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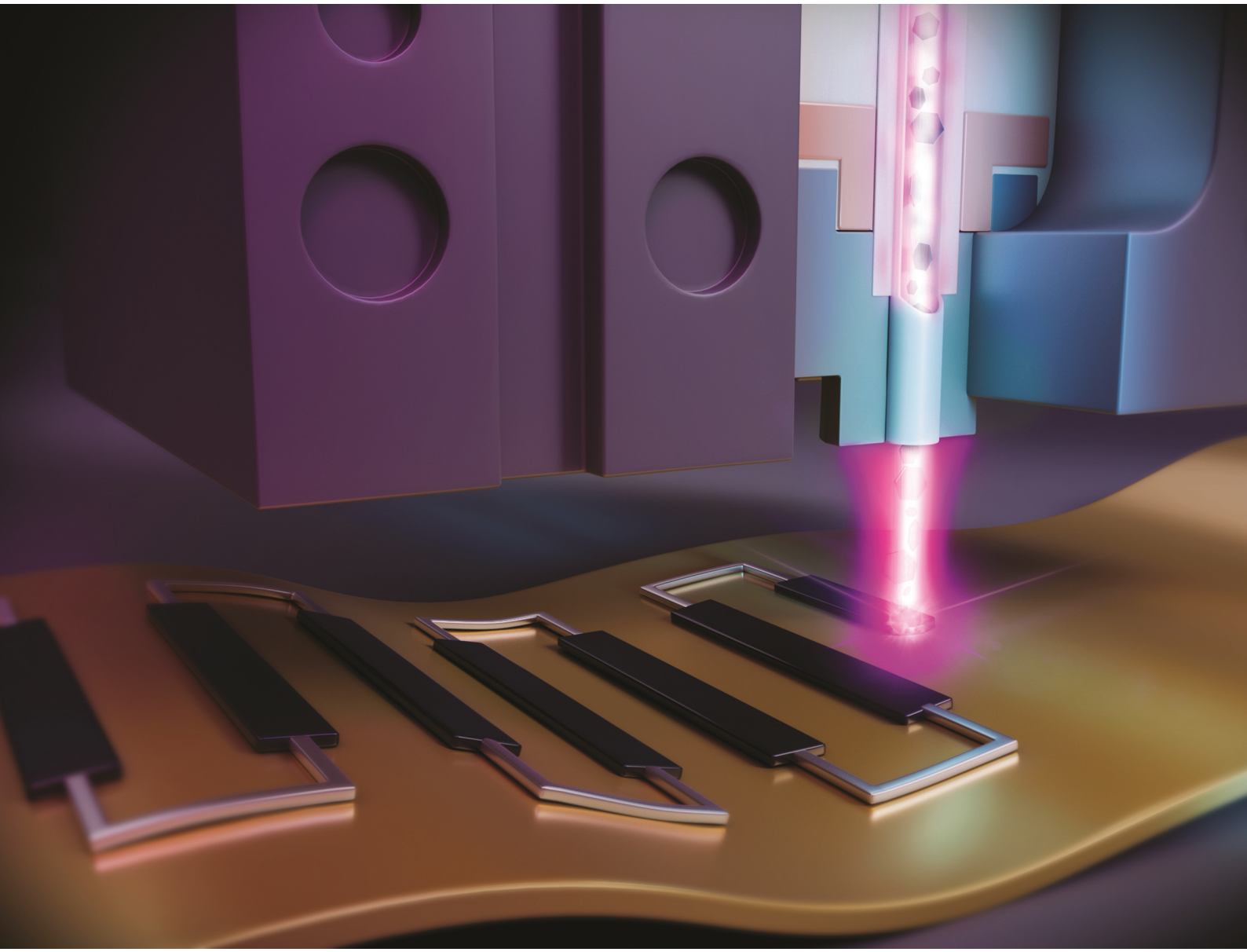

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Plasma-jet printing of colloidal thermoelectric Bi_2Te_3 nanoflakes for flexible energy harvesting†

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Thermoelectric generators (TEGs) convert temperature differences into electrical power and are attractive among energy harvesting devices due to their autonomous and silent operation. While thermoelectric materials have undergone substantial improvements in material properties, a reliable and cost-effective fabrication method suitable for microgravity and space applications remains a challenge, particularly as commercial space flight and extended crewed space missions increase in frequency. This paper demonstrates the use of plasma-jet printing (PJP), a gravity-independent, electromagnetic field-assisted printing technology, to deposit colloidal thermoelectric nanoflakes with engineered nanopores onto flexible substrates at room temperature. We observe substantial improvements in material adhesion and flexibility with less than 2% and 11% variation in performance after 10 000 bending cycles over 25 mm and 8 mm radii of curvature, respectively, as compared to previously reported TE films. Our printed films demonstrate electrical conductivity of 2.5×10^3 S m^{-1} and a power factor of 70 μW m^{-1} K^{-2} at room temperature. To our knowledge, these are the first reported values of plasma-jet printed thermoelectric nanomaterial films. This advancement in plasma jet printing significantly promotes the development of nanoengineered 2D and layered materials not only for energy harvesting but also for the development of large-scale flexible electronics and sensors for both space and commercial applications.

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Introduction

Integrated energy harvesters for flexible hybrid electronics are in high demand following advancements in lower power consumption electronic devices for Internet of Things (IoT) and wearable electronics.[1–3] Flexible thermoelectric generators (TEGs) integrated into heat sources such as radioisotope thermoelectric generators (RTG) are ideal candidates as energy sources in space industries and microgravity environments. Flexible TEGs offer many advantages over various energy harvesting methods, including long-term reliability, lightweight and not requiring sunlight to operate, offering a longer mission lifetime. They are insensitive to the extreme cold and high radiation fields in space and have no moving parts involved in producing uninterrupted power using available temperature differences.[4,5] The ability of thermoelectric materials to convert heat energy into electrical energy can be described by a dimensionless figure of merit,

$$ZT = S^2\sigma T/\kappa \quad (1)$$

where S, σ, T, and κ represent Seebeck coefficient, electrical conductivity, temperature, and thermal conductivity, respectively.[4,5]

Metal chalcogenides, such as bismuth telluride (Bi_2Te_3), are commonly used materials for low-temperature TEGs due to their superior ZT at room temperature.[6,7] There have been many attempts to develop Bi_2Te_3 nanoparticle-based flexible TEGs using nanostructuring to improve the Seebeck coefficient and reduce thermal conductivity.[8–10] The topological behavior of these materials offers high surface mobility of charge carriers in the nanocrystal due to the non-parabolic band structure, demanding precise control of nanomaterial morphology and thickness to improve thermoelectric performance.[11] Phonons typically have a longer mean free path compared to electrons, allowing particle and grain size engineering to be used as a mechanism for enhancing ZT by optimizing the σ/κ ratio.[12,13] It has been shown that solvothermal synthesis temp-

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erature can be used to introduce a single nanopore in the center of Bi_2Te_3 nanoflakes.[14,15] It is possible that these nanopores will improve thermoelectric properties by acting as an additional scattering site for phonons.

