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## Development and optimisation of a $\text{SiO}_2$ PVD technique based on the thermal decomposition of PDMS†

Paul Cannon, <sup>\*a</sup> Enda McGlynn, <sup>ab</sup> Brian Freeland <sup>c</sup> and Jennifer Gaughran <sup>a</sup>

This work reports the development of a novel and facile physical vapour deposition (PVD) system for  $\text{SiO}_2$  deposition with a wide and controllable range of final film thicknesses. An investigation of the steady-state deposition temperature, heating rate, and PDMS source mass dependence of the deposited  $\text{SiO}_2$  layer thickness was performed using a variety of experimental techniques.  $\text{SiO}_2$  layers were characterised by scanning electron microscopy (SEM), energy dispersive x-ray spectroscopy (EDX), x-ray photoelectron spectroscopy (XPS), grazing incidence attenuating total reflection Fourier transform infrared spectroscopy (GATR-FTIR), contact profilometry (CP), and white light profilometry (WLP). It was found that the thickness of the  $\text{SiO}_2$  layer was linearly proportional to the PDMS source mass for large source masses with a nonlinear (parabolic) relationship for smaller source masses, but a non-monotonic relationship was observed between thickness and source material heating rate. The steady-state deposition temperature above the decomposition threshold did not directly affect layer thickness within the range investigated but, the lower the temperature, the greater the film uniformity.

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### Introduction

Silicon dioxide (silica or  $\text{SiO}_2$ ) has a broad range of applications throughout many industries. In the electronics industry, it is the most widely used dielectric as a gate insulator for field-effect transistors (FETs) due to its high resistivity, dielectric strength, large band gap, and high melting point.<sup>1,2</sup> Silica is also widely utilised in biomedical diagnostics, where it is employed in the current state-of-the-art technique for DNA isolation and purification.<sup>3</sup> This technique utilises the affinity between silica surfaces and proteins/nucleic acids.<sup>4</sup> Silica thin films have been deposited on various structures including silicon micropillars for enhanced DNA capture,<sup>5,6</sup> and on gold/noble metal surfaces to bind molecules for low cost surface plasmon resonance detection methods.<sup>7,8</sup> Historically,  $\text{SiO}_2$  deposition was performed at high temperatures and was based on the pyrolysis of silane in the presence of oxygen at atmospheric pressure.<sup>9</sup> As computer components increased in complexity, electronic layers required more uniform, conformal, and

controllable layer deposition at lower temperatures (less than the  $\sim 900$  °C used in traditional chemical vapour deposition (CVD)), in order to not adversely affect underlying layers in multilayer structures and to reduce long processing times. Additionally, high temperature deposition may not be suitable for all substrates, especially when it comes to low-cost substrates like quartz crystal microbalances for point-of-care medical applications. These quartz crystals have a phase transition temperature of 573 °C, after which they no longer function as a resonator.<sup>10</sup> Low pressure CVD (LPCVD) was developed to significantly increase film uniformity and conformity, but it still requires high temperatures. Plasma enhanced CVD (PECVD) was invented to satisfy both criteria, as the plasma conditions alter the thermodynamics of surface reactions, considerably lowering the temperature at which reactions are possible, allowing for much lower temperature deposition with superior uniformity.<sup>11,12</sup> However, each CVD technique comes with significant drawbacks, with CVD providing low step coverage, LPCVD requiring high temperatures, and PEVCD requiring constant chamber cleaning due to risks of contamination from particle build-up, and all of these techniques requiring expensive and highly toxic precursor gases, usually silane.<sup>13</sup> We also note that thin films of a range of other metal oxide materials are being studied for a variety of applications, including as gate oxides in FET structures.<sup>14–17</sup>

Many alternative techniques have been developed to improve individual aspects of the  $\text{SiO}_2$  deposition process, such

<sup>a</sup> School of Physical Sciences, Dublin City University, Dublin 9, Ireland.

E-mail: paul.cannon3@mail.dcu.ie

<sup>b</sup> National Centre for Plasma Science and Technology, Dublin City University, Dublin 9, Ireland

<sup>c</sup> School of Biotechnology, Dublin City University, Dublin 9, Ireland

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as sol-gel processes,<sup>18</sup> magnetron sputtering,<sup>19</sup> electron beam deposition,<sup>20</sup> with the most promising being atomic layer deposition (ALD).<sup>21</sup> ALD provides unrivalled step coverages and conformity/uniformity, allowing controllable sub-nanometre thicknesses with pinhole free layers due to the atomic layer by layer growth mechanism.<sup>22,23</sup> However, this comes with a time, instrumentation and material cost, with significantly increased processing times and very low material and energy utilization efficiency.<sup>24</sup>

In addition, low pressure and vacuum-based technologies come with high manufacturing costs, which is further increased when attempting to accommodate large area depositions. Thus, research into lower cost and scalable deposition techniques have gained increased focus in recent years. Physical vapour deposition (PVD) has emerged as a lower cost, and safer alternative to other deposition techniques. PVD shares many similarities with CVD, but the differences occur in the precursor materials.<sup>25</sup> CVD utilises precursor gas/gases which initiate chemical reactions near or on the heated substrate surfaces, producing chemical by-products, resulting in by-product deposition on the substrate while other by-products and unreacted precursor gases are exhausted out of the reaction chamber. PVD is a much simpler process, involving the thermal evaporation of a precursor material to produce a vapour phase. The vapour atoms are transported, typically through a low pressure zone in a straight line path, and deposit directly on the substrate.<sup>26</sup> The aforementioned magnetron sputtering, and e-beam evaporation methods are examples of PVD techniques, with the former a plasma-based technique, and the latter a high-power technique, both requiring high vacuum environments.

In this report we demonstrate a low-cost, facile, and novel experimental setup for  $\text{SiO}_2$  thin film PVD under atmospheric pressure at relatively low temperatures using small amounts of precursor source material. Our work modifies the experimental conditions created by Hu *et al.*,<sup>27</sup> and is based on the thermal degradation mechanisms of polydimethylsiloxane (PDMS) investigated by Camino *et al.*<sup>28,29</sup> That is, PDMS thermally decomposes at temperatures above  $\sim 450$  °C, into volatile cyclic oligomers. In air, these volatile oligomers become oxidised, leading to the formation of gaseous  $\text{SiO}_2$  species that nucleate and grow heterogeneously on the surface of solid substrates.  $\text{SiO}_2$  films were deposited on p-type Si wafers, and the influence of heating rate, steady-state deposition temperature, and mass of PDMS on the final film thickness was studied for the first time. The thickness can be precisely controlled by changing either the amount of PDMS precursor material or the heating rate used to reach the steady-state deposition temperature, or both. The lower the steady-state deposition temperature is, above the PDMS decomposition threshold, the greater the film uniformity.

## Materials and methods

### Synthesis of PDMS

Thin films were deposited *via* thermal evaporation of PDMS. PDMS was synthesised using the Sylgard 184 silicone elastomer kit from Dow Corning Corporation. The PDMS base and curing

agent were mixed in a 10:1 ratio by weight, respectively, and allowed to cure at room temperature for at least 48 hours.

