


 Cite this: *RSC Adv.*, 2023, **13**, 8901

# Co-deposition of Co–Ni alloy catalysts from an ethylene glycol system for the hydrogen evolution reaction

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The preparation of active, stable and low-cost non-noble electrocatalysts for the hydrogen evolution reaction (HER) using the electrochemical water splitting process is crucial for the promotion of sustainable energy. In this study, Co–Ni alloys with various Co contents are prepared using a galvanostatic method and the co-deposition behavior of  $\text{Co}^{2+}$  and  $\text{Ni}^{2+}$  in ethylene glycol (EG) is reported. These results indicate that the presence of additional  $\text{Ni}^{2+}$  species can accelerate the Co–Ni co-deposition process and  $\text{Co}^{2+}$  species in the system can inhibit the reduction of  $\text{Ni}^{2+}$ . Moreover, the two effects are improved with an increase in  $\text{Ni}^{2+}$  or  $\text{Co}^{2+}$  species concentration in the EG system, respectively. Chronoamperometry records show that the Co–Ni electro-crystallization mechanism is one of 3D instantaneous nucleation and growth. Moreover, the Co–Ni alloy with 59.46 wt% Co exhibits high electrocatalytic activity for HER with an overpotential of 133 mV at  $10 \text{ mA cm}^{-2}$  in 1 M KOH due to a high value of electrochemical active surface area (ECSA) ( $955.0 \text{ cm}^2$ ). Therefore, the Co–Ni alloy electrocatalyst obtained from the EG system could be a promising candidate for practical hydrogen production.

Received 26th December 2022

Accepted 23rd February 2023

DOI: 10.1039/d2ra08233k

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## 1. Introduction

Normally, the electrodeposition technique has been employed as a surface treatment method with high preparation efficiency under ambient conditions. The technique can also be expediently scaled up on a large surface area matrix to achieve large-scale production. In addition, it can also be easily applied to various matrices to prepare various functional materials, particularly suitable for the preparation of non-noble metal transition metal-based catalytic materials.<sup>1</sup> The electrodeposited Co–Ni alloy is a typical non-noble metal transition material and has inevitably been studied extensively due to its good corrosion resistance and wear resistance, high mechanical strength, moderate thermal conductivity and excellent electrocatalytic and magnetic properties and thus it has been widely applied in various industrial fields, such as advanced energy storage materials, electroactive materials, electronic materials and corrosion prevention. For instance, Co–Ni alloy coatings were prepared by K. R. Marikkannu *et al.*<sup>2</sup> from an acetate electrolyte containing any one of the additives saccharin, dextrin, 1,4-butyne diol, coumarin, 1,3-naphthalene sulfonic acid, formaldehyde, glycine and crotonaldehyde, and they found that the microhardness and corrosion resistance of the obtained Co–Ni coatings could be improved by adding these

additives. Coincidentally, A. C. Lokhande *et al.*<sup>3</sup> found that Co–Ni alloy coatings obtained from sulfate bath electrodeposition at room temperature with saccharin ( $10 \text{ g L}^{-1}$ ) as an additive exhibited superior microhardness and corrosion resistance. Meanwhile, as well as adding various additives to the electroplating solution to improve the performance of the Co–Ni alloy coatings, some scholars and researchers have also tried to improve the performance of these Co–Ni alloy coatings by applying external auxiliary factors in the electroplating process. For example, Co–Ni and Co–Ni/SiC coatings were electrodeposited by Xiaoyun Hu *et al.*<sup>4,5</sup> under the introduction of a supergravity field, and it was found that the two prepared coatings showed better degrees of smoothness and microhardness compared with the corresponding coatings electrodeposited under a standard gravity field, especially under the condition of a supergravity field, and the corrosion resistance of the obtained Co–Ni/SiC coatings with various Co contents was greatly improved. Cansen Liu *et al.*<sup>6</sup> found that the Co–Ni alloy coating obtained by supercritical carbon dioxide assisted electrodeposition exhibited better properties, such as wear resistance, surface appearance and surface roughness, and a smaller grain size than that of the Co–Ni alloy obtained by conventional electrodeposition. Even if both additives and external auxiliary factors can improve the performance of these coatings, the prepared materials are inevitably doped with impurities and their cost and complexity for the electrodeposition process can also be increased.<sup>3,6</sup> It should be noted that all the above obtained Ni–Co alloys were electrodeposited from aqueous

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solution systems (as shown in Table 1) and these electrodeposition processes were normally anomalous co-deposition mechanisms due to the fact that the adsorption of  $\text{Co(OH)}_{\text{ads}}^+$  is preferential to that of  $\text{Ni(OH)}_{\text{ads}}^+$  on a cathode electrode, and  $\text{Co(OH)}_{\text{ads}}^+$  as an intermediate species plays an important role in metallic cobalt deposition, while these intermediate species can obstruct the access of  $\text{Ni(OH)}_{\text{ads}}^+$  to the cathode electrode surface.<sup>7–9</sup> That is to say, the reduction of  $\text{Ni}^{2+}$  with a relatively positive initial reduction potential may be inhibited, while the reduction of  $\text{Co}^{2+}$  with a relatively negative initial reduction potential may be promoted during electrodeposition in aqueous systems, and then the molar ratio of Co/Ni in the prepared Co–Ni coatings is greater than that of  $\text{Co}^{2+}/\text{Ni}^{2+}$  in the electrolyte. In this case, there is a higher Co content in the obtained Co–Ni coatings. It should be noted that another comprehensive steady-state model for Co–Ni alloy co-deposition in an acidic aqueous solution containing sulfate was proposed by Jorge Vazquez-Arenas *et al.*<sup>10</sup> They found that the anomalous behavior could be attributed to the much faster charge-transfer of  $\text{Co}^{2+}$  reduction than that of  $\text{Ni}^{2+}$  reduction instead of the preferential adsorption of  $\text{Co(I)}_{\text{ads}}$  over that of  $\text{Ni(I)}_{\text{ads}}$  on a cathode surface. Thus, for different systems or baths, the abnormal co-

deposition model of the Co–Ni alloy may be different. Although these Co–Ni alloys with different surface morphologies and various Co contents could be prepared from aqueous systems containing  $\text{Co}^{2+}$  and  $\text{Ni}^{2+}$  (as seen in Table 1), these electrodeposition processes were usually accompanied by an intensive hydrogen evolution reaction (HER), resulting in a profound effect on the current efficiency and quality of the Co–Ni alloy coatings.<sup>3,5,6,8–23</sup> Importantly, a few holes<sup>6,9,11,19,21</sup> and/or microcracks<sup>3,5,16</sup> (as seen in Table 1) could be found on the Co–Ni alloys electrodeposited from aqueous systems, resulting in a profound effect on the catalytic stability for the HER.

The ionic liquid (IL) system has become a vital type of electrolyte for success in an aqueous solution system because it represents an important development in the field of environmental protection and shows enormous potential in the synthesis of functional materials.<sup>24–28</sup> More importantly, ILs can provide a wide electrochemical window, low volatility and high electrical conductivity for electrolysis without the presence of HER. Thus, compared with traditional aqueous systems, these plating techniques from ILs can improve the current efficiency and quality of the electrodeposited coatings, and eliminate the

**Table 1** Comparison of HER activity, surface morphology and Co content of Co–Ni alloys obtained in previous work

Alloy coating	Employed electrolyte	Co content	Surface morphology	$\eta_{10}^a$ (mV)	$b$ (mV dec <sup>-1</sup> )	$C_{dl}$ (mF cm <sup>-2</sup> )	Reference
Co–Ni	EG	22.6–82.8 wt%	Spherical structure/ fibrous structure	–139	117.5–187.6	0.6–41.3	This work
Co–Ni	ChCl-urea	2.34–19.68 wt%	Needle like structure	—	—	0.0103–0.0905 (3.5% NaCl)	26
Co–Ni	ChCl-EG	4/18/40 wt%	Pine-leaf-like/spherical structure	—	—	—	28
Co–Ni	ChCl-EG	2.94–11.56 wt%	Spherical structure	—	—	0.0222–0.0503 (3.5% NaCl)	27
Co–Ni	[EMIM]HSO <sub>4</sub> (ionic liquid) and EG	10.48–42.83 wt%	Spherical “nodules”	–139	82.5–119	—	24
Co–Ni	Aqueous solution	15.63–46.39 wt%	Colony-like structures or hemispherical structures	—	—	—	5
Co–Ni	Aqueous solution	10.87–38.3 wt%	Nanocone structure	–107	120	17.5–50.5	8
Co–Ni	Aqueous solution	7–27 at%	Spherulites structure with some microcracks	—	—	—	3
Co–Ni	Aqueous solution	12.6–90.3 wt%	Cellular-like network or spherical grains	—	—	—	9
Co–Ni	Aqueous solution	73.66/76.55 wt%	Wheat-like structure	—	—	—	6
Co–Ni	Aqueous solution	58.47 wt%	Nanocone structure	—	—	—	22
Co–Ni	Aqueous solution	29–75 wt%	Nanocones and/or lamellar structure	–180	127–308.9	—	20
Co–Ni	Aqueous solution	3.88–50.38 wt%	Granule structure	–181	108	0.0256	11
Co–Ni	Aqueous solution	83/79%	Acicular or nodular morphology	—	—	—	18
Co–Ni	Aqueous solution	50–84 wt%	Acicular or nodular grain shapes	—	—	—	17
Co–Ni	Aqueous solution	29.8–61 wt%	Cauliflower-like/coral- like/spongy-like	—	—	—	21
Co–Ni	Aqueous solution	42 at%	Spherical particles	–162	60	—	41
Co–Ni–Fe	Aqueous solution	8.05 wt%	Nanocone structure	–91	86	44	12
NiCoP/rGO	—	—	Nanosheet	–206	—	—	48

