



Cite this: *J. Mater. Chem. A*, 2023, **11**, 2360–2366

## A high voltage aqueous proton battery using an optimized operation of a $\text{MoO}_3$ positive electrode<sup>†</sup>

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Aqueous proton batteries have attracted increasing attention owing to their potential of high safety standard, high rate capability, and long cyclability. While some inorganic negative electrode materials for proton batteries have recently been found, inorganic positive electrode materials have rarely been reported. In this work, we investigate the proton insertion–extraction mechanism of  $\text{MoO}_3$  using *operando* X-ray diffraction and density functional theory calculation to optimize its operating conditions as a positive electrode. It is found that the phase transition between  $\text{MoO}_3$  and phase-I  $\text{H}_x\text{MoO}_3$  can reversibly be utilized by preventing irreversible phase transition from phase-I to phase-III involving the change of proton accommodation from the intralayer to interlayer sites. A  $\text{MoO}_3$  electrode using the phase transition between  $\text{MoO}_3$  and phase-I shows an average reduction potential of 0.44 V vs. SHE with a maximum reversible capacity of 100 mA h g<sup>-1</sup>. A  $\text{MoO}_3$ ||50 wt%  $\text{H}_2\text{SO}_4$  aq.|| $\text{H}_x\text{MoO}_3$  full-cell exhibits a maximum discharge capacity of 73 mA h g<sup>-1</sup> and maintains nominal discharge voltage above 0.47 V, which is the highest voltage among aqueous proton batteries composed of insertion-type oxide active materials.

Received 3rd November 2022  
Accepted 3rd January 2023

DOI: 10.1039/d2ta08581j  
[rsc.li/materials-a](http://rsc.li/materials-a)

## 1. Introduction

Aqueous proton batteries with two insertion-type electrodes, where protons go back and forth between these electrodes during charging and discharging, are attractive candidates for post-lithium-ion batteries.<sup>1</sup> These battery systems potentially satisfy high safety standards owing to aqueous electrolyte solutions and have high rate capabilities because of protons' high mobility. In addition, the protons' small ionic radius possibly contributes to the high cyclabilities of insertion-type active materials. However, aqueous proton batteries have not been commercialized due to the lack of active materials for practical applications. Acid electrolyte solutions are generally used for aqueous proton batteries to ensure high proton conductance and prevent the insertion of other cations. Therefore, active materials for aqueous proton batteries are required to have not only the ability of reversible proton insertion/extraction but also stability in acidic electrolyte solutions. Examples of electrode materials for proton batteries are organic materials<sup>2</sup> and cyanide complexes<sup>1,3</sup> but they are relatively bulky, which is unfavorable for high energy density of the cells. Promising compact materials are oxides, and some insertion-type oxide negative electrode materials, such as

$\text{MoO}_3$ ,<sup>4</sup>  $\text{WO}_3$ ,<sup>5</sup> and  $\text{TiO}_2$ ,<sup>6</sup> have been reported. However, insertion-type oxides as a positive electrode material, which is needed to establish aqueous proton batteries composed of insertion-type active materials for both electrodes, have rarely been found.

In this study, we focused on  $\text{MoO}_3$  as a positive electrode material for aqueous proton batteries.  $\text{MoO}_3$  has long been studied as a hydrogen insertion material.<sup>7,8</sup> Besides pristine  $\text{MoO}_3$  (space group *Pbnm*, number 62), four stable phases are reported as the proton-inserted product  $\text{H}_x\text{MoO}_3$ : phase-I ( $0.23 < x < 0.40$ ; *Cmcm*, 63), phase-II ( $0.85 < x < 1.04$ ; *C2/m*, 12), phase-III ( $1.55 < x < 1.72$ ; *C2/m*), and phase-IV ( $x = 2.0$ ; space group unknown, monoclinic).<sup>7,8</sup> In addition, phase-IIa ( $0.6 < x < 0.8$ ; *C2/m*) has also been reported as a metastable phase.<sup>9</sup> Although the space group symmetry changes by reduction and oxidation, the layered structure framework of  $\text{MoO}_3$  is retained. Recently,  $\text{MoO}_3$  has been recognized as a negative electrode material for aqueous proton batteries, which has a relatively high reversible capacity of *ca.* 220 mA h g<sup>-1</sup> in sulfuric and phosphoric acid electrolytes.<sup>10,11</sup> In addition, W. Xu *et al.* have very recently found that  $\text{H}_x\text{MoO}_3$  can also be utilized as a positive electrode material though its operating potential was relatively low (*ca.* 0.3 V vs. standard hydrogen electrode (SHE)).<sup>12</sup>  $\text{MoO}_3$  shows two reversible redox reactions at around 0.3 and  $-0.1$  V vs. SHE and also shows an irreversible reduction reaction around 0.5 V vs. SHE (Fig. S1<sup>†</sup>). On the other hand, the phase transition behavior during the reduction–oxidation processes is not fully understood due to *ex situ* characterization used in most of the previous research.<sup>11,13</sup>

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<sup>†</sup> Electronic supplementary information (ESI) available. See DOI: <https://doi.org/10.1039/d2ta08581j>



In this study, we conducted *operando* X-ray diffraction (XRD) measurements and density functional theory (DFT) calculations to investigate the reduction–oxidation mechanism of  $\text{MoO}_3$  both experimentally and theoretically. We clarify the phase transition process of  $\text{MoO}_3$  during reduction–oxidation, including irreversible phase transition from phase-I to phase-III in the first reduction by exploring the thermodynamically stable sites for proton insertion in phase-I and phase-III (or phase-II). Furthermore, we show that the reduction reaction around 0.5 V *vs.* SHE could reversibly utilize by optimizing the cut-off potential and successfully construct an aqueous proton battery composed of insertion-type oxide active materials with an average discharge potential of 0.47 V.

