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# X-ray scattering as an effective tool for characterizing liquid metal composite morphology†

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Quantitative analysis of particle size and size distribution is crucial in establishing structure–property relationships of composite materials. An emerging soft composite architecture involves dispersing droplets of liquid metal throughout an elastomer, enabling synergistic properties of metals and soft polymers. The structure of these materials is typically characterized through real-space microscopy and image analysis; however, these techniques rely on magnified images that may not represent the global-averaged size and distribution of the droplets. In this study, we utilize ultra-small angle X-ray scattering (USAXS) as a reciprocal-space characterization technique that yields global-averaged dimensions of eutectic gallium indium (EGaIn) alloy soft composites. The Unified fit and Monte Carlo scattering methods are applied to determine the particle size and size distributions of the liquid metal droplets in the composites and are shown to be in excellent agreement with results from real-space image analysis. Additionally, all methods indicate that the droplets are getting larger as they are introduced into composites, suggesting that the droplets are agglomerating or possibly coalescing during dispersion. This work demonstrates the viability of X-ray scattering to elucidate structural information about liquid metal droplets for material development for applications in soft robotics, soft electronics, and multifunctional materials.

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## 1 Introduction

Soft, stretchable materials with unique combinations of thermal and electrical functionalities have the potential to play a pivotal role in diverse fields ranging from soft robotics to deformable electronics.<sup>1–3</sup> These fields have seen tremendous growth in materials research and development in the past decade. In particular, soft, conformal material systems based on low melting point metal alloys have garnered attention as solid–liquid composite systems. These metals include room temperature liquids such as gallium, eutectic gallium indium (EGaIn) and Galinstan (GaInSn), as well as Field’s metal that melts at 62 °C.<sup>4–7</sup> The gallium-based liquid metal alloys are attractive due to their low toxicity and viscosity, high thermal and electrical conductivity, and a surface oxide which rapidly forms a nanometer thick shell on droplets.<sup>8</sup> Liquid metal materials and their

composites have enabled unprecedented combinations of high thermal conductivity,<sup>9–11</sup> electrical conductivity,<sup>12</sup> and self-healing abilities in soft elastomers.<sup>13,14</sup> To increase their adaptation in industry and to promote further development at the academic level, methods to tune the material properties and expand characterization techniques to elucidate the governing morphological features are being explored.

Soft composite systems have traditionally utilized rigid phase inclusions to enhance the functionality of the polymer matrix, including solid metal, ceramic, or carbon-based fillers. However, these rigid inclusions often result in undesirable changes to the bulk mechanical behavior, such as reduced extensibility and increased stiffness, owing to the interfacial incompatibilities and the compliance mismatch that arises from the different mechanical properties of the rigid filler and the soft matrix.<sup>15–17</sup> These tradeoffs in mechanical and functional properties are common features of rigid phase inclusion-based polymer composites. Composites with liquid phase fillers can overcome this compliance mismatch for high stretchability and multifunctionality that is generally uncommon in polymer composites. As such, liquid filler composites are promising in applications of soft robotics, soft electronics, and reconfigurable matter that are pushing towards unconventional combinations of functional properties with soft and highly deformable

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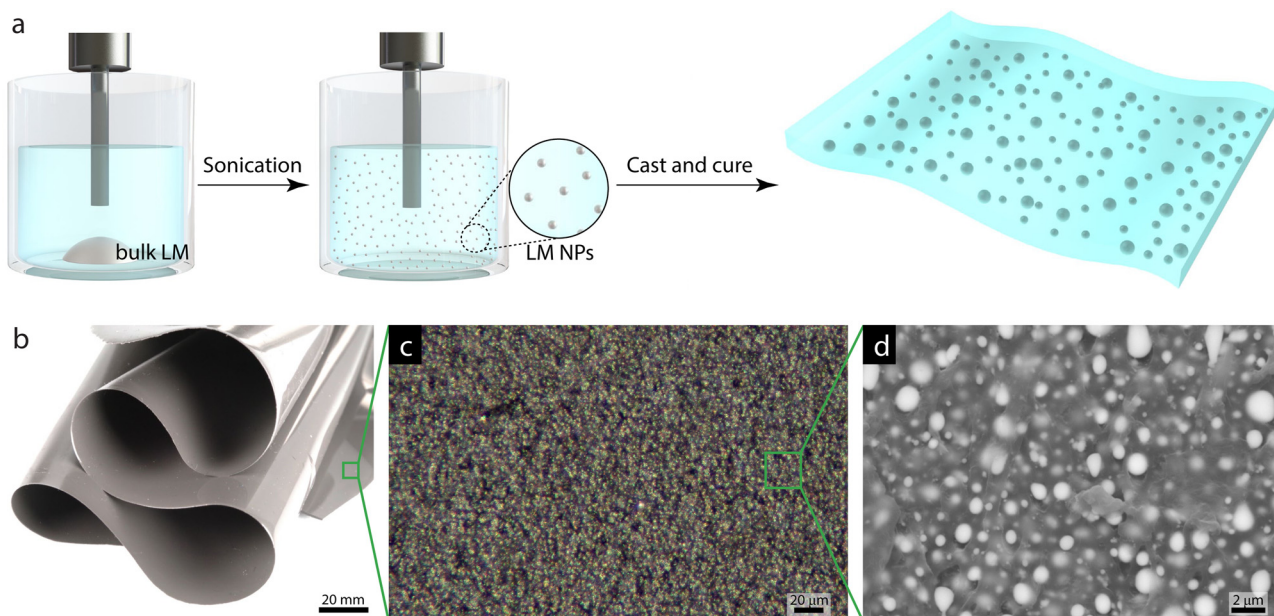
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mechanical responses. To this end, liquid metal-based soft composites have been developed, where the liquid metal droplets are dispersed in an elastomer matrix. In the composites, the droplets are dispersed in the liquid polymer phase through mixing or sonication and rapidly form an oxide shell during processing, which can help aid in dispersion without the need for surfactants or emulsifying agents.<sup>18–20</sup> The composites are then cured, resulting in a solid elastomer phase which encapsulates the dispersed liquid metal droplets. With liquid phase inclusions, the composite architecture must be designed to achieve desirable properties. For example, in liquid metal-based soft composites, a number of droplet features can affect the ultimate material behavior, namely the droplet shape, size, loading, and size distribution.<sup>21–23</sup> Therefore, characterization of droplet dimensions is critical to the design and development of soft composite materials.

In conventional composites, solid filler particle dimensions are often prescribed prior to composite fabrication; however, in liquid filler composites, liquid inclusions can change size and shape during material processing.<sup>24</sup> Thus, in order to determine liquid droplet structures, post-fabrication analysis is required. Present techniques utilize imaging, either through optical or electron microscopy, and often image analysis to determine number-averaged size distributions of the inclusions.<sup>25–29</sup> While these procedures are widely accepted, they are time-intensive and are only capable of analyzing a limited number of inclusions that are visible within a particular field of view. A technique for determining bulk, volume-averaged size distributions is currently lacking. Thus, an alternative droplet characterization technique that can be effectively applied to reliably analyze the composite morphology is essential.

