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## Pattern formation in thin polymeric films via electrohydrodynamic patterning

Guowei Lv,<sup>ab</sup> Hongmiao Tian,<sup>c</sup> Jinyou Shao<sup>c</sup> and Demei Yu<sup>b</sup>   <sup>\*a</sup>

The free surface of a thin polymeric film is often unstable and deforms into various micro-/nano-patterns under an externally applied electric field. This paper reviews a recent patterning technique, electrohydrodynamic patterning (EHDP), a straightforward, cost-effective and contactless bottom-up method. The theoretical and numerical studies of EHDP are shown. How the characteristic wavelength and the characteristic time depend on both the external conditions (such as voltage, film thickness, template-substrate spacing) and the initial polymer properties (such as rheological property, electrical property and surface tension) is theoretically and experimentally discussed. Various possible strategies for fabricating high-aspect-ratio or hierarchical patterns are theoretically and experimentally reviewed. Aligning and ordering of the anisotropic polymers by EHDP is emphasized. A perspective, including novelty and limitations of the methods, particularly in comparison to some conventional patterning techniques, and a possible future direction of research, is presented.

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### 1 Origin of EHDP

Over the past few decades, the urgent need of micro- and nano-structures for manufacturing high-performance devices, such as integrated circuits, optoelectronic devices, and sensor arrays, has motivated the development of new patterning techniques.<sup>1–5</sup> In 1999, Chou *et al.* observed that a periodic pillar

array with a micrometer scale was formed in a thin polymer film.<sup>6–14</sup> Although without the external electric field, the key driving force for the formation of the micro-/nano-structures is the internal localized electrical field generated between the contactor and the polymer film. In 2000, Schaffer *et al.* reported a straightforward, cost-effective and contactless (positive replica) patterning technique, electrohydrodynamic patterning (EHDP), that creates and replicates lateral hierarchical structures with a submicrometre length scale on various kinds of materials (e.g. thermoplastic polymer,<sup>15–22</sup> thermosetting polymer,<sup>23–29</sup> photocurable resin,<sup>30–34</sup> ceramic,<sup>35–37</sup> and so on) under an externally applied electric field.<sup>38–47</sup> Especially, the capability of EHDP with a featureless template to fast and economically create large-scale three-dimensional micro-scale structures,

<sup>a</sup>School of Chemistry, State Key Laboratory of Electrical Insulation and Power Equipments, MOE Key Laboratory for Non-Equilibrium Synthesis and Modulation of Condensed Matter, Xi'an Jiaotong University, Xi'an 710049, Shaanxi, P. R. China. E-mail: dmyu@xjtu.edu.cn

<sup>b</sup>Xi'an Aerospace Chemical Propulsion Co., Ltd., Xi'an 710025, Shaanxi, P. R. China

<sup>c</sup>State Key Laboratory of Manufacturing Systems Engineering, Xi'an Jiaotong University, Xi'an 710049, Shaanxi, P. R. China



Guowei Lv received his PhD degree in materials science and engineering from Xi'an Jiaotong University, Xi'an, China, in 2017. He is currently an Assistant Research Fellow of Xi'an Aerospace Chemical Propulsion Co., Ltd. He has authored/coauthored more than 20 research papers in international journal and conference proceedings. His research interests include conducting polymer and patterning.



Hongmiao Tian received his PhD degree in mechanical engineering from Xi'an Jiaotong University, Xi'an, China, in 2014. He is currently an Associate Professor with the State Key Laboratory for Manufacturing Systems Engineering, Xi'an Jiaotong University. He has authored/coauthored more than 70 research papers in international journal and conference proceedings and authorized 30 national invention patents. His research interests include bionic manufacturing and soft actuators.



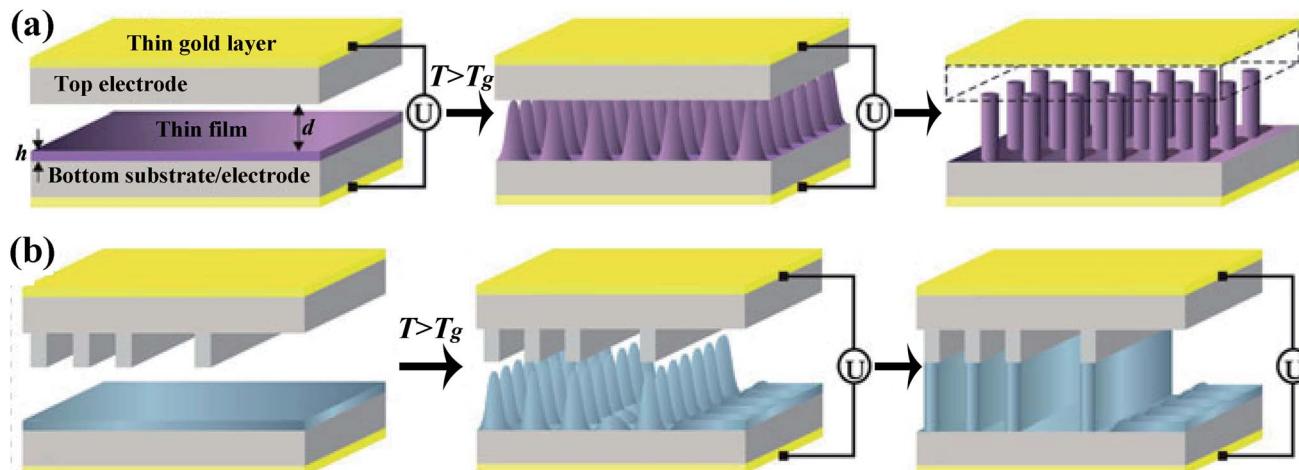
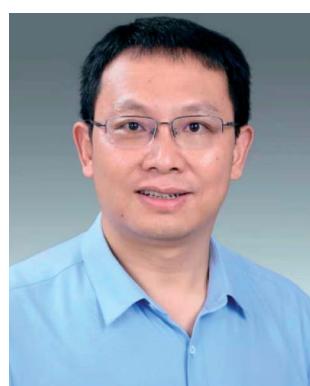


Fig. 1 The diagrammatic sketch of EHDP with (a) a featureless template and (b) a patterned template. Reproduced with permission.<sup>66</sup> Copyright 2013, Springer International Publishing Switzerland.

even though no long range order, is particularly attractive because the difficulty, time, and cost in designing and making pre-patterned templates limit the flexibility and wide application of conventional lithography, especially when large numbers of different patterns are to be fabricated.<sup>48</sup> It is worth noting that a higher value of  $f(h/H)$ , the ratio of the polymer film thickness to the template-substrate spacing, leads to a denser packing of the polymer columns and to an enhanced electrostatic repulsion between the equally charged columns, resulting in columns with a perfect hexagonal symmetry and, however, an accelerating coarsening,<sup>15</sup> a lower value of  $f$  leads to the suppression of coarsening.<sup>49,50</sup> Hence, the highly ordered arrays of columns only can be obtained in a very narrow  $f$  range.<sup>51</sup> In addition, EHDP just need a minimized external force to maintain a proper air gap between the liquid polymer and the

template, avoiding a poor geometrical integrity of the duplicated micro-/nano-structure or even to an irreversible damage of the substrate and the template.<sup>52</sup>