While precise control of nanostructure and morphology of metal chalcogenide materials has been studied extensively to improve ZT values, a scalable and reliable manufacturing method for flexible TEGs with good mechanical and thermoelectric properties remains a challenge. Namely, improved adhesion between the thermoelectric material and substrate is required to improve device performance. A common approach is to apply chemical or plasma treatment to the substrate surface, however, this introduces limitations when integrating the substrate with flexible hybrid electronic (FHE) devices. Additionally, it adds an undesirable step in the fabrication process of flexible TEGs.

Additive manufacturing (AM) offers many advantages for the fabrication of TEG and FHE devices, including rapid processing speeds, design flexibility, and the ability to convert colloidal suspensions into functional devices.[16,17] Recently, many AM modalities have been developed for the fabrication of thermoelectric films by direct deposition of colloidal inks. Direct writing[18,19] screen printing[6,20] inkjet printing[21] and aerosol jet printing[22,23] have shown promise as scalable and cost-effective methods for fabricating flexible TEGs compared to other processes, such as thermal evaporation, vacuum filtration, and spray coating. Despite these advances, current AM methods are inadequate for meeting the needs of device manufacturing in microgravity environments and/or *in situ* plasma-assisted chemical modification of surfaces or inks.

Here we report the use of a novel plasma-assisted and gravity-independent printing technique for developing TEGs with direct conversion of nanomaterials into flexible devices with improved adhesion and high resolution. Plasma-jet printing is a new AM technology that has been shown to sinter metal nanoparticles *in situ*, reduce material oxidation states, promote substrate adhesion, and increase packing density.[24–26] The use of a dielectric barrier discharge (DBD) plasma in the plasma-jet printer enables atmospheric printing of nanomaterial films without the need for expensive vacuum equipment. DBD plasmas have been shown to assist in etching and deposition of materials, modification of surface energy, and oxidizing, reducing, and removing organic films.[27,28] Atmospheric plasma jets have been shown to operate both by electrical phenomenon and plasma flow, enabling high flow directionality independent of gravity.[28,29]

Recently, plasma-jet printing of nanomaterial inks onto flexible substrates has been demonstrated with carbon nanotubes,[25] silver nanowires,[26] metal oxide nanoparticles,[24,30] and graphene oxide.[31,32] In this work, we present the first reporting to our knowledge of plasma-jet printed thermoelectric nanoparticles. The development of this new printing technology opens up novel opportunities for integrating flexible energy harvesters in self-powered electronic devices and marks significant progress in developing AM technologies for microgravity and space environments.

Thermoelectric ink synthesis

Material synthesis. A solvothermal synthesis setup was used to synthesize Bi_2Te_3 nanoflakes (Fig. 1a), following work performed by Hollar *et al.*[22] After washing, the nanoflakes were dispersed in a cosolvent solution consisting of ethylene glycol, nanopure water and ethanol (Fig. 1b) for printing or spin coating onto various substrates, such as SiO_2 or polyimide. Nanoflakes were synthesized at 190 °C to form a single nanopore in the center of the nanoflake following work by Hosokowa *et al.*[15] Nanoflake morphology includes crystalline nanoflakes, nanoflakes with single nanopores, and dislocations (Fig. 1f and Fig. S1a–c†). From the atomic force microscopy (AFM) images, the nanoflakes' average thickness and width are observed to be ~59 nm and ~598 nm, respectively (Fig. 1d and e). The yield of nanoflakes with nanopores is observed to be ~13% and the average nanopore diameter is ~64 nm. A 3D rendering of a pair of nanoflakes shows a tri-

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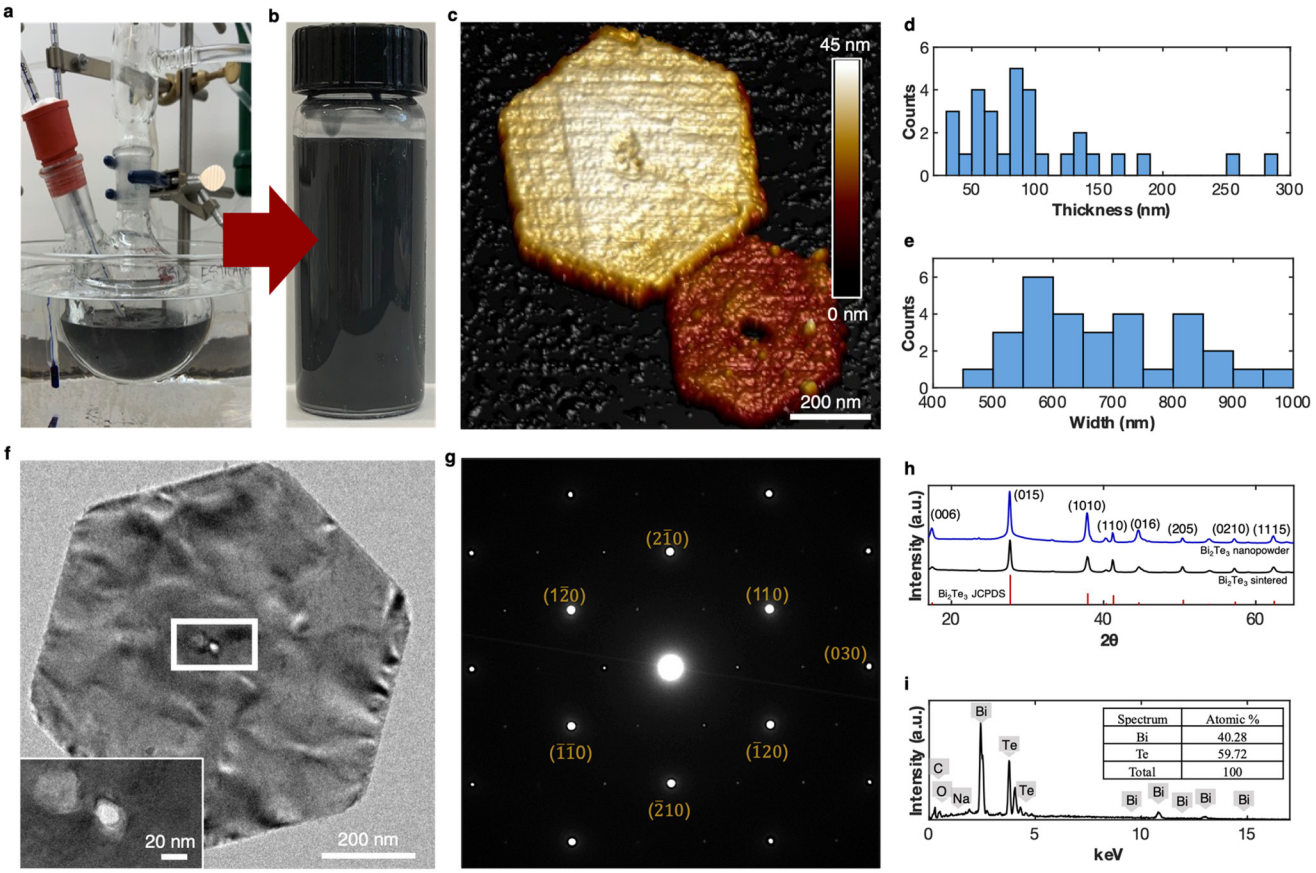

