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# Microwave catalytic activities of $\text{MFe}_2\text{O}_4@ \text{CMT}$ (M = Ni, Co) supported catalysts for the degradation of dimethyl phthalate†

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Meso-macroporous  $\text{MFe}_2\text{O}_4@ \text{CMT}$  (M = Ni, Co) catalysts were synthesized by coating carbon microtubes (CMTs) employing a calcination method. The obtained materials  $\text{NiFe}_2\text{O}_4@ \text{CMT}$  (PCNF) and  $\text{CoFe}_2\text{O}_4@ \text{CMT}$  (PCCF) were characterized via X-ray powder diffraction (XRD), pore structure analysis, X-ray photoelectron spectroscopy (XPS), and scanning electron microscopy (SEM). The electromagnetic (EM) wave absorption of catalysts was measured and it was found that the maximum reflection loss value of PCCF and PCNF was about  $-41.50$  dB at a thickness of 1.85 mm and  $-24.70$  dB at a thickness of 6.55 mm, respectively. The composite catalysts were prepared for the microwave (MW)-induced Fenton-like catalytic degradation of dimethyl phthalate (DMP). The microwave catalytic activity of PCNF was higher than that of PCCF, which was closely related to its higher concentration of active species, better microwave-absorbing ability and high interaction between  $\text{NiFe}_2\text{O}_4$  and CMT. Moreover, the degradation kinetics could be well-fitted by the pseudo-first-order kinetic model. With an increase in the MW power, initial pH, catalyst dosage, and  $\text{H}_2\text{O}_2$  concentration, the DMP degradation rate initially increased and then decreased, while it declined continuously with an increase in the initial DMP concentration. The introduction of metal oxides increased the mobility of the surface oxygen, playing a crucial role in the generation of surface oxygen species. The catalysts maintained high stability after five reaction cycles. The overall findings provide new insight into PCCF and PCNF under MW irradiation for the degradation of DMP and other relevant organic pollutants.

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## 1 Introduction

Phthalate acid esters (PAEs) comprise a large family of chemical compounds extensively used as cellulose film coating, adhesives, and plasticizers in industrial production. Dimethyl phthalate (DMP) ester is a common short-chained ester from the class of PAEs, which has been detected in the natural environment including water and sediments.<sup>1</sup> DMP is relatively recalcitrant to biodegradation in the natural environment because of its benzene carboxylic group and its hydrolysis half-life of about 3 years.<sup>2</sup> Moreover, DMP can be bioconcentrated and biomagnified in the aquatic food chain. It is considered that the potential sources of DMP are mainly through the release of wastewater from production and processing activities and from the usage and disposal of materials containing PAEs.

Long-term exposure to DMP can cause functional disturbances in the nervous system and liver of animals. Also, it is suspected to have endocrine-disrupting activity and result in decreased fertility in human beings and other organisms. Because of its ecological toxicity and hazard, it has been listed as a priority organic pollutant by the U.S. Environmental Protection Agency because of its toxicological properties and potential risks to human health, wildlife, and the environment.<sup>3,4</sup> Thus, it is necessary to identify appropriate treatment technologies to remove DMP and remediate its adverse effects.<sup>5</sup>

The methods for the removal of DMP mainly include adsorption, electrocatalysis, photocatalysis, microwave catalysis, and other advanced oxidation processes (AOPs).<sup>6,7</sup> Among the many wastewater treatment technologies, adsorption technology stands out because of its flexible operation and design; however, it also has the drawback of adsorbent regeneration and the rerelease of adsorbed organics into the environment.<sup>8</sup> Photocatalysis and electrocatalysis technology present high removal efficiency but with high energy consumption.<sup>9,10</sup> The Fenton reaction, a type of highly efficient and widely used AOP, degrades persistent organic pollutants in water by activating  $\text{H}_2\text{O}_2$  to produce  $\cdot\text{OH}$ . However, it has a relatively low reaction efficiency and usually requires long reaction times to reach

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equilibrium. For faster reaction speeds, external energy such as UV-Vis light,<sup>11</sup> electricity<sup>12</sup> and microwaves (MW)<sup>13</sup> are often introduced. MW-induced catalytic oxidation (MICO) is regarded a promising AOP because of its high energy utilization, quick reaction rate, and high degradation efficiency.<sup>14,15</sup> It has been reported that appropriate MW-absorbing catalysts (*i.e.*, carbon materials, metals, and metal oxides) coupled with MW can facilitate the degradation efficiency of organic pollutants.<sup>16–18</sup> Liu *et al.*<sup>19</sup> proved that MW has an enhanced effect on the degradation of methylene blue (MB) by rice hull-based ferrite nanocomposites. It seems that efficient catalysts are extremely important to achieve a high MW catalytic performance.

Ferrite has the advantages of strong electromagnetic wave absorption and wide absorption band. The combination of ferrite with a porous carbon matrix can prevent aggregation of the ferrite to improve its electromagnetic wave absorption performance. Accordingly, Shu *et al.*<sup>20</sup> synthesized  $\text{ZnFe}_2\text{O}_4$ , graphene oxide, and multi-walled carbon nanotubes in a highly connected three-dimensional conductive network structure ternary mixture, which achieved the maximum reflection loss (RL) of  $-22.2$  dB. Wang *et al.*<sup>21</sup> coated  $\text{NiFe}_2\text{O}_4$  with polyaniline (PANI), obtaining the maximum RL of  $-42.5$  dB. Zhang *et al.*<sup>22</sup> encapsulated  $\text{MnFe}_2\text{O}_4$  into the tubular structure of aragonite, resulting in a turbine effect and the maximum RL of  $-36$  dB. Carbon microtubes (CMT) based on corncob with a tubular structure and low density were used as a catalyst carrier, which could improve the interaction between the catalyst and the contaminant, and further facilitate electron transfer to enhance the photocatalysis performance.<sup>23</sup> However, the use of CMT as a carrier of ferrite to form light MW-absorbing materials has been rarely studied.

In this study, we report a strategy for the preparation of porous-structured ferrite supported on CMT ( $\text{MFe}_2\text{O}_4$ @CMT (M = Ni, Co)) catalysts, which were based on the use of newly made

CMT as a hard template. The as-prepared materials were utilized as MW-induced Fenton-like catalysts and their catalytic degradation behavior for DMP was compared. The role of pH, MW power, catalyst dosage,  $\text{H}_2\text{O}_2$  dosage, and DMP concentration in the MW catalytic degradation process was studied and the probable mechanism was also proposed.

## 2 Method and materials

### 2.1 Materials

Corn cob powder was obtained from Yanggu Ruikang Technology Co., Ltd (China).  $\text{Fe}(\text{NO}_3)_3$ ,  $\text{Co}(\text{NO}_3)_2$ , and DMP were purchased from Shanghai Aladdin Biochemical Technology Co., Ltd. Hydrogen peroxide ( $\text{H}_2\text{O}_2$ ) was purchased from Shanghai Sinopec Chemical Reagent Co., Ltd (China). Yier sea salt was purchased from Haoyangze Aquarium Pet Supplies, Nanshan District, Shenzhen City (China). All solutions used in this study were prepared to have a water conductivity of  $18.2 \text{ M}\Omega \text{ cm}^{-1}$ . All chemical reagents were of analytical grade and used without further refinement. High-purity nitrogen (purity > 99.999%) was purchased from Ningbo Baifang Gas Co., Ltd (China). Mixed cellulose ester filters with a pore size of  $0.45 \mu\text{m}$  were purchased from Shanghai Xingya Purification Plant (China).

### 2.2 Preparation of catalyst

Corn cob powder was designated as CC, and acidified corn cob powder was prepared according to our previous work,<sup>23</sup> which was designated as AC. The precursor aqueous (PA) solution was obtained by mixing 100 mL 1.5 M  $\text{Fe}(\text{NO}_3)_3$  with 100 mL 0.75 M  $\text{Co}(\text{NO}_3)_2$  or  $\text{Ni}(\text{NO}_3)_2$ , respectively. A total of 50 g acidified corn cob powder was mixed with the PA solution, stirring at a constant temperature of  $70 \text{ }^\circ\text{C}$  for 2 h. Then, it was kept at  $60 \text{ }^\circ\text{C}$  for 24 h, and finally dried at  $100 \text{ }^\circ\text{C}$  to yield a dry precursor. The dried precursor powder was further heated to

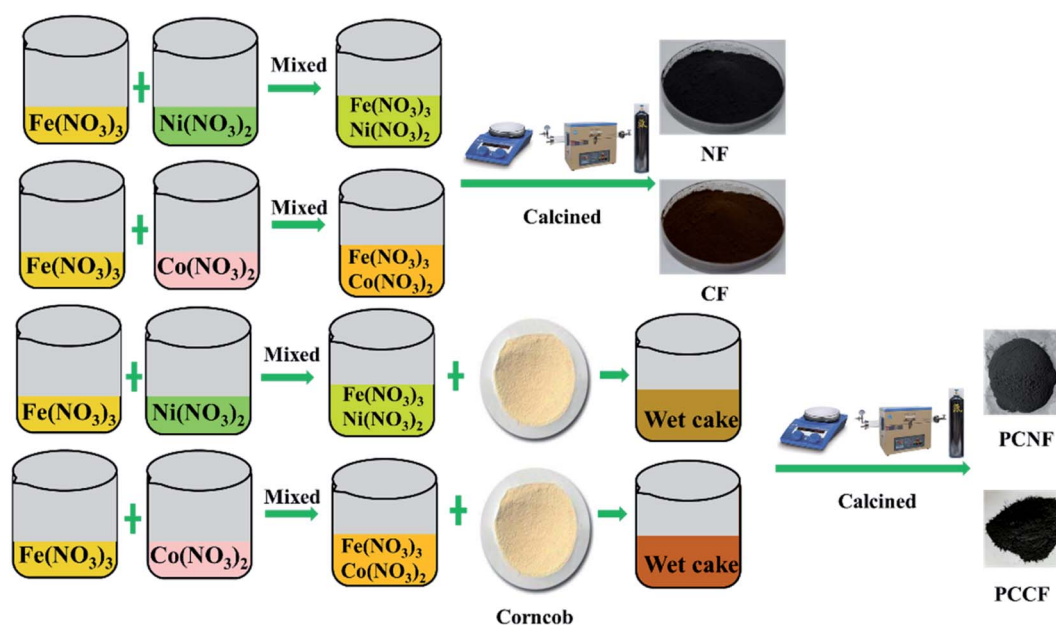


Fig. 1 Preparation of NF, CF, PCNF, and PCCF.