The diagrammatic sketch of EHDP is shown in Fig. 1.<sup>53</sup> Firstly, a thin film of the polymer is spin-coated on a conductive substrate (bottom electrode). Then a template (top electrode) is put on the top of the polymer film, leaving an air gap. Secondly, the assembly is then thermally maintained above the glass transition temperature ( $T_g$ ) of the polymer, and then an external voltage is applied between the bottom and top electrode. This applied voltage causes a destabilizing electrostatic force due to the mismatch of the dielectric constant or the electrical conductivity between polymer and air. Once the destabilizing electrostatic force overcomes the stabilizing surface tension and the viscous resistance, the flat polymer surface will be



*Jinyou Shao received his PhD degree in mechanical engineering from Xi'an Jiaotong University, Xi'an, China, in 2009. He is currently the President of Frontier Institute of Science and Technology (FIST), a Professor at the State Key Laboratory for Manufacturing Systems Engineering, Xi'an Jiaotong University, and the leader of the Youth Innovation Team of Shaanxi Universities.*

*His research interests include micro/nano-manufacturing techniques, flexible electronics, nanosensors and devices, etc. Dr Shao is awarded NSFC Fund for Distinguished Scholars, NSFC Fund for Excellent Young Scholars, Changjiang Scholars -Young Category, New Century Excellent Talents by MoE of China, Shaanxi Young Talents in Science and Technology, etc.*



*Demei Yu received her PhD degree from Xi'an Jiaotong University, Xi'an, China, in 1998. She joined Xi'an Jiaotong University in 1984, and served as professor and founding chair of the Department of Applied Chemistry in Xi'an Jiaotong University since 2001. In addition, she is also a professor and lab committee member of State Key Lab of Electrical Insulation and Power Equipment in Xi'an Jiaotong University since 2004. Her research interests include: (1) design and fabrication of functional micro-/nano-materials; (2) synthesis and preparation of smart polymer (conductive polymers, electroactive polymers); (3) design and preparation of polymer micro-/nano-composites with high performance (electrical, thermal and mechanical properties); (4) polymer processing and polymer rheology.*



destabilized and forced to flow upward to the top electrode. The growth of peaks reduces the air gap between the polymer film and the template, which strengthens the electrical field and accelerates the evolution. As the peaks grow, the capillary pressure also increases. Therefore, the competition between destabilizing electrostatic pressure and the stabilizing capillary pressure selects a maximum characteristic wavelength  $\lambda$  and a characteristic time  $\tau$ .<sup>48</sup> Finally, the micro-/nano-structure of the polymer will fully contact with the top electrode and then reach a steady state. After that, a slow cooling of the assembly to room temperature or UV light cures the micropillars array. In this process, the template can be either featureless (Fig. 1a),<sup>15,17,27</sup> generating an array of periodic pillars, or patterned (Fig. 1b),<sup>15,37,39,41,46,54–65</sup> forming a positive replica of the template.

## 2 Theoretical and numerical studies

The overall pressure distribution at the viscous film surface is

$$p(h) = p_0 + p_{\text{vdw}}(h) + p_{\gamma}(h) + p_e(h) \quad (1)$$

where  $p_0$  is the atmospheric pressure,  $p_{\text{vdw}}(h)$  is the disjoining pressure (arising from dispersive van der Waals interactions),  $p_{\gamma}(h)$  is the Laplace pressure (stems from the surface tension  $\gamma$ ) and  $p_e(h)$  is the electrostatic pressure.<sup>16</sup>

For high enough values of electric field intensity, only the Laplace and electrostatic terms need to be considered. In a stability analysis, a small sinusoidal perturbation of the interface with wave number  $q$ , growth rate  $\omega$ , and amplitude  $u$  is considered:  $h(x, t) = h_0 + ue^{iqx+it\omega}$ . The modulation of  $h$  gives rise to a lateral pressure gradient inside the film, inducing a Poiseuille flow  $j$

$$j = \frac{h^3}{3\eta} \left( -\frac{\partial p}{\partial x} \right) \quad (2)$$

where  $\eta$  is the viscosity of the liquid. A continuity equation enforces mass conservation of the incompressible liquid

$$\frac{\partial j}{\partial x} + \frac{\partial h}{\partial t} = 0 \quad (3)$$

Eqn (1)–(3) establish a differential equation that describes the dynamic response of the interface to the perturbation. In a linear approximation, a dispersion relation is obtained

$$\omega = -\frac{h^3}{3\eta} \left( \frac{\partial p_e}{\partial h} q^2 + \gamma q^4 \right) \quad (4)$$

As opposed to the inviscid, gravity-limited case ( $\omega \propto q$ ), the viscous stresses lead to a  $q^2$ -dependence of  $\omega$  in the long-wavelength limit, typical for dissipative systems. Fluctuations are amplified if  $\omega > 0$ . With time, the fastest growing fluctuation will eventually dominate

$$\frac{\partial \omega}{\partial q} = -\frac{h^3}{3\eta} \left( 2q \frac{\partial p_e}{\partial h} + 4\gamma q^3 \right) = 0 \Rightarrow q = \sqrt{\frac{-\partial p_e / \partial h}{2\gamma}} \quad (5)$$

When mobile free charge is absent (*i.e.* perfect dielectric), the characteristic wavelength  $\lambda$  and the characteristic time  $\tau$  is

$$\lambda = \frac{2\pi}{U} \sqrt{\frac{2\gamma}{\varepsilon_0 \varepsilon_p (\varepsilon_p - 1)^2}} [\varepsilon_p H + (1 - \varepsilon_p)h]^{3/2} \quad (6)$$

and

$$\tau = \frac{12\eta\gamma [h + \varepsilon_p(H - h)]^6}{U^4 h^3 (\varepsilon_p \varepsilon_0)^2 (\varepsilon_p - 1)^4} \quad (7)$$

where  $\varepsilon_0$  is the dielectric constant of free space,  $\varepsilon_p$  is the dielectric constant of the polymer film,  $\gamma$  is the surface tension of the polymer film,  $U$  is the applied voltage,  $h$  is the thickness of the polymer film, and  $H$  is the template-substrate spacing.

When mobile free charge is present (*i.e.* leaky dielectric), the dielectric constant and a dimensionless conductivity parameter  $S$  jointly play roles. The latter represents a ratio of the process time scale to the time for charge conduction ( $\varepsilon_g \varepsilon_0 / \sigma$ )

$$S = \sigma \eta \gamma H^3 / \varepsilon_0^3 U^4 \quad (8)$$

Especially, when  $S \gg 1$ , the characteristic wavelength  $\lambda$  and the characteristic time  $\tau$  is

$$\lambda = \frac{2\pi}{U} \sqrt{\frac{2\gamma}{\varepsilon_0}} (H - h)^{\frac{3}{2}} \quad (9)$$

and

$$\tau = \frac{12\eta\gamma (H - h)^6}{U^4 h^3 \varepsilon_0^2} \quad (10)$$

where  $\sigma$  is the electrical conductivity of the thin polymer film.<sup>67–70</sup>

## 3 Effect of the external conditions on the pattern formation

In continuing the steady development of integrated circuit-related fabrication, the ability to rapidly pattern polymers into smaller feature size and/or higher aspect ratio in order to realize

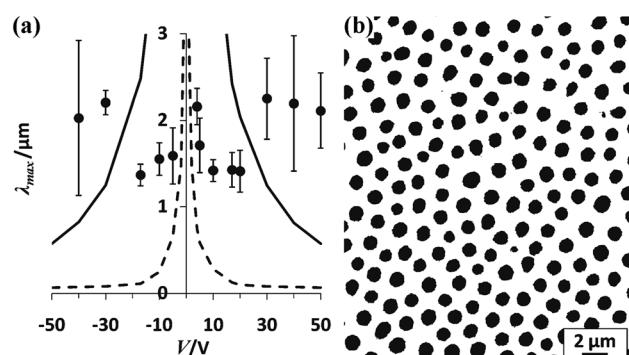


Fig. 2 EHDP of PMMA2K-air. (a) Plot of the characteristic wavelength  $\lambda$  vs. the applied voltage. (b) An optical micrograph of pillars formed at 10 V. Reproduced with permission.<sup>71</sup> Copyright 2011, American Chemical Society.



