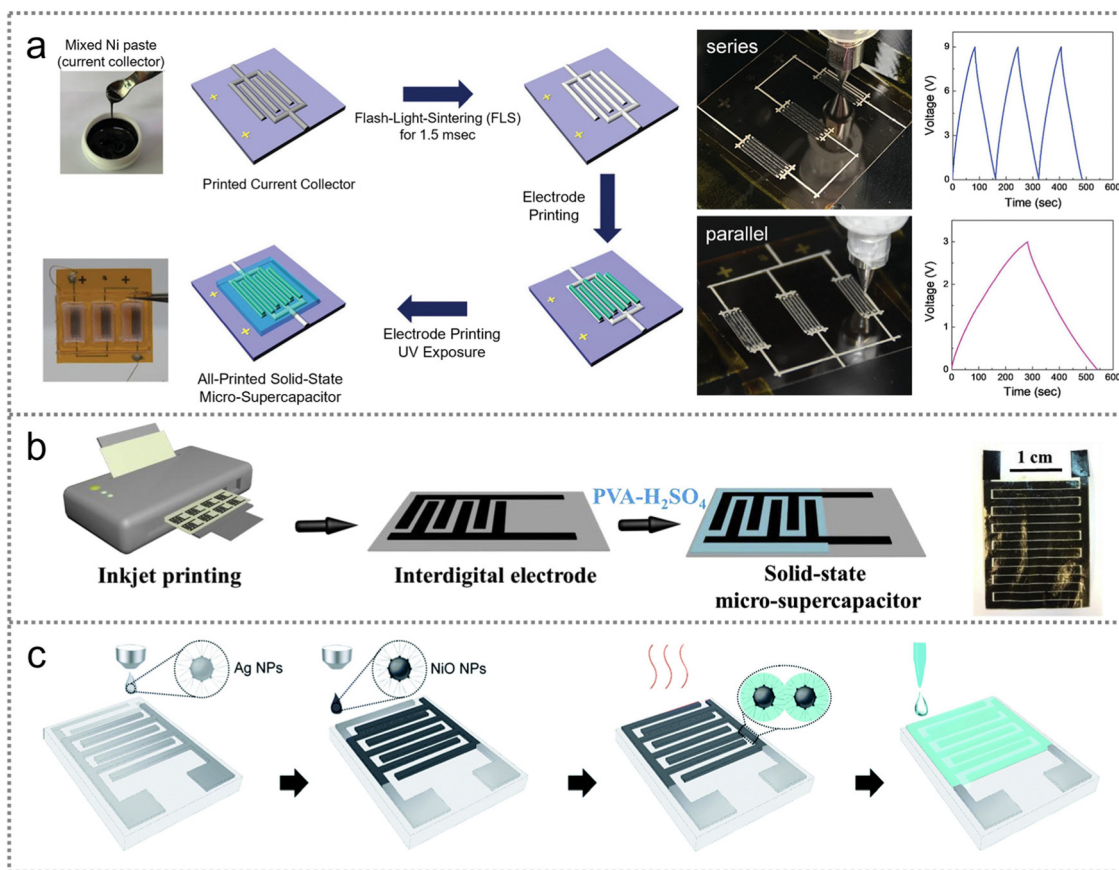
Fig. 4 PMSC fabrication by an electrolytic and electrophoretic deposition strategy. (a) Schematic illustration of the fabrication process of a flexible PMSC. Reproduced with permission.<sup>62</sup> Copyright 2021, Elsevier. (b) Schematic diagram of the preparation and assembly process of the ZIHMSC and the corresponding SEM image. Reproduced with permission.<sup>63</sup> Copyright 2021, Elsevier. (c) Schematic preparation procedures of IE SMSCs. Reproduced with permission.<sup>64</sup> Copyright 2019, American Chemical Society. (d) Illustration of the construction process of a carbon/TiO<sub>2</sub> PMSC. Reproduced with permission.<sup>65</sup> Copyright 2017, Royal Society of Chemistry.

(Fig. 5(b)).<sup>71</sup> The SA-MXene showed enhanced dispersity and stability over 80 days in the water solution owing to the strong

bonding of ascorbate and Ti atoms, enabling the SA-MXene to be a stable ink for mixing with Triton X-100 and propylene glycol.







**Fig. 5** PMSC fabrication with the inkjet printing technique. (a) Schematic illustration of the sequential preparation process for the all-printed solid-state Ni S-MSC and a photograph of devices connected in series and parallel and the corresponding GCD curves. Reproduced with permission.<sup>70</sup> Copyright 2020, Wiley-VCH. (b) Schematic illustrating the procedure of the fabrication for SA-MXene nanocomposite PMSCs and the photograph of an interdigital structure device. Reproduced with permission.<sup>71</sup> Copyright 2019, Elsevier. (c) Schematic illustration of the fabrication process for inkjet-printed planar MSCs. Reproduced with permission.<sup>72</sup> Copyright 2019, Royal Society of Chemistry.

The current collector is critically needed on account of the poor conductivity of composite ink-state electrode materials. The single layer conductive substrate can ameliorate the inferior charge transfer between the bulk electrodes instead of mixing the active materials with binders and conductive components. Recently, a layer-by-layer printing strategy was developed to fabricate planar NiO MSCs by using the printed Ag nanoparticles (NPs) as the current collector (Fig. 5(c)).<sup>72</sup> The conductivity of the film electrode was up to  $210 \text{ S m}^{-1}$ . The adhesion between the Ag NPs and NiO NPs was enhanced by the sintering process to guarantee the high conductivity of the device.

In brief, the inkjet printing strategy can greatly shorten the manufacturing time for the scalable fabrication of PMSCs. But the remaining obstacle consists in the uncertain rheological characteristics of printing inks as well as the hydrophilicity of the substrates. The strong surface tension of inks and hydrophobic substrates may severely deteriorate the quality of printed electrodes. The size of ink drops is uncontrollable for designing a high-resolution micro electrode. Therefore, the forementioned bottlenecks require in-depth research on novel printing inks and substrates to ensure the scalable fabrication of printed PMSCs.