750 °C for 2 h at a rate of 1 °C min<sup>-1</sup> in a tube furnace under a high-purity nitrogen atmosphere. After heating, the products were designated as PCCF (powder of CoFe<sub>2</sub>O<sub>4</sub> coated on corncob) and PCNF (powder of NiFe<sub>2</sub>O<sub>4</sub> coated on corncob), respectively. Using the same method, CoFe<sub>2</sub>O<sub>4</sub> and NiFe<sub>2</sub>O<sub>4</sub> were synthesized without corncob powder, which were designated as CF and NF, respectively. The experimental process is shown in Fig. 1.

### 2.3 Degradation process

The adsorption and subsequent degradation of DMP by CC, CF, NF, PCCF and PCNF were measured. Firstly, 50 mL of 500 µg L<sup>-1</sup> DMP solution and 0.1 g catalyst were placed in a glass beaker, followed by 10 min of ultrasonic to equilibrate the catalyst. The suspension was initially stirred in the dark at a speed of 250 rpm, and subsequently 120 min. Then, the supernatant (3 mL) was centrifuged at the speed of 10 000 rpm for 5 min, and then the extent of DMP adsorption by the catalyst was determined. The characteristic absorption peaks of the DMP functional groups were analyzed by scanning the sample with a UV-2550 spectrophotometer (Shimadzu Corporation of Japan) in the wavelength range of 200–900 nm, while the concentration of the DMP solution was calculated using the maximum absorption peak (229 nm and 275 nm) according to the Lambert–Beer formula. To evaluate the catalytic activity, an identical experiment was performed. Hydrogen peroxide (10 mg) was added after the equilibration step, and then the catalyst and DMP solution were exposed to MW at a frequency of 2450 MHz. To prevent overheating bumping, the MW oven was closed for 15 s, and then reheated after an interval of 15 s. Subsequently, a sample of the DMP solution was removed and subjected to the same analysis, as described above. To ensure the consistency of the solid–liquid ratio, only one sample was taken from each experiment. All experiments were conducted in triplicate and the average value was taken. The same procedure was repeated with simulated wastewater instead of ultrapure water. The content of the main elements in the simulated wastewater is shown in Table S1 (ESI†).

### 2.4 Characterization

The composition of the catalyst was determined by X-ray diffraction (XRD) using a D/Max 2550 X-ray diffractometer (Rigaku, Japan). The microstructure of the catalyst was measured *via* scanning electron microscopy (SEM) (Zeiss Merlin FESEM, Germany). The specific surface area of the catalyst was tested using the Brunauer–Emmett–Teller (BET) method (AUTOSORB-IQ-MP, US). All data were analyzed using a Quantachrome ASiQWin (version 3.01). High-resolution X-ray photoelectron spectroscopy (XPS) was performed using a pass energy of 20 eV, with a step size of 0.02 eV. The UHV chamber base pressure was maintained at <10<sup>-9</sup> Mbar throughout the measurements. To compensate for any type of charging effect, the C 1s binding energy peak at 284.5 eV was used as a reference. The electromagnetic (EM) parameters were determined using an HP8720ES vector network analyzer (Agilent, USA) using a *T/R* coaxial line method in the EM wave frequency range of 1–

18 GHz with a thickness of 2 mm, using paraffin as the substrate. The filling rate was 50%. The relative complex permittivity ( $\epsilon = \epsilon' - j\epsilon''$ ) and permeability ( $\mu = \mu' - j\mu''$ ) were calculated from the measured *T/R* coefficients. The measurement errors were less than 10% when  $\epsilon' < 15$ . The concentration of leached metal ions of the materials after the degradation was measured by ICP-AES (Optima 2000, PerkinElmer Co., Ltd, USA), and the metal leaching ratio was calculated using eqn (1):

Metal leaching ratio (%) =

$$\frac{\text{amount of metal leached in solution (mg)}}{\text{amount of metal in catalyst (mg)}} \times 100\% \quad (1)$$

## 3 Results and discussion

### 3.1 Catalyst characterization

**3.1.1 Composite determination.** The XRD patterns of the as-fabricated samples are exhibited in Fig. 2a. It can be observed that the characteristic reflection peaks of AC, PCNF, and PCCF appeared at the  $2\theta$  values of 20.64° ( $d_{100}$ ), 26.43° ( $d_{011}$ ), 36.15° ( $d_{110}$ ), 43.099° ( $d_{211}$ ), and 62.04° ( $d_{204}$ ), corresponding to SiO<sub>2</sub> (JCPDF # 74-1811), similar to the finding reported for corncob in which SiO<sub>2</sub> was preserved during calcination.<sup>23,24</sup> However, the main peaks shift to higher  $2\theta$  values when loaded with NiFe<sub>2</sub>O<sub>4</sub> or CoFe<sub>2</sub>O<sub>4</sub>, indicating a decrease in the crystal interplanar distances of SiO<sub>2</sub>. Besides, the decrease in the diffraction peak intensities is probably owing to the dilution of the crystal structure of SiO<sub>2</sub> by doping with NiFe<sub>2</sub>O<sub>4</sub> or CoFe<sub>2</sub>O<sub>4</sub>. In the PCCF sample, the XRD  $2\theta$  peaks at 18.28° ( $d_{111}$ ), 30.08° ( $d_{220}$ ), 35.43° ( $d_{311}$ ), 37.05° ( $d_{222}$ ), and 45.05° ( $d_{400}$ ) can be ascribed to the CoFe<sub>2</sub>O<sub>4</sub> phase (JCPDF # 22-1086). In the PCNF sample, the diffraction signals at the  $2\theta$  values of 18.33° ( $d_{111}$ ), 30.15° ( $d_{220}$ ), 35.15° ( $d_{311}$ ), 37.15° ( $d_{222}$ ), and 44.16° ( $d_{400}$ ) are ascribed to the NiFe<sub>2</sub>O<sub>4</sub> phase (JCPDF # 87-2336). The average crystallite size of NiFe<sub>2</sub>O<sub>4</sub> is smaller than that of CoFe<sub>2</sub>O<sub>4</sub> according to the Scherrer equation, which is more conducive to the formation of structural defects, resulting in an improvement in the oxidative reaction.

**3.1.2 Pore structure analysis.** The pore structure of PCCF and PCNF was analyzed *via* nitrogen adsorption–desorption curves (Fig. 2b). All the curves show a type IV pattern with an H<sub>3</sub> hysteresis loop, indicating that PCCF and PCNF are mesoporous materials.<sup>25</sup> The BET specific surface area, pore volume, and the pore diameter of PCCF and PCNF are summarized in Table S2.† The BET specific surface area of PCCF and PCNF is 8.995 and 11.22 m<sup>2</sup> g<sup>-1</sup>, respectively. After the introduction of NiFe<sub>2</sub>O<sub>4</sub>, the BET specific surface area increased, which is attributed to the fact that NiFe<sub>2</sub>O<sub>4</sub> was successfully supported on CMT and increased the amount of pores. Fig. 2c shows the pore distribution of PCCF and PCNF calculated using the BJH method. It can be found that the introduction of NiFe<sub>2</sub>O<sub>4</sub> has no significant influence on the pore structure of the samples. The total pore volume of PCCF and PCNF is 0.289 and 0.323 cm<sup>3</sup> g<sup>-1</sup>, respectively. Obviously, compared with PCCF, PCNF possesses a larger pore volume, which may be ascribed to the fact that NiFe<sub>2</sub>O<sub>4</sub> entered the pore of CMT and enlarged the pore volume