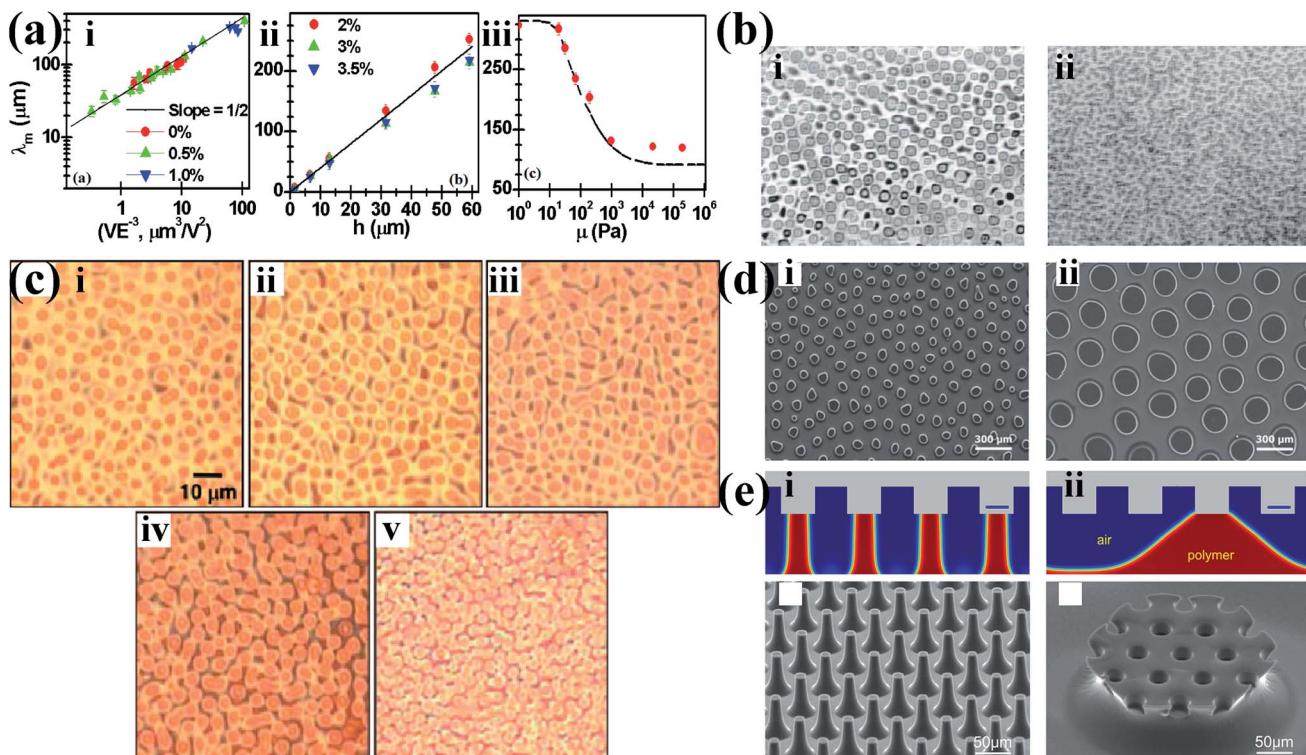


Fig. 3 (a(i)) The characteristic wavelength  $\lambda$  vs.  $VE^{-3}$  in log–log scale for viscoelastic liquidlike films. (ii) The characteristic wavelength  $\lambda$  vs. the film thickness  $h$  for viscoelastic solidlike films. (iii) The characteristic wavelength  $\lambda$  vs. the storage modulus  $\mu$  for viscoelastic films between the liquidlike and the solidlike regimes. Reproduced with permission.<sup>24</sup> Copyright 2009, American Physical Society. (b) Optical microscopy image of EHDP patterns of (i) a thin liquid film of PI and (ii) a bilayer of PI and ODMS. Reproduced with permission.<sup>77</sup> Copyright 2001, American Institute of Physics. (c) EHDP patterns of various Au(PS) thin films: (i) Au(PS) 0 vol%; (ii) Au(PS) 0.05 vol%; (iii) Au(PS) 0.25 vol%; (iv) Au(PS) 0.5 vol%; (v) Au(PS) 1.0 vol%. Reproduced with permission.<sup>78</sup> Copyright 2008, American Chemical Society. (d and e) Simulated and experimental deformation of EHDP with (d) a featureless template and (e) a structured template for (i) the leaky dielectric and (ii) perfect dielectric. Reproduced with permission.<sup>33</sup> Copyright 2016, Royal Society of Chemistry. Reproduced with permission.<sup>31</sup> Copyright 2014, American Chemical Society.

devices with enhanced performance or even wholly new properties begins to take a more prominent role in their advanced applications.

According to eqn (6)–(10), changing the external conditions such as decreasing the template-substrate spacing ( $H$ ),

increasing the polymer film thickness ( $h$ ) and increasing the applied voltage ( $U$ ) can fabricate micro/nano-patterns with a shorter characteristic time and a smaller characteristic wavelength *via* EHDP for both the perfect and leaky dielectric. For example, Russel *et al.* showed that the characteristic

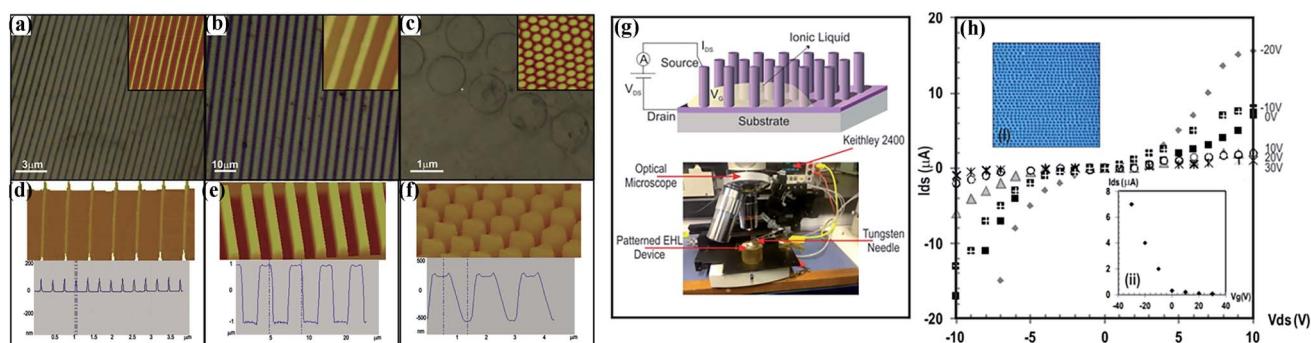


Fig. 4 (a–f) Optical microscopy images with height AFM images (inset) and three-dimensional AFM micrographs with cross section analysis of EHDP patterns of PPy. (g) Schematic representation (top) and an overview image (bottom) of the configuration of a liquid-ion gate vertical FET using the EHDP patterns on the top of a Si-SiO<sub>2</sub> substrate. (h) Drain current versus drain voltage characteristics of PPy electrolyte-gated transistor based on (i) EHDP pillars shown in a top-view optical image and (ii) gate voltage performance of the PPy-FET. Reproduced with permission from <https://pubs.acs.org/doi/10.1021/acsnano.6b01246>.<sup>100</sup> Copyright 2016, American Chemical Society (notice: further permissions related to the material excerpted should be directed to the ACS).