### PVD configurations

The first configuration adopted the setup of Hu *et al.*<sup>27</sup> The PDMS block was loaded into an alumina boat and the substrate was placed vertically above the PDMS, across the top opening of the boat. This boat, containing both PDMS and substrate, was placed in a Nabertherm Muffle Furnace LT 3/11/B410 and heated in air to 650 °C (the steady-state deposition temperature) at a rate of 12 °C minute<sup>-1</sup>, remaining at this temperature for 2 hours.

The second configuration utilised the same apparatus as configuration one, however the sample was placed downstream along the alumina boat, with a lateral distance of  $\sim 5.5$  cm from the PDMS block.

The third and final configuration was identical to configuration two, except the entire alumina boat containing PDMS and substrate was placed within a hollow quartz tube of 3.8 cm inner diameter. The tube was pointed towards the furnace exhaust, with the substrate positioned between the PDMS block and exhaust (Fig. 1). This configuration was utilised for the entire subsequent investigations of the influence of PDMS mass (1.5–48 mg), steady-state deposition temperature (450–650 °C), and heating rate (1–40 °C minute<sup>-1</sup>) on  $\text{SiO}_2$  deposition thickness.

### Film characterisation

$\text{SiO}_2$  films were imaged using a Karl-Zeiss EVO 50 series scanning electron microscope (SEM) with an Oxford Instruments Xplore detector mounted within to provide additional chemical information *via* energy dispersive x-ray spectroscopy (EDX).

Further chemical properties were characterised by grazing-angle attenuated total reflection Fourier Transform Infrared Spectroscopy (GATR-FTIR) using a Nicolet iS50 FTIR equipped with a Harrick VariGATR attachment, and X-ray photoelectron spectroscopy (XPS) using a Scienta Omicron X-ray photoelectron spectrometer with a monochromated Al K $\alpha$  source (1486.7 eV) and a 128 channel Argus CU detector. FTIR measurements were

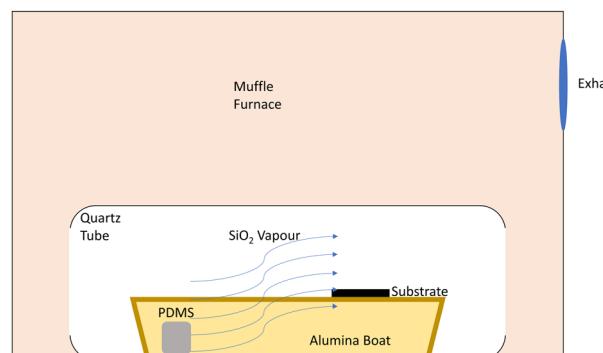


Fig. 1 Schematic diagram of novel PVD system for  $\text{SiO}_2$  deposition on solid substrates. The substrate is placed between the heated block of PDMS and the exhaust of the muffle furnace, utilising the difference in temperature to drive the  $\text{SiO}_2$  vapour over the substrate. The quartz tube ensures most of the vapour is directed over the substrate, providing more controlled deposition.



taken from an average of 128 scans with  $8\text{ cm}^{-1}$  resolution, using a force of  $\sim 700\text{ N}$ , for an optimum signal to noise ratio as per manufacturer specifications for measuring thin films on silicon. XPS measurements were taken using a 0.1 eV step size.

Film thicknesses were determined using a Bruker Dektak XT Profilometer with a  $2.5\text{ }\mu\text{m}$  radius stylus. Scan parameters varied depending on sample and scan length, but all scan speeds were  $\leq 100\text{ }\mu\text{m s}^{-1}$  and were generally chosen to produce 300 nm per pt resolutions. CP data was filtered using a two-sided ( $\pm 10\text{ }\mu\text{m}$ ) moving average to better illustrate the average thicknesses, but the raw data can be found in the ESI.<sup>†</sup> Grey highlighted areas in the CP measurements indicate uncoated substrate regions, and blue highlighted areas indicate where the average thickness measurement was taken from. The average thickness measurements were taken from the areas of the sample located along the centre of the alumina boat. These measurements were supported by white light profilometry (WLP) measurements using a Bruker Contour GT Profilometer. Due to the transparent nature of the thinner  $\text{SiO}_2$  films ( $<200\text{ nm}$ ), gold coating was required for WLP measurements. Gold coating was carried out in an Edwards AUTO 306 Vacuum Coater, using a tungsten filament operated under a  $\sim 1.5\text{ kV}$  voltage and  $\sim 20\text{ mA}$  current, to produce a  $24.6\text{ nm}$  reflective layer on top of the  $\text{SiO}_2$  which was monitored and confirmed by a resonating crystal detector within the instrument.

## Results and discussion

### Development and optimisation of PVD system

Firstly, we sought to achieve coatings similar to the technique described by Hu *et al.* using the same experimental setup and conditions.<sup>27</sup> However, it is important to note that they were coating only the internal walls of a porous anodic aluminium oxide template, which would allow only a fraction of the vapour to enter and coat the nanopores, whereas we wished to coat the surfaces of solid, nonporous substrates. This setup labelled “configuration one” from this point onwards, resulted in coatings

that were millimetres, rather than nanometres, thick (Fig. 2). This is because our nonporous substrate caused build-up of the material due to its impermeable nature and close proximity to the vapour source. Additionally, we found that the PDMS expands greatly and physically came into contact with the substrate, which drastically reduced the quality of the deposited coating, as shown in Fig. 2.

To overcome the issues of PDMS expansion, and to reduce the coating thickness, we developed configuration two. Configuration two was the same as configuration one (Fig. 2), except the PDMS was placed at one end of the alumina boat, and the substrate was placed at the opposite end, rather than directly on top of one another. However, while this produced a significantly thinner coating, it was entirely uneven across the sample surface (Fig. 3a). The work reported by Favors *et al.*<sup>30</sup> however adopted a similar deposition technique, where they used a tube furnace, sub-atmospheric pressures, and controlled gas flows to produce nanometre thickness coatings and circumvent the aforementioned problems of the technique of Hu *et al.*<sup>27</sup> Their technique also required significantly less PDMS, using 50 mg compared to the 600 mg used in the original work. We modified the approach of Favors *et al.*<sup>30</sup> to one which requires neither a tube furnace nor sub-atmospheric pressures and controlled gas flows to achieve conformal nanometre coatings by using a standard muffle furnace/oven, open to air at atmospheric pressure, as described in the materials and methods. By simply placing the alumina boat containing PDMS with the sample downstream, all inside a hollow cylindrical quartz tube with similar length to the alumina boat (Fig. 1), the vapour is directed entirely over the sample surface, resulting in more deposition and uniformity of  $\text{SiO}_2$ , as seen in Fig. 3c.