<sup>a</sup> Overpotential ( $\eta_{10}$ ) was recorded at  $j = 10 \text{ mA cm}^{-2}$ .



necessity to employ additional additive agents.<sup>2,3,12</sup> For instance, Co–Ni alloy coatings with various Co contents (4, 18 and 40 wt%) were successfully prepared by Y. H. You *et al.*<sup>28</sup> from choline chloride IL/ethylene glycol containing nickel and cobalt chlorides at room temperature, and the electrodeposition mechanism, microstructure, and corrosion resistance of the obtained films were also investigated in detail. They found that the electrodeposition process showed an absence of an anomalous co-deposition mechanism, while anomalous co-deposition for the Co–Ni alloy could frequently be observed in the aqueous systems.<sup>7,10</sup> In addition, they found that their corrosion resistance could be improved with an increase in Co content. Subsequently, Co–Ni alloys were also successfully electrodeposited by Wenruo Li *et al.*<sup>26,27</sup> from choline chloride IL-urea and choline chloride IL-ethylene glycol systems, respectively. They found that the reduction process of the Co–Ni alloy in the choline chloride IL-urea system was irreversible under diffusion control and its electro-crystallization process was three-dimensional instantaneous nucleation growth. However, these systems containing choline chloride are normally highly hygroscopic and their drying indicates a crucial process for minimizing water intake in these systems. In addition, large amounts of chloride ions can bring about an aggressive environment for deposits and substrates. A simple method to obtain stable systems is to remove choline chloride using only ethylene glycol as solvent. For instance, G. Panzeri *et al.*<sup>29</sup> investigated the electrodeposition of cobalt films and nanowires from ethylene glycol solutions containing metal chloride precursor salts and found that the cobalt reduction process occurred with high cathodic efficiency (CE  $\sim$  85%), indicating the limited presence of secondary reactions. G. Panzeri *et al.*<sup>30</sup> investigated ethylene glycol as a solvent for the electrodeposition of iron from both bivalent and trivalent iron chloride solutions, and nanostructured iron films with high purity were successfully electrodeposited. Therefore, ethylene glycol can be used as a simple and practical organic solvent for Co–Ni alloy electrodeposition. It should be noted that the electrodeposited Co–Ni alloys normally exhibit excellent electrocatalytic activity and stability for the HER. Thus, in recent years, they have been employed as catalysts for hydrogen production. For instance, when Co–Ni alloy coatings with different Co contents were successfully prepared by Sung Hoon Hong *et al.*<sup>19</sup> from acidic sulfate aqueous solutions, it was found that the Co–Ni coating with 51 wt% Co showed the highest catalytic performance for the HER. Similarly, nanostructured Co–Ni alloys with various Co contents (varying from 0% to 75 wt%) were fabricated by Ya Li *et al.*<sup>20</sup> They found that the morphologies of Co–Ni alloys were changed from nanocones to a lamellar structure with the change in Co content and the Ni-60% Co alloy coating exhibited optimal electrocatalytic activity for the HER with a small overpotential of 180 mV at 10 mA cm<sup>-2</sup>. In addition, F. Ganci *et al.*<sup>31</sup> prepared nanostructured Co–Ni alloy electrodes by pulsed potential electrodeposition and found that the nanostructured Co–Ni electrode with 94.73 at% Co exhibited the best HER electrocatalytic performance.

In our previous work, a nanocrystalline Co coating with a fibrous surface morphology was successfully electrodeposited

from an [EMIM]HSO<sub>4</sub>-EG mixture system, and it exhibited excellent catalytic activity and stability with an overpotential of 199 mV for the HER at a geometrical current density of 10 mA cm<sup>-2</sup> in 1 M KOH solution.<sup>32</sup> Subsequently, in order to further improve the catalytic performance and stability of the electrode material toward hydrogen evolution, Co–Ni alloy was electrodeposited in the [EMIM]HSO<sub>4</sub>-EG system,<sup>24</sup> and exhibited better catalytic activity and stability with an overpotential of 139 mV for the HER at a geometrical current density of 10 mA cm<sup>-2</sup> in 1 M KOH solution. In addition, the co-deposition behavior of Co<sup>2+</sup> and Ni<sup>2+</sup> in the [EMIM]HSO<sub>4</sub>-EG system and the anomalous co-deposition phenomenon due to the inhibition of Ni<sup>2+</sup> reduction by Co<sup>2+</sup> were investigated. However, the [EMIM]HSO<sub>4</sub>-EG mixture as an electrolyte can increase the plating cost due to the additional [EMIM]HSO<sub>4</sub> IL, which is not conducive to industrial mass production. Therefore, in this study, a pure EG system was used as solvent to electrodeposit Co–Ni alloy by a galvanostatic electrodeposition method, expecting that it could present better catalytic activity for the HER. Hence, the co-deposition behavior of Co<sup>2+</sup> and Ni<sup>2+</sup> in the EG system and its electro-crystallization mechanism were observed by cyclic voltammetry (CV) and chronoamperometry (CA) techniques, respectively, and Co–Ni alloy coatings with different Co contents were prepared from the system. The surface morphology, composition, microstructure and elemental valence states of the Co–Ni alloy coatings were also characterized using SEM, EDS, XRD and XPS techniques. Moreover, the catalytic property for the obtained Co–Ni coatings was also recorded by linear sweep voltammetry (LSV) and electrochemical impedance spectra (EIS) techniques in a 1 M KOH system.

## 2. Experimental

### 2.1. Chemicals

EG ( $\geq$ 99.5%), anhydrous NiCl<sub>2</sub> (99.9%) and CoCl<sub>2</sub> (99.7%) were bought from Shanghai Aladdin Bio-Chem Technology Co, Ltd. All other chemicals and reagents employed in this work were commercially available and of analytical reagent grade. It should be noted that EG was dried under vacuum for 15 h at 333 K and the anhydrous CoCl<sub>2</sub> and NiCl<sub>2</sub> were also dried under vacuum for 6 h at 393 K before use. The concentration of NiCl<sub>2</sub> was 0.2 M in the EG system. In order to prepare the Co–Ni coatings with various Co contents, the CoCl<sub>2</sub> concentration in the EG solution was varied from 0.1 to 0.7 M.

### 2.2. Plating and electrochemical experiments

All the electrochemical experiments were performed using a conventional three-electrode configuration with the help of an electrochemical workstation (CHI 660B) and the EG solution system was not agitated. The working electrode was a GC electrode (0.07 cm<sup>2</sup>), the counter electrode was platinum foil (3 cm<sup>2</sup>) and the reference electrode was a saturated calomel electrode (SCE). Before use, the GC electrode was preprocessed based on previous literature.<sup>26,27</sup> Nevertheless, in the electrodeposition experiments, a DC power supply and galvanostatic method were



used to prepare Co–Ni alloy coatings and a copper sheet (99.9 wt%) with an exposed area of  $0.5 \text{ cm}^2$  ( $0.5 \times 1.0 \text{ cm}$ ) was used as the plating substrate (cathode) and platinum foil ( $3 \text{ cm}^2$ ) as the anode. The distance between the cathode and anode in the plating bath was 2 cm, and before use the plating substrate was also preprocessed based on previous literature.<sup>6,8,17</sup> In addition, these deposited Co–Ni coatings were cleaned successively in acetone and deionized water to remove the residues after plating and then dried under vacuum before measurement. All experiments were performed in a glove box and electrochemical experiments were carried out in an argon atmosphere containing less than 2 ppm moisture and oxygen.

### 2.3. Characterization of Co–Ni coatings

A scanning electron microscope (SEM, HITACHI S-3000 N) and an energy dispersive spectroscopy (EDS) were employed to observe the surface morphology and composition of the obtained Co–Ni alloy coatings. In addition, an X-ray diffractometer (XRD, Siemens D-5000) was employed to explore the crystal structures of the prepared Co–Ni alloy coatings; its testing parameter were: Cu target  $K\alpha$  ( $\lambda = 0.1541 \text{ nm}$ ) radiation, continuous scan, scanning range  $2\theta = 30\text{--}100^\circ$ , scanning speed  $2^\circ \text{ min}^{-1}$ . X-ray photoelectron spectroscopy (XPS, Thermo Scientific K-Alpha) was employed to confirm the chemical composition and elemental valence states.