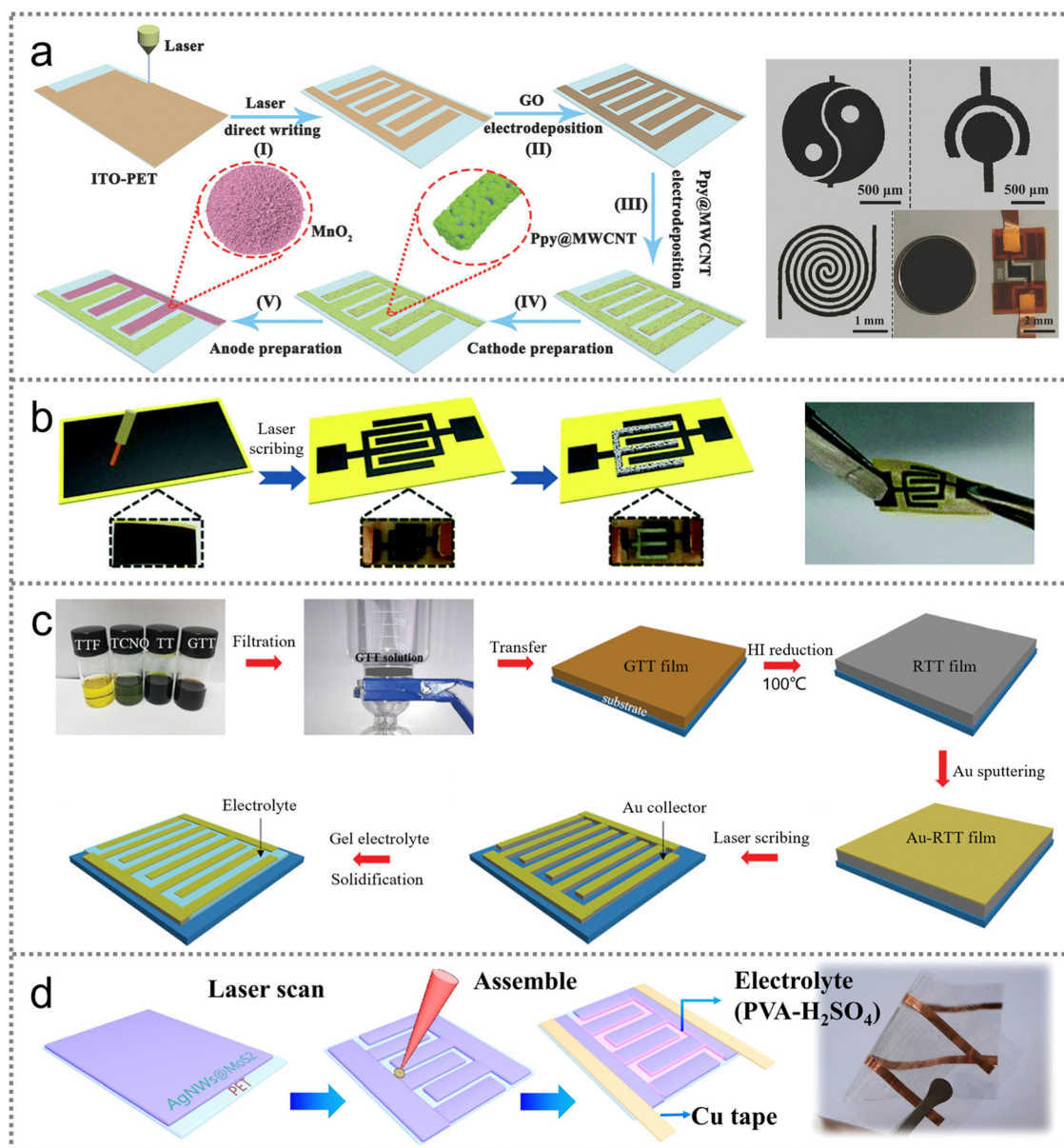
**3.2.3 Laser scribing.** The laser scribing strategy has emerged as a scalable and time-saving technique to engrave high-resolution patterns with precisely controlled laser parameters, including laser power, processing speed, processing time, resolution, frequency and Z axis offset.<sup>73</sup> Various laser wavelengths ranging from ultraviolet (UV) to infrared (IR) regions have been developed to scribe film structure materials into patterned electrodes.<sup>74,75</sup> According to the requirements of processing efficiency and precision, the laser wavelength should be rigorously controlled by computer systems. For example, a UV laser of 355 nm can be used for cutting, scribing and carving electrode materials with high precision and short interspace. While a 266 nm laser may damage the structure of the material due to the high photon energy. IR laser wavelengths ranging from 1064 nm and 1343 nm are available for the *in situ* fabrication of carbonized and graphitized electrodes due to their unique thermal effects.<sup>76</sup>

The laser scribing strategy is commonly used in combination with other techniques to fabricate high-quality PMSC devices. The fundamental procedures can be divided into two types.<sup>77,78</sup> In the first type, the finger-structured current collectors are designed by the laser direct writing technique.<sup>79,80</sup>



The active materials can be loaded on conductive substrates *via* electrochemical deposition and mask-assisted coating methods. For example, a  $\text{MnO}_2$ @polypyrrole(Ppy)@MWCNT asymmetric PMSC was developed by laser scribing and a successive electrodeposition process (Fig. 6(a)).<sup>81</sup> In step I, six interdigital electrodes ( $0.5 \text{ mm} \times 5 \text{ mm}$ ) were designed through computer-controlled laser direct writing on an indium tin oxide-polyethylene terephthalate (ITO-PET) film. Then, the reduced graphene oxide (rGO) flakes were electrodeposited onto the interdigital ITO-PET substrate to serve as the current collector (step II). In the following steps, a Ppy@MWCNT cathode and

$\text{MnO}_2$  anode were anchored respectively on the patterned electrodes by an electrodeposition strategy. The asymmetric PMSC delivered a five-fold higher energy density of  $12.16 \mu\text{W h cm}^{-2}$  at  $5 \text{ mV s}^{-1}$  than the symmetric PMSC ( $2.58 \mu\text{W h cm}^{-2}$ ). Commercial CNT paper could also be used as the raw material to construct PMSCs by laser engraving. The interdigital conductive substrate could be designed for further electrodeposition due to its superior conductivity ( $1\text{--}2 \times 10^5 \text{ S m}^{-1}$ ) (Fig. 6(b)).<sup>82</sup> The zinc ions were reduced and deposited onto the working electrode to serve as the anode of the zinc-ion micro-supercapacitor (ZmSC) by using the patterned CNTs as



**Fig. 6** Laser scribing strategy for fabricating PMSCs. (a) Schematic illustration of the fabrication process for AMSC and digital photographs of electrodes with different shapes. Reproduced with permission.<sup>81</sup> Copyright 2018, Wiley-VCH. (b) Schematic diagram of the preparation process for the ZmSC and corresponding photograph. Reproduced with permission.<sup>82</sup> Copyright 2018, Royal Society of Chemistry. (c) Schematic illustrating the fabrication process of RTT-MSCs. Reproduced with permission.<sup>86</sup> Copyright 2019, Wiley-VCH. (d) Direct laser-patterning technique for fabricating the TFE-TMSC. Reproduced with permission.<sup>87</sup> Copyright 2018, Elsevier.



the working and counter electrode in 1 M ZnSO<sub>4</sub> aqueous electrolyte. The entire manufacturing process was simple and efficient to ensure the replenishment of Zn without additional electrodes and electrolytes.