Given that the entire vapour is confined and directed over the sample, the coating was much thicker than it was when using the same setup without the quartz tube (configuration two), going from an average thickness of 500 nm to  $\sim 1700\text{ nm}$  in the central regions (Fig. 3b). The configuration three results show full sample coverage when compared to the technique performed without the quartz tube in configuration two, however the profilometry results show large variations in thickness of the order of microns over length scales of microns. The contact profilometry results in isolation would suggest the quartz tube gives rise to significantly poorer quality coatings, but the visual images show a clear difference in sample coverage and uniformity on the scale of centimetres (Fig. 3). The results prompted us to continue with the quartz tube method, and to significantly reduce the amount of PDMS used.

The sample grown using configuration three was imaged under SEM (Fig. 4) to better understand the large roughness observed in Fig. 3. EDX was also performed to confirm that we were indeed obtaining a pure  $\text{SiO}_2$  coating. By using a relatively low accelerating voltage (9.00 keV) in combination with the  $\sim$  micron thickness of the coating, we obtained EDX spectra without substrate contamination due to a  $\sim 300\text{ nm}$  penetration depth for the primary electron beam. The SEM image in Fig. 4a shows clear island growth which is consistent with the contact profilometry results observed. Calculating the atomic

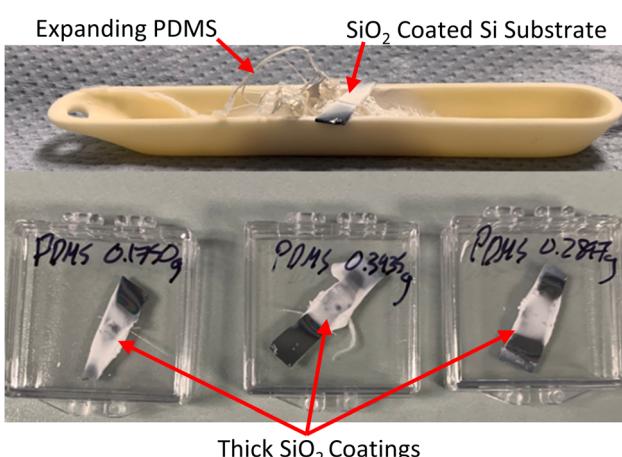


Fig. 2 Photograph of  $\text{SiO}_2$  deposition following the procedure of Hu *et al.*,<sup>27</sup> i.e. configuration one, showing the thick coatings and expansion of PDMS during heating.



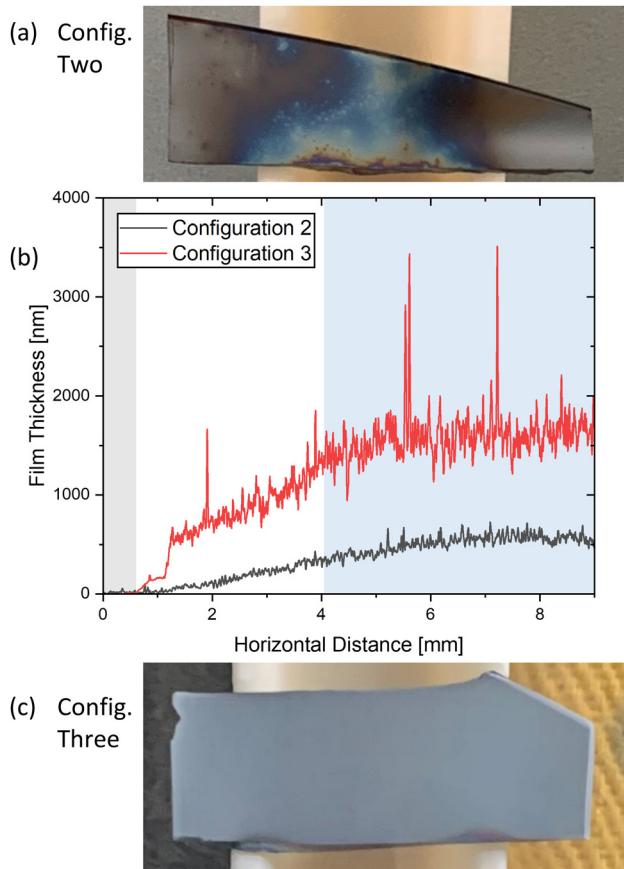


Fig. 3 (a) Photograph of  $\text{SiO}_2$  deposition by PVD configuration two *i.e.*, alumina boat without quartz tube. (b)  $\text{SiO}_2$  film thickness measurements across samples (a) and (c). (c) Photograph of  $\text{SiO}_2$  deposition by configuration three *i.e.*, the alumina boat contained within a hollow quartz tube configuration. Both depositions were carried out under the same conditions ( $\sim 47.5$  mg PDMS,  $650$   $^\circ\text{C}$  steady-state deposition temperature,  $12$   $^\circ\text{C min}^{-1}$  heating rate).

percentages from the weighted EDX results in Fig. 4b gives a  $69.3\% : 30.7\%$  or  $2.26 : 1$  ratio of oxygen to silicon, which is again consistent with the result expected for silicon dioxide and is in agreement with the values obtained by Favors *et al.*<sup>30</sup> The coating in Fig. 4 shows large, spherical island features. These may indicate that the  $\text{SiO}_2$  preferentially homogeneously nucleates on already deposited  $\text{SiO}_2$ . If these features are present on the thinner coatings discussed later, they cannot be seen by SEM.

#### Film thickness vs. PDMS mass

Hu *et al.*<sup>27</sup> found that the  $\text{SiO}_2$  thickness was linearly proportional to the amount of PDMS used, so the next step was to significantly reduce the amount of PDMS used in the process to produce thinner coatings of nanometre dimensions. We performed depositions using 47.5, 30.6, 12.0, 6.0, and 1.5 mg of PDMS source material and measured the resulting thicknesses. The results are shown in Fig. 5.

A rough linear trend in thickness *versus* source material mass is seen for source masses of 47.5, 30.6 and 12.0 mg.

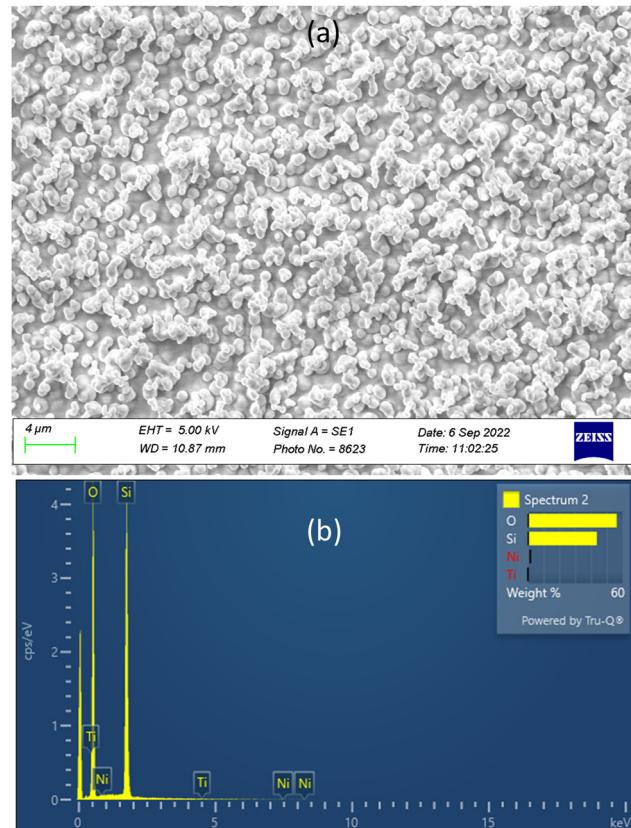


Fig. 4 (a) SEM image of the sample grown using 47.5 mg of PDMS via configuration three, as shown in Fig. 3c. The coating displays island-type growth, characteristic of  $\text{SiO}_2$  on Si using PVD, with individual islands of  $\sim 1\ \mu\text{m}$  in size, alongside multi-island structures. (b) EDX spectra of the same sample imaged in (a) showing the weight percentages of Si and O signals.