## 2. Experimental methods

### 2.1. Electrochemical measurements and characterization

$\text{MoO}_3$  composite electrodes were composed of  $\text{MoO}_3$  (Kanto Chemical) : carbon black (Li-250, Denka) : polyvinylidene difluoride (KF polymer L#9305, Kuraray) = 85 : 10 : 5 wt%. The electrode slurry in an *N*-methyl pyrrolidone (Kanto Chemical) solvent was coated on a graphite sheet current collector (Panasonic, thickness: 25  $\mu\text{m}$ ) and dried at 80 °C for 12 h in a constant temperature oven (DX302, Yamato).

*Operando* XRD measurements were carried out using an electrochemical three-electrode cell (Fig. S2(a)†), an electrochemical measurement system (SP-50, Bio-Logic), and an XRD system (SmartLab, Rigaku) using Mo  $\text{K}\alpha$  radiation at 60 kV and 150 mA. The electrochemical three-electrode cell consisted of the  $\text{MoO}_3$  composite electrode as the working electrode, a commercial  $\text{Ag}|\text{AgCl}|\text{saturated KCl}$  aq. electrode (RE-1CP, BAS) as the reference electrode, a Pt mesh as the counter electrode, and 50 wt% (*ca.* 7.1 mol  $\text{dm}^{-3}$ )  $\text{H}_2\text{SO}_4$  aq. as the electrolyte solution. The XRD patterns of the  $\text{MoO}_3$  electrode were recorded from the backside of the electrode through the graphite sheet current collector (Fig. S2(a)†). The geometrical area of the working electrode was defined as 1.77  $\text{cm}^2$  with a fluororubber o-ring.

The reduction–oxidation measurements of  $\text{MoO}_3$  half-cells were conducted using an electrochemical three-electrode cell (Fig. S2(b)†) composed of the same components as those of the *operando* XRD cell and a multichannel charge–discharge system (HJ1001SM8A, Hokuto Denko). The geometrical area of the working electrode was defined as 0.50  $\text{cm}^2$  with a fluororubber gasket. The charge–discharge measurements of  $\text{MoO}_3|50$  wt%  $\text{H}_2\text{SO}_4$  aq. |  $\text{H}_2\text{MoO}_3$  full-cells were performed using an electrochemical three-electrode cell with the commercial  $\text{Ag}|\text{AgCl}|\text{saturated KCl}$  aq. reference electrode (Fig. S2(c)†) and a multichannel charge–discharge system (EF-7100p, Electrofield). The geometrical areas of the positive and negative electrodes were defined as 0.50  $\text{cm}^2$  with a fluororubber gasket, and the loading masses of the positive and negative electrodes were set to the same value. Before the full-cell construction, the positive and negative electrodes were electrochemically preconditioned with the half cells. The positive electrode was reduced and oxidized in the potential range from 0.1 to 0.5 V at 100  $\text{mA g}^{-1}$  for 30 cycles, and the cycle was terminated in the reduced state. The negative electrode was reduced and oxidized

in the potential range from –0.3 to 0.0 V at 100  $\text{mA g}^{-1}$  for 3 cycles, and the cycle was terminated in the oxidized state.

All the electrochemical measurements were performed at 25  $\pm$  2 °C, and the electrodes were exposed to a 5 min open-circuit period between charge and discharge.

The electrodes as-prepared and taken out from the cells were characterized using field emission scanning electron microscopy (FE-SEM) (SU8230, Hitachi High-Tech) and energy dispersive X-ray spectroscopy (EDS) (XFlash FlatQUAD 5060F, BRUKER).

### 2.2. DFT calculations

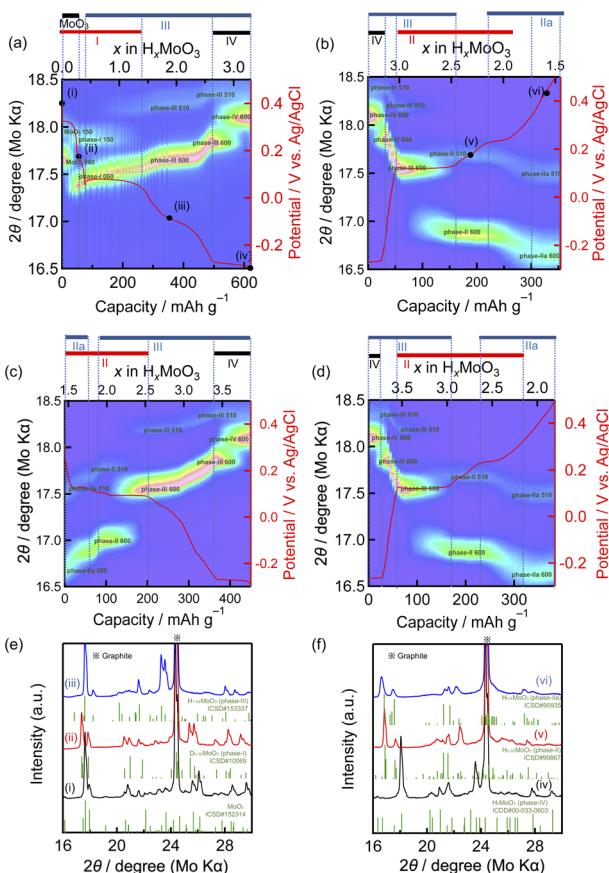
DFT calculations were performed using the plane-wave basis projector augmented wave (PAW) method as implemented in the Vienna *ab initio* simulation package (VASP) 6.1.<sup>14,15</sup> The generalized gradient approximation (GGA) parameterized by Perdew, Burke, and Ernzerhof<sup>16</sup> and the Hubbard *U* extension<sup>17</sup> with an effective *U* of 4.38 eV for the Mo-4d orbital were used as the exchange–correlation functional. The cut-off energy was set at 520 eV. A gamma-centered  $8 \times 2 \times 8$  *k*-point mesh was used for the unit cell, and the number of divisions were adjusted for supercells by their size. The total energy converged to  $10^{-6}$  eV per atom. Atomic positions and lattice constants were relaxed until the total energy converged to  $10^{-5}$  eV per atom.