In the second type, the film structured active material should be firstly prepared through spray coating and vacuum filtration strategies.<sup>83</sup> The laser scribing technique can be used to tailor the film-shaped materials into a customized interdigital pattern.<sup>84,85</sup> For example, the vacuum filtration method was conducted to fabricate graphene and tetrathiafulvalene-tetracyanoquinodimethane (GTT) based films for laser scribed reduced GTT (RTT) PMSCs (Fig. 6(c)).<sup>86</sup> The obtained GTT film was transferred onto the PET substrate for the further reduction of GTT to RTT. After being covered with a 150 nm thick Au layer, the Au-RTT film was manufactured into finger structure electrodes by the laser scribing technique. Apart from the vacuum filtration method, the film-structured materials can also be prepared by a spray coating strategy. Recently, a spray coating combined with laser scribing strategy was developed to fabricate MoS<sub>2</sub>-based PMSCs on PET film (Fig. 6(d)).<sup>87</sup> The Ag nanowires (AgNWs) were mixed with MoS<sub>2</sub> in a water/ethanol solution to obtain a homogenous ink for spray coating, enabling the enhanced conductivity of the bulk electrode owing to the superior conductivity of the AgNWs. The interdigital pattern was designed on microelectrodes *via* a laser scribing process followed by coating PVA/H<sub>2</sub>SO<sub>4</sub> gel electrolyte to assemble the PMSC device. Although the laser scribing strategy can directly fabricate microelectrodes without tedious procedures, the expensive equipment may restrict the widespread application in large-scale industrial production.

**3.2.4 Plasma jet.** Plasma jet has been considered as a promising etching technique to manufacture high-resolution interdigital microelectrodes for PMSCs. Similar to the laser scribing strategy, the active material used in the plasma jet etching step should be pre-designed in the form of a film structure *via* vacuum filtration, coating and electrochemical deposition strategies. The film can be engraved by micro plasma jet toward high-resolution patterned electrodes.<sup>88</sup> For example, a MWCNT/AgNW based PMSC was fabricated with a successive vacuum filtration and plasma jet etching technique (Fig. 7(a)).<sup>89</sup> The MWCNT/AgNW composite film in the PET substrate could be subsequently etched into the interdigital configuration by a He and O<sub>2</sub> gas-based micro plasma jet, which was generated under pulsed direct current (DC) power. The microdevice was constructed by coating the conductive Cu foil and PVA/H<sub>3</sub>PO<sub>4</sub> gel electrolyte. Besides, electrochemical strategies can also be implemented to prepare film-structured electrodes, demonstrating the potential to combine with the plasma jet technique for the fabrication of microelectrodes. For instance, the viologen-linked ionic porous polymer (IPP-V) was electropolymerized on the Au-coated Si wafer at the potential of 0.02 V for 5 min (Fig. 7(b)). The IPP-V/Au was pyrolyzed at 500 °C to obtain IPP-V-500/Au in step ii.<sup>90</sup> Then, the interdigital pattern could be designed with the electrode width of 200 μm and interspace of 64 μm by successive O<sub>2</sub>, Ar and CF<sub>4</sub>/O<sub>2</sub> plasma etching (step iii), indicating the superiority of the plasma jet etching technique in the manufacture of micro-scale devices.

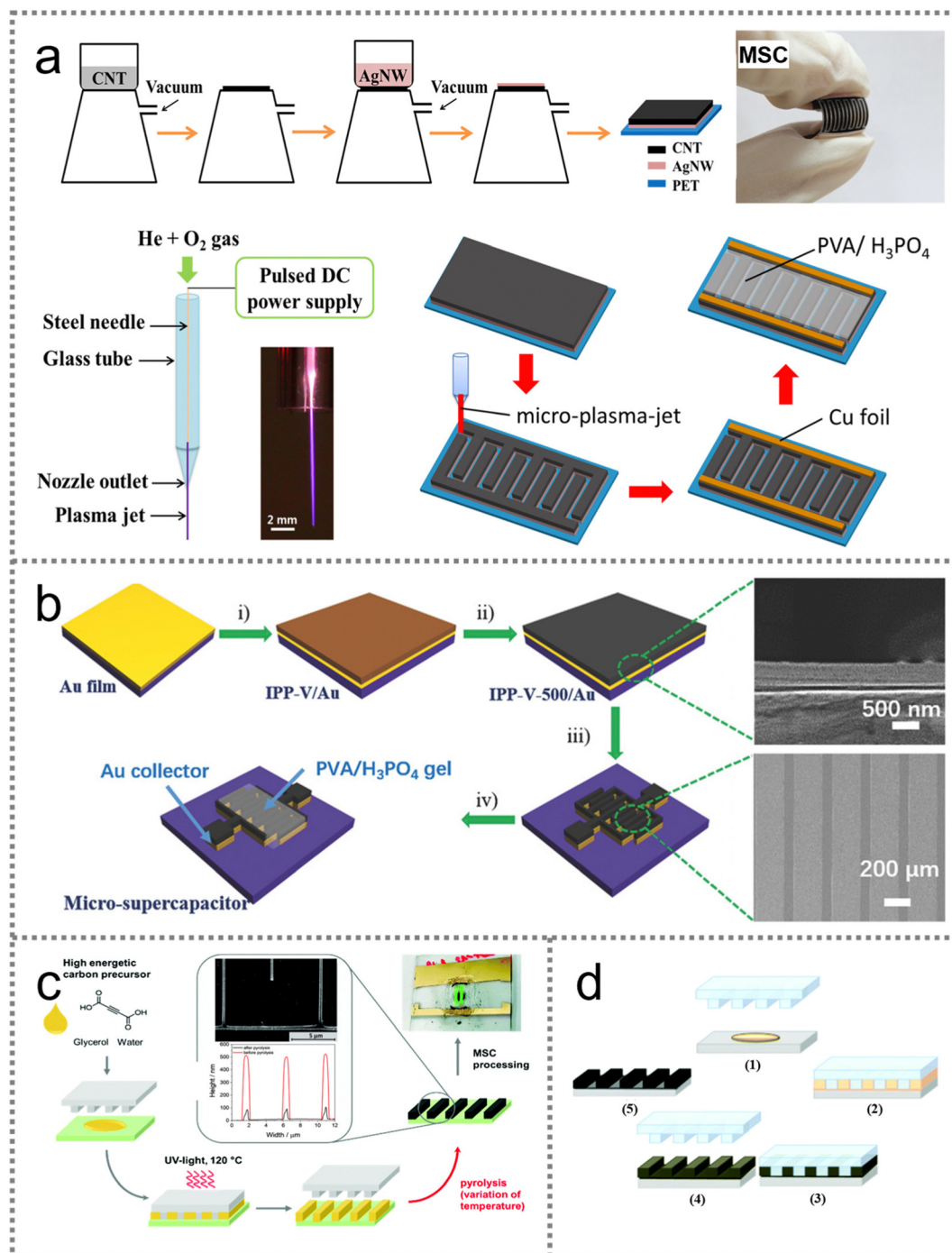
The IPP-V-500 based PMSC was assembled by PVA/H<sub>3</sub>PO<sub>4</sub> gel electrolyte (step iv) and delivered a high volumetric energy density of 0.35 mW h cm<sup>-3</sup> at the power density of 12.5 mW cm<sup>-3</sup>. In general, the plasma jet etching strategy shows great potential in manufacturing high-resolution microdevices. However, the limited scope in carbon-based materials and the time-consuming process in thick film etching may hinder the scalable fabrication of microelectrodes.