However, there is only a 4% reduction in film thickness when reducing the PDMS mass from 6.0 to 1.5 mg. This result was replicated four times and similar behaviour was seen on each occasion. A nonlinear relationship is seen for smaller source masses, with the film thickness seeming to plateau at 6 mg of PDMS and below. This reasoning for this result was not clear initially, so we opted to investigate the influence of both furnace steady-state deposition temperature and heating rate on the resultant film thickness to shed some light on the process.

#### Film thickness vs. steady-state deposition temperature

Keeping the mass of PDMS constant at 12 mg, we initially performed the  $\text{SiO}_2$  deposition using a large range of steady-state deposition temperatures ( $450$ – $650$   $^\circ\text{C}$ , in  $50$   $^\circ\text{C}$  intervals). The lower point of the range chosen was the minimum threshold temperature required to initiate the degradation mechanism for PDMS, and the largest temperature was the one used by both Hu *et al.*<sup>27</sup> and Favors *et al.*<sup>30</sup> Each sample was heated at a rate of  $12$   $^\circ\text{C minute}^{-1}$  and maintained at the steady-state temperature for two hours to ensure complete degradation of PDMS, and the results can be seen in Fig. 6.

Fig. 6 shows the effect of the steady-state temperature on the  $\text{SiO}_2$  deposition process. The most obvious result is that lower

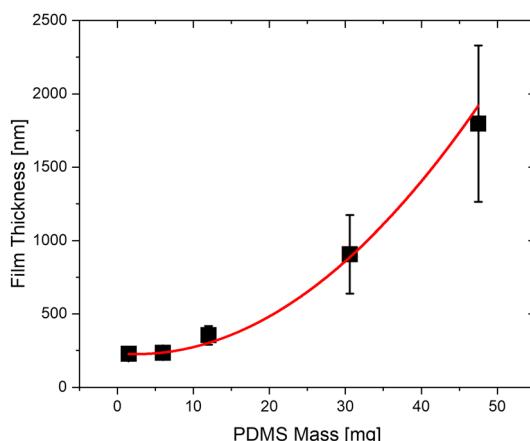


Fig. 5 Film thickness vs. PDMS mass using a  $12\text{ }^{\circ}\text{C min}^{-1}$  heat rate, and a steady-state deposition temperature of  $650\text{ }^{\circ}\text{C}$ . The red line is a guide to the eye, using a parabolic form with a constant offset.

temperatures give much less surface roughness, although the coatings themselves do not visually appear flat and are continuing to increase in thickness across the substrate, whereas the higher temperature samples have much rougher surfaces, but the thicknesses seem to plateau. Surface roughness measurements, as determined by the Dektak XT software, give surface roughness values of 34.7, 15.8, 16.9, 8.3, and 0.4 nm from higher to lower temperature, with the bare Si wafer reference sample (with no deposition) having a roughness of 0.1 nm.

The observed film increase in thickness of  $\text{SiO}_2$  deposition across individual samples appears to be due to the influence of the piece of bare Si placed on top of the sample surface in order to provide an uncoated area to use as a point of reference for the coating measurements. This is used to provide a flat measurement of the bare Si surface, and this “marked” region can be seen as the flat region highlighted in grey on the left-hand side of Fig. 6. The higher temperature coatings appear relatively unaffected by this, given the step edge between the flat region and the coated region. We see more gradual changes

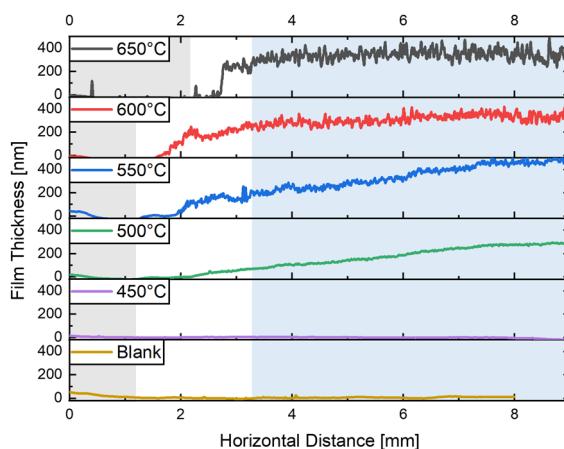


Fig. 6 Steady-state deposition temperature dependence of  $\text{SiO}_2$  film thickness using 12 mg of PDMS at a heating rate of  $12\text{ }^{\circ}\text{C minute}^{-1}$ .

between the flat and coated regions at lower temperatures. We believe the large Si piece is deflecting the vapour more at lower deposition temperatures, causing thicker coatings to occur as the distance is increased from this piece.

In order to test this hypothesis, we performed a  $500\text{ }^{\circ}\text{C}$  deposition without this Si piece (Fig. 7) and the  $\text{SiO}_2$  film was quite flat compared to the data illustrated in Fig. 6, showing only an average 50 nm increase in thickness in the substrate centre. The thickness increases between 5–15 mm correspond to the area of the wafer directly above the alumina boat. These positions are where the silicon contacts the boat, so it is expected that we would see an increase in coating thickness in the centre of the boat.

We also performed the standard “Scotch Tape” test (Fig. 7) on this same sample to qualitatively measure the strength of adhesion, alongside repeated washing with isopropyl alcohol and deionised water, and the coating appeared unaffected, indicating good adhesion. A sticky residue remained after the test, which can be seen on the right-hand side of the profilometry data of Fig. 7. For all subsequent tests, this Si piece was cleaved to be as small as possible and the substrates to be coated were increased in length from their initial size, equal to the width of the alumina boat (1–1.2 cm), to over double the width (2.5 cm) of the boat in order to have the Si piece as far from the boat centre as possible.

By applying the above sample modifications, we performed further depositions between  $460$ – $500\text{ }^{\circ}\text{C}$  using only 6 mg of PDMS (Fig. 8). We observe no evidence of  $\text{SiO}_2$  deposition at  $450\text{ }^{\circ}\text{C}$  because this is the threshold temperature required for the bond scission of cyclic oligomers. This temperature must be exceeded to generate the  $\text{SiO}_2$  vapour. Fig. 8a shows there is no significant dependence of the film thickness on the steady-state deposition temperature in this temperature range. Findings from Camino *et al.*<sup>28</sup> suggest that there could be a temperature dependence, as the weight of the PDMS block gradually decreases with increasing temperature after thermal degradation begins, until it eventually plateaus at a higher temperature.