As an alternative to microscopy analysis of composite materials, X-ray scattering has been extensively used to characterize the shape, size, and interfaces of fillers in a wide variety of matrix materials.<sup>30,31</sup> Due to the reciprocal relationship between dimension and scattering angle, wide angle X-ray scattering (WAXS) provides structural information on the atomic scale ( $< 1$  nm), small angle X-ray scattering (SAXS) characterizes structures on the order of 1–100 nm, and ultra-small angle X-ray scattering (USAXS) characterizes structures up to several microns in size. Thus, by measuring scattered X-rays over a broad angular range, information spanning several decades of length scales can be acquired. Most reports of X-ray scattering of composites consist of solid particles embedded in a solid matrix.<sup>32–34</sup> In contrast, examples of scattering by liquid metal (LM) fillers are sparse. Wide angle X-ray diffraction has been used to probe the composition of multi-phase LM materials,<sup>17,35,36</sup> while SAXS has been used to confirm the presence of Ga particles in GaInSn<sup>37</sup> and to study orientation effects in an LM-embedded fiber.<sup>38</sup> A systematic morphological study of LM composites using X-ray scattering, particularly at length scales greater than 100 nm, is absent.

In this study, we report a systematic investigation of liquid metal soft composites using microscopy and X-ray scattering techniques. The purpose of this research was to demonstrate that X-ray scattering can be used as a complementary characterization tool to provide information about the droplet sizes and size distributions in liquid filler polymer composites. To study the effects of filler loading, soft composites were prepared with nanodroplets ( $\sim 300$  nm) of EGaIn LM dispersed as a filler in a poly(dimethylsiloxane) (PDMS) elastomer matrix at different volume loadings ( $\phi = 0.1\%$  to  $\phi = 20\%$  LM) (Fig. 1(a) and (b)). The local, real-space morphologies of the composites were analyzed using optical and scanning electron microscopy



**Fig. 1** Liquid metal soft composites. (a) Schematics showing the fabrication of LM nanodroplets using probe sonication. (b) Photograph showing the soft, flexible nature of the LM composites. (c) Optical micrograph and (d) SEM image of a composite showing LM microstructure.

(SEM) (Fig. 1(c) and (d)) and compared to the global morphologies of the composites from analysis of USAXS. Through this work, X-ray scattering is shown to be a facile route to obtaining global-averaged droplet size distributions and informing how materials processing can influence the droplet sizes. One outcome of this analysis is that as LM droplets prepared in solution are dispersed into elastomeric composites, we find increasing droplet sizes, suggesting that the droplets are agglomerating or possibly coalescing in the composites. Given the myriad of materials based on liquid metal, the broader impact of this work is to accelerate the development of soft, functional composites through the establishment of structure–property–processing relationships in liquid metal-based materials.

## 2 Methods

### 2.1 LM droplet and composite fabrication

Bulk LM was prepared by mixing Ga:In at a 3:1 ratio by mass, which forms the eutectic alloy eGaIn. LM droplets were prepared by sonicating ~200 mg of bulk LM in 5 mL toluene solvent using a QSonica Q700 tip sonicator for 80 min at an amplitude of 30% (Fig. 1(a)). The LM–polymer composites were fabricated by dispersing the LM droplets in a two-component silicone elastomer (Dow Corning Sylgard 184). Initially, the silicone prepolymer was prepared by combining parts A (base) and B (curing agent) at a 10:1 ratio by mass in a planetary centrifugal mixer (FlackTek Speedmixer). The toluene was decanted from the droplet dispersion prior to adding the droplets to the prepolymer mixture. For higher LM loadings ( $\phi = 10, 20\%$ ), multiple batches of sonicated droplets were combined to achieve the desired mass and then toluene was decanted. The prepolymer/LM droplet mixture was mixed again for *ca.* 20 min under vacuum to create an emulsion and to remove any residual toluene. The final mass of the mixture was measured and compared to the amount of LM droplets and prepolymer added to ensure complete toluene removal before casting. The final mixture was cast on a glass slide with a Universal applicator (ZUA 2000; Zehntner Testing Instruments), creating a composite film approximately 70  $\mu\text{m}$  thick. The films were cured in a convection oven at 80 °C for 12 hours. All the fabrication procedures were carried out at ambient conditions.

### 2.2 Optical microscopy

The optical micrograph of the composite film was obtained using a Zeiss Axio Zoom v16 stereo microscope.

### 2.3 Scanning electron microscopy characterization

To characterize the droplets prior to loading them into the PDMS matrix, a sample of the pristine droplets was prepared. The LM droplet sample was prepared by pipetting the LM droplet/toluene dispersion onto an adhesive carbon tape attached to an SEM standard pin stub and leaving overnight at room temperature to allow for toluene evaporation. To prepare the composite films for SEM analysis, a 500  $\mu\text{m}$  layer

of PDMS was first cast on a glass slide using the ZUA 2000 Universal applicator and cured at 80 °C for 2 hours. Next, the cured composite film was placed on the PDMS layer and then a second 500  $\mu\text{m}$  layer of PDMS was cast on top and cured at 80 °C for another 2 hours. This procedure to sandwich the 70  $\mu\text{m}$  composite film with thicker PDMS layers was performed to facilitate easy handling of the film during the subsequent steps. The sandwiched composite film was frozen in liquid nitrogen to crystallize the LM droplets and a razor blade was used to cut the sandwiched sample, exposing the interior of the LM composite. The sample cross-section was then attached to an adhesive carbon tape on the SEM standard pin stub and sputter coated with a Pt–Pd layer of ~10 nm thickness prior to SEM analysis. The micrographs were obtained on a FEI Quanta 600 FEG-SEM in back-scattered electron (BSE) mode at a spot size of 4 and an accelerating voltage of 20 kV. The BSE mode was chosen as this provides enhanced contrast between the matrix and the droplets and allows for a higher penetration depth into the sample compared to the secondary electron mode (Fig. S1, ESI†). The droplet sizes in the SEM micrographs were analyzed using Fiji image analysis software. Details about the method used to analyze these images are discussed in Section 3.1.

### 2.4 X-Ray scattering characterization

The LM droplets were prepared for X-ray scattering analysis by pipetting the LM droplet emulsion in toluene onto a polyimide substrate and allowing the toluene to evaporate at room temperature overnight. The LM droplet/polyimide sample was then mounted onto a solid sample plate for analysis. The composites were analyzed by mounting the as-prepared LM composite films onto a solid sample plate.