wavelength  $\lambda$  decreases with the increase in the applied voltage (below 10 V) at a given system, as shown in Fig. 2a.<sup>71</sup> However, the characteristic wavelength  $\lambda$  no longer decreases or even increases with the increase in the applied voltage (above 10 V) due to the dielectric breakdown in at least one of the layers. If layers break down, submicrometer features are unlikely, as shown in Fig. 2b. Hence, though theory predicts that changing the external conditions will decrease the characteristic wavelength  $\lambda$  to nanoscale level, the limit is set by the dielectric field strength of the layers. In addition, increasing the pattern growth velocity not only shortens the patterning time but also exhibits enhanced scalability for replicating small and geometrically diverse features.<sup>72</sup>

## 4 Effect of the polymer properties on the pattern formation

In EHDP, polymer film materials have played a critical role, since some limitations in accessing better-performance EHDP, such as higher efficiency, smaller feature size, and greater aspect ratio, are of material origin; moreover, the functionality of the generated EHD patterns is governed by EHD materials owing to the interesting properties these materials can offer.

Hence, the performance of EHDP depends on the comprehensive properties of the polymer film to a certain extent.

### 4.1 Rheological property

The rheological property of the polymer noticeably governs the characteristic wavelength  $\lambda$  and the characteristic time  $\tau$  of EHDP.<sup>23–27,73–75</sup> Sharma *et al.* has systematically studied the role of the viscoelastic property of the polymer film in the pattern formation of EHDP.<sup>24</sup> The viscoelastic films behaving like a liquid display long wavelengths governed by applied voltage (or electrostatic pressure) and surface tension, independent of its elastic storage and viscous loss moduli (Fig. 3a(i)); the viscoelastic films behaving like a solid display wavelengths always scales as  $\sim 4 \times$  film thickness, independent of its surface tension, applied voltage, loss and storage moduli (Fig. 3a(ii)); and the viscoelastic films behaving in a narrow transition zone between the liquidlike and the solidlike regimes display a wavelength governed by the storage modulus (Fig. 3a(iii)). It is interesting to note that the viscosity of the polymer film influences the characteristic time  $\tau$  of EHDP. This offers an advantage in EHDP for decoupling time by varying the types or the molecular weight of polymers. For example, Dickey *et al.* showed that the photocurable systems (e.g. thiol vinyl ether,

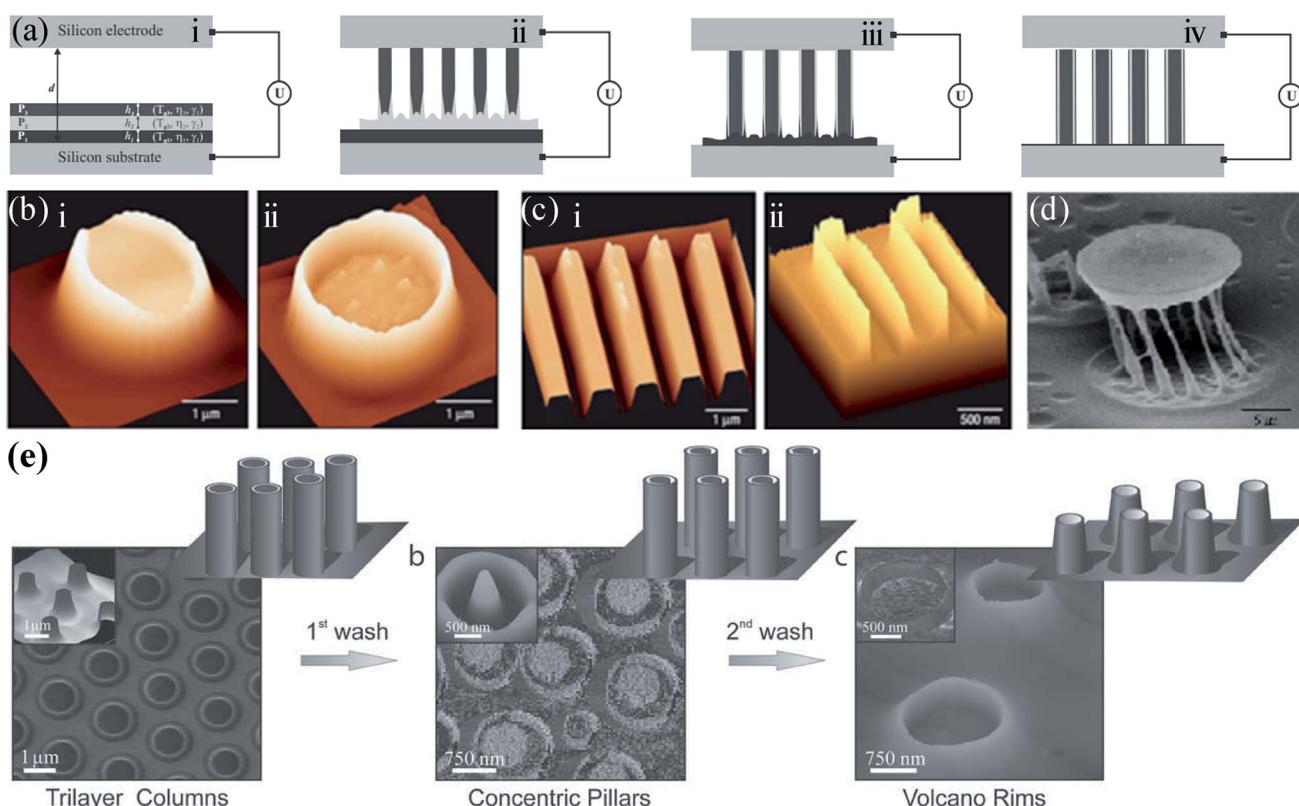


Fig. 5 (a) Mechanism of the EHDP structure formation process for multilayer system. Reproduced with permission.<sup>106</sup> Copyright 2012, WILEY-VCH. (b and c) EHDP with (b) a featureless template and (c) a patterned template patterns of a PMMA-PS-air bilayer: AFM image of a single column before (i) or after (ii) removing the PS core by washing in cyclohexane. Reproduced with permission.<sup>103</sup> Copyright 2002, Nature Publishing Group. (d) EHDP patterns of a PS-PMMA-air bilayer: SEM image of a single "cage" after removing the PS core by washing in cyclohexane. Reproduced with permission.<sup>105</sup> Copyright 2006, American Chemical Society. (e) EHDP patterns of an EC-PVA-PVAc-air trilayer: AFM and SEM images of structures derived from (i) the trilayer coaxial pillars, (ii) central PVAc pillars surrounded by thin EC rims, and (iii) EC nanovolcanos. Reproduced with permission.<sup>106</sup> Copyright 2012, WILEY-VCH.