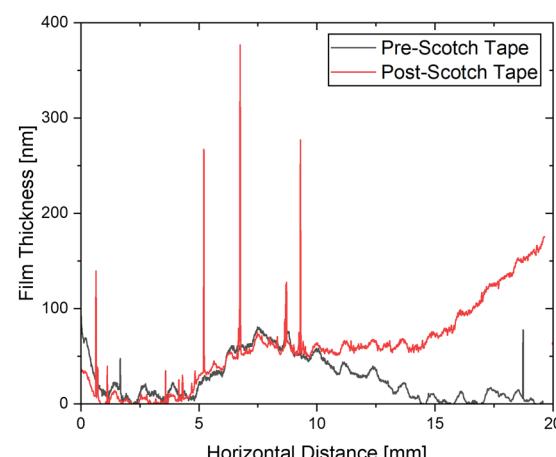


Fig. 7  $\text{SiO}_2$  coating without Si piece to mark uncoated areas alongside a scan across the same sample after the “Scotch-Tape” test performed on the latter half of the surface (10–20 mm).



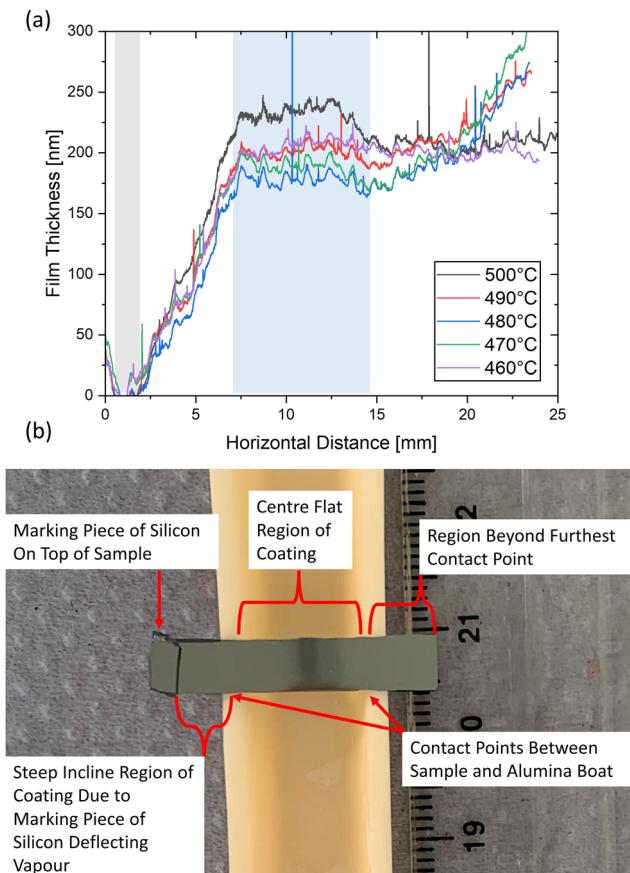


Fig. 8 (a) Steady-state deposition temperature dependence of  $\text{SiO}_2$  coating using 6 mg PDMS at a heating rate of  $12\text{ }^\circ\text{C minute}^{-1}$  using updated sample preparation. (b) Annotated top-down photograph of  $\text{SiO}_2$  PVD sample highlighting the different coating regions observed in (a).

However, we maintain the steady-state deposition temperature for two hours, whereas they measured the change in mass with increasing temperature without maintaining each temperature for a set amount of time. Our lower temperature deposition for longer periods of time may be broadly equivalent to increasing the temperature until the PDMS has been completely degraded. The steep incline seen at the left-hand side of Fig. 8a ( $\sim 2\text{--}7.5\text{ mm}$ ) occurs between the silicon piece and the nearest contact point between the sample Si and the alumina boat, and the flat central region of the coating ( $\sim 7.5\text{--}15\text{ mm}$ ) corresponds to the centre of the alumina boat (illustrated in Fig. 8b). The thickness of the coating begins to vary beyond this, starting roughly at the second contact point between sample and alumina (located at  $\sim 15\text{ mm}$ ), and continuing along the sample in the region overhanging the alumina. We believe the upward thickness trend after the horizontal position labelled 15 mm onwards seen for some of the samples is a result of a slight tilt of the sample/boat during the deposition process.

With this updated sample preparation, we performed a deposition at  $500\text{ }^\circ\text{C}$  and  $650\text{ }^\circ\text{C}$  using 1.5 mg of PDMS to compare the impact of steady-state deposition temperature on  $\text{SiO}_2$  film thickness over a large temperature range. Fig. 9 shows very similar thicknesses at each temperature across a 1.6 cm

long substrate, with the higher temperature deposition showing an increased surface roughness, which was to be expected based on the results shown in Fig. 7 and 8. These data further strengthen our conclusions based on the earlier data.

### Film thickness vs. heating rate

While flat and uniform coatings were being produced, they were still  $\sim 200\text{ nm}$  thick. To further reduce the coating thicknesses, we reviewed the work done by Camino *et al.*, who studied the thermal degradation mechanisms/kinetics of PDMS.<sup>28,29</sup> They discovered that the products of the thermal degradation of PDMS depend on the heating rate, as this strongly affects the degree of depolymerization. Lower heating rates and steady-state temperatures produce the volatile cyclic oligomers required as the precursors for  $\text{SiO}_2$  vapour generation. However, the lower the heating rate is, the lower the degree of depolymerization is and hence less  $\text{SiO}_2$  vapour will be produced in this case. Rapid heating rates result in increased depolymerization, but these cyclic oligomers are then accompanied by linear oligomers, with the latter dominating the reaction products. Here, a radical mechanism occurs through homolytic  $\text{Si-CH}_3$  bond scission. Cross-linking of macro-radicals here decreases the flexibility of the PDMS chain and hinders the splitting of cyclic oligomers. So rather than getting more  $\text{SiO}_2$  vapour, bond reorganisation takes place with the formation of ceramic silicon-oxycarbide, which represents the majority of the reactant product, producing less  $\text{SiO}_2$  vapour.