Proton inserted models were constructed as follows: protons were attached to O atoms. The OH units were directed to adjacent O atoms to form hydrogen bonds. The O–H distances were set to be one third of the O–O distances. All symmetry-independent configurations were employed as initial structures. Atom positions were randomly displaced by 0.01 Å to break the symmetry before the structural relaxation. Notes that are specific to individual models will be described in the Results and discussion section. Pymatgen<sup>18</sup> and enumlib<sup>19–21</sup> packages were used to construct the structural models.

## 3. Results and discussion

### 3.1. *Operando* XRD

*Operando* XRD measurement of the  $\text{MoO}_3$  electrode during reduction–oxidation was carried out in the potential range between 0.50 and –0.30 V at a current density of 100  $\text{mA g}^{-1}$  to investigate the phase transition behavior between  $\text{MoO}_3$  and the fully protonated phase-IV. Fig. 1(a)–(d) show the *operando* XRD patterns during the first and second reduction–oxidation processes, while Fig. 1(e) and (f) show the full XRD profiles of selected states, showing that the states (i), (ii), (iii), (iv), (v) and (vi) correspond to  $\text{MoO}_3$ , phase-I, phase-III, phase-IV, phase-II, and phase-IIa, respectively. In the first reduction,  $\text{MoO}_3$  shows three phase-transitions from  $\text{MoO}_3$  to phase-IV *via* phase-I and III (Fig. 1(a), (e) and (f)). First, a  $\text{MoO}_3$ /phase-I biphasic reaction is observed on the potential plateau at around 0.35 V evidenced by the gradual decrease of  $\text{MoO}_3$  060 (17.7°) diffraction intensity and concurrent increase of phase-I 060 (17.4°) diffraction. Second, a phase-I/phase-III biphasic reaction occurs on the plateau at around 0.05 V indicated by gradual decrease of the phase-I 150 (17.9°) diffraction and concurrent increase of the

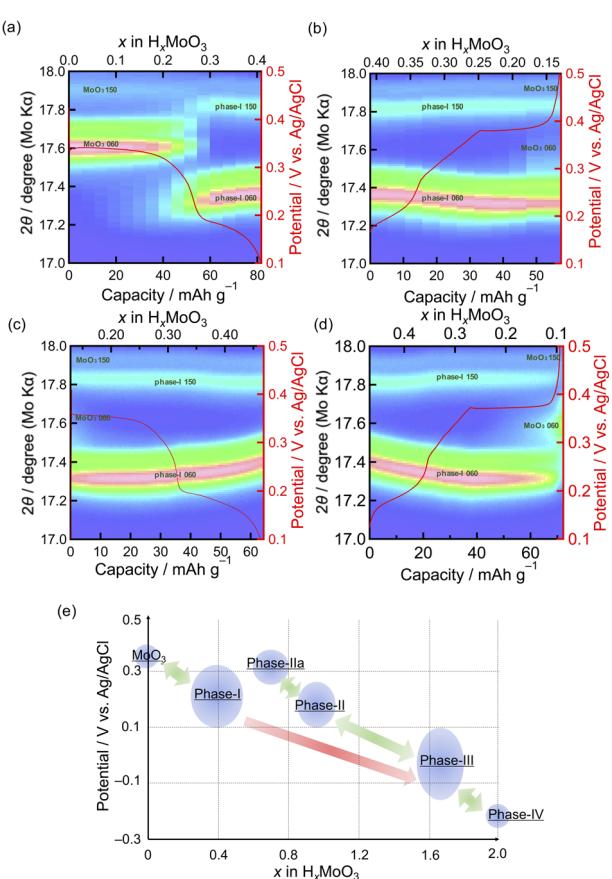


**Fig. 1** Operando XRD patterns of the  $\text{MoO}_3$  electrode during reduction–oxidation in the potential range from  $-0.30$  to  $0.50$  V at  $100 \text{ mA g}^{-1}$ ; contour plots of (a) the 1st reduction, (b) the 1st oxidation, (c) the 2nd reduction, and (d) the 2nd oxidation; (e and f) line plots with reference patterns.

phase-III 510 ( $18.2^\circ$ ) diffraction. Finally, the phase-III/phase-IV biphasic reaction on the plateau at around  $-0.27$  V is shown by the gradual decrease of the phase-III 600 ( $17.8^\circ$ ) diffraction and concurrent increase of the phase-IV 600 ( $18.1^\circ$ ) diffraction. Monophasic reactions of phase-I and phase-III are also observed after the  $\text{MoO}_3$ /phase-I and phase-I/phase-III biphasic reactions, respectively, evidenced by the continuous shifts of the diffraction peaks, such as phase-I 060 and phase-III 600. During the first oxidation, while the phase-III/phase-IV biphasic reaction is observed on the plateau at around  $-0.27$  V, phase transitions in higher potential regions are totally different from those in the first reduction process, as shown in Fig. 1(b). After the phase-III monophasic reaction between  $-0.27$  V and  $0.05$  V, the phase-III/phase-II biphasic reaction on the plateau at around  $0.05$  V is shown by the gradual decrease of the phase-III 600 ( $17.5^\circ$ ) diffraction and concurrent increase of the phase-II 600 ( $17.0^\circ$ ) diffraction. Then, the phase-II/phase-IIa biphasic reaction is suggested by the gradual decrease/increase of the phase-II 42-2 ( $26.3^\circ$ )/phase-IIa 51-2 ( $27.8^\circ$ ) diffractions (Fig. S3†). In the second reduction, the change was reverse to that observed during the first oxidation, and  $\text{H}_x\text{MoO}_3$  shows reversible phase transitions between phase-IIa and phase-IV

afterward, as shown in Fig. 1(c) and (d). These results indicate that the phase transition from phase-I to phase-III is an irreversible process.