Ultra-small-angle X-ray scattering (USAXS) measurements were conducted at beam line 9-ID-C at the Advanced Photon Source at Argonne National Laboratory (Lemont, Illinois).<sup>39,40</sup> The USAXS/SAXS instrument was configured with an X-ray energy of 21 keV ( $\lambda = 0.5895 \text{ \AA}$ ), an X-ray photon flux of  $\approx 5 \times 10^{12} \text{ mm}^{-2} \text{ s}^{-1}$ , and a combined  $q$  range of  $1 \times 10^{-3} \text{ nm}^{-1}$  to  $1 \text{ nm}^{-1}$  ( $q = 4\pi/\lambda \sin(\theta)$ , where  $q$  is the scattering vector,  $\lambda$  is the wavelength and  $\theta$  is 1/2 of the scattering angle). The Irena program was used to reduce the 2D USAXS detector profiles into 1D datasets (intensity vs. scattering vector,  $q$ ) and to remove the effects of collimation-dependent instrumental smearing to generate desmeared USAXS scattering profiles.<sup>41</sup> The observed scattering features of the desmeared USAXS profiles were analyzed using the Unified fit by Beaucage,<sup>42</sup> and the maximum entropy size distribution method<sup>43</sup> described in the Irena tool suite.<sup>41</sup> The open-source McSAS software package developed by Breßler and coworkers was used to obtain Monte Carlo droplet size distributions from the desmeared USAXS data.<sup>44</sup> Wide angle X-ray scattering experiments were performed to confirm the presence of the amorphous composite components using a Xenocs Xeuss 3.0 SAXS/WAXS, equipped with a GeniX 3D Cu HFVLF microfocus X-ray source with a wavelength of 0.154 nm (Cu K $\alpha$ ) (Fig. S2, ESI†). The sample-to-detector distance was 55 mm for WAXS, and the  $q$ -range was calibrated

using a lanthanum hexaboride standard. The 2D WAXS patterns were obtained using a Dectris EIGER 4M detector and reduced into 1D intensity *vs.* *q* profiles using XSACT software. The scattering length densities (SLD) of PDMS and EGaIn were calculated using the NIST Scattering Length Density Calculator.

### 3 Results and discussion

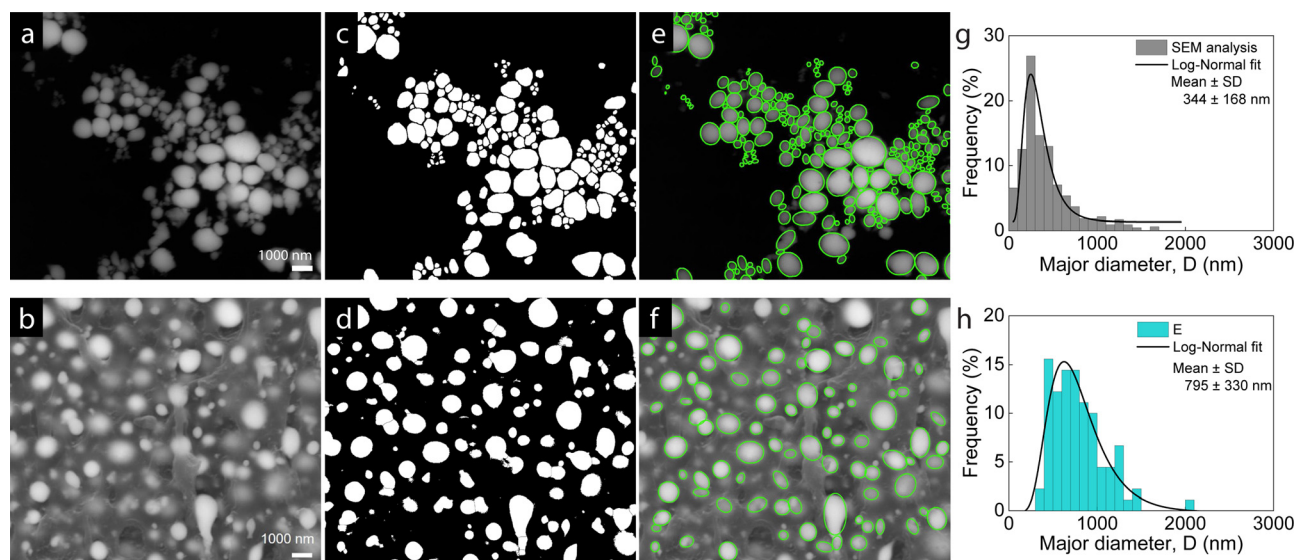
#### 3.1 SEM image analysis

Analysis of the SEM micrographs of the pristine LM droplets and the LM composites was performed to characterize the real-space morphology and to determine the droplet dimensions. The general method sequence is shown in Fig. 2 with the SEM micrographs for LM droplets in Fig. 2(a) and  $\phi = 20\%$  LM composite in Fig. 2(b). Using image analysis (Fiji software), the SEM images were first adjusted for brightness and contrast and converted into a binary format (Fig. 2(c) and (d)). The bright regions indicate LM droplets and the dark regions represent background or PDMS for the pristine droplets or composites, respectively. Next, the connected particles were separated, requiring careful observation of the pre- and post-processed images to ensure correct boundaries. The resulting isolated bright regions were considered individual droplets, and their areas were calculated by generating the best fit ellipse for the respective area. The ellipse fits are overlaid on the original micrograph as green outlines and represent the particles well (Fig. 2(e) and (f)), the green outline overlays for remaining LM composite SEM images are shown in Fig. S3 (ESI<sup>†</sup>). In each image, the major and minor axes of the fit ellipses were obtained with the droplet size represented by the major axis. The size distributions are shown as the frequency % droplets analyzed *vs.* major diameter (*D*), with representative examples of the LM droplets and  $\phi = 20\%$  LM composite shown in

Fig. 2(g) and (h). A log-normal fit was performed on the plotted size distribution histograms, providing the mean diameter and standard deviation ranging from  $344 \pm 168$  nm for the pristine LM droplets to  $795 \pm 330$  nm for the  $\phi = 20\%$  LM composite. These results indicate that the initial measured LM droplet size of 300 nm increases to approximately 800 nm as the droplets are incorporated as a filler into the PDMS elastomer matrix. To determine why the droplets are larger in the composites compared to the precursor droplet dispersion, an experiment was conducted to determine when during the fabrication procedure the droplets increase in size. This was done by comparing the sizes of the pristine, sonicated droplets to the droplets in a 20% LM composite that used the same batch of LM droplets. The initial droplet diameter after sonication in toluene was  $302 \pm 202$  nm and increased to  $468 \pm 306$  nm upon shear-mixing in PDMS in a Flacktek speedmixer at 800 rpm for 15 min (SEM image analysis presented in Fig. S4, ESI<sup>†</sup>). Thus, the shear forces of mixing the LM droplets into the uncured matrix are likely responsible for the droplet size increase, by either aggregation or coalescence of smaller particles.