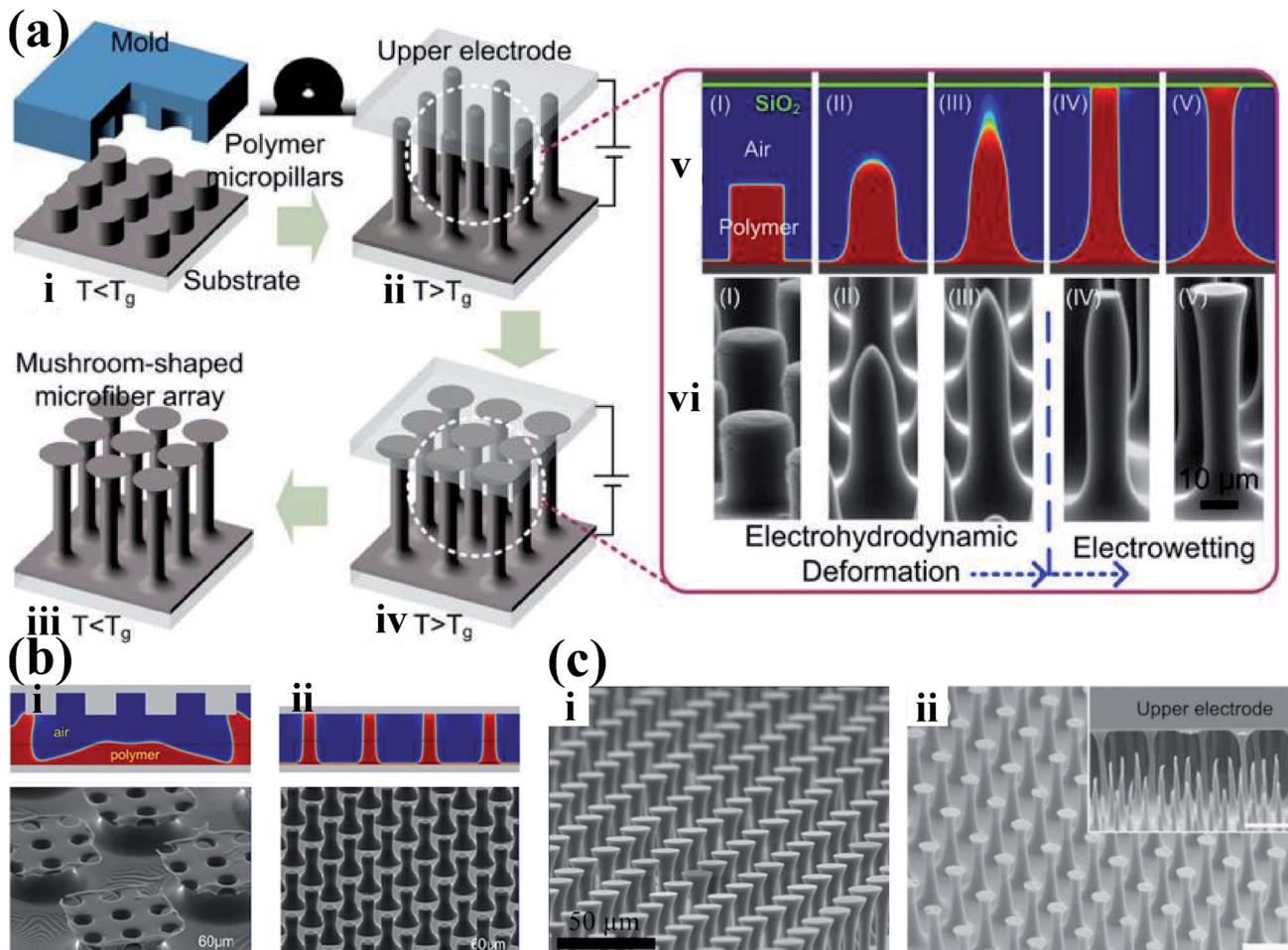


Fig. 6 (a) Illustration of a three-step process for fabricating a bioinspired mushroom-shaped microfiber array with a high aspect ratio. Reproduced with permission.<sup>115</sup> Copyright 2014, American Chemical Society. (b) Simulated and experimental structures fabricated by (i) EHDP-PPT and by (ii) EHDP-PPP. Reproduced with permission.<sup>114</sup> Copyright 2014, American Chemical Society. (c) The mushroom-shaped micropillars with a well-controlled aspect ratio and tip diameter using various polymers: (i) polymethyl methacrylate (PMMA) and (ii) polyvinylidene fluoride (PVDF). Reproduced with permission.<sup>115</sup> Copyright 2014, American Chemical Society. Reproduced with permission.<sup>116</sup> Copyright 2015, Royal Society of Chemistry.

vinyl ether, thiol acrylate, DMS acrylate, epoxy) with a low viscosity (0.1–1.8 Pa s) formed pillar arrays nearly instantaneously under ambient conditions.<sup>30,76</sup> Goldberg-Oppenheimer *et al.* showed that the use of the polymers with a low-viscosity (0.073–1.032 Pa s) evidently reduced the characteristic time.<sup>19</sup> It is worth noting that the rheology property of the polymer is closely related to its temperature. For instance, Cheng *et al.* showed a faster growth of the surface patterns of polystyrene film at a higher temperature due to the lower viscosity.<sup>20</sup> However, the molding temperature cannot exceed the decomposition temperature of the polymer in the pattern formation process.

#### 4.2 Surface/interface tension

The decrease of the surface/interface tension of the polymer film is advantageous to fabricating the micro-/nanostructures with a smaller characteristic wavelength  $\lambda$  and a shorter characteristic time  $\tau$ .<sup>75,77,79–85</sup> For example, a clear reduction in length

scale (2 times) and time scale (50 times) of polyisoprene (PI) film is observed by substituting the air gap with oligomeric dimethylsiloxane (ODMS) film, as shown in Fig. 3b. However, there is a trade-off by replacing air with another fluid because it may decrease the dielectric contrast difference of the system.<sup>48</sup>

#### 4.3 Electrical property

**4.3.1 Dielectric constant.** According to the linear stability analysis based on the perfect dielectric model, when free charges absent (*i.e.*, the perfect dielectric), the dielectric constant  $\epsilon_p$  of the polymer film is important. A smaller characteristic wavelength  $\lambda$  and a shorter characteristic time  $\tau$  is expected with increasing the dielectric constants  $\epsilon_p$  of the layers.<sup>78,86</sup> For instance, Bae *et al.* demonstrated that the increased dielectric constant of the polymer film by the incorporation of nanoparticles into the polymer film led to a significant reduction in the characteristic wavelength  $\lambda$ , as shown in Fig. 3c.<sup>78,86</sup> However, the enhancement of the dielectric constant