We performed  $\text{SiO}_2$  coating at three different heating rates under a steady-state deposition temperature of  $500\text{ }^\circ\text{C}$ ; the original  $12\text{ }^\circ\text{C minute}^{-1}$  used by Hu *et al.*<sup>27</sup> and Favours *et al.*,<sup>30</sup> and also at the minimum ( $1\text{ }^\circ\text{C minute}^{-1}$ ) and maximum ( $40\text{ }^\circ\text{C minute}^{-1}$ ) rates achievable with our system. We can clearly see this non-monotonic relationship in Fig. 10, with  $1$  and  $40\text{ }^\circ\text{C minute}^{-1}$  heating rates producing significantly thinner coatings than a heating rate of  $12\text{ }^\circ\text{C minute}^{-1}$ . The film thickness for the  $1\text{ }^\circ\text{C minute}^{-1}$  deposition peaks at  $60\text{ nm}$  and ranges consistently between  $25\text{--}50\text{ nm}$  in the centre of the boat. These results provide

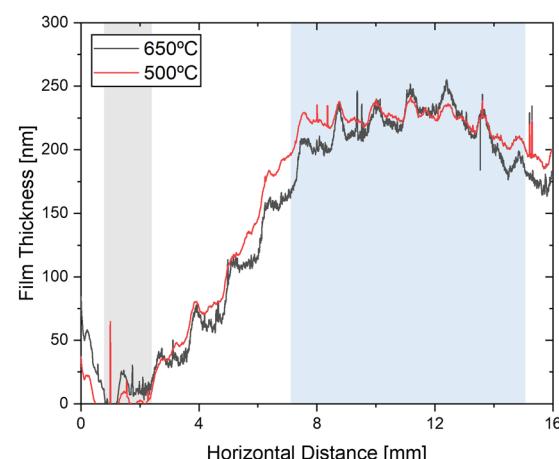


Fig. 9  $\text{SiO}_2$  coating at steady-state deposition temperatures of  $500\text{ }^\circ\text{C}$  and  $650\text{ }^\circ\text{C}$ , each using 1.5 mg of PDMS and a heating rate of  $12\text{ }^\circ\text{C minute}^{-1}$ .



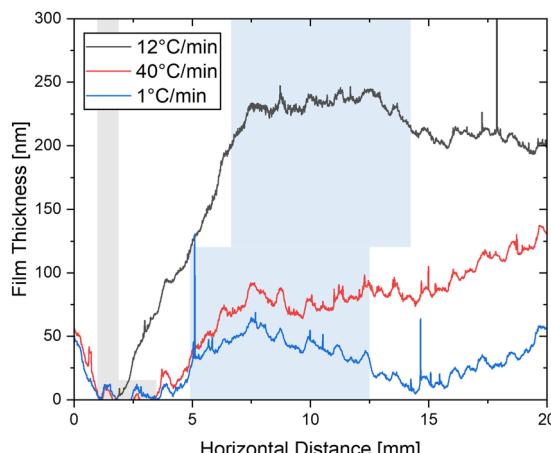


Fig. 10  $\text{SiO}_2$  thickness dependence on heat rate for a steady-state deposition temperature of  $500\text{ }^\circ\text{C}$  using 6 mg of PDMS.

additional context for those observed during the film thickness *vs.* PDMS mass investigation. The 1.5 mg blocks of PDMS are very small, with a significantly higher surface to volume ratio than the other blocks used. These smaller blocks undergo more rapid depolymerisation at high heating rates as a result of their small size and high surface to volume ratio, resulting in an altered reactant product compared to the larger masses. The  $1\text{ }^\circ\text{C minute}^{-1}$  heating rate depositions were repeated to demonstrate the reproducibility of the PVD system, and the results in Fig. 11 demonstrate good process reproducibility.

Considering the results of each deposition parameter, alongside the thermogravimetric analysis of PDMS at different heating rates performed by Camino *et al.*,<sup>28</sup> the effect of steady-state deposition temperature on film thickness is likely more apparent at lower heating rates than the  $12\text{ }^\circ\text{C minute}^{-1}$  utilised here. At large heating rates, there is rapid degradation of PDMS per unit temperature above the decomposition threshold, whereas slower heating rates show a much lower amount of degradation per unit temperature, with two distinct stages of degradation emerging. However, we choose not to investigate this due to the tunability already available from varying the PDMS mass and heating rate alone.

In addition, characterisation *via* WLP was carried out to complement the CP measurements. The WLP results of the  $1\text{ }^\circ\text{C minute}^{-1}$  heat rate sample can be seen in Fig. 12, and it shows very good agreement with the data of Fig. 10 and 11. Due to the transparent nature of the  $\text{SiO}_2$  film, secondary fringes would occur due to reflections from the top of the film, as well as from reflections from the silicon wafer surface which arose from white light transmitted through the film. For this reason, a thin ( $\sim 25\text{ nm}$ ) layer of gold was deposited on top of the  $\text{SiO}_2$  film to attenuate the white light and prevent these secondary transmission fringes from occurring. The gold layer was deposited by e-beam evaporation to better maintain the  $\text{SiO}_2$  surface topography compared to other sputter coating techniques. The gold layer was slightly thinner at the step between uncoated Si and  $\text{SiO}_2$  which can be seen as a sharp increase in thickness around the  $1600\text{ }\mu\text{m}$  position. Comparing the

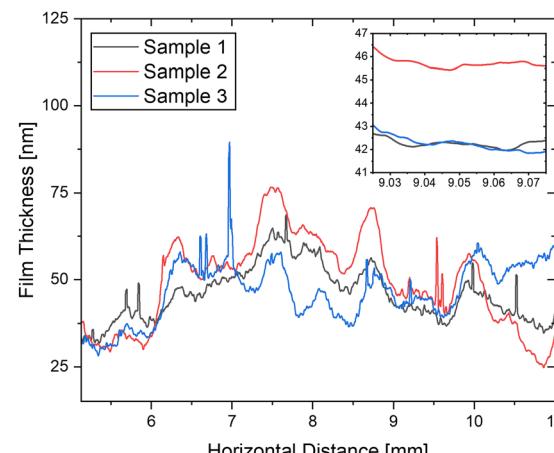


Fig. 11 Profilometry scans of three different substrates subjected to  $\text{SiO}_2$  PVD using 6 mg PDMS and  $1\text{ }^\circ\text{C minute}^{-1}$  heat rates using a steady-state deposition temperature of  $500\text{ }^\circ\text{C}$ , demonstrating the process reproducibility for deposition of very thin films across a large area along the centre of the alumina boat. (Inset; Higher magnification view of the  $\text{SiO}_2$  thickness across a  $50\text{ }\mu\text{m}$  long region on the sample).

heights between the uncoated Si and the centre region of the  $\text{SiO}_2$  coating, we obtain a film thickness measurement of  $79.6\text{ nm}$ , which, when corrected for the gold layer thickness, gives a thickness of  $55.0\text{ nm}$ , in excellent agreement with the CP results. The uniformity of the  $\text{SiO}_2$  film thickness was determined to be less than  $1.0\text{ nm}$  both transversely and longitudinally across the entire region imaged in Fig. 12a. The periodic peaks and troughs which occur in the CP data were also present in the line profiles of the WLP data, with similar widths of 500 microns. The periodic peaks and troughs also occur in the uncoated regions of the  $\text{SiO}_2$  coated samples, as well as the untreated Si substrates. The presence of these similar features in each set of measurements made by two different techniques indicates they are characteristics of the Si substrate rather than the  $\text{SiO}_2$  coating. The gold coated  $\text{SiO}_2$  film was also imaged *via* SEM and can be seen in Fig. 12b–e. The top-down view images (Fig. 12b and c) verify the uniformity of the film due to the lack of contrast seen in the images. Small surface topographical features (Fig. 12c) can be seen on some areas of the film, but these occurred relatively infrequently. Cross-sectional (at  $90^\circ$ ) images of the sample labelled 2 in Fig. 12 can be seen in Fig. 12d and e, which show very good agreement between the film thicknesses determined by both techniques. The coating in the centre of the substrate (Fig. 12d) corresponds to  $(90 \pm 20)\text{ nm}$ , which, when corrected for the additional  $\sim 25\text{ nm}$  of gold, is in very good agreement with the results shown in Fig. 11. Fig. 12e shows the decreased thickness of the film ( $45 \pm 10\text{ nm}$  including the  $\sim 25\text{ nm}$  gold contribution) outside the central region of the sample, in this case at a position of approximately 5 mm along the substrate (see Fig. 11 also).