Fig. 1 Synthesis and characterization of Bi_2Te_3 nanoflakes. Optical images of (a) solvothermal synthesis process and (b) as-synthesized thermoelectric ink dispersed in a cosolvent system. (c) Atomic force microscopy rendering of representative nanoflakes. (d and e) Histograms of lateral width and thickness of flakes from AFM. (f) Transmission electron microscopy image with inset showing the nanopore in the center of the nanoflake. (g) SAED pattern of the imaged rhombohedral Bi_2Te_3 nanoflake indexed in yellow to the [00*l*] zone-axis. (h) X-ray diffraction of Bi_2Te_3 powder and sintered film. (i) Energy dispersive spectroscopy scan of as-printed Bi_2Te_3 films.

angular growth region in the center (Fig. 1c), the presence of which can be explained by a growth mechanism proposed by Subrati *et al.* in which nanoflakes form out of a Bi-rich triangular nuclei centered on a Te nanorod.[33] Further, the height of this raised triangular region is ~3 nm, corresponding to one monolayer of Bi_2Te_3, indicating that this is the nucleation

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Nicholas McKibben

Nicholas McKibben is a 5th year Ph.D. student in materials science and engineering at Boise State University. He is a classically trained chemist who received his B.S. in Chemistry from Northwest Nazarene University and began his graduate studies in inorganic chemistry at Texas Tech University. Nick is currently working in the Advanced Nanomaterials and Manufacturing Laboratory under the tutelage of Dr David Estrada. His primary area of research is additive manufacturing, with specific interest in nanoparticle ink development and sensor fabrication.

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Table 1 Rheological properties of various inks. The volume ratio of water : ethylene glycol : alcohol is the same for each composition

	Water : ethylene glycol : ethanol	Water : ethylene glycol : isopropanol	Water : ethylene glycol : 2-butanol
Mean contact angle (°)	48.49	41.31	19.14
Mean viscosity (cP)	2.648	2.912	2.985
Surface tension (mN m^{-1})	37.05	33.52	27.18

stage for the growth of the next monolayer on the surface of the nanoflake.

Material characterization. Transmission electron microscopy (TEM) was performed to further investigate the particle morphology, crystal structure, and phase purity of the synthesized Bi_2Te_3 nanoflakes. Bi_2Te_3 has a rhombohedral crystal structure and belongs to the space group $R\bar{3}m$, no. 166. The crystal structure is comprised of five alternating layers of covalently bonded tellurium and bismuth atoms, forming a quintuple layer Te(1)–Bi–Te–Bi–Te(1). These quintuple layers stack due to weak electrostatic interactions, and a van der Waals bond forms between the Te(1)–Te(1) atoms of adjacent quintuple layers. These unique crystallographic features result in lattice parameters with a higher than usual c/a ratio. The unit cell, or one monolayer, consists of three stacked quintuple layers, with reported lattice parameters of c = 3.045 and a,b = 0.438 nm.[34] The anisotropy of the unit cell and nanometer dimensionality of the particles are largely credited for the excellent thermoelectric properties exhibited by this material.[15] TEM imaging of a well-defined hexagonal particle shows an edge length of 420 nm and a particle width of 840 nm (Fig. 1f).

A magnified image of the two nanopores intrinsic to this Bi_2Te_3 nanoflake is shown as the inset, with measured pore sizes of 20 and 35 nm. Dimensions of the nanoflakes measured by TEM were in good agreement with the statistical data acquired from AFM for particle and pore size. A selected area electron diffraction pattern was generated for the imaged hexagonal nanoflake, zone-axis [000l] (Fig. 1g). The material was phase pure and single crystalline in nature with a hexagonal symmetry pattern. Powder X-Ray diffraction was also performed to confirm bulk purity (Fig. 1h), and the d-spacing of the 110 peak was calculated to be 0.219 nm, which is confirmed by SAED and supported by existing literature.[34]

The rheological properties of Bi_2Te_3 dispersed in the cosolvent inks were extensively studied (Table 1). The alcohol component of the cosolvent system was varied to determine the optimal cosolvent composition. The alcohols are present in the exact same ratio compared to the other co-solvent chemicals. The cosolvent system containing ethanol demonstrated superior stability compared to the other ink composition, as indicated by the nanoparticles staying dispersed in solution even after one week while the other cosolvent inks had sedimented completely (Fig. S2†). The viscosity and surface tension of the various inks in Table 1 are similar and within the plasma-jet printer's allowed parameters. In comparison, the mean contact angle varies significantly with alcohol type. Due to the method of printing, the high contact angle of the ink is not a barrier; however, further tuning of the ink composition would be necessary to make the cosolvent system compatible with drop-on-demand printing modalities, such as inkjet printing offering multi-printer compatible inks.

Printer optimization and film fabrication

Plasma-jet printer optimization. A SpaceFoundry plasma-jet printer (Fig. 2a) was used to produce the reported flexible TE films. The printer operates by passing aerosolized nano-

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Mia Busuladzic-Begic is an undergraduate student at Brown University. While at Boise High School, she worked at the Advanced Nanomaterial and Manufacturing Laboratory as a research assistant in Dr David Estrada's and Dr Harish Subbaraman's research group. During her time at Boise State University, she worked in synthesizing materials and conducting experiments, gathering stability and rheology data on several co-solvent systems to improve the morphology of printed black phosphorus thin films. Additionally, she analyzed additively manufactured thermoelectric films and participated in nanomaterial synthesis and characterization.