**3.2.5 Nanoimprint lithography.** Similarly, nanoimprint lithography has also emerged as a versatile technique for fabricating carbon-based microelectrodes. The interdigital electrodes can be manufactured with liquid carbon precursors under the constant pressing of patterned elastomeric stamps, followed by the solidification and pyrolysis process after peeling off from the stamps.<sup>91</sup> Recently, an energy-rich carbon-based MSC was fabricated by the solvent-assisted nanoimprint lithography strategy (Fig. 7(c)).<sup>92</sup> A mixture of acetylene dicarboxylic acid, glycerol and sulfuric acid could be polymerized under heating and UV-light conditions followed by the pyrolysis process. The configuration of the microelectrodes varied with the structure of the patterned stamps. With the line widths of 10 μm, 5 μm and 1 μm, three types of MSCs were prepared. The device with 1 μm line width presented a specific capacitance of 1.32 mF cm<sup>-2</sup> and superior cycling stability of 97% capacity retention after 10 000 cycles at 8.3 μA cm<sup>-2</sup>. In addition, sucrose-derived carbon was used as an EDLC type material to fabricate interdigital electrodes *via* the nanoimprint lithography technology (Fig. 7(d)).<sup>93</sup> The width of the micro-structured fingers in the MSC could be further reduced to 500 nm. The interdigital carbon-based electrodes were peeled off from the stamps and the morphology remained intact after the pyrolysis process. Therefore, the nanoimprint lithography technique can be extensively used in the scalable production of micro- and nanoscale devices, indicating the feasibility of fabricating miniaturized electronic components.

**3.2.6 3D printing.** 3D printing has encountered ever-increasing attention as an emerging advanced technique for the precise fabrication of microdevices. The materials used for the 3D printing technique are commonly in the ink-state with a high viscosity and superior rheological capability. The inks can be smoothly extruded through the nozzle and vertically printed onto the substrate layer-by-layer.<sup>94-96</sup> Asymmetric finger-structured microelectrodes were fabricated by using graphene-vanadium nitride quantum dots (G-VNQDs) as the anode ink and vanadium pentoxide (V<sub>2</sub>O<sub>5</sub>) as the cathode ink (Fig. 8(a)).<sup>97</sup> Specifically, GO was mixed with G-VNQDs and V<sub>2</sub>O<sub>5</sub> inks to improve the conductivity of the printed electrodes. The LiCl/PVA ink was subsequently printed into the gaps between the interdigital anode and cathode to serve as a gel-like electrolyte. The all-printed MSC device showed a high areal mass loading of 3.1 mg cm<sup>-2</sup> with a wide potential window of 1.6 V. Moreover, a linear relationship between the areal energy density and printed layers was presented from single layer to four layers at the low power density of 0.5 mW cm<sup>-2</sup>. But the higher layer number delivered a deteriorated rate capability due to the longer electron transfer pathway in the thick electrode. The quality of the printed electrodes was determined by the inks, which should be scrupulously prepared with charming