### 2.4. Electrocatalytic measurements

The electrocatalytic property for HER on the Co–Ni alloy coatings in 1 M KOH aqueous solution was recorded at 298 K using LSV, EIS and Tafel techniques, employing the above-mentioned electrochemical workstation and three-electrode configuration. The main variations were that a copper sheet coated with Co–Ni ( $0.5 \text{ cm}^2$ ) was employed as the working electrode and a graphite rod as the counter electrode. It is worth noting that EIS was recorded using an overpotential of  $-0.1 \text{ V}$  with an amplitude of 5 mV at frequencies of 100 kHz to 100 mHz. The CV technique with 1000 cycles at a scanning rate of  $50 \text{ mV s}^{-1}$ , as well as a chronoamperometry technique, was performed at 298 K to evaluate the catalytic stability for the Co–Ni coating. It should be noted that the potentials in this work were converted into a reversible hydrogen electrode (RHE) potential based on the method described in the literature.<sup>33,34</sup>

## 3. Results and discussion

### 3.1. Cyclic voltammetry study

Fig. 1 presents the typical cyclic voltammograms of the EG system containing  $0.2 \text{ M Ni}^{2+}$  or/and  $0.4 \text{ M Co}^{2+}$  recorded at 298 K using a scan rate ( $\nu$ ) of  $50 \text{ mV s}^{-1}$ . It can be inferred from curve 1 in Fig. 1 that the EG system exhibits prominent electrochemical stability due to the fact that no apparent reduction or oxidation peaks are found in the range from  $+1.800$  to  $-2.400 \text{ V}$ . However, these CV curves (curves 2, 3 and 4 in Fig. 1) are changed in the presence of  $0.2 \text{ M Ni}^{2+}$  or/and  $0.4 \text{ M Co}^{2+}$  in the EG solution. For curve 2, the cathodic current density increases from  $-1.022 \text{ V}$  (the so-called nucleation overpotential,

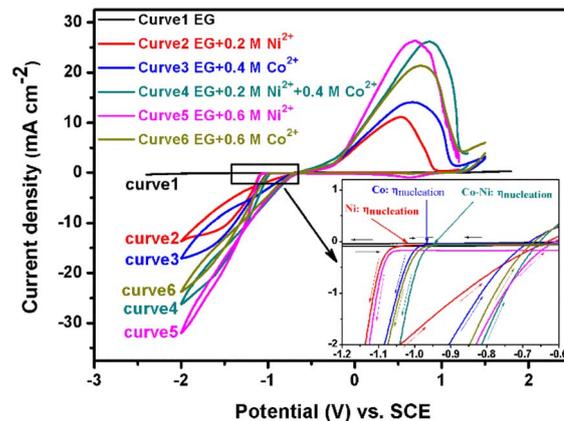


Fig. 1 Cyclic voltammograms of the EG system (curve 1), the EG system containing 0.2 or 0.6 M  $\text{Ni}^{2+}$  (curves 2, 5), the EG system containing 0.4 or 0.6 M  $\text{Co}^{2+}$  (curves 3, 6) and the EG system containing 0.2 M  $\text{Ni}^{2+}$  and 0.4 M  $\text{Co}^{2+}$  (curve 4) recorded on a GC electrode at 298 K with scan rate of  $50 \text{ mV s}^{-1}$ .

$\eta_{\text{nucleation}}$ ) to  $-1.611 \text{ V}$  (clearly presented in the inset in Fig. 1), and then a well-defined cathodic shoulder can be found between  $-1.611$  and  $-1.891 \text{ V}$ . During the reversal scanning, a current density loop (crossover), implying the presence of a nucleation and crystal growth process, can be found at  $-1.159 \text{ V}$ , and the anodic current density peak is observed at  $0.557 \text{ V}$ , which is ascribed to the anodic stripping of the electrodeposited metal Ni onto the GC electrode. These results are basically in accordance with the electrochemical behavior for  $\text{Ni}^{2+}$  reduction in some ILs.<sup>26</sup>

For curves 3 and 4, the cathodic current density increases sharply from  $-0.971$  and  $-0.942 \text{ V}$  to  $-1.641$  and  $-1.609 \text{ V}$ , respectively, and then two mild cathodic shoulders can be found (curve 3: between about  $-1.641$  and  $-1.999 \text{ V}$ ; curve 4: between about  $-1.609$  and  $-1.999 \text{ V}$ ). During the reversal scanning, two obvious current density loops can be found at  $-1.195$  (curve 3) and  $-1.245 \text{ V}$  (curve 4), and the two corresponding anodic current density peaks are recorded at  $0.679$  (curve 3) and  $0.857 \text{ V}$  (curve 4). The two cathodic shoulders are due to the electrochemical reduction of  $\text{Co}^{2+}$  to Co and the co-deposition of  $\text{Ni}^{2+}$  and  $\text{Co}^{2+}$ , respectively, while the two anodic density peaks can be attributed to the corresponding stripping of Co and Co–Ni alloy. Interestingly, it can be observed that the nucleation overpotential ( $\eta_{\text{nucleation}}$ ) for  $\text{Ni}^{2+}$  reduction to Ni ( $-1.022 \text{ V}$ ) is more negative than that of  $\text{Co}^{2+}$  reduction to Co ( $-0.971 \text{ V}$ ), implying that it is easier to prepare a cobalt-rich Co–Ni alloy, which is different from the result found in other literature.<sup>24</sup> Meanwhile, the co-deposition nucleation overpotential for Co–Ni alloy ( $-0.942 \text{ V}$ ) in the system is more positive than that of pure nickel or pure cobalt, indicating that Co–Ni alloy co-deposition process is easier than that of metal Ni or Co.<sup>35</sup> More interestingly, the cathode current density for curve 4 ( $0.2 \text{ M Ni}^{2+}$  and  $0.4 \text{ M Co}^{2+}$ ) is smaller than that of curve 5 ( $0.6 \text{ M Ni}^{2+}$ ) and bigger than that of curve 6 ( $0.6 \text{ M Co}^{2+}$ ) at the same potential during the cathodic scanning. These results indicate that the presence of additional  $\text{Ni}^{2+}$  species can



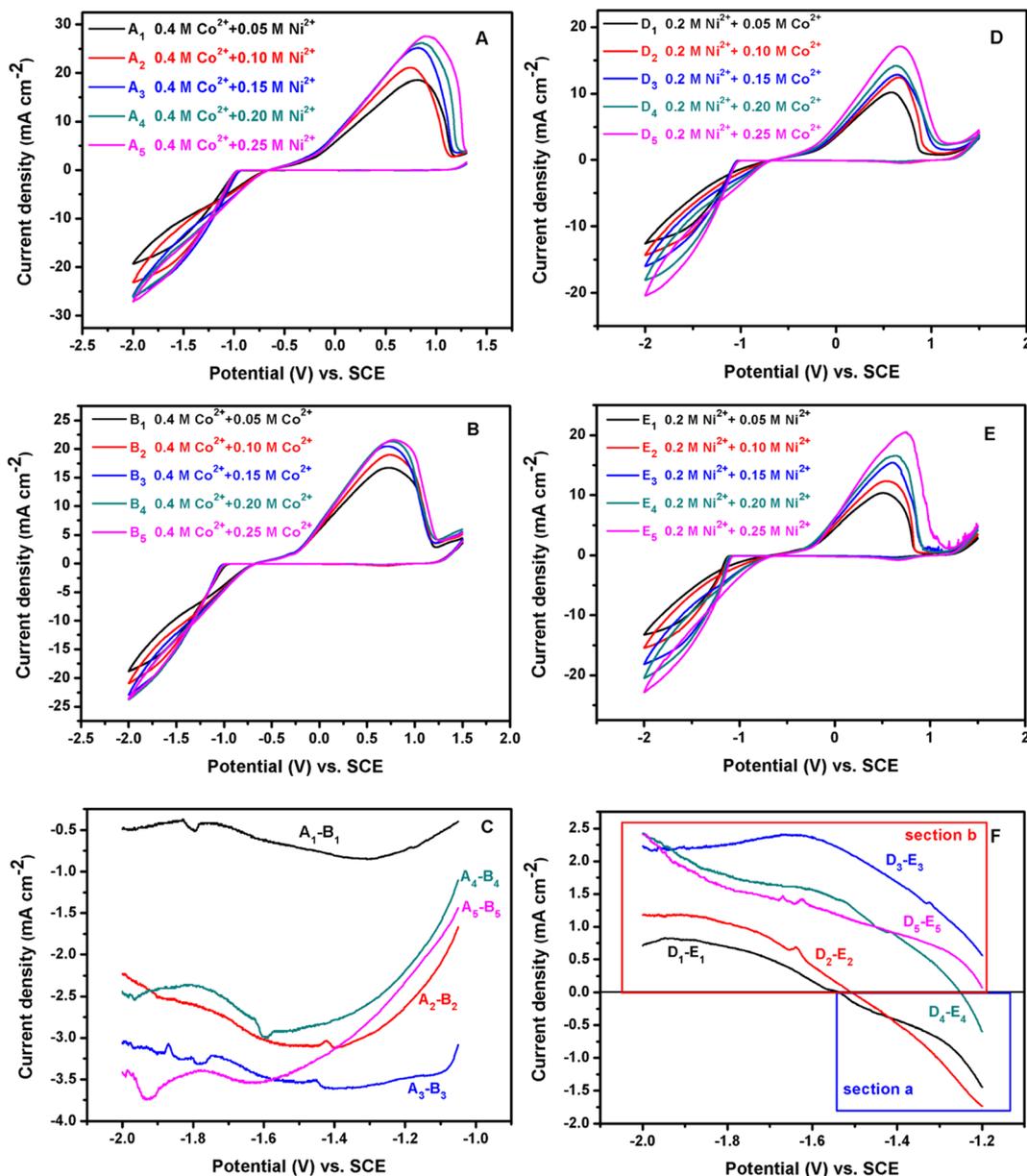


Fig. 2 Cyclic voltammograms of EG-0.4 M  $\text{Co}^{2+}$  containing various  $\text{Ni}^{2+}$  concentrations (A) and EG-0.2 M  $\text{Ni}^{2+}$  containing various  $\text{Co}^{2+}$  concentrations (D), EG containing various  $\text{Co}^{2+}$  (B) or  $\text{Ni}^{2+}$  (E) concentrations. The difference value for the cathode current density based on (A–C), and the difference value for the cathode current density based on (D–F).