David Estrada

Dr David Estrada is an associate professor of Materials Science and Engineering at Boise State University. He is the Associate Director for the Center of Advanced Energy Studies, Deputy Director of Academic Research at Idaho National Laboratory, and the Site Director of the NSF IUCRC Center for Atomically Thin Multifunctional Coatings. He received his M.S. in Electrical Engineering 2009 and his Ph.D. in Electrical Engineering in 2013 from the University of Illinois at Urbana-Champaign, under the direction of Professor Eric Pop. His research interests are in the areas of emergent additive manufacturing, semiconductor nanomaterials, and bionanotechnology.

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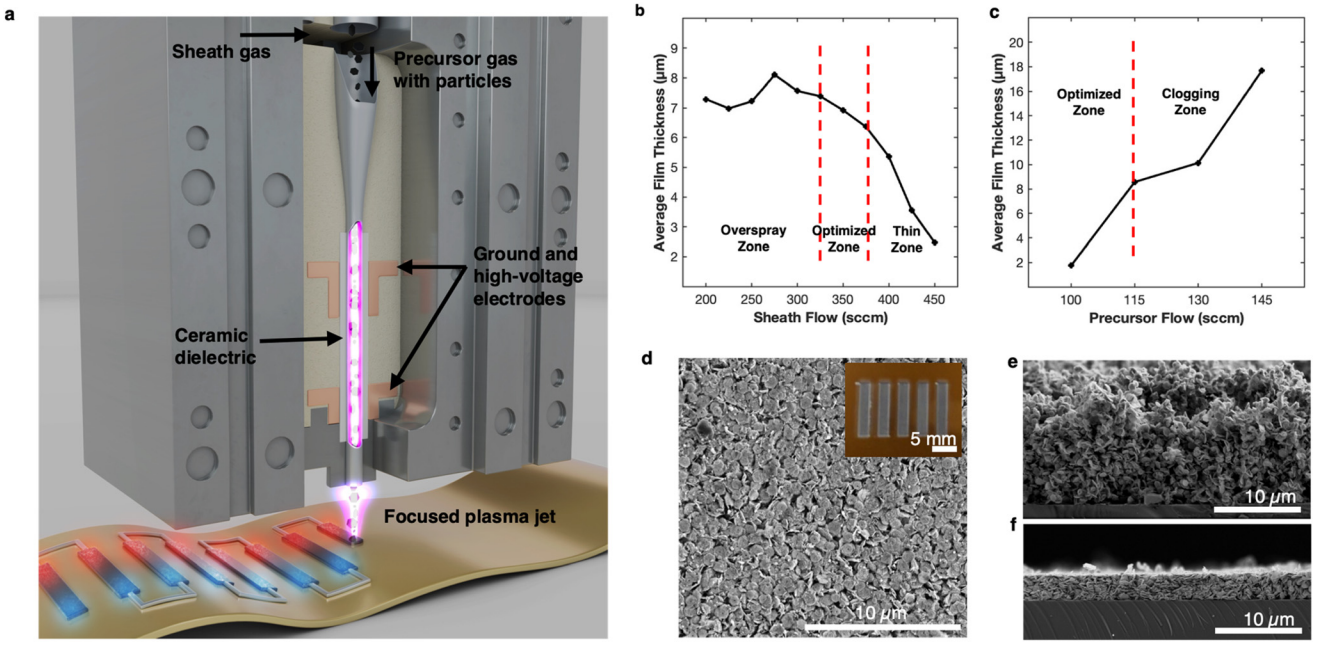

Fig. 2 Print and film optimization. (a) Schematic diagram of the PJP printhead. Average thickness by (b) sheath flow and (c) precursor flow showing optimized conditions. (d) Top-down scanning electron microscopy image of the printed film (inset) after mechanical pressing. Cross sectional SEM of the printed film (e) as printed and (f) after pressing and sintering.

materials from a colloidal ink through a cold atmospheric pressure plasma-jet and onto a target substrate. First, the ink is pumped to the atomizer and atomized into a glass chamber by an ultrasonic mesh. Positive pressure from the helium precursor gas flow pushes the atomized particles into a secondary chamber, where larger droplets collect on the bottom or sides of the chamber while smaller droplets are directed as a fine mist to the printhead. The double chamber system is advantageous for achieving a more uniform size distribution of droplets in the mist passing through the printhead. The printhead consists of two electrodes, an alternating current and a ground electrode, positioned around a ceramic tube, which acts as a dielectric barrier for the DBD plasma. This plasma is generated in the ceramic tube by a high voltage (0–30 kV) and low frequency (20–30 kHz) power supply. The resonant frequency of the plasma is determined by the manufacturer's recommendations for optimal plasma generation and is used for the duration of the print time. The plasma power supply voltage, atomizer power, line spacing, print speed, and flow rate are adjusted to tailor print quality *in situ*. Each parameter plays a part in the printed line morphology and the quality of the thin film that can be printed. The flow rates and plasma power are directly responsible for how much material is deposited onto the substrate and the quality of the line. For this work, the sheath and precursor flow rates were varied to achieve an optimal printed line with minimal overspray. Each must be tailored experimentally to produce a quality TE film.

In the plasma-jet system during operation, the atomized particles are carried by the precursor flow through the helium plasma and then through a 0.5 mm nozzle. The helium sheath gas surrounds the particles in the nozzle and is used to generate the plasma. The optimal precursor-to-sheath gas ratio is ~1 : 3.5. To optimize the printer for the thermoelectric colloidal ink for plasma jet printing, a series of 0.2 × 10 mm long lines were printed with sheath flow ranging from 200 to 450 sccm at a constant precursor gas flow of 100 sccm (Fig. 2b and c). These lines were evaluated using a Nikon optical microscope and Bruker DektakXT stylus profilometer to determine flow that optimizes

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Harish Subbaraman earned the M.S. and Ph.D. degrees in electrical engineering from The University of Texas at Austin in 2006 and 2009, respectively. Until 2016, he worked as a Senior Research Scientist at Omega Optics, Inc (Austin, TX), where he led and managed several SBIR/STTR projects in the areas of printed and flexible hybrid electronics and silicon/polymer photonics. In 2016, he joined The Department of Electrical and Computer Engineering at Boise State University (Boise, ID). At Boise State, he served as the Associate Site Director for NSF I/UCRC (ATOMIC) and the Advanced Manufacturing BSU lead for the Center for Advanced Energy Studies. He joined The School of Electrical Engineering and Computer Science at Oregon State University in Fall 2022, where he is currently an Associate Professor. He has published in over 200 refereed journals and conferences. He is a senior member of IEEE.