Next, we performed *operando* XRD to investigate the reversibility of  $\text{MoO}_3$ /phase-I biphasic and phase-I monophasic reactions for their possible use as high-potential electrode reactions, when there is no phase-III formation with the operating potential range at above  $0.10$  V. Fig. 2(a)–(d) show the *operando* XRD patterns during the first and second reduction–oxidation processes. Gradual decrease/increase of the  $\text{MoO}_3$  060 ( $17.7^\circ$ )/phase-I 060 ( $17.4^\circ$ ) diffractions and continuous shifts of the phase-I 060 diffraction are observed in both the first reduction and oxidation though the appearance of the  $\text{MoO}_3$  060 diffraction does not completely proceed in the fully oxidized state (Fig. 2(a) and (b)). In the second cycle, we decreased the reduction–oxidation rate to  $10 \text{ mA g}^{-1}$ , a tenth of the rate in the first cycle, to reduce kinetic factors to the reversibility. Phase-I 060 diffraction shifts to a higher diffraction angle and proton content,  $x$  in  $\text{H}_x\text{MoO}_3$ , becomes higher at the end of the reduction (Fig. 2(c)) compared to the first cycle, indicating that the proton insertion proceeded further with the decrease in the reduction current. In addition, the phase transition from phase-



**Fig. 2** Operando XRD patterns of the  $\text{MoO}_3$  electrode during reduction–oxidation in the potential range from  $0.10$  to  $0.50$  V; contour plots of (a) the 1st reduction and (b) the 1st oxidation at  $100 \text{ mA g}^{-1}$  and (c) the 2nd reduction and (d) the 2nd oxidation at  $10 \text{ mA g}^{-1}$ . (e) A schematic of the phase transitions of the  $\text{MoO}_3$  electrode.



I to  $\text{MoO}_3$  proceeds more than that in the first high-rate cycle, as evidenced by the higher intensity of  $\text{MoO}_3$  060 diffraction and lower proton content  $x$  in  $\text{H}_x\text{MoO}_3$  after the second oxidation (Fig. 2(d)). These results clearly show that the phase-I monophasic reaction and the  $\text{MoO}_3$ /phase-I biphasic reaction are essentially reversible while the phase transition from phase-I to  $\text{MoO}_3$  is kinetically limited. To the best of our knowledge, this is the first study to report the reversibility of these high-potential reactions.

The phase transition of  $\text{MoO}_3$  during reduction–oxidation is summarized in Fig. 2(e). The reduction below 0.10 V causes an irreversible phase transition from phase-I to phase-III. Then the reversible phase transitions between phase-IIa and phase-IV, *via* phase-II and phase-III, are involved in the subsequent cycles when the voltage range is set at –0.3 to 0.5 V. The reversibility of the phase transition between phase-IIa and phase-IV is consistent with the charge–discharge performances of  $\text{MoO}_3$  as the negative electrode.<sup>4,22</sup> On the other hand,  $\text{MoO}_3$ /phase-I biphasic and phase-I monophasic reactions mostly reversibly occur when the voltage range is set at 0.1 to 0.5 V.

The appearance of phase-IV in the fully reduced state and that of phase-II and phase-III in the reverse oxidation process observed in this study agree with previously reported *ex situ* XRD studies.<sup>8,11</sup> R. Schöllhorn *et al.* have reported based on their *ex situ* XRD measurement that the reduction of  $\text{MoO}_3$  in the range of  $0.5 < x < 1.67$  in  $\text{H}_x\text{MoO}_3$ , corresponding to the plateau at 0.05 V in this study, yielded a mixture of phases-I, II, and III, which is probably caused by the decomposition of metastable phases I and III to phase-II in the course of *ex situ* measurement. We speculate that phase transition from phase I to III is kinetically more favourable than that from phase I to II.

Fig. 1(a) and (b) show that our  $\text{MoO}_3$  electrode has a redox plateau at around 0.3 and –0.1 V, which have not been observed in other studies,<sup>4,10</sup> resulting in a relatively high reversible capacity of *ca.* 300 mA h g<sup>–1</sup> at a 100 mA g<sup>–1</sup> rate. This redox plateau disappears when the charge–discharge rate is increased to 1 or 2 A g<sup>–1</sup> (Fig. S4†), explaining why this process was not observed in previous studies with high testing rates. A high cut-off oxidation potential of 0.50 V in this study may also induce this process. We deduce that this process is attributed to some surface reactions on  $\text{MoO}_3$ , because no structural changes are observed in *operando* XRD (Fig. 1(a) and (b)). Further study is needed to identify it. The low rates used in this study would also lead to the hydrogen evolution reaction and composition ambiguity of phases II, IIa, III and IV.