accelerate the Co–Ni co-deposition process, and  $\text{Co}^{2+}$  species in the system can inhibit the reduction of  $\text{Ni}^{2+}$ . Moreover, the two effects should be improved with an increase in  $\text{Ni}^{2+}$  or  $\text{Co}^{2+}$  species concentration in the EG system, respectively. In order to verify this, another two CV tests using a scan rate ( $\nu$ ) of  $50 \text{ mV s}^{-1}$  on GC at 298 K were performed in an EG-0.4 M  $\text{Co}^{2+}$  system with an increase in  $\text{Ni}^{2+}$  concentration from 0.05 to 0.25 M (Fig. 2A) and in the EG-0.2 M  $\text{Ni}^{2+}$  system with an increase in  $\text{Co}^{2+}$  concentration from 0.05 to 0.25 M (Fig. 2D), as exhibited in Fig. 2. In addition, in order to obtain valuable information about the cathode current density change, CV measurements using a scan rate ( $\nu$ ) of  $50 \text{ mV s}^{-1}$  on GC at 298 K in EG with various  $\text{Co}^{2+}$  or  $\text{Ni}^{2+}$  concentrations were also carried out and

are exhibited in Fig. 2B and E. It is found that the nucleation overpotential for the co-deposition of  $\text{Ni}^{2+}$  and  $\text{Co}^{2+}$  fluctuates slightly from  $-0.952$  to  $-0.927 \text{ V}$  with an increase in  $\text{Ni}^{2+}$  concentration (Fig. 2A) and its average value is about  $-0.939 \text{ V}$ , while the nucleation overpotentials for  $\text{Co}^{2+}$  reduction in EG with various  $\text{Co}^{2+}$  concentrations are about  $-0.963 \pm 0.010 \text{ V}$ . The result indicates that their nucleation overpotentials shift more positively in the presence of additional  $\text{Ni}^{2+}$  species, implying that the co-deposition process of  $\text{Ni}^{2+}$  and  $\text{Co}^{2+}$  is easier than the  $\text{Co}^{2+}$  reduction process. That is to say, the additional  $\text{Ni}^{2+}$  species in EG can promote the nucleation/growth process. Moreover, all the cathode current densities for the EG-0.4 M  $\text{Co}^{2+}$  system with an increase in  $\text{Ni}^{2+}$



concentration from 0.05 to 0.25 M are larger than those in EG with the corresponding equal  $\text{Co}^{2+}$  concentration (Fig. 2C). This result indicates that the additional  $\text{Ni}^{2+}$  species in EG can promote  $\text{Co}^{2+}$  reduction. At the same time, the nucleation overpotentials for the co-deposition of  $\text{Ni}^{2+}$  and  $\text{Co}^{2+}$  fluctuate slightly more from  $-0.997$  to  $-1.016$  V with an increase in  $\text{Co}^{2+}$  concentration (Fig. 2D) and their average value is about  $-1.006$  V, while the nucleation overpotential for  $\text{Ni}^{2+}$  reduction in EG with various  $\text{Ni}^{2+}$  is about  $-1.066 \pm 0.015$  V. This result indicates that the Co–Ni alloy nucleation/growth process is also easier than that of metal Ni. However, the cathode current densities for the EG-0.2 M  $\text{Ni}^{2+}$  system with an increase in  $\text{Co}^{2+}$  concentration from 0.05 to 0.25 M are larger than those in EG with the corresponding equal  $\text{Ni}^{2+}$  concentration at a relatively low overpotential (section a in Fig. 2F), and smaller at a relatively high overpotential (section b in Fig. 2F).

Moreover, the switch overpotential is positively shifted with an increase in  $\text{Co}^{2+}$  concentration from 0.05 to 0.15 M, and is then slightly negatively shifted with a further increase in  $\text{Co}^{2+}$  concentration. In addition, the difference value for the cathode current density between the EG-0.2 M  $\text{Ni}^{2+}$  system containing additional various  $\text{Co}^{2+}$  concentrations and the EG system containing only various corresponding equal  $\text{Ni}^{2+}$  concentrations increases with an increase in  $\text{Co}^{2+}$  concentration from 0.05 to 0.15 M, and then decreases slightly with a further increase in  $\text{Co}^{2+}$  concentration. All these results imply that the additional  $\text{Co}^{2+}$  species in the EG system can inhibit the co-deposition process of  $\text{Ni}^{2+}$  and  $\text{Co}^{2+}$  at a relatively high overpotential and the inhibition effect can be encouraged as the  $\text{Co}^{2+}$  species increases. The inhibition behavior can be attributed to the much faster charge-transfer of  $\text{Co}^{2+}$  reduction than that of  $\text{Ni}^{2+}$  reduction on a GC surface at a relatively high overpotential.<sup>10</sup> However, at a relatively low overpotential, the charge-transfer for  $\text{Co}^{2+}$  reduction may be not faster than that of  $\text{Ni}^{2+}$  reduction, while the above acceleration effect for  $\text{Ni}^{2+}$  species in EG plays a dominant role in the Co–Ni alloy co-deposition. Thus, the cathode current density for the EG-0.2 M  $\text{Ni}^{2+}$  system containing various  $\text{Co}^{2+}$  species is larger than that in EG with the corresponding equal  $\text{Ni}^{2+}$  concentration at a relatively low overpotential. It should

be noted that inhibition behavior for  $\text{Ni}^{2+}$  reduction was also observed in an ([EMIM]HSO<sub>4</sub>) IL and EG system,<sup>24</sup> implying that the result is reliable.

### 3.2. Chronoamperometry study

Representative current–time transient curves for an EG solution containing 0.2 M  $\text{Ni}^{2+}$  and 0.4 M  $\text{Co}^{2+}$  are exhibited in Fig. 3a.

From this figure, it is clear that all of these curves look like universal current density transients recorded for the ordinary 3D nucleation and growth of a new phase.<sup>26,27,36–38</sup> In the initial stage, due to the existence of active sites on the non-ideal cathode surface, Co–Ni bimetallic clusters grow radially, employing these active sites as growth centers. It should be noted that all these Co–Ni clusters are in steady-states and small, growing under diffusion control. During this growth process, the current density gradually rises to a maximum value due to the fact that there is no overlap among these cluster diffusion layers. After a period of time, these diffusion domains around Co–Ni nuclei overlap and ultimately the growth of the Co–Ni deposits is controlled by planar diffusion to the entire cathode surface, and then nuclear growth slows down. Therefore, all these current densities at the various applied potentials can decrease and tend to level off.<sup>27</sup> In order to further clarify the mechanism of the Co–Ni alloy nucleation and growth process, non-dimensional  $(j/j_{\text{max}})^2$  vs.  $(t/t_{\text{max}})$  curves deduced from the Sharifker–Hills model<sup>38,39</sup> was employed based on eqn (1) and (2) from current–time transient curves and exhibited in Fig. 3b.

Instantaneous nucleation:

$$\frac{j^2}{j_{\text{max}}^2} = \frac{1.9542}{t/t_{\text{max}}} \left[ 1 - \exp\left(-1.2564 \frac{t}{t_{\text{max}}}\right) \right]^2 \quad (1)$$

Progressive nucleation:

$$\frac{j^2}{j_{\text{max}}^2} = \frac{1.2254}{t/t_{\text{max}}} \left[ 1 - \exp\left(-2.3367 \frac{t^2}{t_{\text{max}}^2}\right) \right]^2 \quad (2)$$

where  $j$  is current density,  $t$  is time, and  $j_{\text{max}}$  is the maximum current density at time  $t_{\text{max}}$ . As shown in Fig. 3b, it is found that