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the film thickness while minimizing overspray. With increasing sheath gas flow, the average thickness of the printed line decreases (Fig. 2b). When the flow is above the optimal zone, the film thickness decreases. The width of the line also decreases as more of the material does not adhere to the substrate because of the higher pressure from the increased gas flow. Below the optimal zone, the printed line becomes quite wide with overspray and has a non-ideal and non-uniform pointed cross-section. The optimal zone for the sheath flow was chosen to achieve an optimal film thickness with minimal overspray.

Additionally, the precursor gas was varied from 100 to 145 sccm, and a series of 10 mm lines were printed holding the sheath gas at 300 sccm. With increasing precursor flow, the average film thickness increases (Fig. 2c). This is expected since more atomized particles will be directed to the printhead and deposited with higher precursor flow. While printing, it was noted that after about 120 sccm, the nozzle would clog in about 20 minutes, which is not ideal for long print times or printing multiple TE legs on the same substrate. The optimal zone was chosen from 100–120 sccm precursor flow where a sufficient amount of material is deposited while mitigating the printhead clog. After printing, the films were mechanically pressed to densify the films and improve contact between nanoflakes for better electrical conductivity.[6,20] A top-down SEM image of a printed film after pressing and sintering highlights the hexagonal structures packed on the substrate (Fig. 2d). Cross-sectional SEMs of the films before (Fig. 2e) and after pressing and sintering (Fig. 2f) show the thickness is reduced from about 14 μm to 4 μm.

Fluid dynamic analysis. While fluid dynamic properties of atmospheric pressure plasma-jets[35–39] and buoyant helium jets[40,41] have been studied previously, the laminar and turbulent flow regions of the PJP have not been evaluated for determining ideal deposition parameters. It has been shown that the voltage and helium fluid velocity play a significant role in the length of the plasma plume.[35,38,42] The jet Reynold's number (Re) is defined as

$$\mathrm{Re} = v\rho D/\mu = 2.12 \times 10^{-5}\left(\frac{\rho}{\mu}\right)\left(\frac{Q_{\mathrm{sccm}}}{D_{\mathrm{mm}}}\right) \quad (2)$$

where v is the fluid velocity in m s^{-1}, ρ is the fluid density in kg m^{-3}, μ is the viscosity in Pa s, and D is the diameter of the tube in meters. The fluid velocity can be described as $v = q/A$ in terms of flow rate q and area A. Re can then be redefined for the PJP in eqn (2) where Q_{sccm} is the flow rate in cm^3 min^{-1} and D_{mm} is the diameter of the nozzle in mm. When discussing buoyant jets, it is also helpful to look at the Richardson number (Ri).[40,43] Ri compares the buoyancy of the fluid to its shear flow properties. Ri is expressed by

$$\mathrm{Ri} = \frac{gD(\rho_{\mathrm{air}} - \rho_{\mathrm{He}})}{v^2\rho_{\mathrm{He}}} \quad (3)$$

where g is the acceleration due to gravity, and ρ_{air} and ρ_{He} are the density of the air and helium, respectively. The flow is considered significantly buoyant at Ri $\gg$ 1, and the buoyancy effects on the jet can be assumed negligible at Ri < 10^{-3}.[43] The density of air and helium at 25 °C used to calculate Ri were 1.168 kg m^{-3} and 0.1601 kg m^{-3}, respectively. At printing parameters of 100 sccm and 350 sccm precursor and sheath flow, the average fluid velocity of the helium exiting the nozzle was 38.2 m s^{-1}. Ri was calculated to be 2.1×10^{-5}, so it is appropriate to assume the influence of the buoyant force is negligible compared to the flow velocity. Using a Nikon D5000 DSLR camera, optical images of the helium plasma were collected at total flow rates from 250 to 1250 sccm and power supply voltages from 7.5 to 20 kV. The plasma was photographed without the atomization of the material so that pure helium density and viscosity could be assumed at 25 °C. In the actual system, aerosolized ink could change the properties of the fluid flow, altering the Reynold's number. The images collected were threshold analysed in Gwyddion to determine the length of the plume for each parameter. Plume length (L_{plume}) *vs.* Re was observed for total flow of 250 to 1250 sccm (Fig. 3a). The trend is similar to that observed by Karakas *et al.*[42] and Xiong *et al.*[44] It was observed for the plasma-jet printer when Re is below 200, the plasma plume behaved under laminar flow characteristics, and the plume length increased with increasing flow. Between 200 and 350, the plume transitioned to the turbulent region, decreasing in length with increased flow. Above Re = 350, the plasma-jet was in the turbulent flow region. The regions and corresponding plume images (Fig. 3a) were acquired at 15 kV with a constant 100 sccm precursor flow. The thermoelectric films were printed at 100 sccm precursor flow and ~350 sccm sheath flow, which corresponds to a Re of ~156. The deposition parameters are in the laminar flow region, supporting the optimized zone observed during printed line characterization The plume length *vs.* the voltage was also studied (Fig. 3b), and it can be seen that the plume length increases with increasing voltage. While the voltage chosen for our experiments was based upon the packing density of the printed films, which will be discussed later, it is important to note that the voltage affects the plasma-jet fluid dynamics. While a constant printhead height of 2 mm was held during deposition, changing the working distance from the substrate could change the optimal voltage required to focus the ink onto the substrate. Further experimentation will be carried out to more deeply understand the plasma voltage effect on the deposition process as it is related to working distance. Initially, printing was conducted using the as-prepared ink without further processing. However, it was quickly observed that the printhead clogged after 5–10 minutes of printing and needed to be cleaned before printing could continue. Centrifugation processing of the ink was used to mitigate nozzleclogging by sedimenting out the largest nanoflakes and collecting the supernatant for printing. A centrifugation setting of 3 minutes at 4500 rpm was used to prevent nozzle cloggingwhile maintaining a high particle concentration. AFM images and nanoflake size histograms at various centrifugation settings are shown and discussed further (Fig. S3 and S4†).