### 3.2. DFT calculations

DFT calculations were carried out to obtain theoretical insights into the proton accommodation sites in  $\text{H}_x\text{MoO}_3$  and the irreversible phase transition from phase-I to phase-III. For clarifying the proton accommodation sites, the crystal structure of  $\text{MoO}_3$  is schematically illustrated in Fig. S5.†  $\text{MoO}_3$  has an orthorhombic structure of the *Pbnm* (62) space group with one Mo site and three O sites. Mo atoms are coordinated by six O atoms forming  $\text{MoO}_6$  octahedra.  $\text{MoO}_6$  octahedra share their edges to form corrugated chains along the *c*-axis and share their

corners along the *a*-axis. The edge- and corner-sharing  $\text{MoO}_6$  octahedra form  $\text{MoO}_3$  layers with intralayer channels, and the  $\text{MoO}_3$  layers are stacked along the *b*-axis with van der Waals gaps. There are two potential sites for inserted protons. One is an O2 site, a bridging site between two corner-sharing  $\text{MoO}_6$  octahedra, and protons are accommodated in the intralayer channels (intralayer site). The other is an O3 site, a terminal site on the surface of  $\text{MoO}_3$  layers, and protons are accommodated in the interlayer gaps (interlayer site). The O1 site, which is shared by edge-sharing  $\text{MoO}_6$  octahedra, is hardly accessible for protons. Calculated structural parameters are summarized in Table S1.† The calculated lattice constants *a* and *c* are in good agreement with the experimental values with an error of *ca.* 1%, whereas the lattice constant *b* is overestimated by *ca.* 12%. The overestimation of *b* is probably due to the use of the conventional GGA exchange–correlation functional, in which van der Waals interaction is not properly considered.

First, preferable proton accommodation sites in  $\text{MoO}_3$  were investigated using a  $2 \times 1 \times 2$  supercell with an additional proton ( $\text{H}_1\text{Mo}_{16}\text{O}_{48}$  supercell). A proton was attached to an O site toward one of its adjacent O atoms within 3.1 Å. All symmetry-independent configurations were employed as initial structures, and the structures converged into several groups after the structural relaxation. The lowest energy group has a proton attached to an O2 site toward an adjacent O2 site. The calculation results show that two Mo atoms sharing the OH unit are a pair of  $\text{Mo}^{5+}$  and  $\text{Mo}^{6+}$  ions. The second group has a proton attached to an O3 site toward an adjacent O3 site in the next  $\text{MoO}_3$  layer, and it is higher in energy by 0.32 eV than the lowest energy group. Structures having a proton attached on an O1 site show 0.58 eV higher energy than the lowest energy group, or the proton was migrated to an adjacent O2 site during the structural relaxation. These results suggest that the protons are preferably accommodated within the  $\text{MoO}_3$  layers and attached to the O2 sites, and this is consistent with the formation of phase-I in the early stage of the first reduction.

Second, preferable proton configurations in the intralayer sites were investigated using a  $2 \times 1 \times 1$  supercell of  $\text{H}_n\text{Mo}_8\text{O}_{24}$  (*n* = 2 and 4). The  $\text{MoO}_3$  framework of phase-I with a space group of *Cmcm* was used as the initial structure, and protons were attached to O2 sites toward their adjacent O2 sites within 3.1 Å. The lowest energy structure of  $\text{H}_4\text{Mo}_8\text{O}_{24}$  consists of  $\text{MoO}_3$  layers having alternate filled and empty channels as illustrated in Fig. 3(b). The lowest energy structure of  $\text{H}_2\text{Mo}_8\text{O}_{24}$  consists of a  $\text{MoO}_3$  layer with alternate filled and empty channels, and another  $\text{MoO}_3$  layer with empty channels only (Fig. 3(a)). This structure has slightly higher energy by 0.02 eV per proton than a mixture of  $\text{H}_4\text{Mo}_8\text{O}_{24}$  and  $\text{MoO}_3$ . Structures with protons in different channels have 0.12 eV per proton or higher energy than the lowest energy structures in both compositions. These calculation results suggest that the inserted protons are not randomly distributed at the intralayer sites and that the protons tend to be aligned in the channels. This is consistent with a previous report.<sup>11</sup> Although structures with less-than-half filled channels were not examined in this study due to a huge number of proton configurations for larger supercells, structures with multiple empty channels between



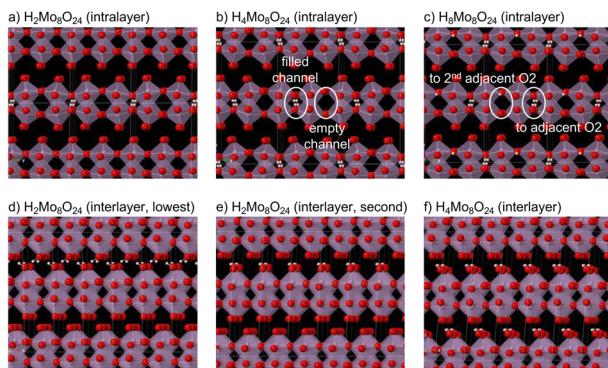


Fig. 3 Schematic views of the lowest energy structure models for (a)  $\text{H}_2\text{Mo}_8\text{O}_{24}$  with intralayer protons, (b)  $\text{H}_4\text{Mo}_8\text{O}_{24}$  with intralayer protons, (c)  $\text{H}_8\text{Mo}_8\text{O}_{24}$  with intralayer protons, (d)  $\text{H}_2\text{Mo}_8\text{O}_{24}$  with interlayer protons, (e)  $\text{H}_2\text{Mo}_8\text{O}_{24}$  with interlayer protons of the second lowest energy, and (f)  $\text{H}_4\text{Mo}_8\text{O}_{24}$  with interlayer protons. Purple polyhedra, red spheres, and white spheres denote  $\text{MoO}_6$  octahedra, O atoms, and protons, respectively.

the filled channels are plausible at lower proton contents than  $\text{H}_{0.5}\text{MoO}_3$ , suggesting wide proton solubility in phase-I. To investigate the accommodation sites for further proton insertion, a  $2 \times 1 \times 1$  supercell of  $\text{H}_8\text{Mo}_8\text{O}_{24}$  was examined. In the lowest energy structure, all protons are attached to  $\text{O}_2$  sites. Half of the protons are directed to the adjacent  $\text{O}_2$  sites, whereas the other half are directed to the second adjacent  $\text{O}_2$  sites (Fig. 3(c)). This suggests that the proton insertion behavior into the intralayer sites significantly changes over the composition of  $\text{H}_{0.5}\text{MoO}_3$ .