Lastly, the thinner  $\text{SiO}_2$  samples were analysed using XPS and GATR-FTIR spectroscopy, to determine physical and chemical characteristics that could not be measured by EDX. GATR-FTIR data (Fig. 13) shows the increased intensity of the

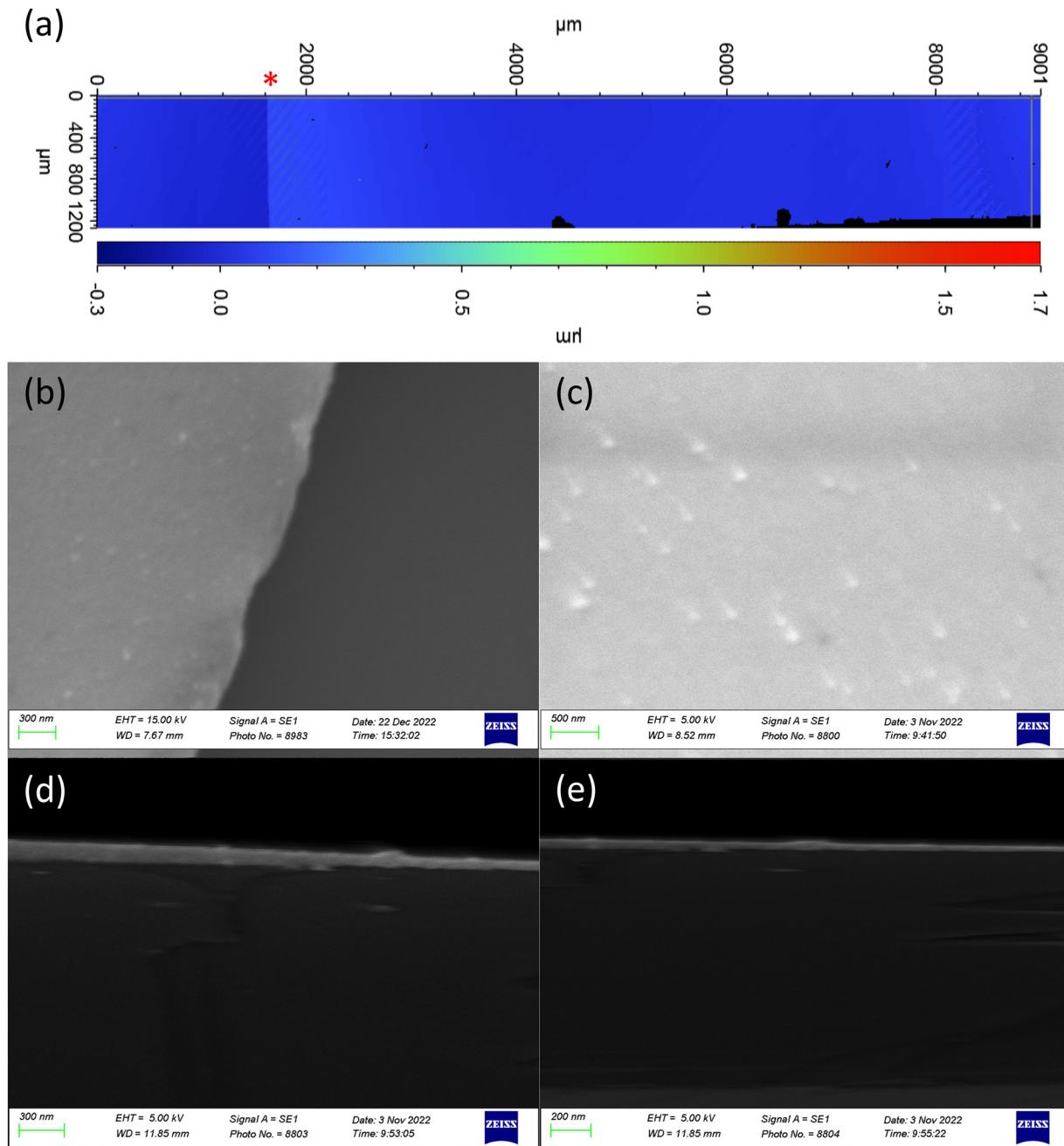


Fig. 12 (a) WLP measurement of the same SiO<sub>2</sub> sample deposited using 6 mg PDMS and a 1 °C minute<sup>-1</sup> heat rate shown in Fig. 10. The sharp step seen around the 1600 μm position (indicated by the red asterisk) is due to the large change in reflection due to the 24.6 nm gold coating on top of the transparent SiO<sub>2</sub> film, and secondary interference fringes occurring here due to a slightly decreased gold layer thickness at the step edge. (b)–(e) SEM images of sample 2 in Fig. 11. (b) Top-down view of the SiO<sub>2</sub> coating, showing the gold coating (left) and the SiO<sub>2</sub> without gold coating (right). (c) Top-down view of the SiO<sub>2</sub> coating, showing <200 nm sized surface topographical features on the surface. (d) Cross-sectional (90°) view of the Au-SiO<sub>2</sub> coating in the centre of the substrate with an average thickness of (90 ± 20) nm (e) Cross-sectional (90°) view of the region of the Au-SiO<sub>2</sub> coating away from the centre (at a position of approximately 5 mm along the substrate) with an average thickness of (45 ± 10) nm.

symmetric and asymmetric stretching vibrations of Si–O–Si, at 800 and 1100 cm<sup>-1</sup> respectively, indicative of the presence of an increased deposit of SiO<sub>2</sub> in the thickest sample. The sharp peak at 1250 cm<sup>-1</sup> observed in the uncoated Si sample is caused by longitudinal optical phonons of the crystalline silicon wafer and its native oxide.<sup>31,32</sup> While GATR-FTIR is

useful for detecting chemical bonds in our samples, we looked at XPS for chemical identification for very thin films, and to better distinguish between Si and SiO<sub>2</sub>.