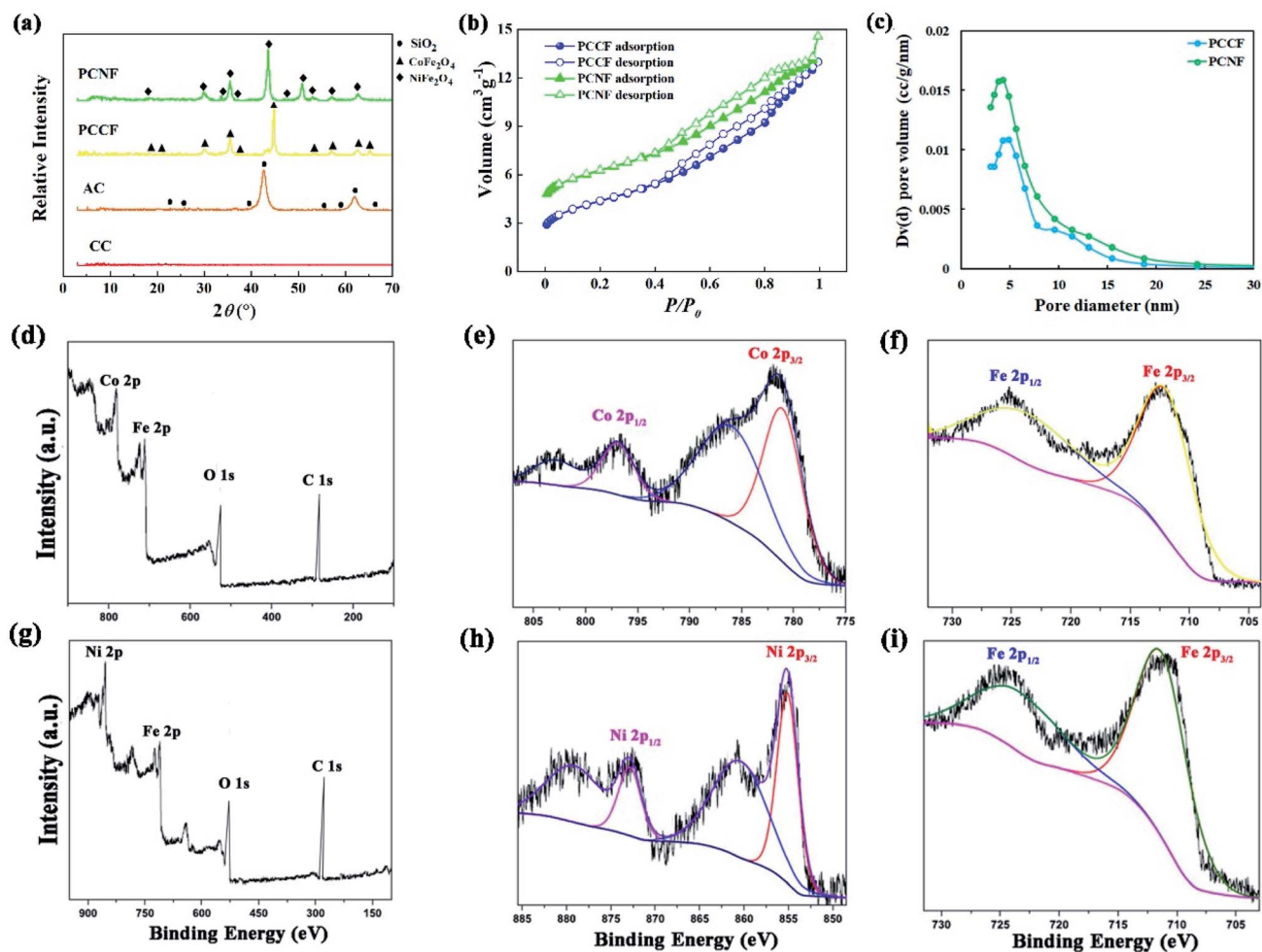


Fig. 2 Determination of the composite and pore structure of  $MFe_2O_4@CMT$  ( $M = Ni, Co$ ): (a) XRD patterns, (b) nitrogen adsorption–desorption isotherms, and (c) pore size distribution calculated by BJH method. XPS spectra of PCCF (d) wide scan, (e) Co 2p, and (f) Fe 2p. XPS spectra of PCNF (g) wide scan, (h) Ni 2p, and (i) Fe 2p.

of its pore size to 9 nm during the preparation process, thus enhancing the total pore volume of PCNF.<sup>26</sup>

**3.1.3 The elemental valences of the materials.** To investigate the components, material composition and elemental valences in the synthesized sheets and plates, XPS analysis of PCCF and PCNF was carried out (Fig. 2d–i). Fig. 2d shows the wide scan survey spectrum of PCCF, which shows the presence of Co 2p, Fe 2p, O 1s, and C 1s. The deconvoluted Co 2p spectrum (Fig. 2e) indicates the existence of a doublet at 781.03 eV and 796.8 eV. The two shake-up satellite peaks at 785.9 eV and 802.8 eV indicate the strong presence of  $Co^{2+}$ .<sup>27</sup> Fig. 2f shows the characteristic signals of Fe 2p at 711.9 eV and 723.5 eV, which are due to  $Fe\ 2p_{3/2}$  and  $Fe\ 2p_{1/2}$ , respectively. This result indicates the presence of  $Fe^{3+}$  and  $Co^{2+}$  in PCCF. The wide scan XPS survey spectrum of PCNF (Fig. 2g) indicates the presence of Ni 2p, Fe 2p, O 1s, and C 1s. After deconvolution of the Ni 2p spectrum (Fig. 2h), it showed four peaks. There are two main peaks at binding energies of 855.1 eV and 872.8 eV, which are followed by two shake-up satellites at the higher binding energy side centered at 860.4 eV and 879.1 eV. These results are in

agreement with the literature.<sup>27</sup> Fig. 2i shows the signals of Fe 2p at 711.2 eV and 723.3 eV for  $Fe\ 2p_{3/2}$  and  $Fe\ 2p_{1/2}$ , respectively. Thus, the XPS analysis confirmed the presence of the  $CoFe_2O_4$  and  $NiFe_2O_4$  phases in our materials.

**3.1.4 Microscopic morphology analysis.** The morphology of PCCF and PCNF was characterized *via* SEM (Fig. 3). For the corncob sample, it has a tubular structure with a diameter of 10  $\mu m$ , and the surface of its tubes became rough after acidification due to the release of some soluble substances.  $CoFe_2O_4$  and  $NiFe_2O_4$  were both loaded on the surface of the corncob powder and agglomerated. The size of  $CoFe_2O_4$  in PCCF was mainly 1  $\mu m$ , while that of  $NiFe_2O_4$  in PCNF was 5  $\mu m$  or even larger. This is because the diameter of the tubular structure of the corncob powder is about 10  $\mu m$ , which reduced the confinement effect and resulted in more crystal agglomeration. According to the elemental energy spectrum, PCCF mainly contained C, Fe, Co, and O elements, while PCNF mainly contained C, Fe, Ni, and O elements. Combined with the microstructure and XRD results,  $CoFe_2O_4$  and  $NiFe_2O_4$  were successfully loaded on the surface of the corncob, but crystal agglomeration occurred in PCCF and PCNF.



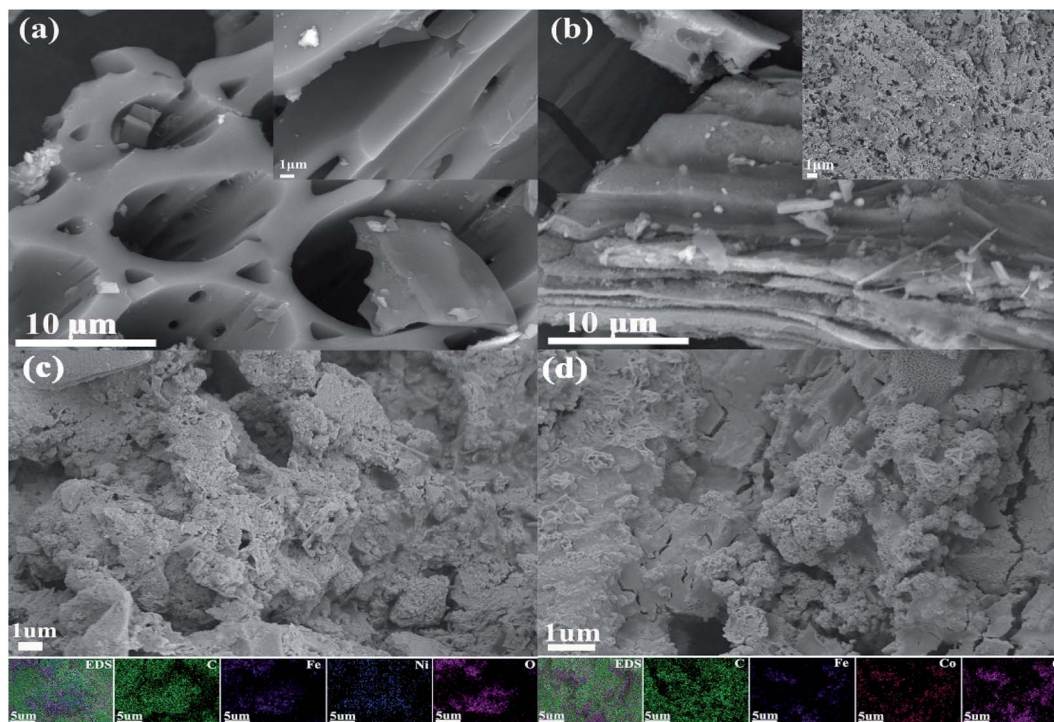


Fig. 3 SEM images and element mapping data (EDS) of (a) CC, (b) AC, (c) PCCF, and (d) PCNF.

### 3.2 MW absorption of ferrite/corncob composite

According to the transmission line theory, the RL of EM wave absorbers can be evaluated from the measured complex permittivity and permeability using the following equations:<sup>28</sup>

$$Z_{in} = Z_0 \sqrt{\frac{\mu}{\epsilon}} \tanh \left[ j \frac{2\pi f d}{c} \sqrt{\mu \epsilon} \right] \quad (2)$$

$$RL \text{ (dB)} = 20 \log \left| \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \right| \quad (3)$$

where  $Z_{in}$  and  $Z_0$  are the impedances of the absorber and air, respectively.  $\epsilon$  and  $\mu$  are the complex permittivity and permeability of the absorber, respectively.  $f$  is the frequency of EM waves,  $d$  is the thickness of the absorber, and  $c$  is the velocity of light. The permittivity and permeability of CC, PCCF, and PCNF are shown in Fig. S1,† indicating that the EM wave absorption of PCCF and PCNF was mainly induced by magnetic loss. The RL of the ferrite/corncob composites as a function of thickness was analyzed to obtain the optimum thickness and frequency for EM absorption (Fig. 4). The maximum RL value of CC, PCCF, and PCNF was about  $-2.00$  dB at the thickness of 1.75 mm,  $-41.50$  dB at the thickness of 1.85 mm, and  $-24.70$  dB at the thickness of 6.55 mm, respectively. This indicates the weak EM absorption by CC, whereas PCCF and PCNF displayed strong EM absorption.