Thermoelectric film analysis

Film processing and properties. Room temperature Seebeck coefficient and electrical conductivity of the films were

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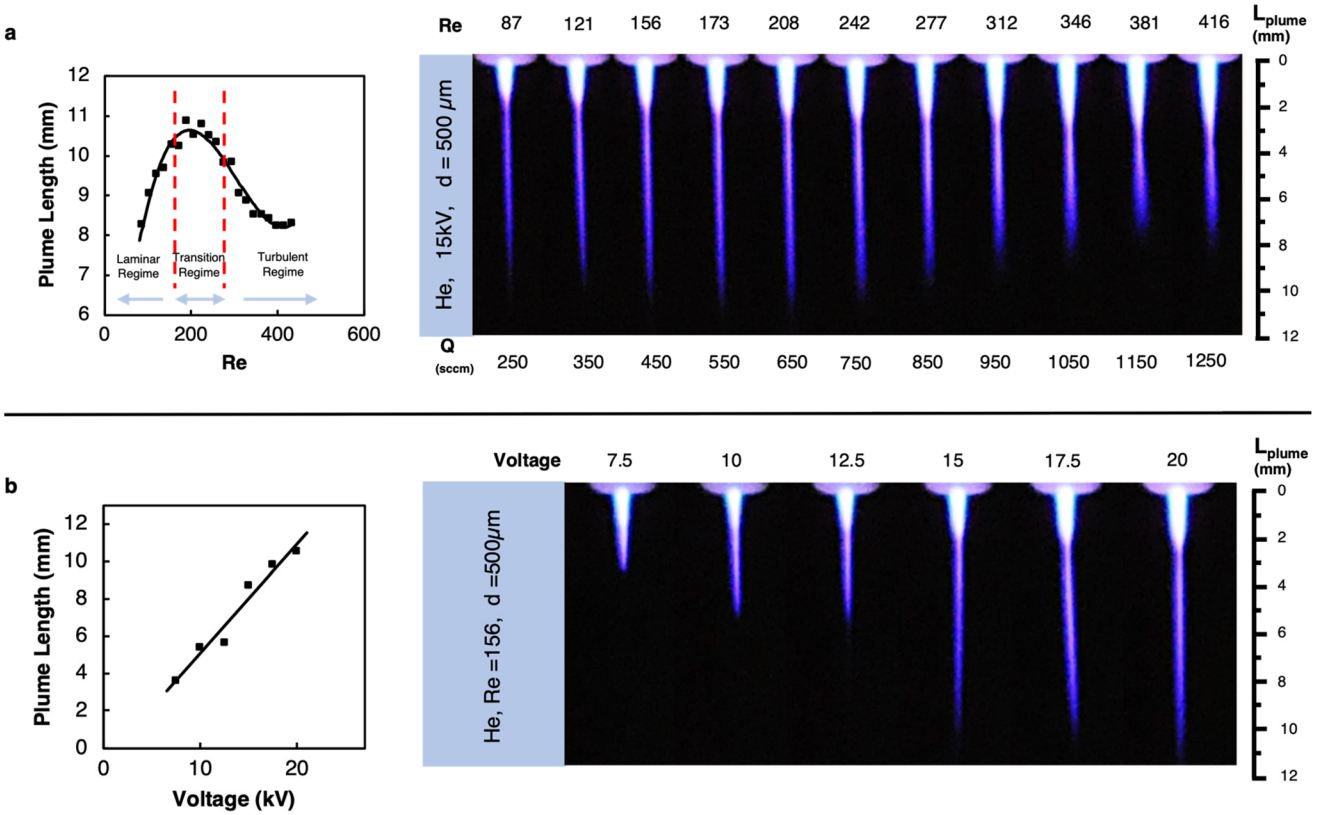

Fig. 3 Fluid dynamics of the plasma plume. (a) Plasma plume length *vs.* Reynolds number showing the laminar, transition, and turbulent regimes. Corresponding optical images of plume length with Reynold's number above and total helium flow below each plume. (b) Plasma plume length *vs.* plasma voltage. Corresponding optical images of plume length *vs.* power supply voltage for Re = 156.

measured after thermally sintered for 60 minutes at various temperatures in the presence of a forming gas (Fig. 4a). The films show a peak Seebeck coefficient of −160 μV K^{-1} at a sintering temperature of 425 °C. The films demonstrate a consistent Seebeck coefficient regardless of sintering condition with a minimal variation from −148 μV K^{-1} to −160 μV K^{-1} over a sintering temperature range of 350 °C to 425 °C. The introduction of nanopores and controlling the crystal dimensions of Bi_2Te_3 nanocrystals improved the room temperature Seebeck coefficient for the thermoelectric materials achieving a similar result comparable to doped bismuth telluride nanocrystals.[20] Further tuning of the thermoelectric properties can be achieved by optimizing the size and crystallinity of the nanopores in the crystals with a selectivity between primary charge carrier and phonon filtering. The maximum electrical conductivity for the plasma printed films was measured to be 2500 S m^{-1} at 375 °C (Fig. 4a). The power factor ($S^2\sigma$) of the PJP printed thermoelectric films were calculated, and a peak value of 70 μW m^{-1} K^2 at 375 °C was observed (Fig. 4b). These results are summarized in Table 2 and compared to other solu-

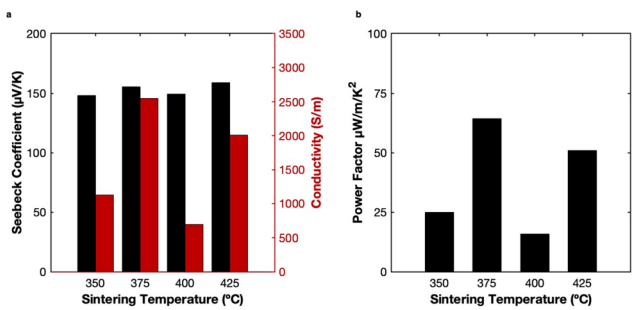

Fig. 4 Electrical and thermoelectric properties. (a) Seebeck coefficient and electrical conductivity and (b) power factor ($S^2\sigma$) after thermal sintering.

Table 2 Comparison of room temperature thermoelectric properties for solution synthesized and jet-printed Bi_2Te_3-based nanostructures

Material	Deposition method	S (μV K^{-1})	σ (S m^{-1})	PF (μW m^{-1} K^{-2})	Ref.
Bi_2Te_3	PJP	−155	2500	70	This Work
PEDOT:PSS + 50 wt% Bi_2Te_3	AJP	17	350	15	45
$Bi_2Te_{2.7}Se_{0.3}$	AJP	−78	44 500	270	46
$Bi_2Te_{2.7}Se_{0.3}$	AJP	−163	27 000	730	23
Bi_2Te_3	AJP	−64	940	3.85	22
$Bi_2Te_{1.7}Se_{0.3}$	IJP	∼−161	∼6200	∼160	47
$Bi_{0.5}Sb_{1.5}Te_3$	IJP	∼207	∼1400	∼60	47
Bi_2Te_3	IJP	∼119	∼5600	∼78	21
$Bi_{0.5}Sb_{1.5}Te_3$	IJP	∼72	∼34 000	∼154	21

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tion-synthesized Bi_2Te_3 films fabricated with jet-based deposition.