Next, preferable proton configurations in the interlayer sites was investigated using a  $1 \times 1 \times 2$  supercell of  $\text{H}_n\text{Mo}_8\text{O}_{24}$  ( $n = 2, 4$ ). We have our interest in comparison of the proton accommodation sites between the intralayer and interlayer sites and getting insights into the irreversible phase transition from phase-I to phase-III, and thus the proton compositions examined in this study were much less than the actually reported compositions of phase-III ( $1.55 < x < 1.72$  in  $\text{H}_x\text{MoO}_3$ ). To reduce the number of configurations, the  $\text{MoO}_3$  framework of the  $Cmcm$  space group, which is a common supergroup of the space groups of  $\text{MoO}_3$  ( $Pbnm$ ) and phase-III ( $C2/m$ ), was used as the initial structure, and protons were attached to  $\text{O}_3$  sites toward their adjacent  $\text{O}_3$  sites of the next  $\text{MoO}_3$  layer within  $3.1 \text{ \AA}$ . For  $\text{H}_4\text{Mo}_8\text{O}_{24}$ , configurations were restricted to two protons in each gap with inter-proton distances more than  $1.8 \text{ \AA}$  to further reduce the configurations. This restriction excludes structures having a proton facing another proton and those having multiple protons attached to a single  $\text{O}_3$  site. In the lowest energy structure of  $\text{H}_2\text{Mo}_8\text{O}_{24}$ , two protons are attached to different  $\text{O}_3$  sites forming a chain of hydrogen bonds (Fig. 3(d)). The second lowest energy structure has two protons attached to a single  $\text{O}_3$  site (Fig. 3(e)). The energy difference between these two structures is  $0.002 \text{ eV}$  per proton, which is negligible in consideration of computation accuracy. Their energies are also close to that of the lowest energy structure with intralayer protons. The lowest energy structure of  $\text{H}_4\text{Mo}_8\text{O}_{24}$  has  $\text{OH}_2$  units at two  $\text{O}_3$  sites (Fig. 3(f)), even though such configurations

are excluded in the initial structures of  $\text{H}_4\text{Mo}_8\text{O}_{24}$ . This structure is lower in energy by  $0.09 \text{ eV}$  per proton than the lowest energy structure of  $\text{H}_4\text{Mo}_8\text{O}_{24}$  with intralayer protons. However, it is still difficult to conclude that the protons are accommodated in the interlayer sites more preferably than in the intralayer sites at  $\text{H}_{0.5}\text{MoO}_3$ . This is because the conventional GGA exchange-correlation functional does not properly take van der Waals interaction into account, which could overestimate the energies of  $\text{MoO}_3$  and  $\text{H}_x\text{MoO}_3$  with intralayer protons (while having no hydrogen bonds between the  $\text{MoO}_3$  layers). As the local structure of the intralayer protons considerably changes in the  $\text{H}_8\text{Mo}_8\text{O}_{24}$  model, the interlayer protons would become stable at  $x > 0.5$  in  $\text{H}_x\text{MoO}_3$ . Singly attached interlayer protons seem rather unstable at  $\text{H}_4\text{Mo}_8\text{O}_{24}$  because all relaxed structures have at least one  $\text{OH}_2$  unit. The hydrogen bonds toward the next  $\text{MoO}_3$  layers cooperatively result in a monoclinic distortion. The  $\text{OH}_2$  units at the interlayer sites have been experimentally observed from inelastic neutron scattering spectra for highly reduced  $\text{H}_x\text{MoO}_3$ .<sup>13</sup>

Even though protons often moved to other sites during the structural relaxation, none of the protons moved between the intralayer and interlayer sites. This implies a high potential barrier between the intralayer and interlayer sites. Hence, the phase transition between phase-I and phase-III (or other phases with interlayer protons) would occur by phase boundary migration, not by rearrangement of protons in the bulk. To transform phase-III (or phase-II) into phase-I, it is necessary to remove all the protons from the interlayer sites and to reinsert them into the intralayer sites. This would require similar potential to form the  $\text{MoO}_3$  phase from phase-III. This is a probable reason why phase-I was never observed during the oxidation processes of phase-III.

### 3.3. Charge-discharge properties as a positive electrode for proton batteries

Since the  $\text{MoO}_3$ /phase-I biphasic and phase-I monophasic reactions occur at relatively high potential (*ca.*  $0.5 \text{ V}$  vs. SHE), they can be used as a positive electrode material for proton batteries. Therefore, repeated reduction-oxidation processes were conducted with  $\text{MoO}_3$  half-cells in the potential range from  $0.10$  to  $0.50 \text{ V}$  to investigate the cyclability as a positive electrode material. Fig. 4(a) and (b) show the reduction-oxidation curves, reduction-oxidation capacities, and coulombic efficiencies of the  $\text{MoO}_3$  electrode at  $100 \text{ mA g}^{-1}$ . The first reduction and oxidation capacities are *ca.*  $80$  and  $60 \text{ mA h g}^{-1}$ . The irreversible capacity in the first cycle comes from the incomplete phase transition from phase-I to  $\text{MoO}_3$  as shown in *operando* XRD (Fig. 2). In the subsequent cycles, the reduction-oxidation capacities increase as the cycle number increases and reach a maximum value of *ca.*  $100 \text{ mA h g}^{-1}$  in the 37th cycle with an average reduction voltage of *ca.*  $0.24 \text{ V}$  ( $0.44 \text{ V}$  vs. SHE). The reason for the capacity increase is described in the next paragraph. When the reduction cut-off voltage was set at  $0.05 \text{ V}$ , the average electrode potential of  $0.24 \text{ V}$  ( $0.44 \text{ V}$  vs. SHE) decreased to  $0.11 \text{ V}$  ( $0.31 \text{ V}$  vs. SHE) (Fig. S6†) due to the irreversible phase transition from phase-I to phase-III in the first