In addition, the RL of the  $M\text{Fe}_2\text{O}_4@\text{CMT}$  ( $M = \text{Ni}, \text{Co}$ ) composites as function of thickness and frequency was measured to obtain the optimum thickness and frequency for EM absorption. There are two maximum bandwidth values of PCCF in the bandwidth–thickness curve. The first maximum

bandwidth for an RL of  $<-10$  dB appears at a thickness in the range of 1.25–3.45 mm, with a value of 4.03 GHz; another appears at the thickness of 3.95–10.00 mm with the maximum bandwidth of 5.04 GHz for RL of  $<-10$  dB and 10.00 GHz for RL of  $<-5$  dB. It was also found that the maximum width of PCNF for RL of  $<-5$  dB with a value of 2.01 GHz is at the thickness of 2.05–2.65 mm, and RL of  $<-10$  dB with a value of 2.69 GHz at the thickness of 5.95–10 mm, while 0 GHz for CC for RL  $<-5$  dB at a thickness in the range of 0–10 mm. These results verified that PCCF and PCNF showed higher permittivity and permeability to absorb EM waves than that of CC. Specifically, introducing metal ions in CMT could substantially improve its microwave absorption capacity. PCNF displayed the strongest reflection loss, suggesting its best microwave absorption property. The smaller particles of  $\text{NiFe}_2\text{O}_4$  will accelerate the space-charge polarization among the metal ions, resulting in an improvement in the dielectric loss value.

Among the EM wave-absorbing materials (Table S3†), due to the absence of magnetic components, CC showed a lower absorption of EM waves than traditional EM wave absorbers, such as porous carbon fiber,<sup>29</sup> porous Fe,<sup>30</sup> and rice husk ash (SiC).<sup>31</sup> However, the maximum RL of PCCF and PCNF was considerably higher than that of Fe pillared in halloysite<sup>22</sup> and montmorillonite blended with polymers.<sup>32</sup> In conclusion,  $M\text{Fe}_2\text{O}_4@\text{CMT}$  ( $M = \text{Ni}, \text{Co}$ ) is a potential EM wave absorber.

### 3.3 MW-assisted Fenton-like catalysis by ferrite/corncob composite

The pretreatment of PAEs for their determination by GC-MS is complex. It was found that there are two conjugated  $\pi$  bonds



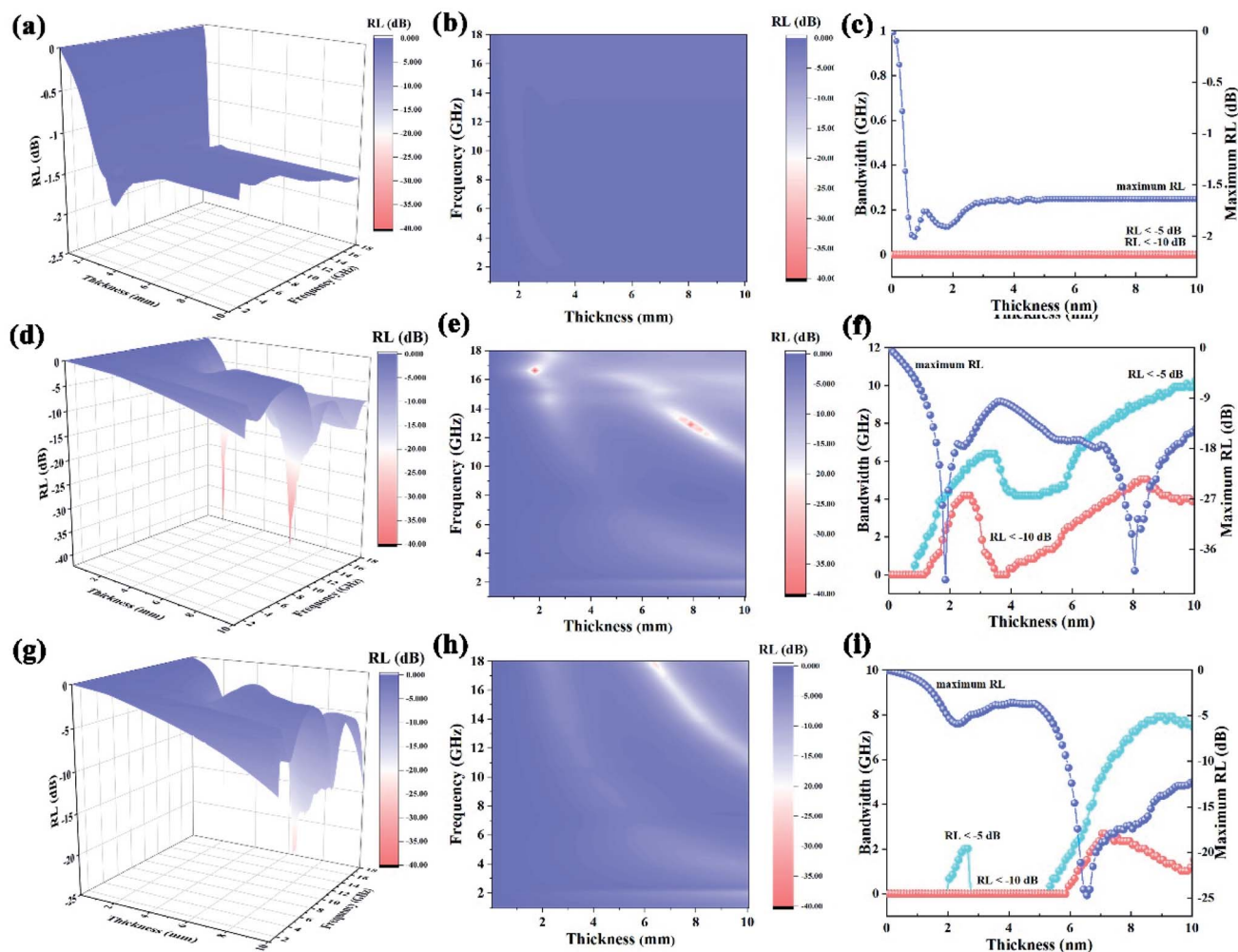


Fig. 4 RL of  $M\text{Fe}_2\text{O}_4@\text{CMT}$  ( $M = \text{Ni}, \text{Co}$ ) composite as a function of thickness and frequency: (a–c) CC, (d–f) PCCF, and (g–i) PCNF, respectively.

(phenyl ester and benzene ring) in the DMP structure (Fig. S2<sup>†</sup>), which have strong absorption peaks at 229 nm and 275 nm in its UV-Vis spectrum, respectively. The standard curve fitted these two peaks well (Fig. S3a<sup>†</sup>), and thus the DMP concentration before and after degradation could be analyzed based on the intensity of these two absorption peaks in its UV-Vis spectrum (Fig. 5). The difference in the decomposition rates at the two wavelengths indicated that the structure of DMP was destroyed. For the fresh water system, the ultraviolet absorption intensity of the two groups decreased gradually with an extension in the irradiation time. For PCCF, after 6 min of MW, the DMP spectrum near 275 nm was almost a straight line, and the absorption peak near 229 nm was red-shifted, but the absorption peak before 210 nm became stronger, which was mainly due to the small molecules or ions produced during the degradation of DMP. For PCNF, the absorption peak of small molecules was stronger, indicating that PCNF had more efficient catalytic activity, where the phenyl ester group degraded to a benzene ring, and then mineralized into small molecules or ions. In the simulated seawater, due to the presence of multiple ions, there were more peaks before 210 nm. Meanwhile, the degradation efficiency of phenyl ester and

benzene groups weakened with the number of free radicals reduced. However, the red shift in the absorption peak at 229 nm still existed, indicating that degradation still occurred.

To study the MW catalytic activity of PCCF and PCNF, experiments on the degradation of DMP by different catalysts were carried out. DMP cannot be degraded without MW irradiation, and only less than 15% of DMP could be removed within 6 min (Fig. 6a and b), indicating that adsorption cannot efficiently remove DMP in a short time. Besides, the CC template showed negligible DMP degradation (5%) under MW irradiation. The DMP degradation efficiency rapidly increased to 95% and 99% after 6 min in the PCCF/MW/ $\text{H}_2\text{O}_2$  and PCNF/MW/ $\text{H}_2\text{O}_2$  systems, respectively, illustrating that the formation of a meso-macroporous structure ( $M\text{Fe}_2\text{O}_4@\text{CMT}$  ( $M = \text{Ni}, \text{Co}$ )) will promote the diffusion of reactant molecules in the active sites, and thus improve the catalytic performance (Fig. 6c and d), respectively. Our previous work showed that carbon microtubes have a much larger interlayer spacing than that of commercial graphite, which may be beneficial for ion transmission.<sup>23</sup> The apparent width of the diffusion layer for the DMP solution can be calculated as follows:<sup>33</sup>