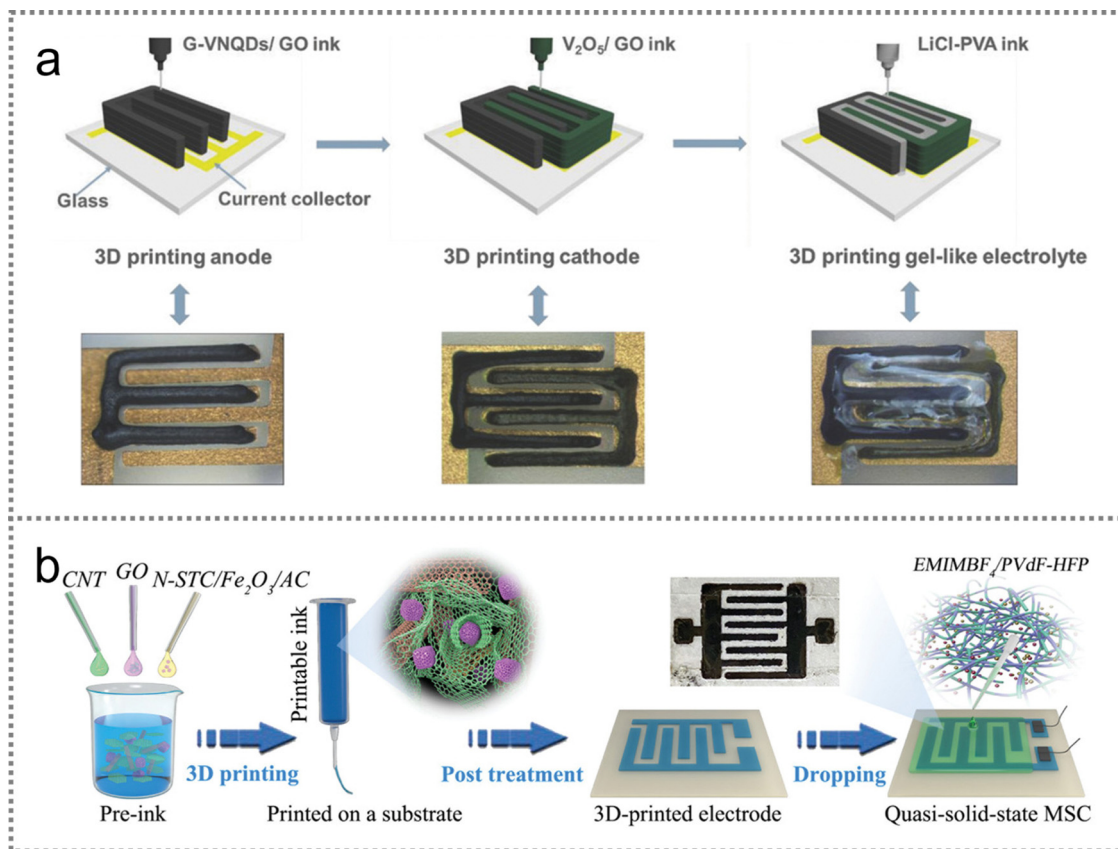




**Fig. 7** PMSC fabrication with plasma jet and nanoimprint lithography strategies. (a) Schematic illustration of the fabrication process of flexible in-plane MSCs and the configuration of the micro-plasma-jet setup. Reproduced with permission.<sup>89</sup> Copyright 2018, IOP. (b) Schematic diagram of the construction procedure for the IPP-V-500 based MSC with plasma etching and the cross-sectional and top-view SEM images. Reproduced with permission.<sup>90</sup> Copyright 2018, Wiley-VCH. (c) Solvent-assisted nanoimprint process for fabricating PMSCs. Reproduced with permission.<sup>92</sup> Copyright 2021, Royal Society of Chemistry. (d) Schematic illustration of the preparation procedure for the printed interdigital electrodes. Reproduced with permission.<sup>93</sup> Copyright 2018, Royal Society of Chemistry.

rheological behaviors. Bingham plastic is an essential element in ensuring that the ink can be extruded smoothly from the nozzles when subjected to shear stress. Recently, a mixture ink was developed with nitrogen-doped cross-coupled micro-mesoporous carbon networks (N-STC), Fe<sub>2</sub>O<sub>3</sub> nanoparticles,

activated carbon (AC), carbon nanotubes (CNTs), and GO for 3D printed MSC (Fig. 8(b)).<sup>98</sup> The N-STC/Fe<sub>2</sub>O<sub>3</sub>/AC/CNT/GO composite ink showed a decreased viscosity under the high shear rate and an infinite viscosity at low shear rates, indicating that the ink is a suitable fluid with typical Bingham plastic



**Fig. 8** 3D printing technology for the fabrication of PMSCs. (a) G-VNQDs/GO anode, V<sub>2</sub>O<sub>5</sub>/GO cathode and LiCl-PVA gel-like electrolyte constructed with the 3D printing method. Reproduced with permission.<sup>97</sup> Copyright 2018, Wiley-VCH. (b) Schematic illustration of the ionogel-based quasi-solid-state MSC. Reproduced with permission.<sup>98</sup> Copyright 2020, Wiley-VCH.

characteristics for 3D printing techniques. The quasi-solid-state MSC was printed by coating EMIMBF<sub>4</sub> based ionic gel electrolyte. The device showed a superior gravimetric capacitance of 377 F g<sup>-1</sup> with a wide working temperature range of -10 to 60 °C.

Overall, the 3D printing technique has showcased practicability in designing on-chip microdevices. Microelectrodes with interdigital patterns can be accurately printed according to pre-designed configurations in computer programs. However, the active material printing ink should be developed with suitable shear-thinning rheological properties and fluidity. A high solid content is also required for printing inks to be extruded through nozzles without structural collapse. Hence, research on 3D printing techniques is still confronted with tremendous challenges for the manufacture of high-precision PMSCs.

In brief, PMSCs can be designed and manufactured through mask-assisted strategies and other advanced techniques. The devices fabricated with the above-mentioned microfabrication technologies are summarized in Table 1, considering the interdigital width, interspace and electrochemical performance. The vacuum filtration and spray coating strategy showed limitations in reducing the size of the microelectrode from millimeters to micrometers. With the assistance of advanced microfabrication machines, the interdigital width of PMSCs could even be reduced to 500 nm with the interspace of 1 μm by the nanoimprint

lithography technique. However, the feasibility of each strategy depends on the structure of the raw materials, and it is still a crucial challenge to develop a facile technique for designing and manufacturing high performance PMSCs.

## 4. Applications

PMSCs have exhibited a variety of advantages including high power densities, superior flexibility and excellent rate capability, showing great potential for integration into electronic components.<sup>98</sup> As demonstrated in previous reports, the development of various micro-electronics has stimulated the miniaturization of energy storage systems. The configuration of PMSCs differs dramatically from conventional batteries and sandwich-structured SCs. The unique planar structure enables fast ion transport kinetics in the horizontal direction, which can contribute to the enhanced rate capability. The reduction in size allows the PMSC to be used as a novel energy storage device for microelectronics. Meanwhile, PMSCs can also be utilized in flexible power supplies and wearable sensors owing to their superior mechanical flexibility.<sup>99,100</sup> With the characteristics of cutting off DC, connecting the alternating current (AC) and preventing low frequency, PMSC-based electric systems can be used as energy filters in power grids to compensate the intermittency of fluctuant input power. In this section, the