#### 3.2 X-ray scattering curves

Based on the size scale of the particles determined from SEM analysis and as noted in the introduction, it was hypothesized that these materials would display size-dependent scattering features from USAXS/SAXS. The morphological characterization of the LM droplets and composites over a wide range of length scales was performed using USAXS/WAXS. Desmeared USAXS profiles (intensity *vs.* scattering vector, *q*) of the LM droplets and composites at various LM loadings ( $\phi = 0.1, 1, 2, 10, 20\%$ ) are shown in Fig. 3(a). This data compares the effects of droplet processing and filler loading on the X-ray scattering features of these materials. The unfilled PDMS matrix is not shown for



**Fig. 2** Image analysis sequence on SEM micrographs of (a) LM droplets fabricated through sonication technique. (b)  $\phi = 20\%$  LM composites made by dispersing the droplets in PDMS. (c) and (d) Binary masks generated from the SEM images in (a) and (b). (e) and (f) Ellipses fit to the bright droplet areas in (c) and (d) and overlaid on the actual image, (g) and (h) major diameter of the ellipses in (e) and (f) are plotted to obtain histograms and mean size using a log-normal fit.

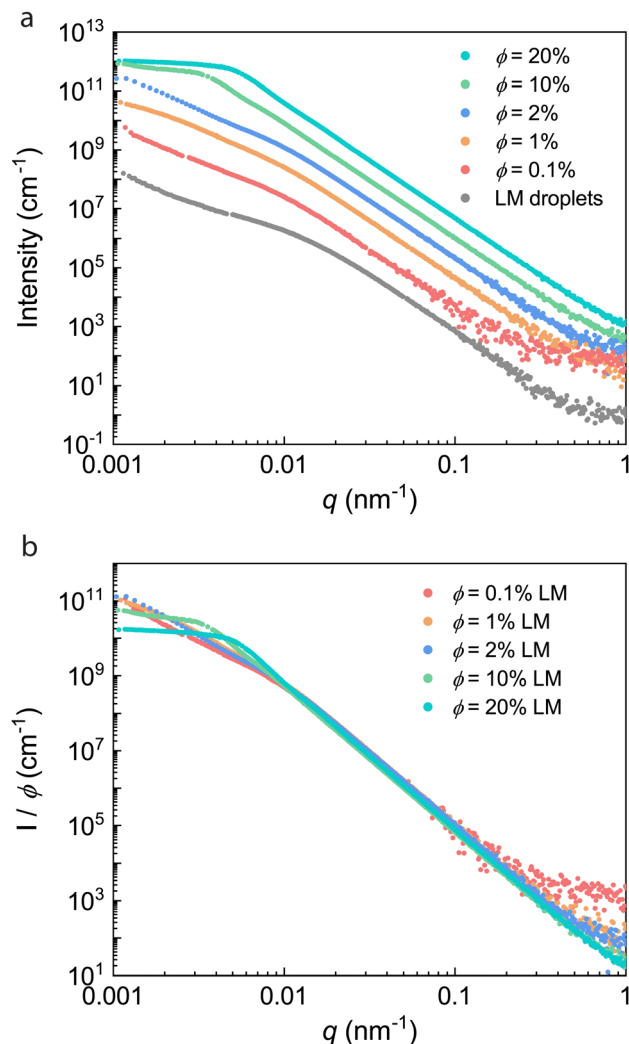


Fig. 3 X-ray scattering curves. (a) Desmeared USAXS profiles of the LM droplets and composites at various LM loadings ( $\phi = 0.1, 1, 2, 10, 20\%$ ). The LM droplet profile is on the original scale and all other profiles are vertically offset for clarity. (b) Reduced scattering curves normalized for the volume loading  $\phi$  of the liquid metal filler.

comparison because the featureless weak scattering in the USAXS region is essentially identical to the background. Given the high contrast in electron density between EGaIn ( $\text{SLD} = 4.5 \times 10^{-5} \text{ \AA}^{-2}$ ) and PDMS ( $\text{SLD} = 8.8 \times 10^{-6} \text{ \AA}^{-2}$ ), the pristine LM droplets and composites show intense scattering, indicating structure on the nanometer to micron length scale (Fig. 3(a)).

Because the scattering intensity depends not only on the form factor (size and shape) of the scattering entities, but also on the structure factor (spatial distribution of particles), it is important to identify the concentration regimes where the structure factor becomes significant.<sup>45</sup> Concentration effects were studied by using the method described by McGlasson,<sup>45</sup> and the concentration series was plotted as  $I/\phi$  vs.  $q$  (Fig. 3(b)). The curves superimpose at intermediate  $q$  ( $0.01 \text{ nm}^{-1} < q < 0.1 \text{ nm}^{-1}$ ), consistent with composites from the same base structure (EGaIn droplets). However, the scattering curves of the  $\phi = 10$  and  $20\%$  LM composites show significantly reduced

scattering intensity at low  $q$  ( $0.001 \text{ nm}^{-1} < q < 0.003 \text{ nm}^{-1}$ ) due to overlap of droplet/aggregate features consistent with a semidilute regime.<sup>45</sup> As will be discussed later, due to the presence of interdroplet interactions in all of the composites, it is likely that the dilute regime is below  $\phi = 0.1\%$ , so all samples reside in the semidilute regime. In order to quantify characteristic dimensions from these data, the scattering profiles were quantitatively analyzed using a modified Unified fit approach and a Monte Carlo model.

### 3.3 Unified fit analysis

The Unified fit approach has been used extensively to quantitatively analyze scattering profiles from heterogeneous systems having hierarchical structure.<sup>42,46,47</sup> In this model, the knee-like features (e.g., the slope change occurring around  $q = 0.01 \text{ nm}^{-1}$  in the LM droplets profile, Fig. 3(a)) are interpreted as corresponding to the Guinier regime, defined by eqn (1) as:

$$I(q) = I_0 e^{\left(\frac{-q^2 R_g^2}{3}\right)} \quad (3.1)$$

where the radius of gyration,  $R_g$ , describes the shape-independent size of the scattering object, and  $I_0$  is the zero-angle scattering.<sup>42</sup> Distinct power law regimes that appear as linear regions in the log/log plot are also modelled using the Unified approach. This region, known as the Porod regime, probes length scales smaller than that of the scattering object, such as the surface of the particle, and is given by eqn (2) as:

$$I(q) = I_0 + Bq^{-P} \quad (3.2)$$

where  $B$  is the power law prefactor,  $I_0$  is the zero-angle scattering, and  $P$  is the power law exponent. The value of the power law exponent  $P$  can provide information regarding the surfaces and interfaces between the particle and matrix in composites.<sup>42</sup> For structures characterized by a sharp and smooth interface between the particle and matrix, Porod's law will be satisfied and the power law regime will scale as  $q^{-4}$  ( $P = 4$ ).<sup>48</sup> However, particles with rough surfaces give rise to power law scaling relationships that are characteristic of the dimensionality of the interface. For example, power law scaling exponents between  $3 < P < 4$  are characteristic of surface fractals with dimension  $d_s = 6 - P$ ,<sup>49</sup> and exponents between  $2 < P < 3$  are characteristic of mass fractals where particles are arranged in a self-similar fashion with a mass fractal dimension of  $d_f = P$ .<sup>49</sup>

The Unified fit approach by Beaucage combines contributions from Guinier and Porod regimes into a single level, i, consisting of a knee and a power law regime in the Unified equation (eqn (3)):<sup>42,50</sup>

$$I_i(q) = G_i e^{\left(\frac{-q^2 R_{g,i}^2}{3}\right)} + e^{\left(\frac{-q^2 R_{g,co,i}^2}{3}\right)} B_i \left\{ \frac{\left(\text{erf}\left(\frac{kq R_{g,i}}{\sqrt{6}}\right)\right)^3}{q} \right\}^{P_i} \quad (3.3)$$

where  $k$  is a constant related to the power law decay,<sup>49</sup>  $G_i$  is the Guinier prefactor for scatterer  $i$ ,  $R_{g,i}$  is the radius of gyration of

the scatterer,  $B_i$  is the power law prefactor, erf is the error function,  $P_i$  is the power law exponent, and  $R_{g,co,i}$  is the high- $q$  cutoff equal to  $R_{g,i-1}$ .