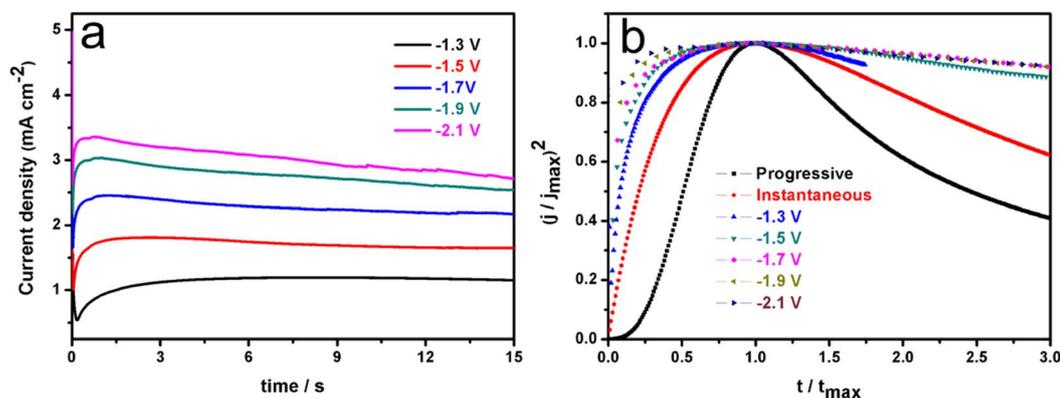


Fig. 3 Chronoamperometric current–time transient curves at different potentials in an EG system containing 0.4 M  $\text{Co}^{2+}$  and 0.2 M  $\text{Ni}^{2+}$  at 323 K (a). Comparison of dimensionless time–current curves with the 3D nucleation model (b).



the Co–Ni alloy nucleation is mainly an instantaneous mode at 323 K at the various applied potentials. The model is similar to the mechanism of Co–Ni alloy nucleation and growth process in ILS.<sup>26,27</sup>

### 3.3. Characterization of Co–Ni alloy coatings

Fig. 4a shows a typical EDS analysis of these deposits obtained at 30 mA cm<sup>-2</sup> for 10 min from an EG system containing 0.4 M Co<sup>2+</sup> and 0.2 M Ni<sup>2+</sup> at 323 K.

It is found that these deposits mainly consist of Co (about 59.46 wt%) and Ni (about 25.71 wt%) with a small residual amount of C and O species, implying that these deposits are the cobalt-enriched Co–Ni alloy. It is worth noting that the C can be attributed to the participation of EG molecules in the co-deposition reaction since these EG molecules can be absorbed on the cathode,<sup>37</sup> while the small O content in these deposits can be attributed to oxidation in air when these deposits were brought out from the EG system. Fig. 4b shows a typical XRD pattern of these deposits obtained at 30 mA cm<sup>-2</sup> for 10 min from an EG system containing 0.4 M Co<sup>2+</sup> and 0.2 M Ni<sup>2+</sup> at 323 K. As shown in Fig. 4b, it becomes clear that four intense copper peaks are found in the spectra, indicating that the thickness of these Co–Ni deposits is so small that the substrate copper is recorded. Meanwhile, the hexagonal close packed (hcp) phase of Co corresponds to (111), (100), (101), (110) and (112) peaks according to PDF#97-004-4990. It is worth noting that none of the diffraction peaks associated with metallic Ni is observed. This may be because the nickel atoms formed a hexagonal close packed (hcp) phase Co (Ni) solid solution by entering the Co crystal lattices.

In addition, X-ray photoelectron spectroscopy (XPS) was employed to investigate the elemental composition and chemical valence states of Co–Ni alloy, metallic Co and metallic Ni in Fig. 5. For the Co 2p region of metallic Co (Fig. 5a), the spectrum could be divided into three peaks, located at Co 2p<sub>3/2</sub> with binding energy values of 780.55, 781.79 and 785.04 eV, which correspond to Co<sup>2+</sup> and Co<sup>3+</sup> species and a shake-up satellite peak, respectively.<sup>40,41</sup> On the Co 2p<sub>1/2</sub> profile, the signal can also be split into three peaks, corresponding to Co<sup>2+</sup>, Co<sup>3+</sup> and

shake-up satellite peaks, with the three binding energy (BE) values of 796.62, 798.15 and 802.41 eV, respectively. For the Ni 2p region of metallic Ni (Fig. 5b), the Ni 2p spectrum peaks with 855.95 and 873.47 eV correspond to the Ni 2p<sub>3/2</sub> and Ni 2p<sub>1/2</sub> profiles, which display the Ni<sup>2+</sup> spin-orbit characteristics.<sup>42,43</sup> Moreover, two shake-up satellite peaks can be observed at about 6 eV more than the peaks for Ni<sup>2+</sup>. Compared with the Co 2p peaks of the metallic Co sample, the Co–Ni alloy sample is shifted prominently to higher binding energy (Fig. 5c). Conversely, the Ni 2p peaks are shifted slightly to lower binding energy (Fig. 5d). The XPS results show that there are strong electron interactions between the Co and Ni atoms in the Co–Ni alloy, leading to a transfer of electrons from Co to Ni, thus reducing the electron density around Co. The lower electron density of Co means more empty d orbitals, which is thought to favor the adsorption of hydrogen and thus improve the electrocatalytic performance for the HER.<sup>44,45</sup> In addition, the negative shift in the Ni XPS spectra indicates that the electron density could be increased, which will improve the ability for electron-donation and may be conducive to the HER. The above analysis shows that the Co–Ni alloy can display a more favorable electronic structure for the HER compared to metallic Co or Ni. It should be noted that the weight ratio of Co to Ni calculated from the XPS measurement is 61 : 39 (Co : Ni), which is similar to the result from EDS.

Fig. 6 presents the surface morphology of metallic Co, metallic Ni and these Co–Ni coatings with various Co contents. The plating solution composition is exhibited in Table 2. As shown in Fig. 6a, metallic Co displays a relatively dense structure with spherical “nodules”, and these spherical nodules can align compactly to form many wirelike crystal bundles distributed throughout these coatings, and there are also visible cracks on the coating surface. Fig. 6b shows the surface of the metallic Ni coating covered with a rice-like crystal structure. In addition, the Co–Ni alloy coatings prepared by electrodeposition still exhibit a spherical “nodule” structure that is similar to metallic Co, with a significant reduction in particle size, which can be attributed to the Ni atoms in the Co crystal lattices to form a solid solution during

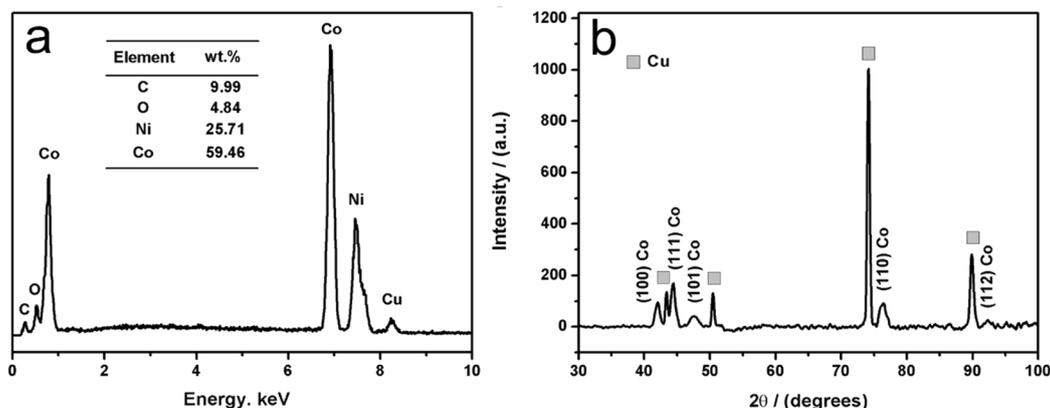


Fig. 4 EDS analysis (a) and XRD pattern (b) of Co–Ni alloy coating obtained at 30 mA cm<sup>-2</sup> for 10 min from an EG system containing 0.4 M CoCl<sub>2</sub> and 0.2 M NiCl<sub>2</sub> at 323 K.



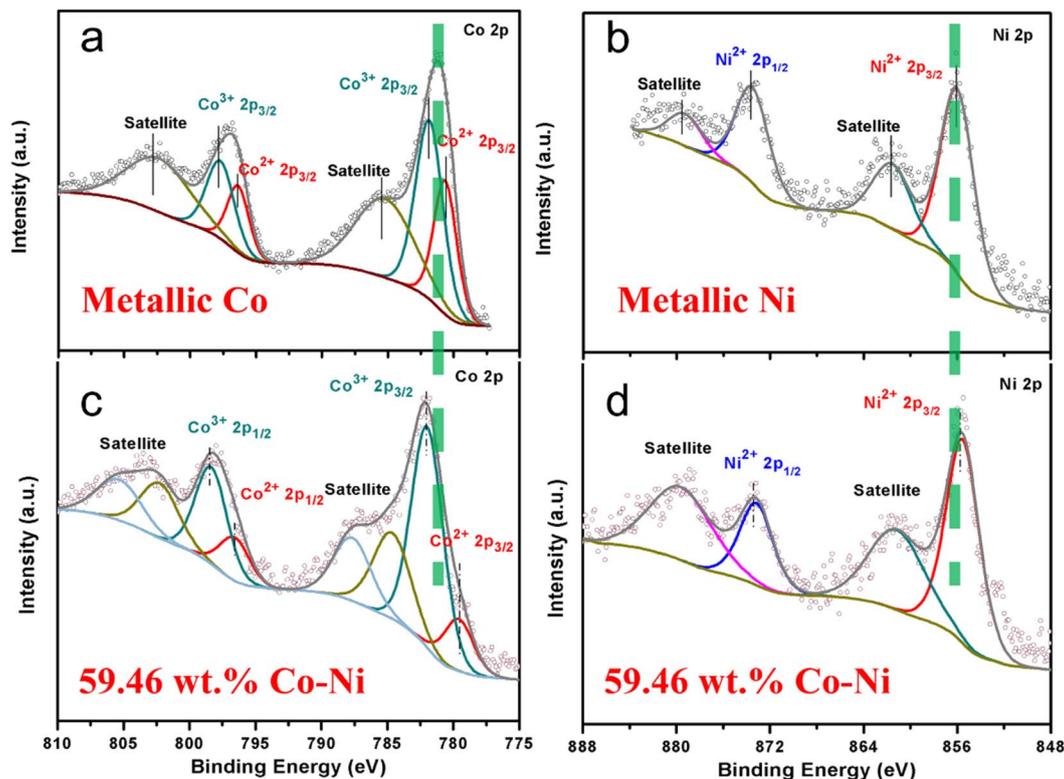


Fig. 5 Co 2p (a, c) and Ni 2p (b, d) XPS spectra of metallic Co (a), metallic Ni (b) and Co–Ni alloy (c, d).