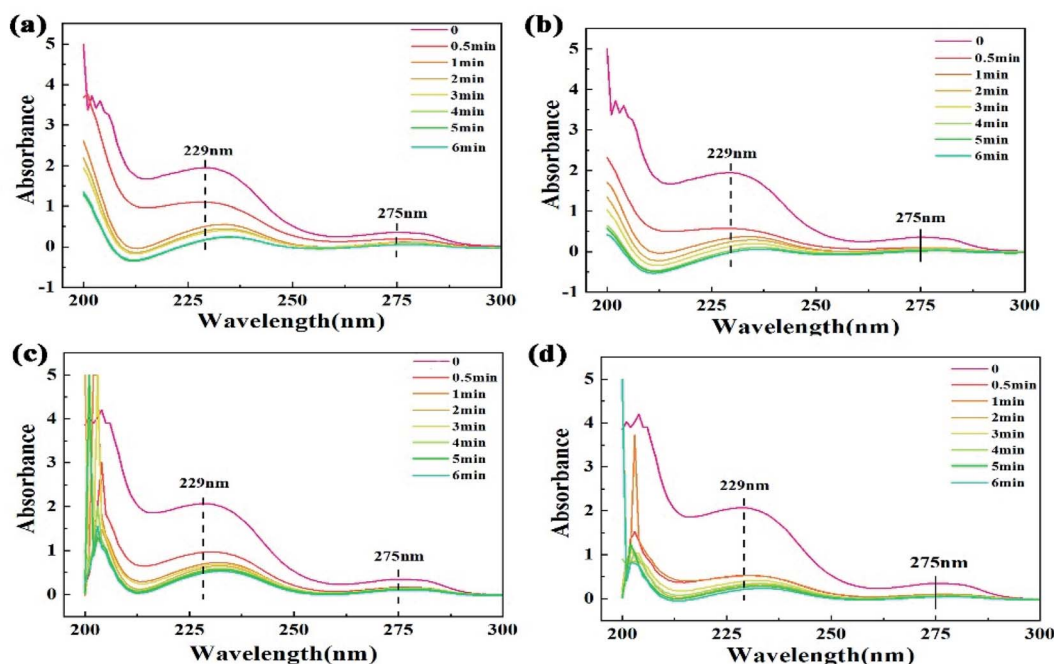
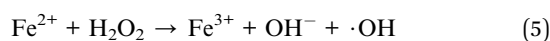


Fig. 5 UV-Vis spectrum of DMP after MW-enhanced Fenton-like degradation by: (a) PCCF and (b) PCNF in fresh water, (c) PCCF and (d) PCNF in simulated real wastewater.

$$\text{Apparent width of the diffusion layer} = 1.548 \frac{\mu^{1/6} L^{1/2} D^{1/3}}{\rho^{1/6} \nu^{1/2}} \quad (4)$$

where  $\rho$ ,  $\mu$  and  $\nu$  are the density in  $\text{kg m}^{-3}$ , viscosity of the solution in  $\text{kg m}^{-1} \text{s}^{-1}$ , and linear rate of the solution inside the electrochemical cell in  $\text{m s}^{-1}$ , respectively.  $L$  is the hydraulic diameter in m, which is defined as the free area for flow over the wet perimeter.  $D$  is the diffusion coefficient. When a carbon microtube electrode was used, the hydraulic diameter and the width of the diffusion layer of the  $\text{MFe}_2\text{O}_4\text{@CMT}$  ( $\text{M} = \text{Ni}, \text{Co}$ ) decreased and the attack of DMP molecules by hydroxyl radicals became easier, leading to an increase in the oxidation rate, considering only the mass transfer improvement. Thus, the reaction rate of PCNF and PCCF was faster than that of NF and CF, confirming that the formation of a mesoporous-macropore structure will promote the diffusion of reactant molecules to the active sites.

In the case of CF, there was a decrease of 5% of phenyl ester and 6% of benzene ring concentration after 1 min, which changed to 18% of phenyl ester and 14% of benzene ring within 6 min MW assistance. In the case of NF, the concentration of phenyl ester and benzene ring decreased by 38% and 22% within 1 min MW assistance, respectively. However, subsequently, the concentration of phenyl ester and benzene ring did not decrease significantly and remained stable within 6 min. Thus, it can be concluded that the degradation of DMP was promoted by the MW-induced reaction with  $\text{MFe}_2\text{O}_4$  ( $\text{M} = \text{Ni}, \text{Co}$ ). The reaction in the Fenton system is based on eqn (5), as follows:



The valence of  $\text{Fe}^{3+}$  changed between 2 and 3 in the  $\text{CoFe}_2\text{O}_4$  or  $\text{NiFe}_2\text{O}_4$  degradation process.<sup>34</sup> There is one more free orbit and outer electron in Ni than that in Co, promoting the valence conversion of  $\text{Fe}^{3+}$ . Thus, the DMP degradation efficiency of NF was higher than that of CF. Secondly, the molecular thermal motion and system temperature increased with MW radiation.<sup>35</sup> The temperature of  $1000^\circ\text{C}$ <sup>36</sup> could be reached within 3 min MW irradiation with ferrite, forming hotspots and accelerating the molecular motion to degrade DMP.

When coated with  $\text{CoFe}_2\text{O}_4$  or  $\text{NiFe}_2\text{O}_4$ , the catalyst displayed an even higher degradation efficiency of 90% and 99% of phenyl ester by PCCF and PCNF, respectively. Therefore, this type of corncob loaded with  $\text{CoFe}_2\text{O}_4$  or  $\text{NiFe}_2\text{O}_4$  has wide application for the degradation of refractory pollutants.

When applied to simulated seawater, the PCCF and PCNF still maintained a high degradation rate (Fig. 6e and f), respectively. Degradation rate by PCCF was 65% after 1 min, and that of PCNF was 78% for phenyl ester. The maximum degradation rate by PCCF and PCNF was 70% and 90% after 6 min, respectively.

The results of the kinetic studies on the degradation of DMP are shown in Fig. S3b and Table S4.† All the kinetic equations obtained from the different catalysts follow the pseudo-first-order model. The calculated rate constant ( $k_{\text{obs}}$ ) values are 0.3975, 0.8902, 0.1561, and 0.3043 for PCCF, PCNF, PCCF and PCNF in salinity, respectively. A higher rate constant leads to a faster reaction rate, illustrating that the DMP degradation rate in the  $\text{NiFe}_2\text{O}_4\text{@CMT}/\text{MW}$ -induced system is the fastest, which verifies that  $\text{NiFe}_2\text{O}_4\text{@CMT}$  possessed the highest catalytic activity. The rate constant was slightly reduced in the salinity system compared with that in the fresh water system. This is



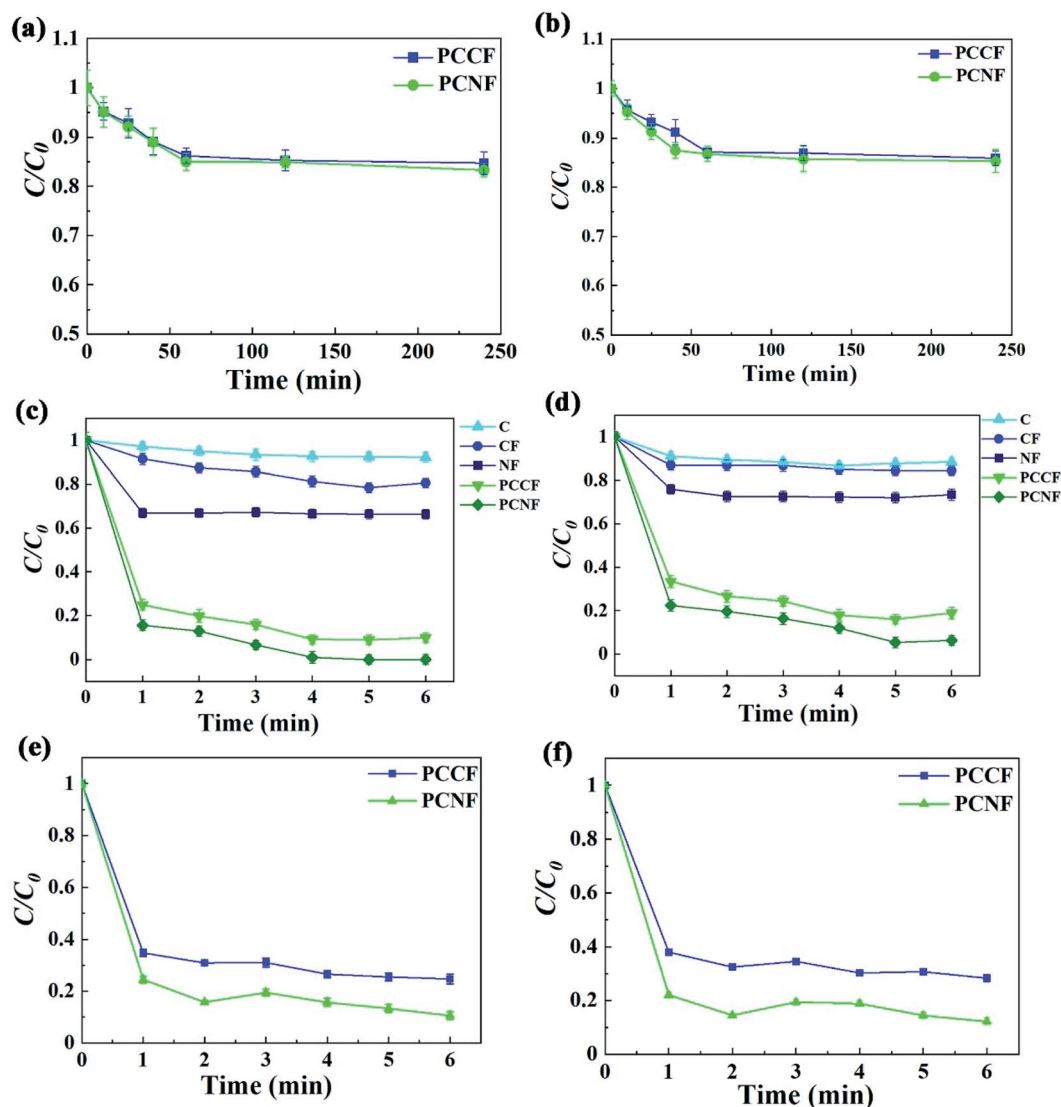


Fig. 6 Adsorption curves of DMP by PCCF and PCNF at: (a) 229 nm and (b) 275 nm. MW-enhanced Fenton-like process for DMP by CC, CF, NF, PCCF and PCNF at: (c) 229 nm and (d) 275 nm. MW-enhanced Fenton-like process for DMP by PCCF and PCNF in simulated real wastewater at: (e) 229 nm and (f) 275 nm.

because the degradation reaction is a free radical reaction and the ions in the salinity system would react with the free radicals. Thus, the concentration of free radicals reacting with DMP molecules was reduced, thus reducing the degradation efficiency.<sup>37</sup> Simultaneously, it can be seen that PCNF was less affected by ions than PCCF because Ni contained one more vacant orbital than Co and could bind with the ions, reducing the probability of the ions bonding with free radicals.<sup>38</sup> Wang *et al.*<sup>26</sup> predicted that the hollow structure of carbon microtubes with a micron size and large aspect ratio reduces the radial stress, presents good electrical conductivity, and a large number of mass transfer pathways. Our previous work tested the electrochemical impedance spectroscopy (EIS) of the prepared photocatalyst, confirming that the confinement effect of CMT could improve the separation and transfer of electron-hole pairs to improve the degradation efficiency.<sup>23</sup> This material also

showed a higher degradation performance than that in the related literature (Table S5<sup>†</sup>).