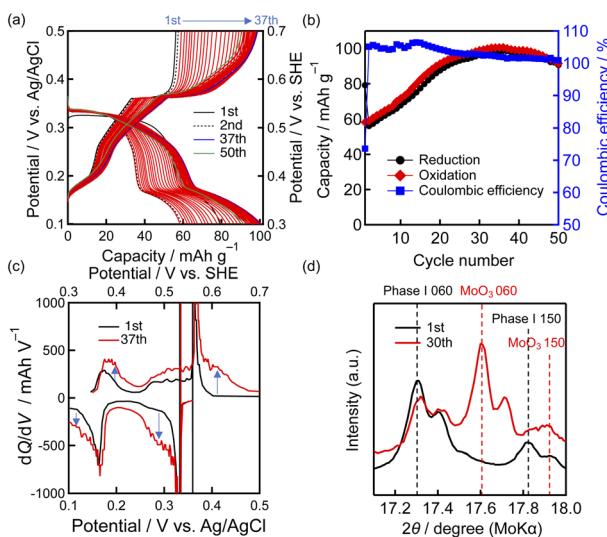


Fig. 4 Reduction–oxidation properties of the  $\text{MoO}_3$  electrode at  $100 \text{ mA g}^{-1}$  in the potential range from  $0.10$  to  $0.50$  V; (a) reduction–oxidation curves; (b) reduction–oxidation capacities and coulombic efficiency; (c)  $dQ/dV$  plots. (d) *Ex situ* XRD patterns of the  $\text{MoO}_3$  electrodes after the 1st and 30th oxidation steps.

reduction. While the use of the reduction–oxidation process between phase-IIa, phase-II, and phase-III has recently been reported,<sup>12</sup> preventing the phase transition from phase-I to phase-III can lead to higher operating potential in aqueous proton batteries.

Fig. 4(c) shows the  $dQ/dV$  plots in the first and 37th cycles. The redox peaks at *ca.*  $0.35$  and  $0.15$  V, which are attributed to the  $\text{MoO}_3$ /phase-I biphasic and phase-I monophasic reactions, are observed in both the first and 37th cycles, showing that the phase transition behavior is basically unchanged. On the other hand, the capacities in the high overpotential regions clearly increase (shown as blue arrows in Fig. 4(c)), which suggests that the promotion of  $\text{MoO}_3$  formation during oxidation and proton insertion during reduction causes the capacity increase. The higher intensity of  $\text{MoO}_3$  diffraction after the 30th oxidation than that after the first oxidation in the *ex situ* XRD patterns (Fig. 4(d)) supports the facilitation of  $\text{MoO}_3$  formation during oxidation in the reduction–oxidation cycles. The *ex situ* FE-SEM/EDS images of the  $\text{MoO}_3$  electrodes (Fig. S7†) show almost no morphological change after the first reduction, which indicates that the  $\text{MoO}_3$ /phase-I biphasic reaction is an insertion reaction rather than a conversion reaction. In contrast, there are some cracks in  $\text{MoO}_3$  particles after the 30th oxidation, which are probably caused by the repeated anisotropic volume changes during the reduction–oxidation cycles. Phase transition from  $\text{MoO}_3$  to phase-I causes *ca.*  $1.5\%$  and  $1.1\%$  increase in the lattice constants  $b$  and  $c$ , respectively, and *ca.*  $1.7\%$  decrease in the lattice constant  $a$ . We speculate that the particle cracking facilitates the phase-transition and proton diffusion, resulting in capacity increase, and thus the optimization of the morphology can improve the reduction–oxidation properties. Fig. S8† shows the reduction–oxidation curves of the  $\text{MoO}_3$  electrode at different current densities. The oxidation capacity

at  $1 \text{ A g}^{-1}$  is *ca.*  $50\%$  of that at  $100 \text{ mA g}^{-1}$ , which shows that the rate capability is not so limited despite the sluggish phase transition from phase-I to  $\text{MoO}_3$ .

### 3.4. Charge–discharge properties of the $\text{MoO}_3|\text{H}_2\text{SO}_4$ aq.|| $\text{H}_x\text{MoO}_3$ full-cell