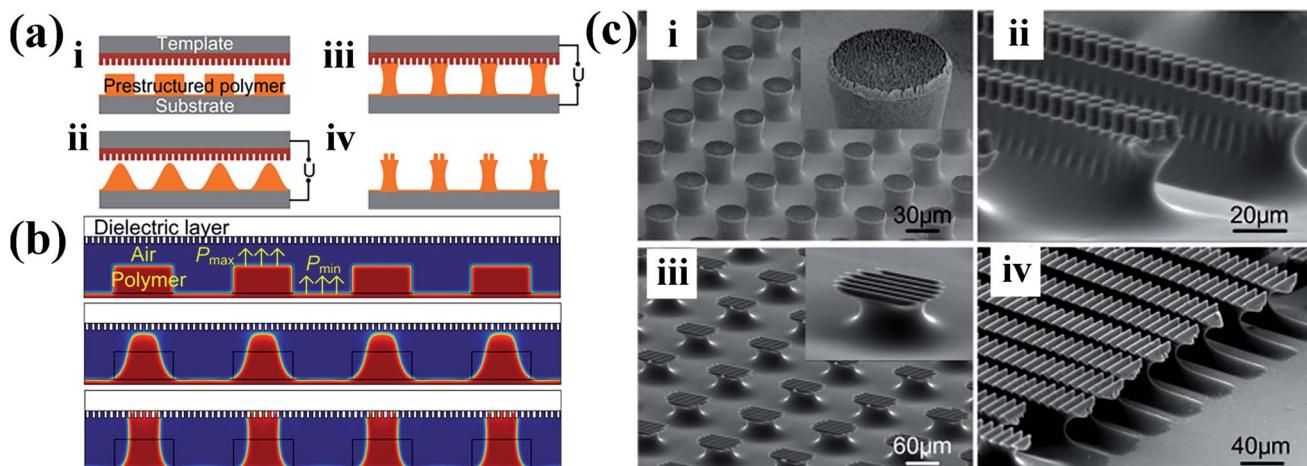


Fig. 7 (a) Scheme and (b) numerical simulations of the process for generating hierarchical structures based on electrohydrodynamic (EHD) structure formation with a prestructured polymer. (c) Hierarchically structured polymer fabricated with different patterned template and prestructured polymer: (i) micropillar/nanopillar structure, (ii) micrograting/micropillar structure, (iii) micropillar/micrograting structure, and (iv) micrograting/micrograting structure. Reproduced with permission.<sup>124</sup> Copyright 2016, American Chemical Society.

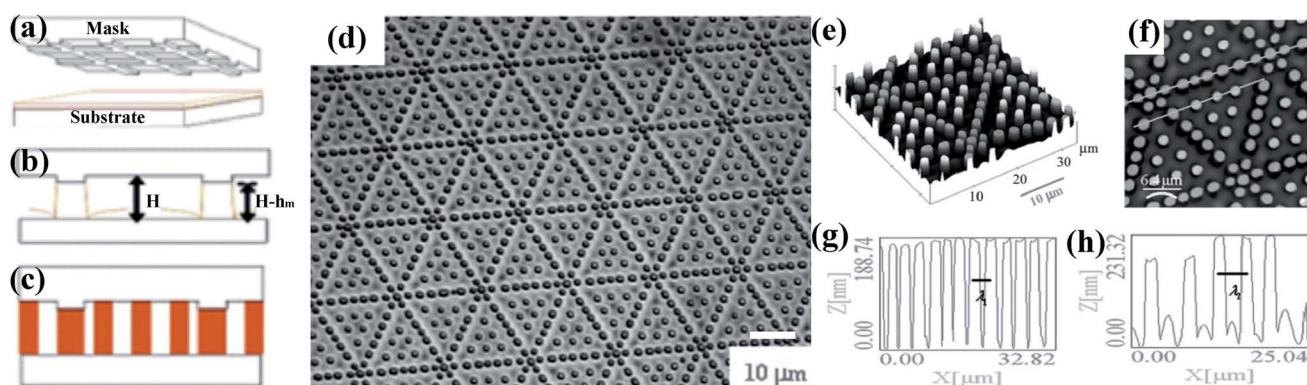


Fig. 8 (a-c) The mechanism of the method used to align the pillars. (d) Optical microscopy images of a 45 nm thick PMMA film patterned on a silicon substrate. (e-h) AFM image of a typical pattern formed on the substrate with central pillars taller than those under the ridges. Reproduced with permission.<sup>126</sup> Copyright 2006, WILEY-VCH.

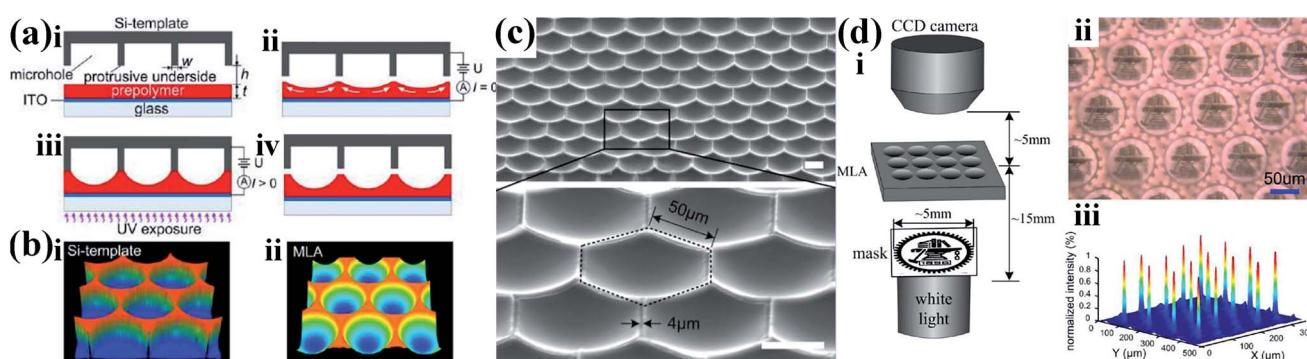
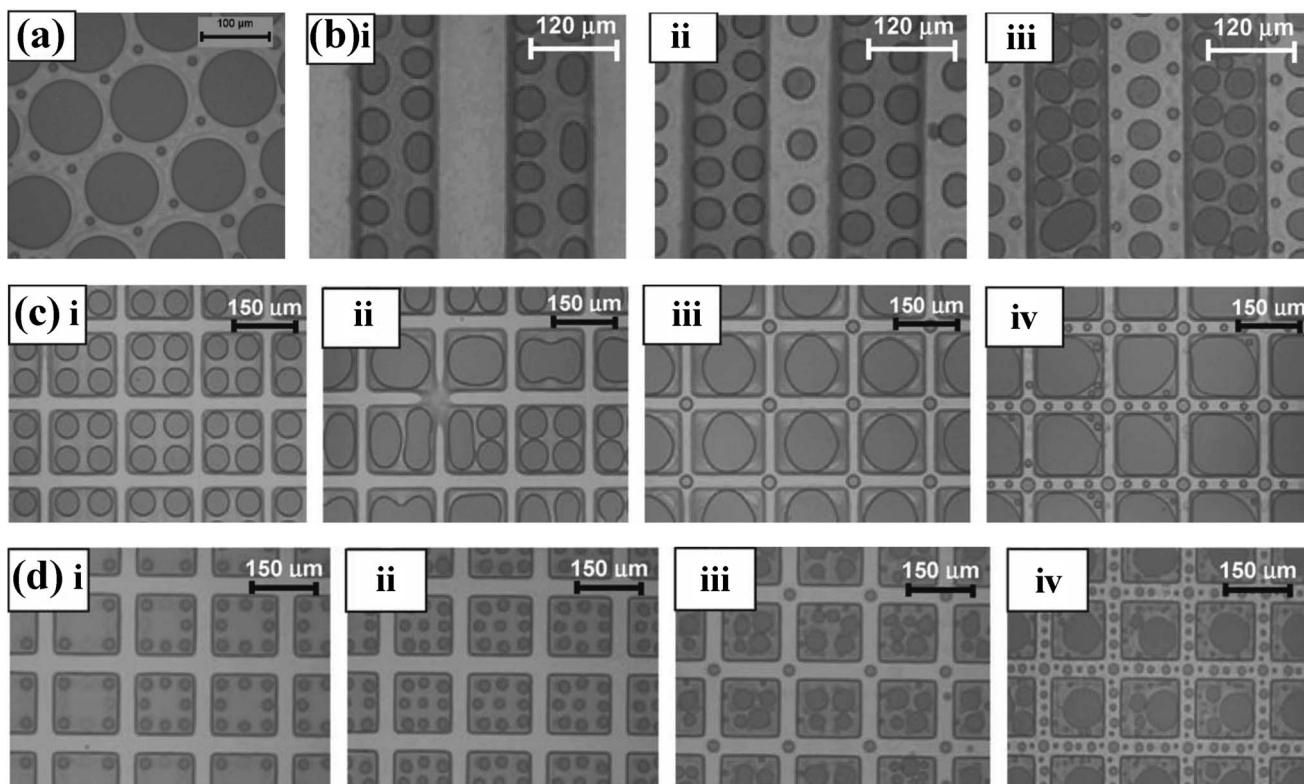