the electrodeposition process. Compared with the metallic Co coating, the cracks on the surface of Co–Ni alloy coatings are significantly reduced, which means that the addition of Ni atoms can reduce the internal stress of the coating. As shown in Fig. 6c–g, the size of the spherical “nodules” for the prepared Co–Ni coatings can be clearly affected by the Co content. When the Co content in the Co–Ni coatings is relatively low, the average size of these spherical “nodules” (crystal particles) is larger (Fig. 6c and d). Conversely, when the Co content in the Co–Ni coatings is relatively high, the average size of the crystal particles is smaller (Fig. 6e–g). This can be attributed to the  $\text{Co}^{2+}$  species in the EG system being able to inhibit the reduction of  $\text{Ni}^{2+}$ , and the inhibition effect can be improved with an increase in  $\text{Co}^{2+}$  species concentration. Normally, the inhibition effect can improve cathodic polarization and then decrease the crystal particles. Thus, the result is also accordance with the CV measurements. It should be noted that the Co–Ni alloy containing 59.46 wt% Co (Fig. 6e) should present a larger ECSA than the other Co–Ni alloys, which is mainly attributed to the fact that more spherical crystals displaying optimal particles size grow on its surface and the arrangement among the spherical crystals will be tighter, which means that a larger surface area can be presented on a limited projection plane, thus allowing for a larger ECSA in the HER process. The conjecture shown by the SEM images was also confirmed in the EIS measurement (Fig. 9). Fig. 6h presents the EDS elemental mapping of Co and Ni for Co–Ni alloy coating with 59.46 wt% Co. It is clear that a Co–Ni

alloy coating exhibits a homogeneous distribution of all elements in the coating, which indicates the formation of a solid solution structure.

### 3.4. Electrocatalytic properties of Co–Ni coatings for HER

In order to obtain valuable information about the electrocatalytic performance of the electrodeposited metallic Co, metallic Ni and Co–Ni alloy coatings for the HER, steady-state polarization curves were recorded using the LSV method in 1 M KOH solution and are shown in Fig. 7.

As shown in Fig. 7, it is found that all these Co–Ni alloy coatings obtained from the EG system exhibit superior HER electrocatalytic properties compared to metallic Co ( $\eta_{10} = 237$ ) or Ni ( $\eta_{10} = 258$ ). Moreover, the overpotential value for catalytic current density reaching  $10 \text{ mA cm}^{-2}$  ( $\eta_{10}$ ) decreases with an increase in Co content from 22.61 to 59.46 wt% in these coatings, while its value increases remarkably when the Co content is over 59.46 wt%. The change tendency is in line with reported Co–Ni alloy coating electrocatalysts for the HER.<sup>20</sup> Normally, the excellent HER electrocatalytic activity can be attributed to the significant synergism in the electrocatalysis because metals of the left half of the transition series with empty or less filled d-orbitals (such as Co, Ni or Mo), are alloyed with metals of the right half of the transition series with internally paired d-orbitals (such as Co or Ni) that are not available for bonding in the pure metal and that can proceed with definite charge transfer.<sup>46</sup> Importantly, for alkaline  $\text{H}_2$  evolution, Co atoms in



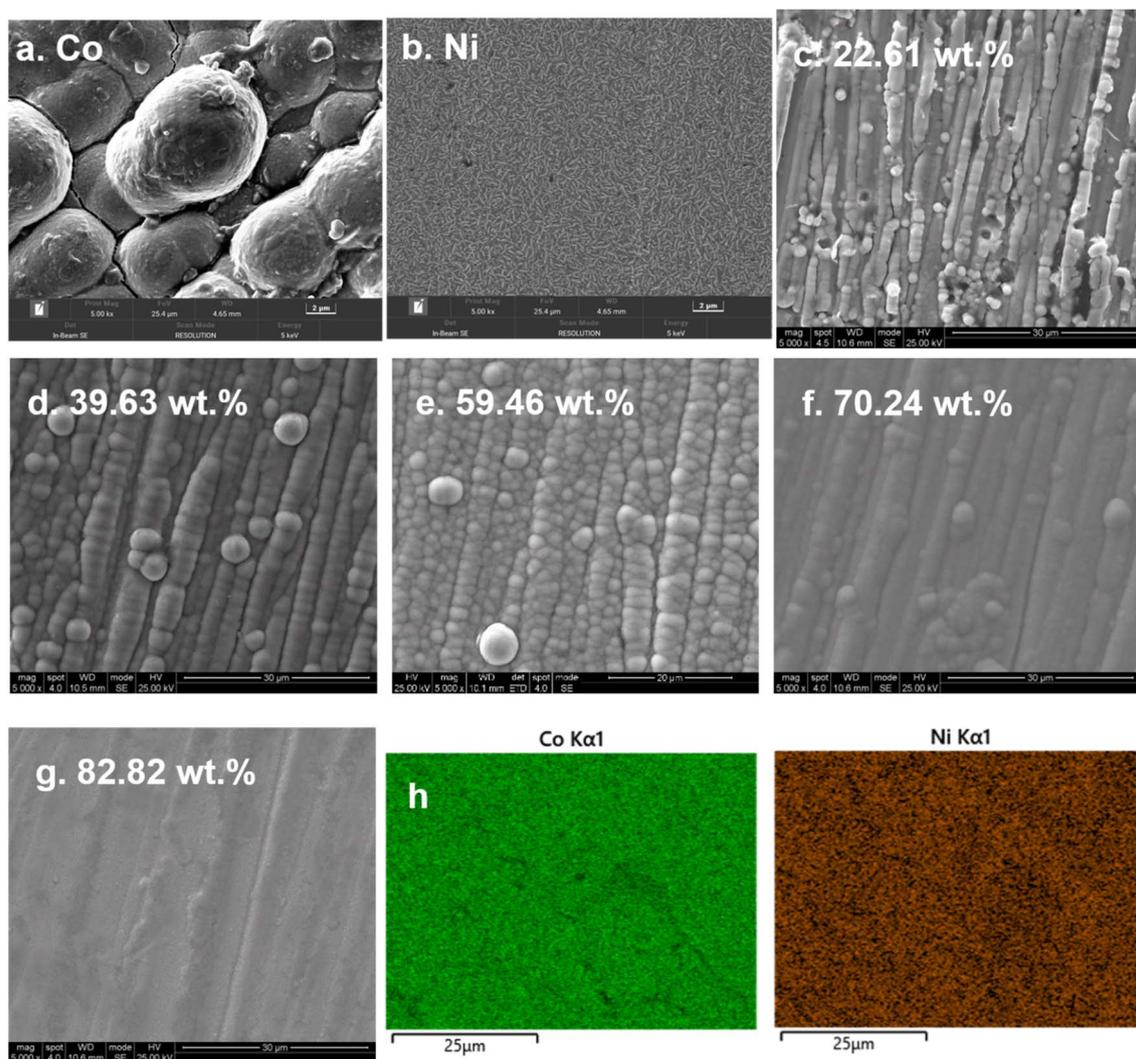


Fig. 6 SEM micrographs of metallic Co (a) and Ni (b); and Co–Ni alloy coatings with various Co contents, 22.61 wt% (c), 39.63 wt% (d), 59.46 wt% (e), 70.24 wt% (f), 82.82 wt% (g) and elemental mapping of Co–Ni alloy with 59.46 wt% Co (h).

the electrodeposited Co–Ni coatings can act as reaction sites employed for the O–H bond cleavage of H<sub>2</sub>O, while these sites for Ni atoms in the Co–Ni coatings can act as H<sub>2</sub>-evolving centers. Thus, the significant HER electrocatalytic activity can

be attributed to the cooperative action of the Co and Ni dual atom sites. In addition, the bonding energy between a Co–Ni alloy coating with 59.46 wt% Co and hydrogen can achieve a relative balance between the rates of adsorption and desorption reactions. Consequently, a Co–Ni alloy coating with 59.46 wt% Co exhibits a relatively high electrocatalytic property. Moreover, the value of the overpotential (133 mV) for the Co–Ni alloy coating obtained from the EG system is smaller than that of other mainly fabricated nanostructured Co–Ni alloys<sup>11,20,47</sup> and partial Co–Ni alloy composite coatings<sup>48</sup> (Table 1). Meanwhile, in order to obtain valuable information about their HER kinetics, their Tafel curves were extracted from the steady-state polarization curves<sup>49–52</sup> (Fig. 7) and are shown in Fig. 8.