### 3.3.1 Mass fractal aggregate analysis via Unified equation.

The  $\phi = 0.1$ , 1, and 2% LM composites display two structural levels of scattering (Fig. 3(a)). As a representative example, the  $\phi = 2\%$  LM composite scattering profile modelled using two structural levels of the Unified equation is shown in Fig. 4. Structural level 1 consists of a Guinier region which is related to the size of the primary LM droplets. The radius of gyration associated with scattering from level 1 ( $q > 0.008 \text{ nm}^{-1}$ ) was determined as  $220 \pm 2 \text{ nm}$ . Based on the SEM images (Fig. 2), the droplets were reasonably assumed to be approximately spherical. The radius of gyration from the Guinier region of the Unified fit can be related to the diameter of a spherical particle,  $D$ , by  $D = 2 \times R_g / \sqrt{3/5}$ .<sup>48</sup> Therefore, the diameter of the corresponding spherical radius for the  $\phi = 2\%$  composite was determined as  $570 \pm 5 \text{ nm}$ . While this size is larger than the mean size determined from image analysis ( $422 \pm 200 \text{ nm}$ ), it is well known that analysis of the Guinier region tends to overestimate the mean particle size in polydisperse systems, as large particles dominate the scattering volume.<sup>51,52</sup> The level 1 power law exponent  $P_1$  for the LM droplets was 4, suggesting a smooth gallium oxide interface at the surface of the spherical LM droplets.<sup>48</sup> A smooth droplet surface is consistent with the SEM images of the droplets (Fig. 2). The parameters obtained from analysis on the samples are tabulated in Table 1 and the additional fits can be found in Fig. S5 (ESI†).

At lower  $q$  ( $0.001 \text{ nm}^{-1} < q < 0.007 \text{ nm}^{-1}$ ), structural level 2 consists of a Guinier and power law region arising from scattering from larger aggregates of primary droplets (Fig. 4). The level 2 power law exponent,  $P_2$ , which ranges from 2.4 to 2.8 in the  $\phi = 0.1$ , 1, and 2% composites, is consistent with mass fractal aggregates comprised of mass-fractal particles arranged

in a self-similar fashion.<sup>49</sup> The level 2 Guinier region was used to determine the radius of gyration of the mass-fractal aggregates as  $R_g \approx 1.2 \mu\text{m}$ . This aggregate size is in good agreement with the aggregates observed via SEM (Fig. 4 inset). Additionally, the degree of aggregation (the number of primary droplets per aggregate) was calculated from the fit parameters according to previously reported methods<sup>53,54</sup> as approximately 100 droplets per aggregate. This is consistent with the number of droplets observed in the aggregates via SEM analysis and will be the focus of future studies related to the aggregation of droplets in LM composites.

The  $\phi = 1\%$  composite also displays a second Guinier and power law region at low  $q$  arising from scattering from the mass fractal aggregates (Fig. 3(b)). The approximate size of the aggregates,  $R_{g,2}$ , is  $1.5 \mu\text{m}$ . This is again consistent with the SEM images that display aggregates of primary droplets approximately  $1\text{--}2 \mu\text{m}$  in size (Fig. 8(b)). Although the  $\phi = 0.1\%$  LM composite displays a second level of power law scattering (Fig. 3(a)), a second Guinier region corresponding to the mass fractal aggregates is not observed. A reasonable explanation for the absence of this feature despite the presence of aggregates in the SEM images (Fig. 8(b)) is that the  $\phi = 0.1\%$  composite is just entering the semidilute regime, where only a small fraction of particles exist as aggregates with minimal contribution in the USAXS region.

### 3.3.2 Correlation analysis via Unified/Born–Green equation.

At higher volume loadings of liquid metal ( $\phi = 10, 20\%$ ), the stronger spatial correlations between particles can be effectively modelled using the Born–Green modification of the Unified function.<sup>55</sup> The Born–Green closure of the Ornstein–Zernike equation modifies the scattering pattern through the structure factor:

$$S(q) = 1/(1 + p \times \theta(q, \eta)) \quad (3.4)$$

where  $S(q)$  is the structure factor,  $p$  is the packing factor, proportional to the ratio of the occupied to available volume, and  $\theta(q, \eta)$  is the spherical amplitude function,

$$\theta(q, \eta) = 3[\sin(q\eta) - q\eta \cos(q\eta)]/(q\eta)^3 \quad (3.5)$$

where  $\eta$  is the correlation distance.  $S(q)$  is multiplied by  $I_i(q)$  to include structure factor contributions to the specified level in the Unified equation.

The scattering data of the  $\phi = 10\%$  and  $20\%$  LM composites were modelled using the Unified/Born–Green approach due to the distinct peak/knee observed near  $q = 0.005 \text{ nm}^{-1}$  (Fig. 3(b)). An example fit to the  $\phi = 20\%$  data is shown in Fig. 5. The Guinier region was used to quantify the size of the primary droplets as  $D = 1.1 \pm 0.2 \mu\text{m}$ . Additionally, the correlation length shown as the interdroplet distance in Fig. 5 inset was determined as  $940 \pm 20 \text{ nm}$ . The Unified parameters for the  $\phi = 10$  and  $20\%$  composites are tabulated in Table 2. The packing factor, which ranges from 0 for uncorrelated systems to 5.92 for closely packed spheres,<sup>42</sup> was determined as  $p = 0.62 \pm 0.06$  and  $0.98 \pm 0.09$  for the  $\phi = 10$  and  $20\%$  composites, respectively. The slight increase in packing factor with increasing volume fraction is expected, and the relatively low packing factors are consistent with semidilute compositions.