### 3.4 MW-assisted Fenton-like degradation of DMP with different factors

**3.4.1  $H_2O_2$  concentration.** The concentration of  $H_2O_2$  in the solution directly affects the yield of  $\cdot OH$ . With an increase in  $H_2O_2$  concentration, the mass transfer rate and the degradation rate of DMP increased (Fig. 7a and b), respectively. This may be due to the fact that more hydroxyl radicals were produced with an increase in  $H_2O_2$  concentration, resulting in a higher DMP degradation efficiency. However, a further increase in the addition of  $H_2O_2$  (more than  $300 \text{ mg L}^{-1}$  for PCCF and  $200 \text{ mg L}^{-1}$  for PCNF) decreased the degradation rate mainly because of the consumption of the produced  $\cdot OH$  by excess  $H_2O_2$ , as follows:



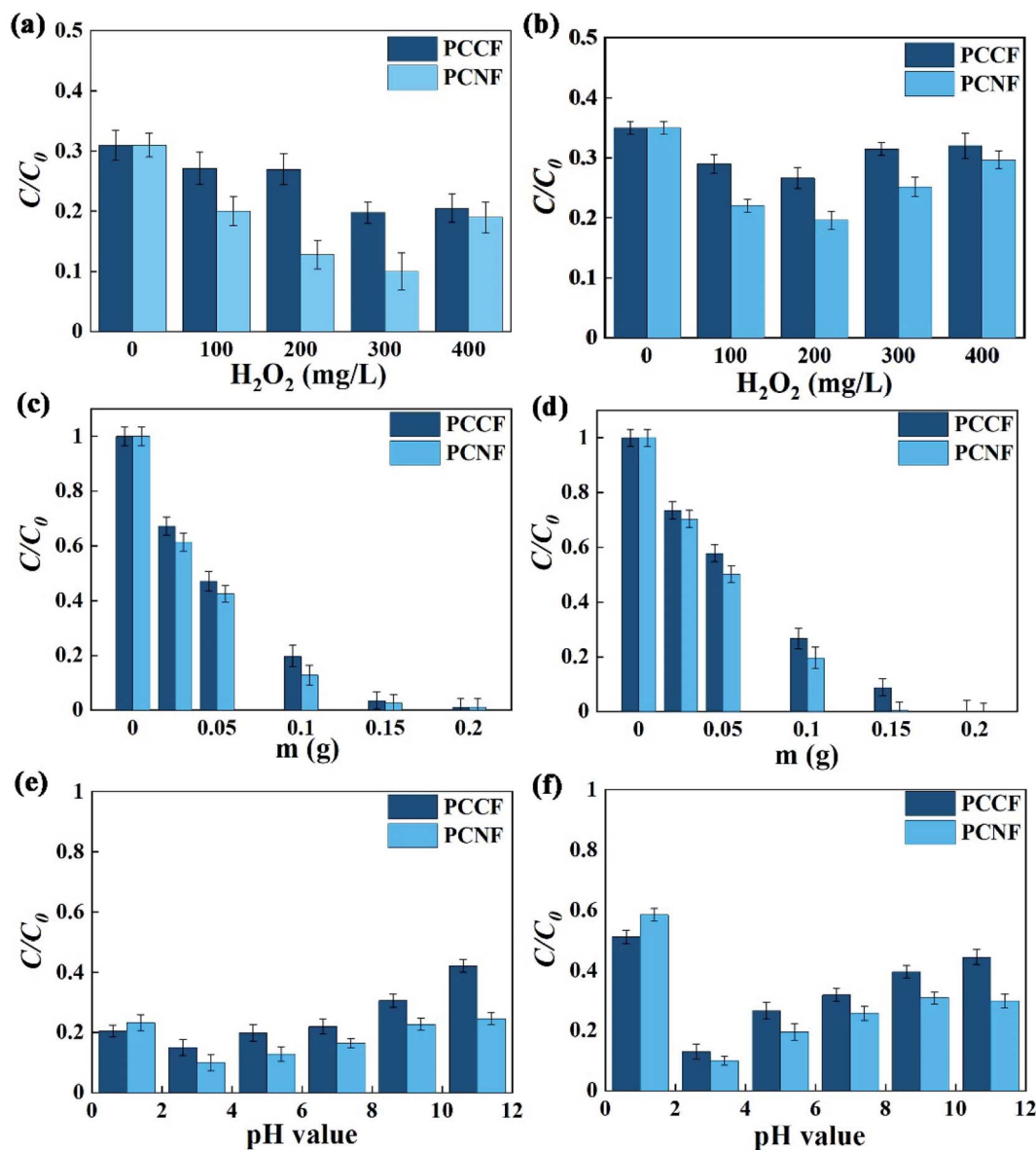
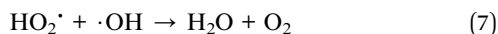
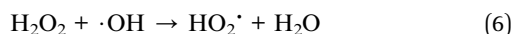


Fig. 7 Effect of different factors on the MW-enhanced Fenton-like performance,  $H_2O_2$  concentration at: (a) 229 nm and (b) 275 nm; catalyst dosage at: (c) 229 nm and (d) 275 nm; and pH value at: (e) 229 nm and (f) 275 nm.



A certain DMP degradation rate without  $H_2O_2$  was observed, indicating that the degradation of DMP not only involved  $\cdot OH$  oxidation, but may also be direct oxidation, which required the catalytic degradation mechanism of DMP by PCCF and PCNF to be investigated.

**3.4.2 Catalyst dosage.** The catalyst dosage affects the amount of active sites and the content of  $Fe^{3+}$ , thus affecting the degradation rate. The larger the catalyst dosage, the more active species generated and more DMP degraded under the same condition (Fig. 7c and d). When the maximum catalyst dosage

was 0.20 g, the degradation rate of both PCNF and PCCF reached more than 99%. Nevertheless, excessive catalyst will cover the activated sites and interfere with MW transmission or absorption, resulting in a decrease in the DMP degradation rate.<sup>39</sup> The optimal dosage of PCCF in this study was 0.15 g, which was the same for PCNF. Due to the differences in the atomic structure of  $NiFe_2O_4$  and  $CoFe_2O_4$  mentioned above,  $NiFe_2O_4$  promoted the degradation reaction, and thus the degradation rate of PCNF was higher than that of PCCF with the same amount of catalyst.

**3.4.3 pH value.** The initial pH value plays a significant role in the removal of DMP, which may be due to its influence on the surface properties of the catalyst and the formation of some active sites. The degradation rate increased with an increase in the initial pH when the pH was <3.0 and decreased at a higher



pH (Fig. 7e and f). At pH = 3.0, the degradation rate became the highest, indicating that acidic condition is conducive for the generation of acidic phenolic hydroxyl groups, which will react with hydroxyl radicals to promote the decomposition reaction.<sup>40</sup> Besides, when the solution pH is high, the oxidizing ability of the valence-hole on the catalysts surface will decline, leading to a reduction in the amount of  $\cdot\text{OH}$ .<sup>41</sup> Under alkaline conditions, iron ions precipitated, which also inhibited the catalytic process. At pH = 1, the degradation rate of the benzene ring of DMP was more affected by pH than that of the phenyl group. This is because the benzene ring formed a  $\pi$  bond under acidic conditions, which is more stable than the phenyl ester group<sup>42</sup> and more difficult to degrade. At the end of the degradation, the pH value of the DMP solution was higher than that of the initial DMP solution (Fig. S3c†), which means that the degradation process consumes  $\cdot\text{OH}$ , resulting in an increase in the pH value of the solution.

**3.4.4 Salinity.** Real wastewater contains many ions, which can also influence the degradation rate. In simulated real wastewater, the effect of sample dosage and pH on the degradation of DMP with MW-induced was consistent with that in fresh water (Fig. 8). An increase in the catalyst dosage improved the degradation rate. Excessive acid and alkali would reduce the DMP degradation rate. When the pH was 1, the degradation rate of DMP was greatly reduced due to the presence of ions and excess  $\text{H}^+$ , which inhibited the production of  $\cdot\text{OH}$ . Under the alkali condition, not only iron ions would produce precipitation, but also  $\text{Mg}^{2+}$ ,  $\text{Ca}^{2+}$ , and other metal ions in simulated real

wastewater would also produce precipitation and reduce the mass transfer rate of free radicals in the chain reaction, thus reducing the degradation rate.