Fig. 9 (a) Illustration of EHDP process for generation of concave MLAs. (b) Experimentally measured 3D profiles of (i) the template arrayed with cylindrical microholes and (ii) the corresponding concave MLA, respectively (acquired by LSCM). (c) SEM images of a concave MLA with a hexagonal aperture. Scale bar: 50  $\mu$ m. (d) Test for the optical properties of concave MLA: (i) diagram of the optical microscopic setup to evaluate imaging and focusing performances of the MLA; (ii) image of the authors' school badge obtained by using a concave MLA with a sag height of  $\sim$ 12  $\mu$ m; (iii) measured light intensity profiles of a concave MLA with a sag height of  $\sim$ 23  $\mu$ m. Reproduced with permission.<sup>44</sup> Copyright 2013, American Chemical Society.





**Fig. 10** (a) Optical micrographs of EHDP under a top flat electrode using the spatiotemporal modulation of the applied electric field. (b) Optical micrographs of EHDP under a top electrode having parallel ridges and stripes of  $w = 120 \mu\text{m}$  using the spatiotemporal modulation of the applied electric field. (c) Optical micrographs of EHDP under a box-patterned top electrode using the spatiotemporal modulation of the applied electric field (box dimension  $\sim 2\lambda$ ). (d) Optical micrographs of EHDP under a box-patterned top electrode using the spatiotemporal modulation of the applied electric field (box dimension  $\sim 3\lambda$ ). Reproduced with permission.<sup>26</sup> Copyright 2011, WILEY-VCH.

by loading nanoparticles is also limited as the excessive filler loading would result in the increase in the viscosity of the polymer and the undesirable nanoparticle agglomeration in the polymer film.

**4.3.2 Electrical conductivity.** Particularly interesting is the characteristic wavelength  $\lambda$  and the characteristic time  $\tau$  that is predicted from leaky dielectric model is smaller than that from the perfect dielectric model.<sup>87-92</sup> Lv *et al.* demonstrated that a leaky dielectric could fulfill high-performance EHDP with a featureless template.<sup>32-34</sup> A significant reduction in the characteristic wavelength  $\lambda$  (from  $325.6 \pm 14.7 \mu\text{m}$  to  $154.5 \pm 15.3 \mu\text{m}$ ) and the patterning time (from 5 s to  $\ll 1$  s) are observed, as shown in Fig. 3d. Furthermore, according to the perfect and leaky dielectric model, the theoretical characteristic wavelength  $\lambda$  is  $368 \mu\text{m}$  (the perfect dielectric) and  $150 \mu\text{m}$  (the leaky dielectric), respectively, hence, the experimental results herein demonstrate a convincing experimental distinction between the “perfect” and “leaky” dielectric models in spite of a slight mismatch between the theoretical and experimental values especially from the perfect dielectric model. Moreover, Tian *et al.* theoretically and experimentally demonstrated that a leaky dielectric could significantly improve the aspect ratio of the micro-/nano-structures fabricated by EHDP with a structured template compared to a perfect dielectric, as shown in Fig. 3e.

Especially, the conducting polymer (CP), as a leaky dielectric, is a promising material for high-performance EHDP in order to realize devices with enhanced performance or even wholly new properties and then take a more prominent role in their advanced applications such as organic electronic devices, chemical sensors, field-effect transistors, superhydrophilic/superhydrophobic surfaces, micro-/nanofluidic systems and micro-/nanoelectromechanical systems (MEMS/NEMS).<sup>93-99</sup> For instance, Rickard *et al.* fabricated well-defined conductive micro-/nano-structures using the thin conducting polymer (*e.g.* polypyrrole, poly(3-hexylthiophene), and so on) films *via* EHDP, as shown in Fig. 4a-f.<sup>100-102</sup> Moreover, they showed the feasibility of the polypyrrole-based structures with a gate length of 700 nm and a pitch of 500 nm for the electrolyte-gated vertical field-effect transistor (FET) devices, as shown in Fig. 4g-h.

## 5 Fabrication of hierarchical structures

To date, several techniques structure a single layer of the polymer. For many applications, however, it is desirable to control the spatial arrangement of more than one component. Morariu *et al.* describes a replication process where multiple materials with an air gap between the film and the contactor are



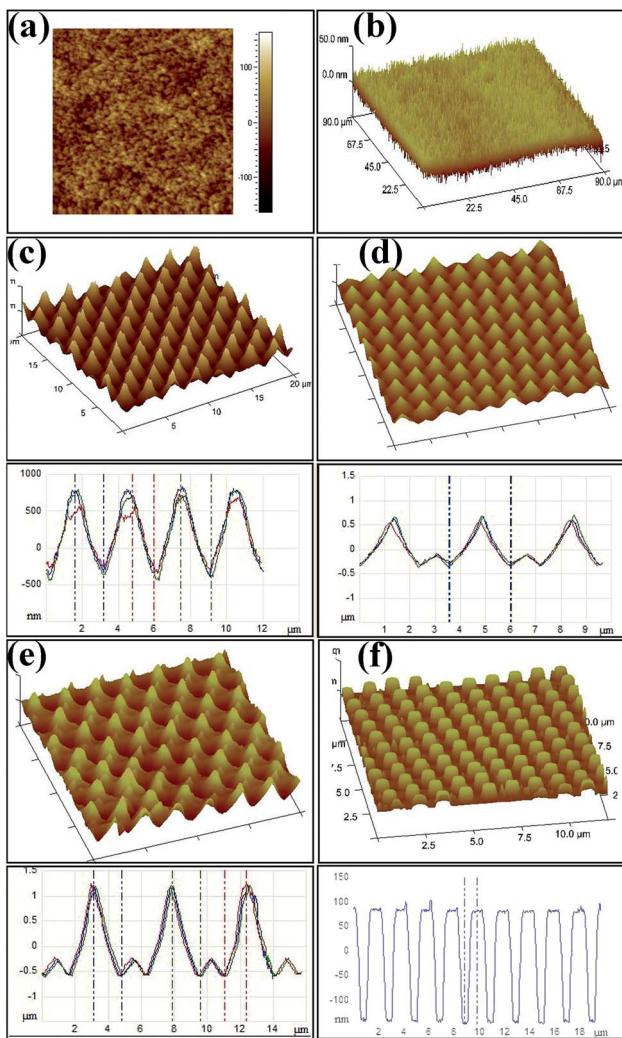


Fig. 11 CNT-EHDP replicated patterns. Atomic force microscopy height and three-dimensional images and the corresponding cross-sections of (a) curly nano-hair (CNH) surfaces, (b) straight nano-hairs (SNH), (c) single-level spikes with rounded edges (S1L), (d) two-levelled spiky cones (S2L), (e) two-tiered heretical spiky cones (S2L2) and (f) hexagonal pillars (HP) replicated from the various imposed CNT-based electrodes. Reproduced with permission.<sup>22</sup> Copyright 2017, Royal Society of Chemistry.

processed simultaneously, as shown in Fig. 5a.<sup>103–112</sup> Using a bilayer or trilayer formed by two or three different polymers, EHDP at both polymer surfaces produce a hierarchic lateral structure that exhibits two or three independent characteristic dimensions, as shown in Fig. 5b–e.<sup>103–112</sup> This approach might provide a simple strategy for large-area, sub-100 nanometre lithography.