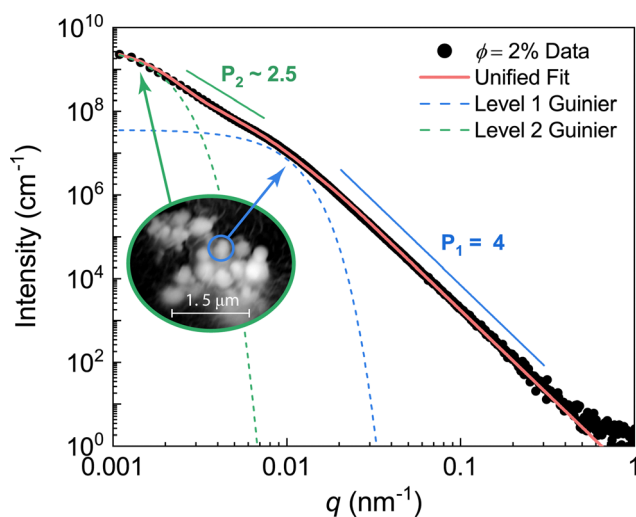


Fig. 4 Two-level Unified fit of  $\phi = 2\%$  LM composite. Structural level 1 represents scattering from the primary droplets, and structural level 2 represents scattering from the mass-fractal LM aggregates. The fit parameters can be found in Table 1.

**Table 1** Unified fit parameters of eqn (3) for the LM droplets and  $\phi = 0.1, 1$ , and 2% composites. Level 1 structural parameters relate to the primary droplet size, whereas level 2 structural parameters relate to the mass fractal aggregate. Because the LM droplets and  $\phi = 0.1\%$  scattering curves did not display a level 2 Guinier knee, only the power law region was fit

	Level 1 Unified fit – primary particle					Level 2 Unified fit – mass fractal aggregate				
Composite	$G_1 \times 10^6 \text{ (cm}^{-1}\text{)}$	$R_{g,1} \text{ (nm)}$	$D_1 \text{ (nm)}$	$B_1 \times 10^{-6} \text{ (cm}^{-1} \text{ \AA}^{-P_1}\text{)}$	$P_1$	$G_2 \times 10^6 \text{ (cm}^{-1}\text{)}$	$R_{g,2} \text{ (nm)}$	$B_2 \text{ (cm}^{-1} \text{ \AA}^{-P_2}\text{)}$	$P_2$	
LM droplets	$2.0 \pm 0.05$	$140 \pm 2$	$360 \pm 5$	$6.6 \pm 0.01$	4	—	—	$1.3 \pm 0.5$	$2.0 \pm 0.01$	
0.1% LM	$1.5 \pm 0.2$	$210 \pm 7$	$540 \pm 20$	$0.81 \pm 0.004$	4	—	—	$0.030 \pm 0.01$	$2.4 \pm 0.04$	
1.0% LM	$20 \pm 2$	$210 \pm 5$	$540 \pm 13$	$9.6 \pm 0.05$	4	$2.5 \pm 0.1$	$1500 \pm 60$	$0.023 \pm 0.01$	$2.8 \pm 0.04$	
2.0% LM	$36 \pm 1$	$220 \pm 2$	$570 \pm 5$	$18 \pm 0.03$	4	$3.9 \pm 0.1$	$1200 \pm 10$	$0.28 \pm 0.08$	$2.5 \pm 0.03$	

### 3.4 Particle size distribution methods

In addition to the mean particle size, the particle size distribution has been shown to impact the bulk properties of nanocomposites,<sup>56</sup> and the presence of both large and small droplets is apparent in the SEM images (Fig. 2). To elucidate the distribution of droplet sizes present in the composites from the X-ray scattering profiles, several scattering models were applied and compared.

**3.4.1 Unified fit size distributions.** Using the Unified particle size distribution method established by Beaucage,<sup>57</sup> the droplet size distributions were obtained from the level 1 parameters of the Unified fit (Tables 1 and 2). This method assumes a log-normal distribution of polydisperse spheres and requires a scaling relationship that follows Porod's law ( $P = 4$ ). The volume-weighted log-normal size distributions for each sample are shown as the solid black curves in Fig. 6. The size distributions clearly reveal that the average droplet size increases as the filler is incorporated into the composite and as the filler volume loading is increased from  $\phi = 0.1\%$  to 20%. This finding is consistent with the droplet size increase observed in the SEM image analysis.

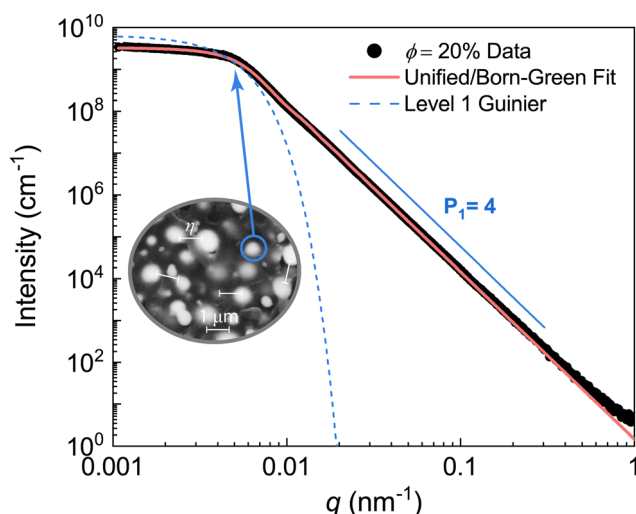
**3.4.2 Arbitrary size distributions.** A reverse Monte Carlo (MC) approach initially developed by Pedersen<sup>58</sup> and later modified by Pauw<sup>59</sup> was also employed to obtain arbitrary size distributions from the X-ray scattering data, as opposed to

log-normal size distributions given by the Unified fit. The MC method has been shown to agree with results from classical model fitting and is capable of fitting arbitrary size distributions with excellent reproducibility and validity.<sup>59–62</sup> The method consists of an iterative rejection–acceptance procedure in which the size of one sphere in a set of spheres is changed, at random, until a solution to the weighted sum of the geometric form factors converges to the data.<sup>59</sup> This model assumes scattering from smooth and sharp interfaces ( $P = 4$ ) and was used without structure factor. Although the model is typically applied to dilute systems, it was used to model these samples which are in the semidilute regime, to compare to the Unified method. The initial estimation of the scattering intensity profile is calculated using eqn (6):

$$I_{\text{MC}}(q) = b + A \sum_{k=1}^{n_s} |F_{\text{sph},k}(qR_k)|^2 \left(\frac{4}{3}\pi\right)^2 R_k^{(6-p_c)} \quad (3.6)$$

where  $I_{\text{MC}}$  is the calculated scattered intensity,  $b$  is a background term,  $A$  is a scaling factor,  $F_{\text{sph},k}$  is the spherical form factor,<sup>48</sup>  $R_k$  is the radius for sphere  $k$ ,  $n_s$  is the number of scattering particles contributing to the calculation, and  $p_c$  is a volume-weighting correction that increases the speed of the model calculations.<sup>59</sup> As recommended by Pauw *et al.*,<sup>59</sup> the limits of the sphere radii were chosen as  $R_{\text{min}} \simeq \pi/q_{\text{max}}$  and  $R_{\text{max}} \simeq \pi/q_{\text{min}}$ . After the initial estimation of the scattering profile, the method employs an optimization cycle that changes the size of a randomly-selected sphere, and accepts the size of that sphere if the calculated scattering intensity more closely matches the experimental data. Convergence to the experimental data results in a set of spheres whose sizes can be represented in a histogram to visualize the size distribution.