**3.4.5 MW intensity.** To evaluate the effect of MW intensity on the degradation of DMP, three levels of MW intensity ranging from 0 to 580 W were studied. Fig. 9a and b show that the degradation efficiency of PCCF and PCNF increased as the MW intensity increased to 580 W, which showed a slight decrease in salinity. The maximum DMP degradation was achieved by PCNF with 580 W. This is expected given that a greater MW energy input can result in the formation of more hotspots and/or active species (such as  $\cdot\text{OH}$  radicals), which accelerate the decomposition reaction rate.<sup>43</sup> However, the lower DMP removal efficiency at 0 W can be attributed to the fact that a small amount of hydroxyl radicals was produced without MW assistance. The lower DMP removal efficiency in salinity can be attributed to the fact that the production of a larger amount of hydroxyl radicals results in the recombination reaction becoming dominant, which hampers the degradation process.

The MW energy consumption ( $U_E$ ,  $\text{kW h mg}^{-1}$ ) for DMP degradation was calculated using eqn (8) to estimate the energy utilization under different MW intensities.

$$U_E = \text{MI} \times t/W \quad (8)$$

where MI is the MW intensity (kW);  $t$  is the MW irradiation time (h); and  $W$  represents the DMP degradation amount during the catalytic reaction (mg). When the MW intensity was 580 W, it

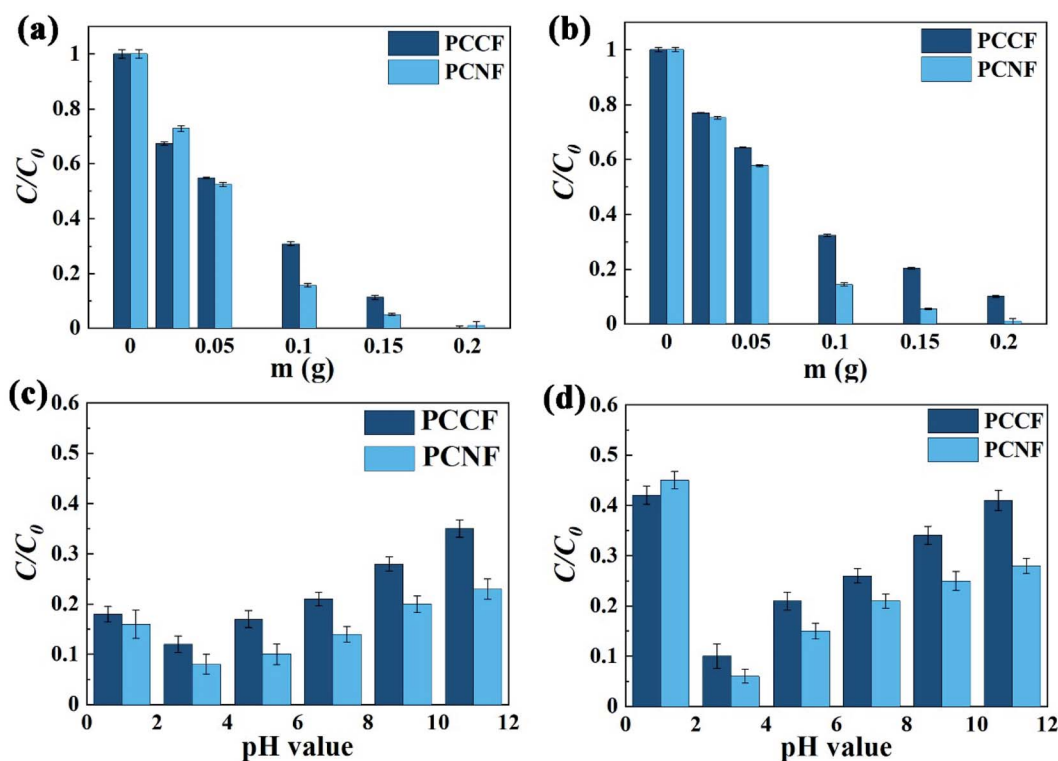


Fig. 8 Effect of different factors on the MW-enhanced Fenton-like performance: catalyst dosage at (a) 229 nm and (b) 275 nm and pH value at: (c) 229 nm and (d) 275 nm.



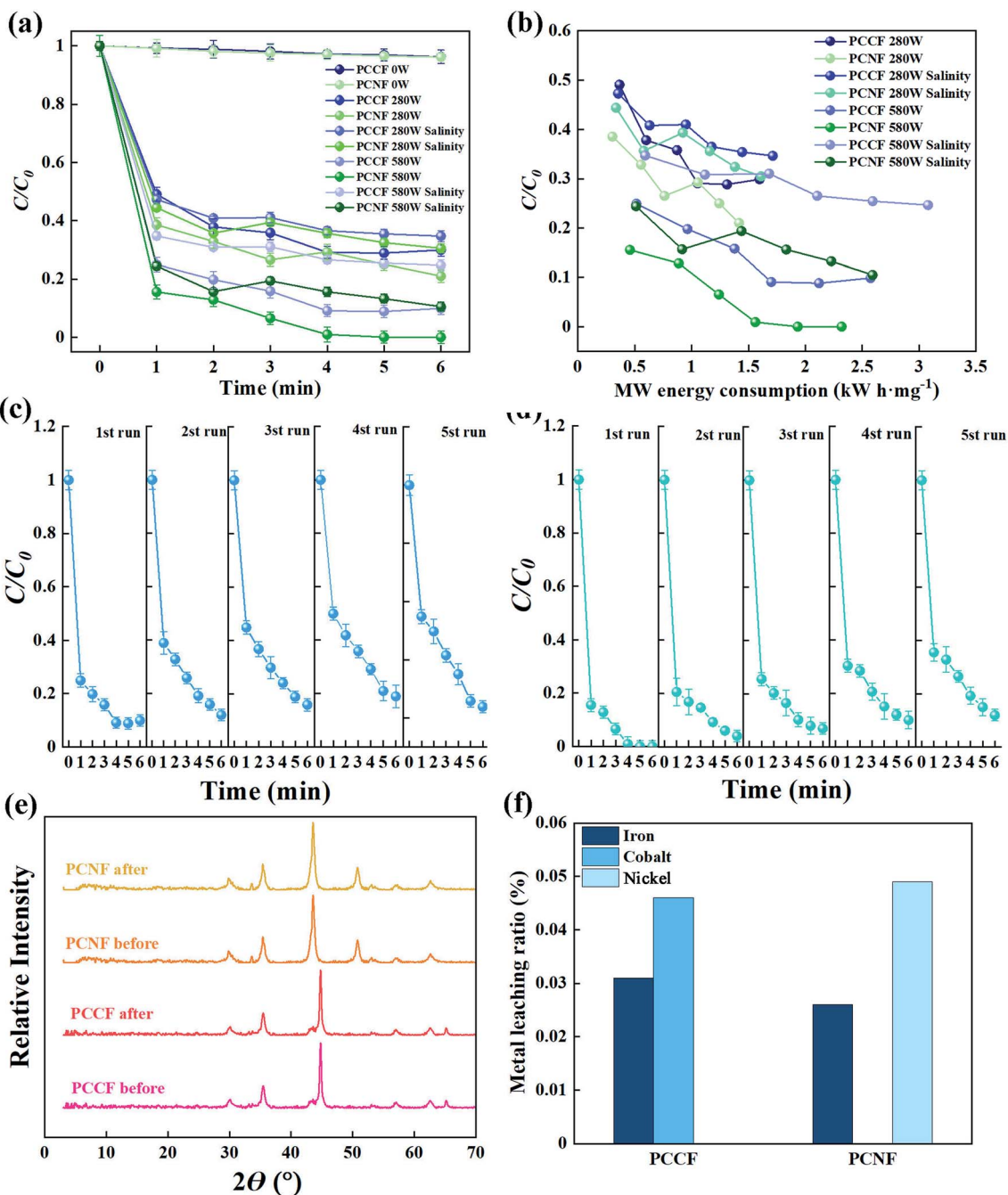


Fig. 9 Effect of (a) MW power and (b) MW energy consumption on the DMP degradation efficiency in the MW-induced process; cycling runs for the degradation of DMP in the presence of (c) PCCF and (d) PCNF; (e) XRD patterns of PCCF and PCNF before and after the reaction; and (f) the concentration of dissolved metal ions from PCCF and PCNF over five reaction cycles.

resulted in the lowest MW energy consumption and the lowest DMP degradation efficiency for all the catalysts, in which the corresponding  $U_E$  was 2.57 and  $2.32 \text{ kW h mg}^{-1}$  for PCCF and PCNF, respectively. This result indicates that insufficient MW energy cannot achieve a satisfactory DMP degradation rate, while excessive MW energy will be wasted to further promote the degradation efficiency.

**3.4.6 Stability.** The stability of PCCF and PCNF was evaluated by repeating the experiments on the degradation of DMP

with MW assistance. The two catalysts were found to exhibit stable activity, achieving a DMP degradation efficiency of 81% for PCCF and 88% for PCNF after five repeated experiments (Fig. 9c and d), respectively. PCCF and PCNF did not undergo corrosion during the degradation of DMP. There was virtually no change in the characteristic peaks between the XRD spectra of PCCF and PCNF obtained before and after the reaction (Fig. 9e), although the relative peak intensities were reduced after the reaction as a result of X-ray shielding caused by the



absorption of carbonaceous material. However, the changes were all less than the 5% error bar of XRD. Besides, there was no additional peak in the XRD spectrum after the reaction. In addition, the ICP-AES analysis of the recovered catalysts after five cycles showed the negligible loss of metal elements from the catalyst (Fig. 9f). Thus, the slight changes detected for the catalysts following the degradation of DMP indicate that both catalysts exhibited good stability.