Table 1 Comparison of the configurations and electrochemical performance of PMSCs reported in recent years

| Techniques                    | PMSCs   | Interdigital Interspace/<br>width/mm | Substrate                                  | Electrolyte   | Potential<br>window/<br>V                        | $C_d$ /mF cm <sup>-2</sup>                                      | $E_{max}$ /<br>mW h cm <sup>-3</sup>  | $P_{max}$ /W cm <sup>-3</sup>                                  | Cycling<br>stability   | Ref.                       |
|-------------------------------|---|--------------------------------------|--|---|--|---|---|--|--|----------------------------|
| Vacuum<br>filtration          | CuHCF/graphene//FeHCF/<br>graphene<br>Ti <sub>3</sub> C <sub>2</sub> T <sub>x</sub> /MnO <sub>2</sub> /Ti <sub>3</sub> C <sub>2</sub> T <sub>x</sub> /<br>MnO <sub>2</sub><br>VN//MnO <sub>2</sub>      | 1.6<br>1<br>1                        | PET<br>PET<br>Nylon<br>membrane            | PVA/LiCl<br>PVA/EMIMBF <sub>4</sub><br>SiO <sub>2</sub> -LiTFSI   | 0–1.8<br>0–2.5<br>0–2.0                          | 19.84<br>24.7<br>16.1   | 44.6<br>21.5 $\mu$ W h cm <sup>-2</sup><br>21.6   | 16.88<br>0.154 mW<br>1.539                                     | 5000 (96.8%)<br>3000 (83.6%)<br>5000 (90%)                         | 48<br>49<br>50             |
| Spray coating                 | g-C <sub>3</sub> N <sub>6</sub> -COF//g-C <sub>3</sub> N <sub>6</sub> -COF<br>NMCSS//NMCSS<br>PANI/C-MWCNTs//PANI/C-<br>MWCNTs<br>LRGO@PANI//<br>LRGO@PANI<br>CF-MnO//CF-Fe <sub>2</sub> O <sub>3</sub> | 1.6<br>1<br>1<br>2<br>1              | PET<br>PET<br>PET<br>PET<br>PET<br>Glass   | PVA/LiCl<br>PVA/H <sub>2</sub> SO <sub>4</sub><br>PVA/H <sub>2</sub> SO <sub>4</sub><br>PVA/H <sub>2</sub> SO <sub>4</sub><br>PVA/H <sub>2</sub> SO <sub>4</sub><br>PVA/KOH | 0–0.8<br>0–1<br>0–0.8<br>–1.0 to<br>1.0<br>0–1.4 | 15.2<br>22.11<br>45.4<br>72.0<br>18.4                           | 7.3<br>0.307<br>2.6<br>2.7<br>5 $\mu$ W h cm <sup>-2</sup>                                | 10<br>0.058<br>1.49<br>—<br>3440.7 $\mu$ W<br>cm <sup>-2</sup> | 5000 (93.1%)<br>—<br>1000 (84.6%)<br>1000 (93.5%)<br>10000 (86.1%) | 53<br>55<br>56<br>57<br>58 |
| Electrolytic<br>deposition    | rGO@PANI-NR//rGO@-<br>PANI-NR<br>Mn/V oxide@MWCNT//<br>Mn/V oxide@MWCNT   | 2<br>—<br>—                          | PET<br>PI                                  | PVA/H <sub>2</sub> SO <sub>4</sub><br>Polycarbonate/sulfonate/<br>LiClO <sub>4</sub>  | –1.0 to<br>1.0<br>0–2                            | 51<br>11.8  | 52.2 W h kg <sup>-1</sup><br>6.58 $\mu$ W h cm <sup>-2</sup>                              | 3722.3 W<br>1.0 mW cm <sup>-2</sup>                            | 1000 (98.3%)<br>5000 (78%)   | 59<br>62                   |
| Electrophoretic<br>deposition | Ti <sub>3</sub> C <sub>2</sub> T <sub>x</sub> /V <sub>2</sub> O <sub>5</sub><br>AC//AC  | 1.5<br>0.5                           | PI   | polyethylmethacrylate<br>Polyacrylamide/ZnSO <sub>4</sub><br>1 M KNO <sub>3</sub>   | 0–1.65<br>0–1.6                                  | 129<br>76.6   | 48.9 $\mu$ W h cm <sup>-2</sup><br>13.61 $\mu$ W h cm <sup>-2</sup>                       | —<br>40.0 mW<br>cm <sup>-2</sup>                               | 10000 (77%)<br>5000 (92.9%)  | 63<br>64                   |
| Inkjet printing               | Carbon//carbon/TiO <sub>2</sub><br>MWCNTs/graphene//<br>MWCNTs/graphene<br>SA-MXene//SA-MXene<br>NiO//NiO   | 0.6<br>0.25<br>—<br>1                | PI   | PVA/H <sub>2</sub> SO <sub>4</sub><br>EMIM-TFSI   | 0–1.0<br>0–3.0                                   | 27.3<br>16.15   | —<br>79 mJ cm <sup>-2</sup>   | —<br>12.8 mW<br>cm <sup>-2</sup>                               | 10000 (100%)<br>—  | 65<br>70                   |
| Laser scribing                | MnO <sub>2</sub> /PPy@MWCNT<br>Zn/CNT//CNT<br>RTT/RTT   | 0.5<br>0.5<br>0.5                    | Photo paper<br>PET<br>ITO-PET<br>PI<br>PET | PVA/H <sub>2</sub> SO <sub>4</sub><br>PVA/Mg(ClO <sub>4</sub> ) <sub>2</sub><br>PVA/LiCl<br>1 M ZnSO <sub>4</sub><br>PVA/H <sub>2</sub> SO <sub>4</sub>                     | 0–1.0<br>0–1.0<br>0–1.6<br>0–1.8<br>0–1.0        | 108.1<br>155<br>21.8<br>83.2<br>151 $\mu$ F<br>cm <sup>-2</sup> | 100.2<br>—<br>12.16 $\mu$ W h cm <sup>-2</sup><br>29.6 $\mu$ W h cm <sup>-2</sup><br>1.57 | —<br>—<br>8 mW cm <sup>-2</sup><br>0.2                         | 4000 (94.7%)<br>5300 (94%)<br>—<br>6000 (87.4%)<br>10000 (98%)     | 71<br>72<br>81<br>82<br>86 |
| Plasma jet                    | AgNWs-MoS <sub>2</sub> //AgNWs-<br>MoS <sub>2</sub><br>MWCNT/AgNW//MWCNT/<br>AgNW   | 1<br>0.8                             | PET  | PVA/H <sub>2</sub> SO <sub>4</sub><br>PVA/H <sub>3</sub> PO <sub>4</sub>  | 0–1.2<br>0–0.8                                   | 27.6<br>274.8 $\mu$ F<br>cm <sup>-2</sup>                       | 2.453 $\mu$ W h cm <sup>-2</sup><br>0.17  | —<br>—   | 20000 (85.2%)<br>10000 (92.3%)                                     | 87<br>89                   |
| Nanoimprint<br>lithography    | IPP-V-500//IPP-V-500<br>Carbon//carbon<br>N-doped carbon//N-doped<br>carbon   | 0.2<br>500 nm<br>500 nm              | Si wafer<br>B-Al silicate<br>Glass         | PVA/H <sub>3</sub> PO <sub>4</sub><br>PVA/H <sub>2</sub> SO <sub>4</sub><br>PVA/H <sub>2</sub> SO <sub>4</sub>  | 0–1.0<br>0–0.8<br>0–1.0                          | —<br>1.32<br>65 $\mu$ F cm <sup>-2</sup>                        | 0.35<br>0.07<br>58  | —<br>—<br>22   | —<br>10000 (97%)<br>1000 (98%)                                     | 90<br>92<br>93             |
| 3D printing                   | G-VNQS/GO//V <sub>2</sub> O <sub>5</sub> /GO<br>N-STC/Fe <sub>2</sub> O <sub>3</sub> //N-STC/Fe <sub>2</sub> O <sub>3</sub>   | 0.2<br>0.75                          | Glass<br>PET                               | PVA/LiCl<br>EMIMBF <sub>4</sub> /PVDF-HFP   | 0–1.6<br>0–4.0                                   | 207.9<br>1.79 F cm <sup>-2</sup>                                | 73.9 $\mu$ W h cm <sup>-2</sup><br>114 W h kg <sup>-1</sup>                               | —<br>0.1 kW kg <sup>-1</sup>                                   | 8000 (65%)<br>10000 (93.2%)  | 97<br>98                   |