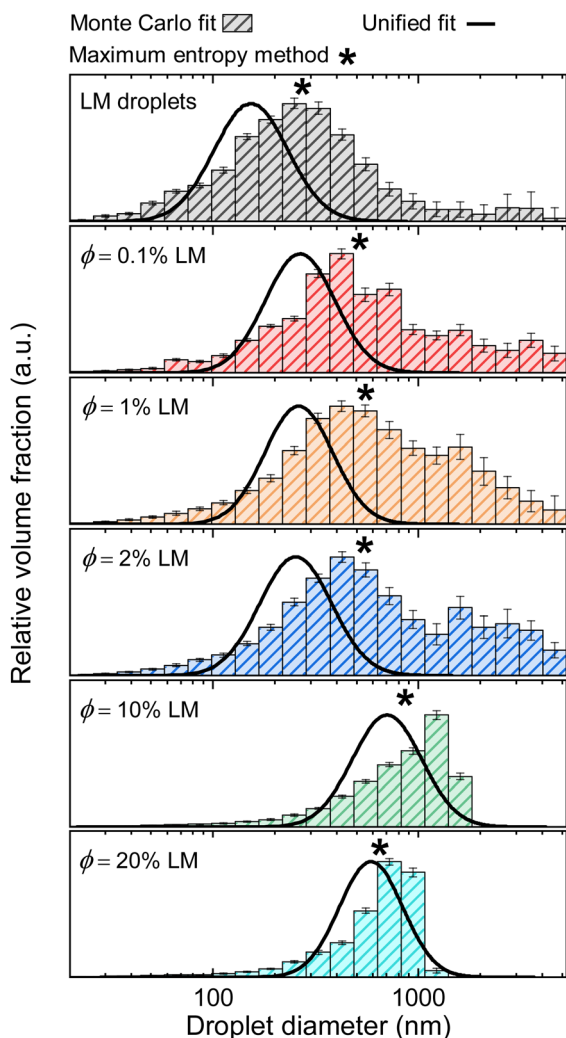
The volume-weighted MC droplet size distributions for the LM droplets and composites are shown in Fig. 6. For the LM droplets and the composites, the histograms reveal a broad distribution of droplet sizes. For the  $\phi = 1$  and 2% composites, an additional population of larger features appears, which is related to the intensity upturn at low  $q$  (Fig. 3). The histograms for the  $\phi = 10$  and 20% LM composites reveal an asymmetric distribution with a limiting size of  $D \approx 1500$  nm. The primary droplet diameter from the Monte Carlo method was chosen as the mode of the histograms (*i.e.*, the most prevalent droplet size corresponding to the height of the histogram distribution) and is shown in Fig. 7. In agreement with the Unified size distribution, the MC method also reveals that the droplet sizes increase as the volume fraction of the filler is increased. The slight weighting of



**Fig. 5** Unified fit of  $\phi = 20\%$  LM composite. The single structural level represents scattering from the primary droplets. The correlation length calculated from the Unified/Born–Green equation is on the order of  $1 \mu\text{m}$ . The fit parameters can be found in Table 2.

**Table 2** Unified/Born–Green fit parameters of eqn (3)–(5) for  $\phi = 10\%$  and  $20\%$  composites

Composite	Level 1 Unified/Born–Green – primary particle						
	$G_1 \times 10^9 \text{ (cm}^{-1}\text{)}$	$R_{g,1} \text{ (nm)}$	$D_1 \text{ (nm)}$	$B_1 \times 10^{-4} \text{ (cm}^{-1} \text{ \AA}^{-P_1}\text{)}$	$P_1$	$\eta$	Packing factor, $p$
10% LM	$6.5 \pm 0.2$	$580 \pm 10$	$1500 \pm 30$	$0.57 \pm 0.001$	4	$1500 \pm 30$	$0.62 \pm 0.06$
20% LM	$6.5 \pm 0.3$	$430 \pm 8$	$1100 \pm 20$	$1.4 \pm 0.003$	4	$940 \pm 20$	$0.98 \pm 0.09$

**Fig. 6** Volume-weighted size distributions from the Unified fit distribution method (solid black curves) and the Monte Carlo method (histogram bars). The droplet size determined from the maximum entropy method is shown as the asterisk (\*).

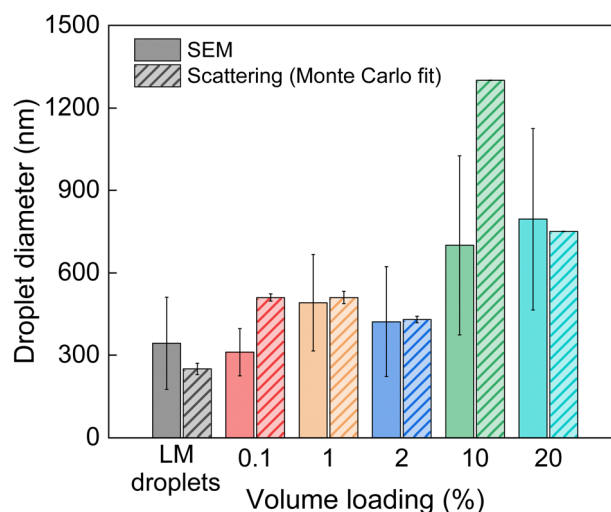
the Monte Carlo distributions towards larger droplet sizes can be attributed to the fact that the Unified method models a single level of the scattering profile, whereas the MC method modelled the whole scattering profile. The MC model fits are shown in Fig. S6 (ESI†). The maximum entropy method, another robust method for determining arbitrary size distributions of dilute scatterers,<sup>43,63,64</sup> was also used to determine the droplet size distribution (Fig. S7 and S8, ESI†) and the median droplet size is denoted by an asterisk (\*) in Fig. 6. Again, the maximum entropy

method reveals reasonable agreement between the particle size distribution methods.

### 3.5 Comparison of SEM and X-ray scattering methods

The droplet sizes obtained from the Monte Carlo method are compared to the sizes obtained from SEM image analysis in Fig. 7. This analysis of the prevalent droplet sizes demonstrates strong agreement between the different characterization methods.