The electrical conductivity is an order of magnitude lower than the conventional bulk Bi_2Te_3 thermoelectric material at room temperature. The cross-sectional SEM images (Fig. 2e and f) show a highly porous network of nanocrystals resulting in high interface resistance, hence lower electrical conductivity. The large porosity formation in the printed films is due to random stacking of nanoplates as they adhere to the polyimide substrate[22] as well as potentially trapping the burn-off residues from the interaction of plasma with the surface capping agents on the nanocrystals. The interaction of plasma ions with the nanomaterial capping agents causes the burning of the polymer capping, resulting in a highly porous stacking of nanocrystals. Optimization of the plasma energies is also essential in improving the density and uniformity of the thin films. With no plasma on, few nanoflakes are deposited, and the glass slide is visible through the material (Fig. S5†). When the plasma is turned on and maintained at 15 kV, a thick layer of nanoflakes is deposited, and the packing density is high. Interestingly, when the plasma voltage is increased to 20 kV, the thickness increases, but the packing density decreases as many voids are formed throughout the material (Fig. S5†). Lower electrical conductivities are also due to the lower sintering conditions of the printed films, limited by the melting point of polymer substrates.

To quantify the as-printed porosity and sintering densification of the films, Gwyddion was used to threshold map the SEM images of the film cross-sections (Fig. 2e and f). The threshold mask was set to 20%, and the relative area function was used to find percentage porosity. Blue masks are displayed over the pores in the film before and after pressing and sintering (Fig. S6a and b†). Before pressing and sintering, the relative area porosity of the film was 38%, and the film was not conductive. After pressing and sintering, the porosity of the film was reduced to 7%.

Thermoelectric film testing. Changes in resistance as a function of bending radius were measured to analyze the flexibility and adhesion of the plasma-jet printed thin films. Radii of curvature (ROC) at 8, 16, and 25 mm were used over 10 000 bending cycles to understand the material property changes. The formation of cracks and delamination of the printed films can be easily detected with a rapid increase in resistance with respect to bending, and hence, electrical resistance was chosen to understand the flexibility of the printed films. As the bending radius changes, the resistance of the printed films increases (Fig. 5a), with a maximum of 11% increase in resistance after 10 000 bending for 8 mm ROC, demonstrating excellent flexibility of the films. In the case of 25 mm ROC, only a 2% change in resistance was observed after 10 000 bends, indicating the superior adhesion and flexibility of plasma-assisted printed 2D thin films on flexible substrates.

The output voltage and power of a single PJP-printed thermoelectric leg was measured (Fig. 5b–d). The output power and device voltage show promise for the development of small-scale flexible thermoelectric generators with superior

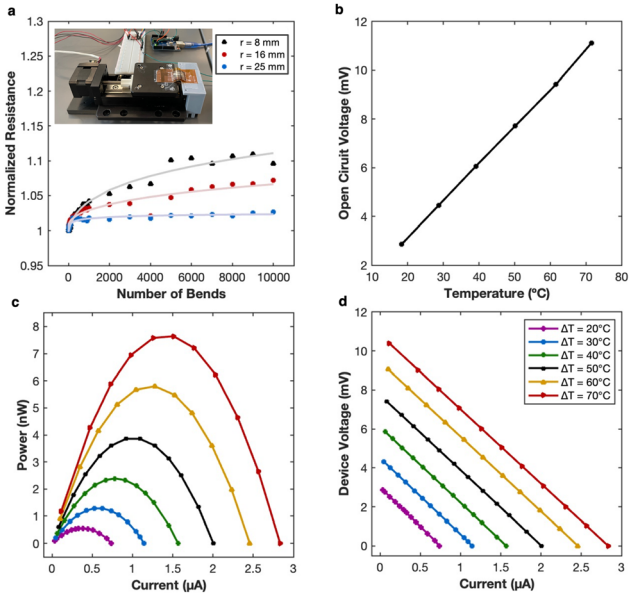

Fig. 5 Electrical characterization of single leg TE film sintered at 425 °C. (a) Resistance as a function of bending cycles for various radii of curvature. Inset shows bending test apparatus. (b) Open circuit voltage as a function of temperature difference, (c) device voltage as a function of current and (d) power curves for several temperature differentials.

flexibility for powering low-power electronic devices. When open-circuit voltage (VOC) is measured as a function of temperature difference (ΔT) (Fig. 5b), the device VOC increases linearly with ΔT by virtue of the Seebeck effect, achieving a maximum output voltage of 11 mV at a 70 °C temperature difference. This high VOC and Seebeck coefficient for a single leg is due to the defect-induced nanostructuring of the Bi_2Te_3 crystals. The device operating voltage and power output as a function of electrical current were tested at different temperature differences, respectively (Fig. 5c and d). A single leg thermoelectric device with a maximum power of over 7 nW was obtained with a ΔT of 70 °C when an external load is resistance matched with the internal resistance of the leg. The performance of a single leg thermoelectric device (Fig. 5d) shows promising opportunities for large-scale, highly flexible devices for low-power applications.

Conclusions

We report the first demonstration of scalable, plasma-jet printed, 2D colloidal nanomaterial inks for flexible and low-cost thermoelectric device fabrication for microgravity and zero-gravity environments. Defect-engineered nanoflakes with adjustable pore size at the center were developed using a scalable solvothermal synthesis process. Detailed ink characterization was performed to optimize ink stability and ink-substrate interactions developing a general ink formulation for novel plasma-jet printing opportunities. An exploration into the fluid dynamics of the commercial plasma-jet printer was per-

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formed, and printing parameters within the laminar region of plasma flow were determined. The samples sintered at 375 °C showed a power factor of 70 μW m^{-2} K^{-1} and a change in resistance of 2% after 10 000 cycles of bending with a 25 mm ROC. A single-leg thermoelectric device developed using PJP on a flexible, polyimide substrate produced 7 nW of power with a temperature gradient of 70 °C. These results mark significant advancement in developing plasma-jet printing of nanomaterial-based devices with superior flexibility and adhesion for microgravity and zero gravity applications.

Materials and methods

Chemicals

Bismuth nitrate pentahydrate ($Bi(NO_3)_3H_2O$, >99.9%), sodium tellurite (Na_2TeO_3, >99.5%), sodium hydroxide (NaOH, >99%), poly(vinyl) pyrrolidone (PVP, MW 40 000) and ethylene glycol were purchased from Fisher Scientific. All chemicals were used as received.