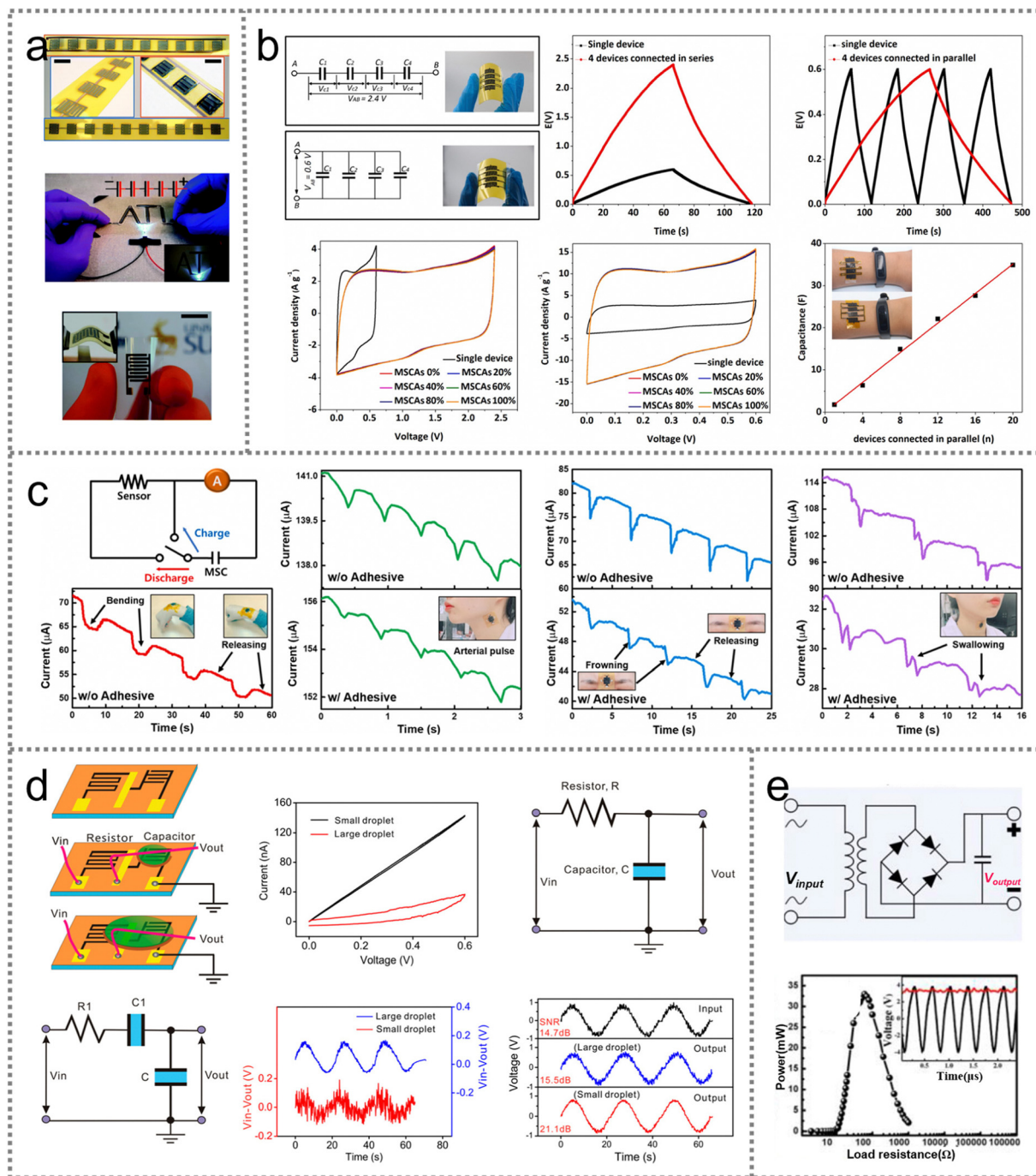


applications of PMSCs in energy storage devices, sensors and filters are discussed for next generation microelectronics.

#### 4.1 Energy storage devices

The emerging PMSCs can meet the requirements of miniaturized energy storage devices with decent power density, high-rate

capability, and an almost indefinite cycling stability. The unique planar configuration allows the micro-sized unit to be integrated into on-chip electronics in parallel and series connections. For instance, ten inkjet-printed NiO MSCs (IPNiO) were connected in parallel and series configurations, respectively (Fig. 9(a)).<sup>72</sup> The parallel connected devices exhibited a ten-fold higher capacity



**Fig. 9** Applications of PMSCs including energy storage devices, sensors and filters. (a) Digital photographs of 10 IPNiO MSCs connected in parallel and series configurations, then used as the energy storage unit for LEDs. Reproduced with permission.<sup>72</sup> Copyright 2019, Royal Society of Chemistry. (b) Electrochemical performance and flexibility of PMSCs with series and parallel connections. Reproduced with permission.<sup>79</sup> Copyright 2021, Elsevier. (c) Schematic diagram of the integrated system and the strain measurement induced by bio-signals including arterial pulse, frowning and swallowing. Reproduced with permission.<sup>62</sup> Copyright 2021, Elsevier. (d) The fsrGO MSCs applied in RC filter circuits. Reproduced with permission.<sup>101</sup> Copyright 2018, American Chemical Society. (e) Schematic circuit diagram of the wireless charging unit and corresponding output power. Reproduced with permission.<sup>85</sup> Copyright 2020, Elsevier.