Finally, we constructed a  $\text{MoO}_3|\text{H}_2\text{SO}_4$  aq.|| $\text{H}_x\text{MoO}_3$  full-cell, to demonstrate the operation of an aqueous proton battery composed of two insertion-type oxide materials. We utilized the phase-III monophasic and phase-III/phase-IV biphasic regions in the potential range from  $-0.3$  to  $0$  V for the negative electrode reactions. Fig. 5(a)–(d) show the charge–discharge curves, charge–discharge capacities, and average charge–discharge voltages of the  $\text{MoO}_3|\text{H}_2\text{SO}_4$  aq.|| $\text{H}_x\text{MoO}_3$  full-cell at  $200 \text{ mA g}^{-1}$  based on the mass of  $\text{MoO}_3$  on one side of the electrode. The loading masses of  $\text{MoO}_3$  in the positive and negative electrodes were set to the same value as described in the Experimental section. The charge–discharge potential curves of the positive and negative electrodes (Fig. 5(b)) indicate that the designed reactions reversibly occur in the full-cell with the main voltage plateau of  $0.6$  V (Fig. 5(a)). We therefore conclude that a rocking-chair-type proton battery composed of insertion-type oxide active materials is successfully established. The highest discharge capacity is  $73 \text{ mA h g}^{-1}$  in the first cycle, and the capacity retention rate in the 50th cycle is *ca.*  $70\%$ . The optimization of the material morphology,<sup>23</sup> positive–negative mass ratio, cell fabrication process and cut-off voltage could improve the slight capacity decrease during cycling. The cell keeps the coulombic efficiency over  $98\%$  until the 50th cycle. The average discharge voltage and the energy density based on the total mass of the active materials are  $0.48$  V and  $17 \text{ W h kg}^{-1}$ , respectively, in the

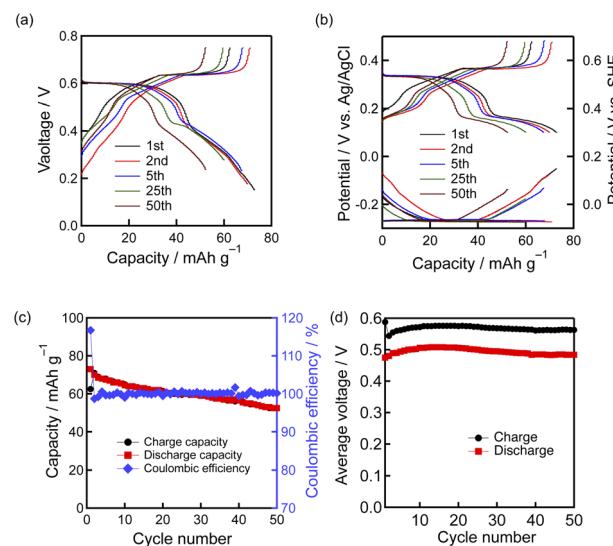


Fig. 5 Charge–discharge properties of the  $\text{MoO}_3|50 \text{ wt\% H}_2\text{SO}_4|\text{H}_x\text{MoO}_3$  full-cell at  $200 \text{ mA g}^{-1}$ ; (a) cell voltage; (b) potentials of positive and negative electrodes; (c) charge/discharge capacities and coulombic efficiency; (d) average charge/discharge voltages. The capacities were calculated based on the mass of  $\text{MoO}_3$  on one side of the electrode.



1st cycle, which are higher than those of the full cell using the conventional positive electrode reaction, 0.33 V and 15 W h kg<sup>-1</sup> (Fig. S9 and Table S2†).

## 4. Conclusions

The proton insertion–extraction mechanism of MoO<sub>3</sub> was investigated using *operando* XRD and DFT calculation. The operating potential of the MoO<sub>3</sub> electrode as a positive electrode for aqueous proton batteries was optimized based on the obtained results, and the MoO<sub>3</sub>–H<sub>2</sub>SO<sub>4</sub> aq.–H<sub>x</sub>MoO<sub>3</sub> full-cell was successfully constructed.

The phase transition behavior of the MoO<sub>3</sub> electrode between MoO<sub>3</sub> and fully protonated phases (phase-IV) was clarified by *operando* XRD, including irreversible phase transition from phase-I to phase-III. It was also shown by *operando* XRD that phase transition from MoO<sub>3</sub> to phase-I could almost reversibly be utilized by preventing the irreversible phase transition from phase-I to phase-III below 0.3 V vs. SHE. DFT calculation suggested that the stable proton accommodation site changed from the intralayer site to the interlayer site at higher proton contents than H<sub>0.5</sub>MoO<sub>3</sub> and implied a high potential barrier between the intralayer and interlayer sites. From these results, it was strongly suggested that the irreversibility of the phase transition from phase-I to phase-III originated from the change of the proton accommodation site from intralayer to interlayer.

The MoO<sub>3</sub> electrode using phase transition between MoO<sub>3</sub> and phase-I showed a maximum reversible capacity of 100 mA h g<sup>-1</sup> and an average reduction potential of 0.44 V vs. SHE. The MoO<sub>3</sub>–50 wt% H<sub>2</sub>SO<sub>4</sub> aq.–H<sub>x</sub>MoO<sub>3</sub> full-cell exhibited an average discharge voltage of 0.47 V, which is the highest among reported aqueous proton batteries (composed of insertion-type oxide active materials) and maintains a maximum discharge capacity of 73 mA h g<sup>-1</sup>.

Considering that commercially available MoO<sub>3</sub> powder with micrometer-order size was used in this study and phase transition from phase-I to MoO<sub>3</sub> was kinetically sluggish, it is strongly expected that the charge–discharge characteristics can be improved by controlling the particle morphology.

## Author contributions

A. I.: investigation (experiments), methodology (*operando* XRD), and writing – original draft, Y. K.: investigation (DFT calculations) and writing – original draft, T. N.: investigation (experiments), and H. A.: project administration, conceptualization, and writing – review & editing.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

FE-SEM and EDS measurements were supported by Prof. Masaaki Hirayama, Prof. Naoki Matsui, Prof. Kota Suzuki, and Prof. Ryoji Kanno (Tokyo Institute of Technology). Electrochemical

measurements were technically supported by Ms Yuko Narita and Mr Teruya Hiramatsu (Tokyo Institute of Technology). Some of the DFT calculations were performed on the Numerical Materials Simulator at the National Institute for Materials Science.

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