### 3.5 Mechanism

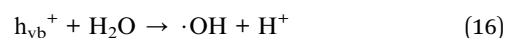
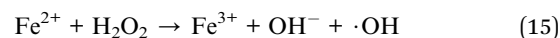
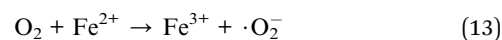
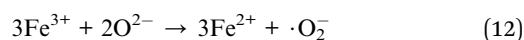
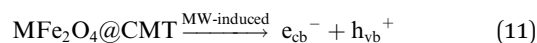
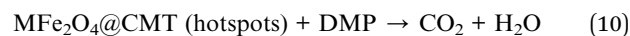
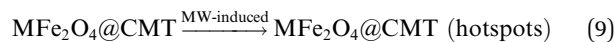
To analyze the mechanism, XPS was performed on the catalysts after the reaction. In the case of the used PCCF (Table S7†), the percentage of lattice oxygen (Fe–O), surface hydroxyl groups (–OH) and oxygen in chemisorbed water molecules changed from 40.31%, 43.87%, and 15.82% to 45.69%, 51.02, and 3.29%, respectively. In the case of the used PCNF, the percentage of lattice oxygen (Fe–O), surface hydroxyl groups (–OH), and oxygen in chemisorbed water molecules changed from 38.32%, 47.36%, and 14.32% to 43.31%, 54.84, and 1.85%, respectively. The increase in the number of surface hydroxyl groups further demonstrated the surface hydroxylation of PCCF in the MICO reaction. Surface hydroxyl groups have been reported to play a key role in the decomposition of H<sub>2</sub>O<sub>2</sub> and generation of reactive radicals, and a high percentage of surface hydroxyl groups in the catalyst may be beneficial for enhancing the oxidative degradation process. Besides, the increase in the percentage of Fe–O indicates that the Fe in the catalyst was oxidized during the MICO process with H<sub>2</sub>O<sub>2</sub>.

The active species for microwave degradation were studied *via* a free radical capture experiment. A series of free radical inhibitors was added to the reaction system. It can be seen from Fig. S3d† that after the addition of these three inhibitors, the removal rate of IPA of all the catalysts proved different degrees of reduction. Taking PCNF as an example, the highest degradation rate reduction occurred after the addition of IPA to capture ·OH, which reached 25.61%, indicating that ·OH was the most important free radical in the degradation process. Simultaneously, the addition of AgNO<sub>3</sub> and KI inhibited the transport of electrons, and thus the degradation rate was also reduced by 23.17% and 18.29%, respectively, indicating that electron transfer occurs in the reaction system. According to some reports, metal oxides can be excited to produce e<sub>cb</sub><sup>–</sup>–h<sub>vb</sub><sup>+</sup> pairs under MW irradiation, and then the absorbed H<sub>2</sub>O and OH<sup>–</sup> can react with h<sub>vb</sub><sup>+</sup> and generate ·OH,<sup>44</sup> and O<sub>2</sub><sup>·–</sup> can also indirectly produce ·OH.<sup>45</sup> Besides, the ·OH generated from the decomposition of H<sub>2</sub>O<sub>2</sub> under the MW hotspots and the reaction of H<sub>2</sub>O<sub>2</sub> with e<sup>–</sup> had moderate contribution to the removal.<sup>46</sup> DMP degradation also occurred without the addition of H<sub>2</sub>O<sub>2</sub> (Fig. 7a and b), indicating that the oxidation degradation was not only ·OH oxidation, but also direct oxidation. Direct oxidation mainly relies on O<sub>2</sub> dissolved in solution and O<sub>2</sub> in the air to generate free radicals, which can be attributed to the MW hotspots. The catalyst as an MW sensitizer, with stronger absorbing ability than water molecules, and it is easier to achieve MW resonance with the surface and lattice defects in the catalyst. Thus, the MW could be quickly transformed into

potential energy, and then the internal part of the catalyst could reach a high temperature electric arc quickly and high temperature could be induced on the catalyst pore surface. Finally, the micro domain explosion induced the decomposition of the adsorbed DMP. This comparison suggests that ·OH and h<sub>vb</sub><sup>+</sup> may play the dominant role, while e<sub>cb</sub><sup>–</sup> and ·O<sub>2</sub><sup>·–</sup> play a minor role in the DMP degradation process.

The preferential reaction mechanism would be the attack of ·OH radicals on the aromatic ring when DMP was used as the model organic pollutant herein. A total of eight products was identified by comparison of the mass spectrometry results after derivatization with BSTFA and their molecular structures are presented in Table S6.† The degradation pathway of DMP is shown in Fig. S4.†

Based on the above-mentioned conclusions, the following degradation mechanism can be concluded:<sup>47</sup>



### 3.6 Health risk evaluation

According to the PAE concentration in the surface water of rivers and lakes in some places in China and overseas (Table S8†), the maximum DMP, DBP, and DEHP concentrations are 173.42 μg L<sup>–1</sup>, 800.95 μg L<sup>–1</sup>, and 1299.54 μg L<sup>–1</sup>, respectively. Thus, 500 μg L<sup>–1</sup> was selected as the initial DMP concentration. DMP is a non-carcinogenic compounds, and thus the non-carcinogenic risk assessment was adopted according to the USEPA health risk assessment model. The non-carcinogenic risk is the ratio of long-term daily intake (CDI) to the reference dose (RfD), and its value is expressed by the risk index (HI), which is calculated according to eqn (S1)–(S4).† The HI value of DMP after degradation by PCCF (degradation rate of 80%) and PCNF (degradation rate of 95%) was smaller than that of initial DMP and less than 1, and thus the degradation process could reduce the health risk and the exposure dose does not cause non-carcinogenic risk to the human body exposed through drinking or the skin (Fig. 10). The HI value through drinking was much higher than that through skin, which means that



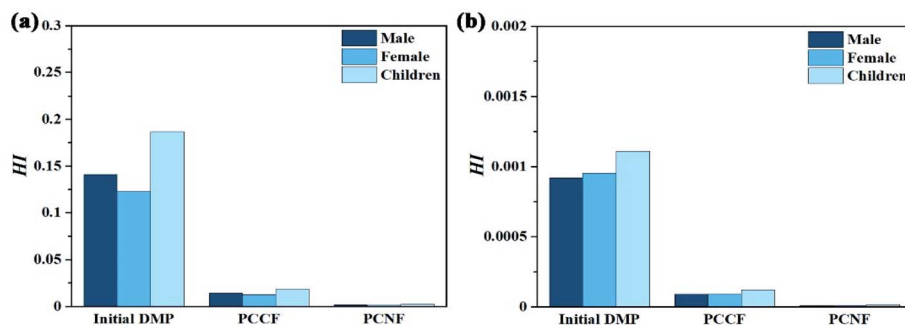


Fig. 10 Non-carcinogenic risk indexes (HI) of DMP before and after degradation by PCCF and PCNF upon exposure through: (a) drinking and (b) skin.

drinking water containing DMP can increase the non-carcinogenic risk for human. It was also found that the HI value for children was the highest, while that of females was the lowest. This may be due to the poor physical resistance of children, making them difficult to resist the risk of various pollutants, and thus the HI value for children was much higher than that for adults under the same dose exposure conditions. The HI drop out value for PCNF was larger than that for PCCF, indicating that process of DMP degradation by PCNF in Fenton-like systems with MW-induced reaction could reduce the non-carcinogenic risk.

## 4 Conclusions

Meso-macroporous  $\text{MFe}_2\text{O}_4@\text{CMT}$  ( $\text{M} = \text{Ni}, \text{Co}$ ) was fabricated by coating carbon microtubes. This study explored the catalytic performance of  $\text{MFe}_2\text{O}_4@\text{CMT}$  ( $\text{M} = \text{Ni}, \text{Co}$ ) in Fenton-like systems with MW-induced reaction. The DMP degradation efficiency and the corresponding rate constant both increased firstly, and then decreased with an increase in the initial solution pH, MW power, catalyst dosage, and  $\text{H}_2\text{O}_2$  concentration. The degradation of DMP by  $\text{MFe}_2\text{O}_4@\text{CMT}$  ( $\text{M} = \text{Ni}, \text{Co}$ ) follows hydroxyl radical reaction and direct oxidation reaction. The mechanism suggested that the catalyst facilitated the generation of more  $\cdot\text{OH}$  under MW irradiation in combination with  $\text{H}_2\text{O}_2$ , therefore accelerating the degradation of DMP. It can be concluded that the enhanced catalytic activity of  $\text{MFe}_2\text{O}_4@\text{CMT}$  ( $\text{M} = \text{Ni}, \text{Co}$ ) is closely related to its high active species concentration and good microwave-absorbing ability. Moreover, owing to its good reusability and stability,  $\text{MFe}_2\text{O}_4@\text{CMT}$  ( $\text{M} = \text{Ni}, \text{Co}$ ) can be used as a promising candidate MW catalyst for the highly efficient degradation of organic wastewater.

## Ethical approval

Not applicable because no animals were used in this study.

## Consent to publish

All the authors have agreed to publish this work in this journal.

## Data availability

The datasets used and/or analyzed during the current study are available from the corresponding author on reasonable request.

## Author contributions

Wenli Qin: methodology, software, and writing-original draft preparation; Xinyi Zhang: methodology, software, and writing-original draft preparation; Zefei Chen: data curation and methodology; Xueya Liu: data curation and software; Manqing Ai: data curation and software; Pingping Zhang: writing-reviewing and editing; Ying Ye: conceptualization and supervision; Zengling Ma: supervision and reviewing.

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## Conflicts of interest

The authors declare that they have no competing interests.

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