than a single IPNIO under the voltage window of 1 V. Meanwhile, devices connected in series presented a higher potential of 10 V, indicating the integratability of PMSCs in energy storage devices. In addition, the PMSC could retain the initial capacitance under bending states due to the planar configuration and flexible substrates. The stretchable PMSC arrays were fabricated and four devices could be connected in series and parallel with satisfactory mechanical flexibility (Fig. 9(b)).<sup>79</sup> The voltage of the series connected devices was four times higher than that of a single PMSC with 0.6 V. The devices connected in parallel showed an equal voltage window to the single device. The flexible measurements demonstrated the superior capacity retention of PMSC arrays with increasing elongation from 0% to 100%. Scalable fabrication could also be realized with a linear relationship between the number of PMSC arrays and the capacitance. These features manifested the integratable characteristics of PMSCs in flexible and integrated microelectronics.

#### 4.2 Sensors

PMSCs have been developed in bio-sensors to detect the strains induced by arterial pulse, respiration and body movements owing to their outstanding flexibility. The planar structure ensures that the device has a highly adhesive attachment onto the human skin. Recently, a skin-attachable bio-signal sensor was designed with a vertically integrated PMSC system to detect wrist bending, arterial pulse, frowning of the brow and swallowing signals (Fig. 9(c)).<sup>62</sup> Adhesive film and PI tape were used in two contact modes to tightly attach the bio-sensor onto the skin for contact enhancement. The output electrochemical data suggested that the forementioned bio-signals could be evidently amplified by the PI attachment rather than the adhesive film. The sharper peaks in PI tape fixed sensors indicated the tighter adhesion between human skin and the bio-sensors, while the adhesive films might hamper the precise detection of bio-signal induced strains. Therefore, the adhesion mode remains an obstacle for PMSC-based planar sensors to accurately detect the bio-signals without skin irritation.

#### 4.3 Filters

High-quality power is critically needed in medical apparatus, signal processors and the communication industry. Filters are of great function for integrated grids to decrease the ripples and output a steady voltage. Similar to conventional SCs, PMSCs can also be used as resistor-capacitor (RC) filters to eliminate the interference signals. In particular, a graphene-based RC filter was assembled by using PMSCs and a fs laser reduced graphene oxide (fsrGO) resistor (Fig. 9(d)).<sup>101</sup> The filters were divided into two types based on the size of the PVA/H<sub>2</sub>SO<sub>4</sub> gel electrolyte droplet. In the first type, the interdigital microelectrode of the PMSC was precisely coated with a small electrolyte droplet, exhibiting a typical resistor feature with a linear loop in the current-voltage (CV) curve. Meanwhile, the filter coated with a large droplet showed a capacitive-type rectangular loop in the CV curve, leading to an increased number of capacitors in the equivalent circuit. When the sinusoidal signal at 0.045 Hz was applied with white noise,

the small droplet-coated filter could output a stronger high-frequency noise with an increased signal-to-noise ratio (SNR) from 14.7 to 21.1 dB compared to that of the large droplet coated filter (15.5 dB). Therefore, the quality of the output signal could be affected by the coating domain of the gel electrolyte. Likewise, the series connected PMSC system was designed to convert the input AC voltage into the output DC voltage of 3.0 V (Fig. 9(e)).<sup>85</sup> The wireless charging unit was assembled with the PMSC system for autonomous electronics, which delivered the maximum output power of 33.0 mW with an external load resistance of 60  $\Omega$ . Meanwhile, the voltage and power of the PMSC system were 3 V and 1.43 mW, demonstrating the feasibility of planar microdevices to be integrated into a self-powered system.

## 5. Summary and outlook

In summary, the demand for miniaturized electronics has boosted the development of microelectrode designs and manufacturing strategies for PMSCs. The interdigital electrodes of PMSCs can be achieved by pre-designed masks in vacuum filtration and spray coating techniques for large-scale fabrication of millimeter-sized devices without time-consuming processes. The electrochemical strategies can further reduce the size of PMSCs and improve the resolution between the adjacent electrodes. Printing strategies and laser-induced techniques are also conducive to manufacturing micro- and nanoscale PMSCs with higher accuracy. Many challenges in the microfabrication techniques need to be conquered to pave the way for the realization of intelligent energy systems.

The intrinsically inferior electrochemical performance of electrode materials hinders the energy and power density upper limit of PMSC devices. Novel EDLC-type and pseudocapacitive materials should be developed to compensate the performance deficiencies of PMSCs. In particular, composite electrodes can be designed by incorporating carbon-derived (EDLC type) and transitional metal-based materials (pseudocapacitive type) to maximize the synergistic effect. Meanwhile, the energy storage mechanisms should be elucidated in depth and the mass transfer dynamics at the electrode/electrolyte interface need to be probed for designing the expected electrode materials. Stable gel/solid-state electrolytes should be further exploited with an enticing potential window to improve the performance of PMSCs.

Advanced microfabrication technologies are needed to design high-resolution PMSCs on a grand scale. The distance between adjacent interdigital electrodes should be narrowed down to micrometers for a shortened ion diffusion pathway in plane. The finger-structure patterns are required to be loaded on a flexible and silicon substrate with tiny footprint areas. The affinity between the substrates and electrode materials should be further reinforced for long-term stability. A low contact resistance is desired to obtain efficient ion transport and charge transfer.

The monolithic integration of PMSCs into autonomous systems should be forged ahead for energy harvesters, sensors,



filters and other untapped fields. We should further focus on miniaturized electronics with high flexibility and responsive capability. The requirement for micro power supplies in IoTs electronics pushes the incorporation of PMSCs into self-powered systems. So, various attempts should be unremittably executed to break the bottlenecks for the development of PMSCs. Interdisciplinary cooperation is indispensable to guide the microelectronic systems towards a higher level.

## Author contributions

Shifan Zhu: methodology, investigation, writing – original draft; Zhiheng Xu: methodology, validation, writing – review & editing; Haijun Tao: writing – review & editing, supervision; Dandan Yang: writing – review & editing; Xiaobin Tang: writing – review & editing, supervision; Yuqiao Wang: conceptualization, writing – review & editing, supervision, funding acquisition.

## Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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