Solution synthesis of nanoparticles

In a standard reaction, 0.2 mmol $Bi(NO_3)_3H_2O$ (0.0970 g), 0.3 mmol Na_2TeO_3 (0.0665 g), 4 mmol NaOH (0.1600 g), and 2 mmol PVP (0.2223 g) was combined with 10 mL ethylene glycol in a 25 mL double-neck flask. The mixture was stirred for 15 minutes using a magnetic stir bar to fully dissolve all solids before equipping with a reflux condenser and heating in an oil bath to 190 °C (Fig. 1a). After three hours, the flask was removed from the oil bath and allowed to cool to room temperature naturally. 20 mL isopropanol (IPA) and 10 mL acetone were added to the mixture, followed by centrifugation at 20 000 rpm (37 560*g*) for 16 minutes at 20 °C. The supernatant was discarded, and the collected solids were redispersed in IPA by bath sonication. The washing steps were repeated two more times to remove excess ethylene glycol, PVP, and other impurities. The final product was dried over a hot plate and massed before dispersing in a water-based co-solvent system to form the colloidal ink.

Plasma-jet printing and thermal sintering

Thermoelectric ink was printed using a commercial helium PJP from Space Foundry (Model #sfas000000074 28) onto polyimide (Kapton®) substrates that had been wiped with IPA. The nozzle size was 0.5 mm in diameter, and the print head was set at a height of 2 mm from the substrate. The samples were printed in 2 × 12 mm rectangles filled with a serpentine pattern of 50 μm spacing. Printed layers varied from 1–3 at a speed of 0.5–1 mm s^{-1}. The atomizer power was set to 40% and the sheath, and precursor gasses were varied from 325–375 sccm and 100–150 sccm between print sessions, respectively. The plasma voltage parameters were set to 12–15 kV and 27.6 kHz, the resonant frequency of the printhead used. These parameters were optimized during each session of printing for good adhesion, sufficient film thickness, uniform coverage, and minimal overspray. After printing, the films were dried on a hot plate in an ambient atmosphere at 150 °C for one hour to remove any remaining solvent. The dried samples were compacted using a cold hydraulic press using two thin layers of mica sheets as the cover plates with pressure up to 40 MPa. Thermal sintering was performed in a commercial tube furnace in an inert atmosphere. The peak temperature varied from 300 °C to 425 °C with a 60-minute sintering duration. The sintering temperature was limited because of the low degradation temperature of 50 μm Kapton substrates.

Atomic force microscope characterization

Bi_2Te_3 nanoflakes were imaged using a Bruker Dimension Icon atomic force microscope (AFM) under atmospheric conditions. Imaging was performed using a ScanAsyst-Air probe (Bruker, 2 nm radius of curvature) operating in PeakForce Tapping mode. Thirty nanoflakes were imaged to derive statistics. The height of each nanoflake was recorded as the peak value from the substrate, excluding any particulates present. Width measurements were obtained for each of the three pairs of sides on the hexagonal nanoflake and averaged to report the lateral dimensions.

Scanning electron microscope characterization

Scanning electron microscopy was used to image the topography of the plasma-deposited thermoelectric films. A Field Emission Scanning Electron Microscope (FEI Teneo) under high vacuum was used for imaging and EDS elemental analysis. The ETD and T1 detectors were used to obtain varying resolutions in imaging the deposited material.

Transmission electron microscope characterization

Bi_2Te_3 nanoflake ink was diluted in isopropyl alcohol and mixed using ultrasonication. The dispersion was drop cast onto a 300-mesh carbon-coated copper TEM grid for characterization using a JEOL 2100 HR TEM operating at 200 kV. Brightfield and high-resolution imaging were performed on the sample, and a selected area diffraction pattern was generated from a fully formed Bi_2Te_3 nanoflake.

Ink rheology measurements

Surface tension and contact angle were measured using a Biolin Scientific Attension optical tensiometer. Viscosity was measured using a Brookfield Ametek rheometer. Both measurements were performed for each cosolvent system with a particle concentration of 20 mg mL^{-1}.

Flexibility testing

The mechanical flexibility and durability of the films after bending were tested using an automated flexibility testing apparatus. The custom flexibility testing machine was constructed using a Micronix USA Translation Stage VT-50L controlled by an Arduino Uno. A base and stationary platform were 3D printed using a stereolithography (SLA) printer to match the height of the stage (Fig. 5a). The thermoelectric leg was placed on a supporting piece of polyimide and taped over the gap between the linear stage and the printed stationary

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platform. By controlling the number of steps and direction the stepper motor moves, the gap between the stage decreased and increased, causing the film to bend. The thermoelectric legs could be repeatedly bent to a precise radius using a set number of steps determined experimentally. Static bend tests were performed for three different ROC of 8, 16, and 25 mm. The resistance of the samples was measured after each bend test. The testing was performed at intervals of 10 bends until 100 total bends, then intervals of 100 bends until 1000 total bends, and then intervals of 1000 bends until 10 000 total bends were achieved. This ensured that the change in resistance of the film from the initial bends was captured more finely than the change in resistance from the latter bends when damage was done, and resistance change was minimal. The normalized resistance was plotted against the number of bends for each radius of curvature, and the curves were fit with exponential trend lines.

Electrical characterization

Conductivity measurements were performed using a linear four-point probe method with an inner probe spacing of 6 mm. A 100 mA current was passed through the sample, and five measurements were taken of the voltage difference of the center probes. The resistance was calculated using Ohm's law, and the average resistance was determined for each sample. The conductivity was calculated using the average thickness and width from the stylus profilometry of the films to find the cross-sectional area. The conductivity for each leg and sintering temperature was calculated and recorded.

Thermoelectric characterization

Seebeck coefficients and power measurements were performed on a custom testbed built using two commercial Peltier modules, one operating as a heater and the other as a cooler. The hot side and cold side of the TE leg were thermally grounded to the Peltier modules to create a temperature gradient. Two E-type thermocouples were mounted with voltage probes on the hot and cold sides with soft indium contacts to measure the temperature and voltage. For better contacts and measurements, an insulating layer was used to thermally insulate and apply pressure at the thermocouples. The device was connected electrically in series to the shunt resistor and a variable resistor for impedance matching at each measurement temperature. The device's open-circuit voltage, load voltage, current, and power output were measured at each temperature difference.

Author contributions

J. M. optimized the printer, fabricated the flexible films descriptions and performed out SEM, flexibility and electrical characterization. A. W. and T. V. synthesized the thermoelectric material and ink. A. W. optimized and performed ink characterization, and performed AFM. N. M. performed the TEM, XRD, and crystallography analysis. M. B., T. V. A. W. carried out thermoelectric property characterization on the films. D. E., H. S., T. V. and J. M. contributed to the conceptualization of this work. D. E. and H. S. supervised the project and H. S. is the PI.

Conflicts of interest

There is no conflicts to declare.

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