A comparison of the particle size distributions obtained from SEM image analysis and the Monte Carlo analysis of the scattering data is visualized in Fig. 8(a), where the size distributions from both SEM and Monte Carlo scattering analyses are plotted together, alongside representative SEM images for the corresponding specimen (Fig. 8(b)). One notable observation is that the results from the Monte Carlo analysis show the presence of scatterers larger than the individual droplets observed in SEM analysis. This observation can be attributed to the mass fractal aggregates that form through agglomeration of primary droplets. Again, this is seen in the SEM images of the low volume loading composites ( $\phi = 0.1, 1$ , and  $2\%$ ) that show distinct agglomeration (Fig. 8(b)). From the comparison in Fig. 6 and 7, it is clear that X-ray scattering is capable of detecting the structures of LM composites across many length scales and revealing size distributions that would require many SEM images to elucidate. While the structure-free Monte Carlo method

**Fig. 7** Droplet sizes for the pristine LM droplets and when dispersed as a filler in PDMS at different volume loadings, as determined from the image analysis on SEM micrographs and Monte Carlo fits on the X-ray scattering data. The values from the Monte Carlo fit correspond to the particle size in the greatest frequency (i.e., the mode).

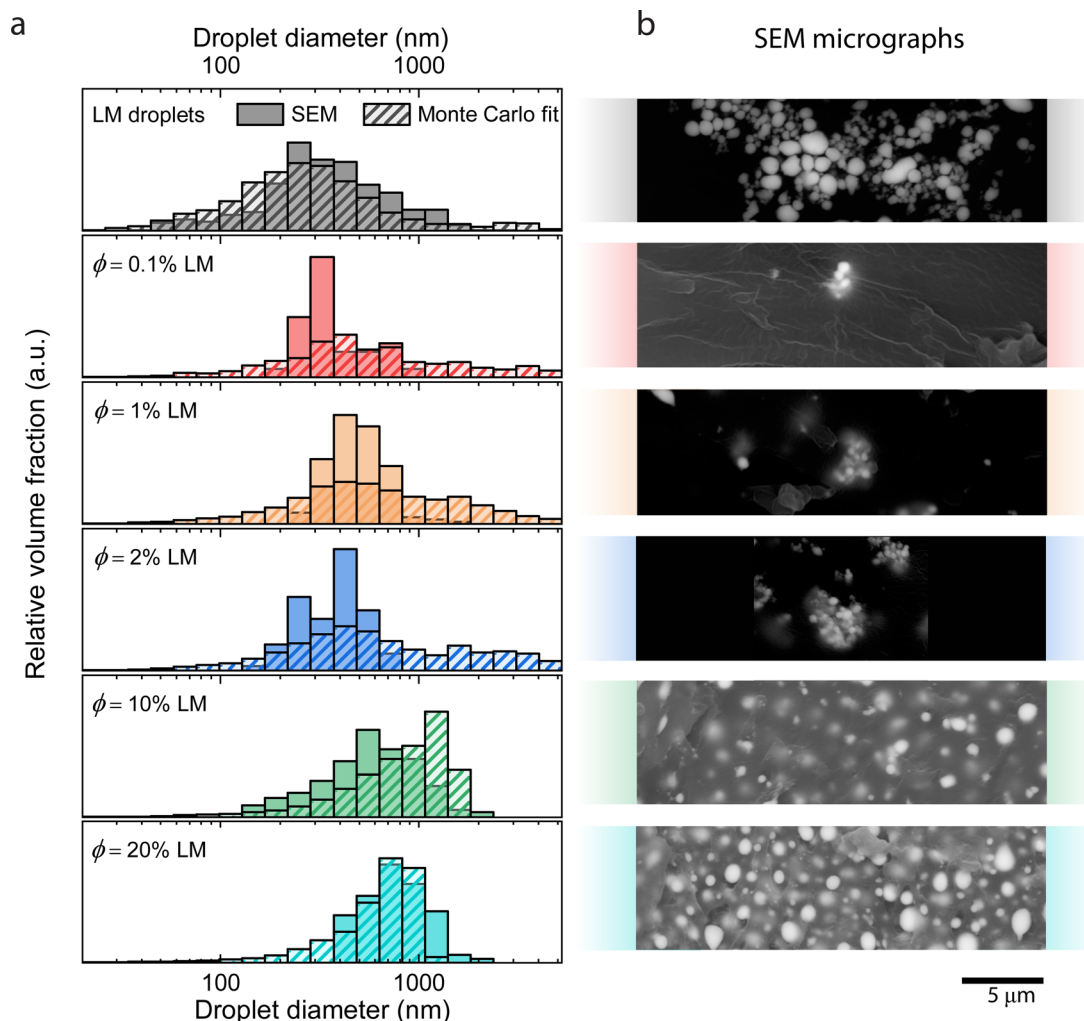


Fig. 8 (a) Size distributions of the LM droplets and composites at various LM loadings ( $\phi = 0.1, 1, 2, 10, 20\%$ ) overlaid on the histograms obtained from Monte Carlo fits on the scattering data. (b) Representative SEM micrographs of the samples corresponding to the histogram overlays. The histograms have been normalized such that the total area of all bins is equal to 100%.

is typically applied for dilute systems, it showed excellent agreement with the Unified model and maximum entropy size distribution methods. The small discrepancies between SEM image analysis and X-ray scattering techniques can be understood by microscopy being a surface technique, providing only a local two-dimensional description of the morphology, whereas scattering is a bulk measurement technique providing more information as it relates to the bulk of the sample.

## 4 Conclusions

This work details the characterization of LM composite morphologies through a combination of scanning electron microscopy and X-ray scattering. Results from USAXS were interpreted using the Unified and Unified/Born-Green approaches to characterize the droplet dimensions, the mass-fractal aggregates, and the interdroplet interactions. The Unified, Monte Carlo, and maximum entropy particle size distribution

methods were used to characterize the primary droplet and aggregate size distributions and revealed the presence of droplets spanning many length scales in size. The results from each method clearly reveal that the LM droplet sizes in the composites are slightly larger compared to the pristine droplets, which suggests that smaller droplets are agglomerating and possibly coalescing to form larger droplets or clusters during the fabrication process. Future studies with varying mixing conditions and higher volume loading composites could provide more insight on coalescing mechanisms. For additional future studies, we will use this X-ray scattering method to systematically study the effects of a variety of important processing parameters such as mixing protocols, solvent choice, and interfacial compatibility on the dimensions of liquid metal composites.

The high electron density of EGaIn and other liquid metals, relative to the polymer matrix, positions X-ray scattering to be a sensitive and effective tool to study the morphology of a variety of nano-structured LM-containing systems. For example, X-ray scattering can be utilized to study the shape and size transformation

of LM droplets in solutions,<sup>65</sup> and soft robots.<sup>66</sup> This method will be particularly useful in light of recent advancements of techniques to carefully control the size and distribution of the droplets in the 1–100 nm size range.<sup>67</sup> We anticipate the USAXS/SAXS/WAXS technique,<sup>68,69</sup> in combination with the scattering models presented here, will be attractive methods to non-destructively characterize global-averaged size distributions and polydispersity in many of these widely studied and utilized materials.

## Author contributions

E. R. C., R. T., R. B. M., and M. D. B. designed research; E. R. C. and R. T. performed research; E. R. C., R. T., R. B. M., and M. D. B. analyzed data; E. R. C., R. T., R. B. M., and M. D. B. wrote and revised the manuscript.

## Conflicts of interest

There are no conflicts to declare.

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