In addition, the exchange current densities ( $j_0$ ) corresponding to these Tafel plots were also calculated using  $j_0 = 10^{(-a/b)}$ ,<sup>53–55</sup> and are exhibited in Table 3.

As shown in Table 3, it is found that all these Co–Ni alloy coatings exhibit a lower Tafel slope and a greater exchange

Table 2 Composition of the bath to obtain metallic Co, metallic Ni and various Co–Ni alloy coatings

Bath composition (mol L <sup>-1</sup> )		Element content of the prepared coatings (wt%)			
CoCl <sub>2</sub>	NiCl <sub>2</sub>	Co	Ni	C	O
0.4	—	90.72	—	5.54	3.74
—	0.2	—	91.43	5.32	3.25
0.10	0.2	22.61	66.22	7.96	3.21
0.25	0.2	39.63	46.83	8.91	4.63
0.40	0.2	59.46	25.71	9.99	4.84
0.55	0.2	70.24	15.73	9.02	5.01
0.70	0.2	80.82	6.49	8.32	4.37



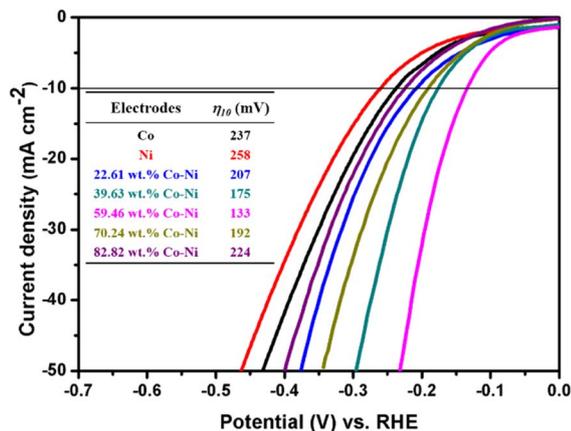


Fig. 7 The steady-state polarization curves of metallic Co, metallic Ni and Co–Ni alloy coatings with various Co contents prepared from the EG system in 1 M KOH solution at 298 K.

current density than metallic Co or metallic Ni coatings, meaning that the Co–Ni alloy coatings can present more beneficial catalytic kinetics for the HER. In addition, all the Tafel slopes of Co–Ni alloy coating catalysts are in the range of 129.7 to 248.9 mV dec<sup>-1</sup>, implying that the HER is controlled by a Volmer adsorption process.<sup>11,56–63</sup> The Tafel slope for the Co–Ni alloy with 59.46 wt% Co is also lower than those of other Co–

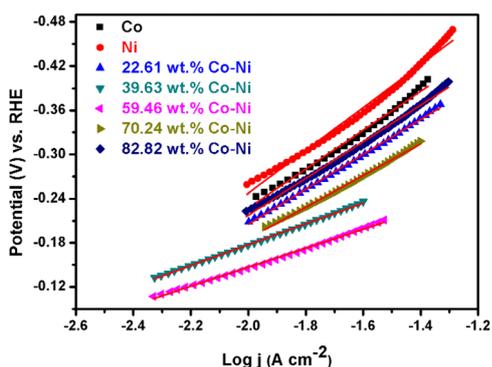


Fig. 8 Tafel plots of metallic Co, metallic Ni and Co–Ni alloy coatings with various Co contents prepared from the EG system in 1 M KOH solution at 298 K.

Table 3 Kinetic parameters for the prepared metallic Co and Ni and Co–Ni alloy coatings with various Co contents obtained by fitting the Tafel plots in Fig. 8

Electrode	$a$ (V)	$b$ (mV dec <sup>-1</sup> )	$j_0$ (mA cm <sup>-2</sup> )
Co	0.7762	254.3	0.88
Ni	0.8399	261.1	0.61
22.61 wt% Co–Ni	0.7015	237.8	1.12
39.63 wt% Co–Ni	0.4331	142.7	0.92
59.46 wt% Co–Ni	0.3768	129.7	1.24
70.24 wt% Co–Ni	0.6356	214.7	1.09
82.82 wt% Co–Ni	0.7566	248.9	0.91

Ni alloys with different Co contents, implying that the Co–Ni alloy with 59.46 wt% Co is more favorable for HER catalytic kinetics. Additionally, the exchange current density ( $j_0$ ) of the HER on the Co–Ni alloy coating with 59.46 wt% Co is the highest (Table 3), indicating that it can display outstanding catalytic activity. This result may be attributed to the fact that Co–Ni alloys with 59.46 wt% Co present an electronic structure that is more favorable to the adsorption of hydrogen atoms in the HER process.

Normally, the interface properties and kinetics of the HER on an electrocatalyst surface can be easily analyzed by the EIS technique; thus, the EIS measurements for metallic Co, metallic Ni and Co–Ni alloy coatings with various Co contents employed as catalysts for HER were carried out in 1 M KOH solution and are shown in Fig. 9.

In addition, the EIS data was fitted by Zview software based on the electrical equivalent circuit (EEC) (inset in Fig. 9) and the parameters are listed in Table 4, where  $R_s$  is solution resistance; CPE (constant phase element) is related to the double-layer capacity of the electrodes; and  $R_{ct}$  is the electrochemical charge transfer resistance. As shown in Table 4, these Co–Ni alloy coatings exhibit better conductivity (lower charge transfer resistance) than metallic Co or Ni, which also means that Co–Ni alloy coatings present an electronic structure that is more

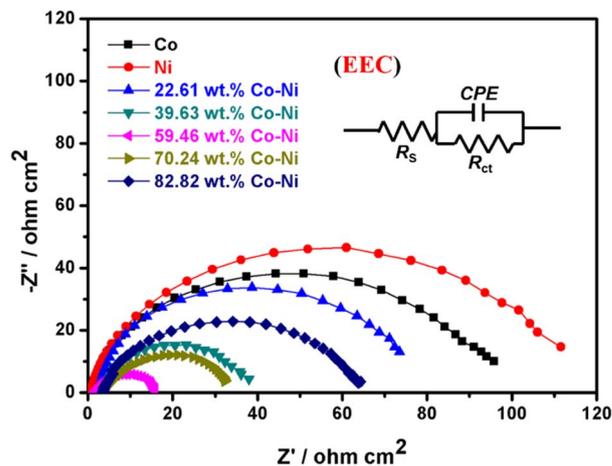


Fig. 9 EIS curves and electrical equivalent circuit (EEC) of metallic Co, metallic Ni and Co–Ni alloy coatings with various Co contents prepared from the EG system in 1 M KOH solution at 298 K.

Table 4 Parameters for the prepared metallic Co and Ni and Co–Ni alloy coatings with various Co contents obtained by fitting EIS data using the EEC models presented in Fig. 9

Electrode	$R_s$ ( $\Omega$ cm <sup>2</sup> )	$R_{ct}$ ( $\Omega$ cm <sup>2</sup> )	$C_{dl}$ (mF cm <sup>-2</sup> )	$A_{ECSA}$ (cm <sup>2</sup> )
Co	2.65	93.47	6.6	165
Ni	2.41	110.61	4.8	120
22.61 wt% Co–Ni	2.54	75.74	5.2	130.0
39.63 wt% Co–Ni	3.31	36.04	28.1	702.5
59.46 wt% Co–Ni	2.02	15.22	38.2	955.0
70.24 wt% Co–Ni	3.33	32.54	3.7	92.5
82.82 wt% Co–Ni	3.32	61.35	0.6	15.0



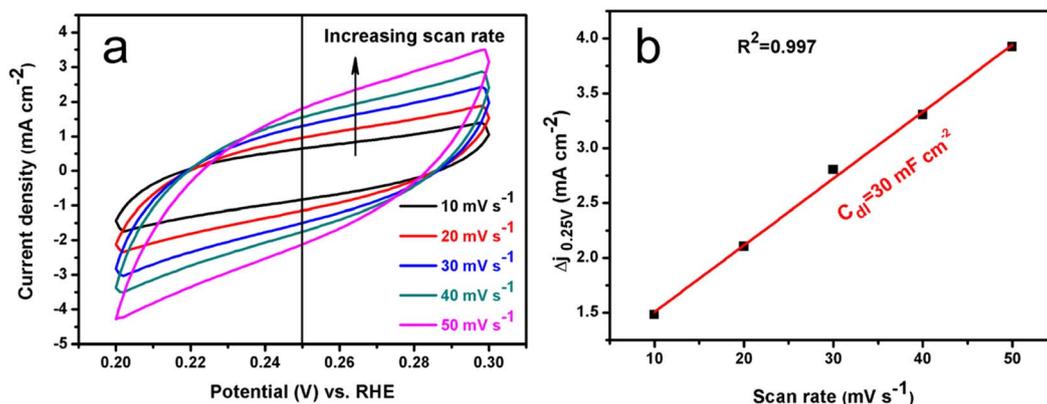


Fig. 10 CV curves of Co–Ni alloy coating with 59.46 wt% Co measured in a non-faradaic region of the voltammogram at different scan rates from 10 to 50 mV s<sup>-1</sup> in 1 M KOH (a), and the corresponding capacitive current density at 0.25 V vs. RHE as a function of scan rate for the Co–Ni alloy coating with 59.46 wt% Co (b).