Fig. 14 shows the XPS data for the Si 2p and O 1s orbital regions, with the Si 2p bulk signal occurring at the expected 99.4 eV position and decreasing with increasing SiO<sub>2</sub> thickness

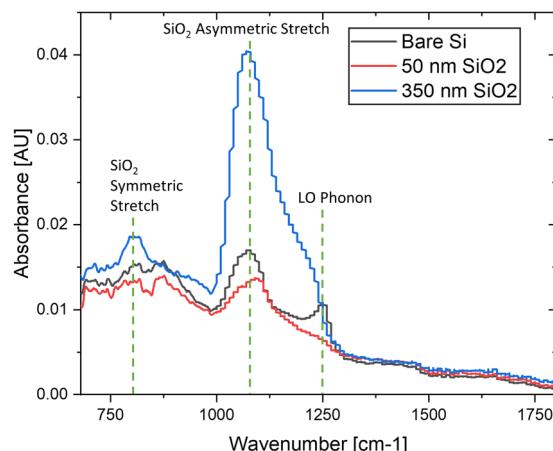


Fig. 13 (a) FTIR spectra of the  $\text{SiO}_2$  coatings at varying thicknesses, showing the symmetric and asymmetric stretching vibrations of  $\text{Si}-\text{O}-\text{Si}$  at  $800$  and  $1100\text{ cm}^{-1}$  respectively, and longitudinal optical phonons of the crystalline silicon wafer and its native oxide at  $1250\text{ cm}^{-1}$  in the uncoated substrate.

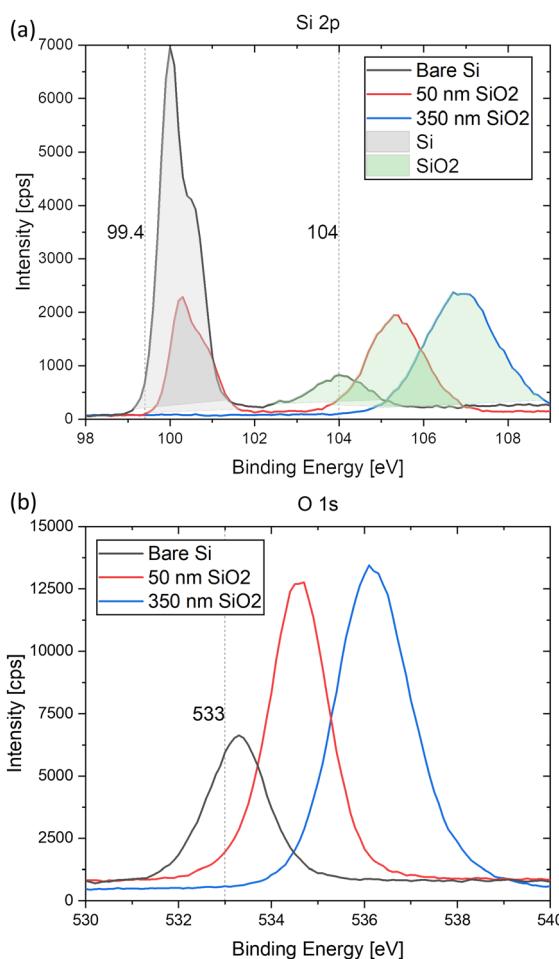


Fig. 14 XPS spectra of  $\text{SiO}_2$  coatings of varying thicknesses of the (a)  $\text{Si} 2p$  region showing the decrease in  $\text{Si}$  signal ( $99.4\text{ eV}$ ) and increasing oxide signal ( $104+\text{ eV}$ ) with increasing  $\text{SiO}_2$  thickness, and the (b)  $\text{O} 1s$  region showing the increasing  $\text{O}$  signal ( $\sim 533\text{ eV}$ ) with increasing  $\text{SiO}_2$  thickness. Both spectra show surface charging effects.

until it becomes completely obscured by the overlying coating.<sup>33</sup> In parallel, we see the characteristic  $\text{SiO}_2$   $2p$  intensity ( $104\text{ eV}$ ) increase with increasing thickness, and we also see the binding energy of this feature increase compared to the expected  $104\text{ eV}$  energy. This shift is due to surface charging effects which occur as photoelectrons are emitted from the  $\text{SiO}_2$  layer (34). As  $\text{SiO}_2$  is insulating, it cannot readily replace emitted electrons, causing a build-up of positive charge which increases the binding energy of remaining electrons. This phenomenon is more pronounced in the thicker coatings. We also performed a  $50\text{ nm}$   $\text{SiO}_2$  coating on conductive  $\text{ZnO}$  nanostructures, and the binding energy decreases from  $105.3\text{ eV}$  when grown on the native insulating oxide of  $\text{Si}$ , to  $104.6\text{ eV}$ , supporting our identification of this energy shift as being due to charging and not the generation of other oxidation states. This is further supported by the corresponding  $\text{O} 1s$  spectra, where similar shifts due to surface charging are observed in these samples. We note that we still see some evidence of the  $\text{Si} 2p$  bulk signal in the  $50\text{ nm}$  coating spectra, although the elastic mean free path should be no greater than  $10\text{ nm}$ . This substrate signal may be due to emission from more thinly coated regions of the sample, or from small pinholes that CP cannot detect due to the large tip diameter ( $5000\text{ nm}$ ) relative to the nanometre dimensions of the coating features. The SEM image in Fig. 4 shows the non-uniform nature of micron scale coatings, with apparent “gaps” between large island-like features which may still be present on a significantly reduced scale in the thinner coatings.

## Conclusions

We have demonstrated a novel and facile PVD setup for the controllable deposition of very thin  $\text{SiO}_2$  films on solid substrates under atmospheric pressure at relatively low temperatures. Our system allows deposition of a wide range of film thicknesses utilising very small amounts of PDMS rubber in a fast and cost-efficient manner. The deposited film thickness can be tightly controlled by varying the deposition temperature, the amount of PDMS used, as well as the heating rate, with more uniform depositions achieved at lower temperatures. Reproducible  $\text{SiO}_2$  layers as thin as  $25\text{--}50\text{ nm}$  were achievable as a result of this investigation, while also achieving much thicker coatings of  $50$  to greater than  $2000\text{ nm}$ . Our work investigated three of the critical factors relevant to the deposition process and deposited film parameters and thus provides an important starting point for the further exploration and exploitation of the process.

In addition, our process set-up and subsequent investigations provide a blueprint for performing depositions on substrates and nanostructures susceptible to deformation or other adverse effects at high temperatures and/or under high heating rates. The depositions achievable at low temperatures and low heating rates show our system to be highly compatible with a diverse array of substrates including flexible substrates and nanostructured substrates.



Future work will involve PVD deposition of  $\text{SiO}_2$  on ordered, high aspect ratio nanostructures to produce uniform and conformal coatings. Preliminary work has shown this technique to be capable of coating 400 nm tall nanorods with good conformality, and the  $\text{SiO}_2$  coating displays DNA binding capabilities in controlled tests. We hope to then utilise these coated nanostructures for biomedical diagnostic applications.

## Author contributions

Paul Cannon: Methodology, validation, formal analysis, investigation, data curation, writing – original draft, visualization, funding acquisition. Enda McGlynn: conceptualization, methodology, resources, writing – review & editing, supervision, funding acquisition. Brian Freeland: writing – review & editing, supervision. Jennifer Gaughran: conceptualization, methodology, resources, writing – reviewing & editing, supervision, funding acquisition.

## Conflicts of interest

There are no conflicts to declare.

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