conductive to the HER. In addition, the conductivity and HER catalytic activity for these Co–Ni alloy coatings are also remarkably related to Co content. The semicircle diameter decreases as Co content changes from 22.61 to 59.46 wt%, implying that both the conductivity and the HER catalytic activity are increased. In contrast, the semicircle diameter can

increase when the Co content is over 59.46 wt%, implying that their conductivity and HER catalytic activity are decreased. Therefore, the Co–Ni alloy catalyst with 59.46 wt% Co exhibits the smallest charge transfer resistance during the hydrogen evolution process, which means that the electron transfer speed is faster on the surface of the Co–Ni alloy catalyst, thereby

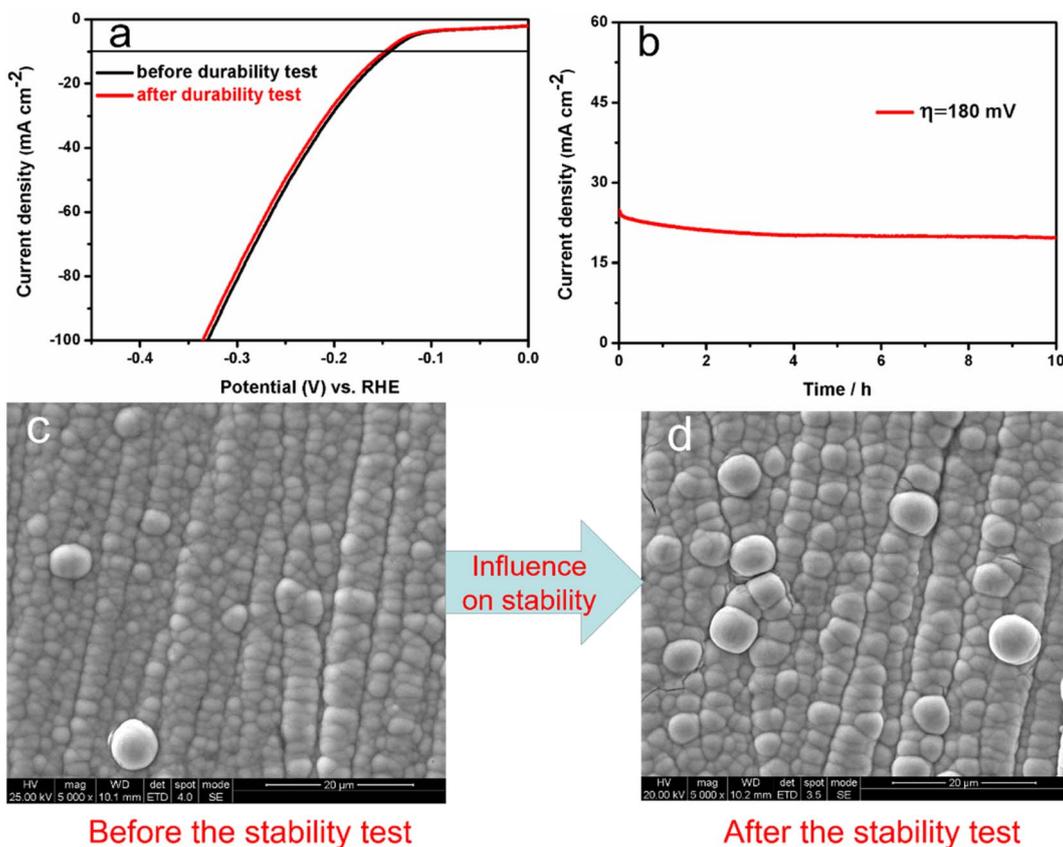


Fig. 11 Polarization curves for the Co–Ni alloy coating with 59.46 wt% Co, recorded initially and after 1000 cycles (a); chronoamperometry curve for Co–Ni alloy coating with 59.46 wt% Co during electrolysis of about 10 h at overpotential 180 mV (b). SEM image before (c) and after (d) the stability test.



exhibiting better catalytic activity for the HER. Generally, ECSA is an important factor associated with the electrocatalytic performance for the HER, and the specific capacitance ( $C_{dl}$ ) can be employed to calculate the ECSA value using the  $C_{dl}$  value for a flat standard with  $1 \text{ cm}^2$  of real surface area.<sup>64</sup> In addition, the  $C_{dl}$  value for a flat surface is normally deemed to be in the range of  $20\text{--}60 \mu\text{F cm}^{-2}$ , and it is always assumed to be  $40 (\mu\text{F cm}^{-2})$ .<sup>65,66</sup> Therefore, in this work, the ECSA values of these Co–Ni coatings were obtained using  $40 \mu\text{F cm}^{-2}$  based on the method described in the literature,<sup>65</sup> and are shown in Table 4. It is found that the Co–Ni alloy with 59.46 wt% Co content expectedly exhibits the largest ECSA value ( $955.0 \text{ cm}^2$ ), also implying better catalytic performance for the HER.

Normally, the electrochemical capacitance ( $C_{dl}$ ) could also be obtained using the CV method in a potential range where there are no faradaic processes with different scan rates.<sup>66</sup> Thus, the potential was recorded between 0.20 and 0.30 V vs. RHE at different rates from 10 to  $50 \text{ mV s}^{-1}$  in 1 M KOH. The typical CV curves for the Co–Ni alloy with 59.46 wt% Co that exhibited the best HER catalytic property can be seen in Fig. 10a.

The measured capacitive current density is plotted as a function of scan rate and is shown in Fig. 10b. The calculated  $C_{dl}$  for the Co–Ni alloy with 59.46 wt% Co is about  $30.0 \text{ mF cm}^{-2}$ . The value is of a similar magnitude to the above EIS measurements ( $38.2 \text{ mF cm}^{-2}$ ). Catalytic stability is another primary property of an electrocatalysts for the HER; thus, it was measured using CV and chronoamperometry techniques. Fig. 11a shows these typical polarization plots of Co–Ni alloy with 59.46 wt% Co before and after performing 1000 CV scans.

It is clear that the two curves exhibit only a slight change in HER overpotential after 1000 cycles, which can be attributed to the high electrocatalytic stability of the Co–Ni alloy coated electrode. To confirm the electrocatalytic stability, the chronoamperometry curve of the Co–Ni alloy coating electrode with 59.46 wt% Co was recorded in 1 M KOH solution by applying an overpotential  $\eta = 180 \text{ mV}$ , and is shown in Fig. 11b. It can be seen from Fig. 11b that during 10 h of testing, the current density initially decreased and was then maintained at about  $20 \text{ mA cm}^{-2}$  after the fourth hour. Fig. 11c and d, respectively, show SEM images taken before and after the stability test. It is evident that the surface morphology has not changed during the stability test due to the electrolysis of water, indicating that the alloy has outstanding hydrogen precipitation stability capabilities.

## 4. Conclusions

(1) The nucleation overpotential for  $\text{Ni}^{2+}$  reduction to Ni is more negative than that of  $\text{Co}^{2+}$  reduction to Co, and the Co–Ni alloy co-deposition process is easier than that of metal Ni or Co, implying that the co-deposition process of Co–Ni alloy in the EG system is typical non-abnormal co-deposition.

(2)  $\text{Ni}^{2+}$  species in the EG system can accelerate the Co–Ni co-deposition process, and  $\text{Co}^{2+}$  species in the system can inhibit the reduction of  $\text{Ni}^{2+}$  at a relatively high overpotential, and then their effect can be improved with an increase in  $\text{Ni}^{2+}$  or  $\text{Co}^{2+}$  species concentration.

(3) The Co–Ni electro-crystallization mechanism in the EG system is a 3D instantaneous nucleation and growth of a new phase under diffusion control.

(4) Co–Ni alloy coatings with various Co contents can be obtained from the EG system containing various  $\text{Co}^{2+}$  concentrations and the surface morphology for the prepared Co–Ni alloy coatings can be affected by the Co content. Thus, the EG system is a promising candidate for commercial application in Co–Ni alloy plating because it can balance the disadvantages of low deposition efficiency in aqueous systems due to the HER during the deposition process and the high cost of ionic liquids, compared to conventional aqueous solution and ionic liquid systems.

(5) The electrocatalytic activity of the obtained Co–Ni alloy coatings can be improved with an increase in Co content from 22.61 to 59.46 wt%, and the prepared Co–Ni coating with 59.46 wt% Co exhibits a high electrocatalytic activity for the HER with an overpotential of 133 mV at  $10 \text{ mA cm}^{-2}$  in 1 M KOH solution due to a high ECSA value ( $955.0 \text{ cm}^2$ ).

## Author contributions

Xinkuai He: conceptualization, methodology, writing – original draft, review & editing. Zhouxi Hu: investigation, data curation, writing – original draft. Qingtian Zou: investigation, data curation, writing – original draft. Jingjing Yang: investigation, data curation, writing – original draft. Ruqing Guo: data curation, visualization. Luye Wu: writing – original draft, funding acquisition, validation.

## Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Acknowledgements

The authors acknowledge the financial supports of the National Natural Science Foundation of China (No. 21476067) and the Project Sponsored by the Scientific Research Foundation for the Returned Overseas Chinese Scholars, State Education Ministry.

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