EHDP with a featureless template shows the capability to fast and economically create large-scale three-dimensional micro-scale structures on various kinds of materials. However, conventional EHDP with a featureless template can only fabricate a low-aspect-ratio micro-/nanostructures. Therefore, much research have been devoted to increase the aspect ratio of the micro-/nanostructures.<sup>113,114</sup> For instance, Tian *et al.* developed a novel EHDP technique, EHDP-prepatterned polymer (PPP), to fabricate a hierarchical micro-/nanostructure with a high aspect ratio, as shown in Fig. 6a.<sup>114</sup> The simulation and experiment showed that EHDP-PPP approach can provide a stronger electric modulation at the same experimental settings, obtaining a hierarchical micro-/nanostructure with a higher aspect ratio compared to EHDP-prepatterned template (PPT), as shown in Fig. 6b. This method can deform various polymers to a mushroom-shaped micropillars with a well-controlled aspect ratio and tip diameter for dry adhesion, nanogenerator, superhydrophilic/superhydrophobic surfaces, microlens arrays, and so on, as shown in Fig. 6c.<sup>115–123</sup> Furthermore, to fabricate a hierarchically ordered structure, Tian *et al.* improved above EHDP-PPP method by substituting the featureless template with a patterned template which feature size is far less than the characteristic wavelength  $\lambda$  of the given system, as shown in Fig. 7a and b. The hierarchically ordered structures with primary and secondary patterns for mass-production, such as, micropillar/nanopillar structure, micrograting/micropillar structure, micropillar/micrograting structure, and micrograting/micrograting structure, were fabricated, as shown in Fig. 7c.<sup>124,125</sup>

Russel *et al.* design and utilize the special template patterns to guide pillars into alignment over regions much greater in extent than their natural domain sizes to pattern thin polymer films *via* EHDP, as shown in Fig. 8a–c. Regular rows of pillars form under ridges, and ordered triangular arrays are generated within each individual triangular domain bounded by the

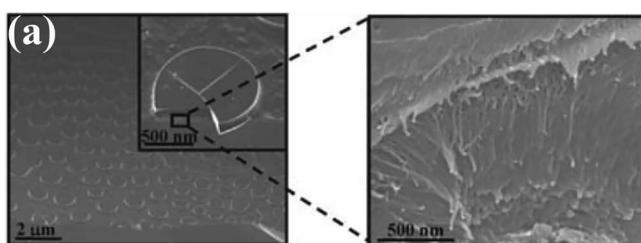


Fig. 12 (a) Low- and high-magnification SEM images of the EHDP micro-pillars that contain vertically aligned MWCNTs. (b) SEM images of the EHDP micro-pillars with partial removal of the PS matrix. (c) SEM top-view of the EHDP micro-pillars with partially exposed vertical MWNTs. Inset: SEM images of the EHDP micro-pillars using CNTs which are slightly longer than the pillar height. Reproduced with permission.<sup>128</sup> Copyright 2011, WILEY-VCH.



ridges, as shown in Fig. 8d. Moreover, the ordered pattern spanned more than 100 periods (400–500  $\mu\text{m}$ ), which is the largest array of ordered pillars from EHDP available in the literature. The ordered pattern had two identified characteristic wavelength: one is the spacing between pillars under the ridges,  $\lambda_1$  ( $\sim 2.7 \mu\text{m}$ ), and the other is the spacing between pillars within each small triangular array,  $\lambda_2$  ( $\sim 4.0 \mu\text{m}$ ), as shown in Fig. 8e–h.

Li *et al.* presented an economical method for fabricating a concave microlens arrays (MLAs) with a high quality and high density, as shown in Fig. 9a and b.<sup>44</sup> The curvature of the MLA can be well-controlled by changing the air gap between the template and polymer film. The MLA has a fill factor calculated as high as up to 93%, as shown in Fig. 9c. Moreover, the MLA has excellent focusing and imaging performances, as shown in Fig. 9d.

Sharma *et al.* showed that the spatiotemporal modulation of the applied electric field influences the pattern morphology in incompletely cross-linked viscoelastic polydimethylsiloxane (PDMS) films, due to the appearance of secondary and tertiary structures, resulting in hierarchical, multiscale patterns, which can be observed in Fig. 10.<sup>26</sup> Park *et al.* also investigated secondary electrohydrodynamic instability in polymer films by controlling the timescale parameter to produce secondary nanosized patterns between the micrometer-sized grooves.<sup>127</sup>

Goldberg-Oppenheimer *et al.* proposed a tunable carbon nanotubes-based electrohydrodynamic patterning (CNT-EHDP) to fabricate unique multiscale structured cones and nanohair-like architectures with various periodicities and dimensions, successfully enabling surface energy minimization, as shown in Fig. 11.<sup>22</sup> By controlling the hierarchy of micro- to nano cones and spikes, these morphologies provide a range of architectures with sufficient roughness for very low wettability, with the highest contact angle achieved of 173° and their properties can be easily switched between lotus-leaf to rose-petal behavior.

## 6 Aligning and ordering of the anisotropic polymers

In order to take full advantage of the synergistic functions in carbon nanocomposites and hybrids, control of the dispersion, orientation, and interfacial chemistry of carbon materials in the organic or inorganic matrix is required. Moreover, anisotropic composite structures with vertically aligned carbon materials are essential to realize the full potential of carbon materials-based composites both for optimization of their mechanical properties and integration into devices. Goldberg-Oppenheimer *et al.* showed that the EHDP micro-patterns along with the alignment of carbon nanotubes (CNTs) within these patterns can be fabricated for carbon nanotube-polymer nanocomposite films by EHDP with a featureless template, as shown in Fig. 12a and b.<sup>128</sup> The degree of the carbon nanotube alignment within these patterns can be tuned by adjusting the EHDP parameters. Furthermore, patterned surfaces decorated by CNT brushes can be obtained using either etching techniques or by embedding relatively long nanotubes, as shown in Fig. 12c.

EHDP enables the structure formation of organic crystalline materials on the micrometer length scale while at the same time exerting control over crystal orientation, as shown in Fig. 13.<sup>129</sup> Well-ordered structures with nearly vertical walls, comprising stacks of crystals were shown for both PCL (Fig. 13a and b) and PDHA (Fig. 13e and f). A set of nested rings have formed in the diffraction plane for both replicated structures of PCL (Fig. 13c and d) and PDHA (Fig. 13g and h), indicating polycrystalline samples.

EHDP of a block-copolymer (BCP) film also gives rise to hierarchical pattern formation with a micrometer-sized polymer pillars and a 10 nm-scaled microphase morphology in one single step, as shown in Fig. 14.<sup>130–132</sup> Schematic drawing of the

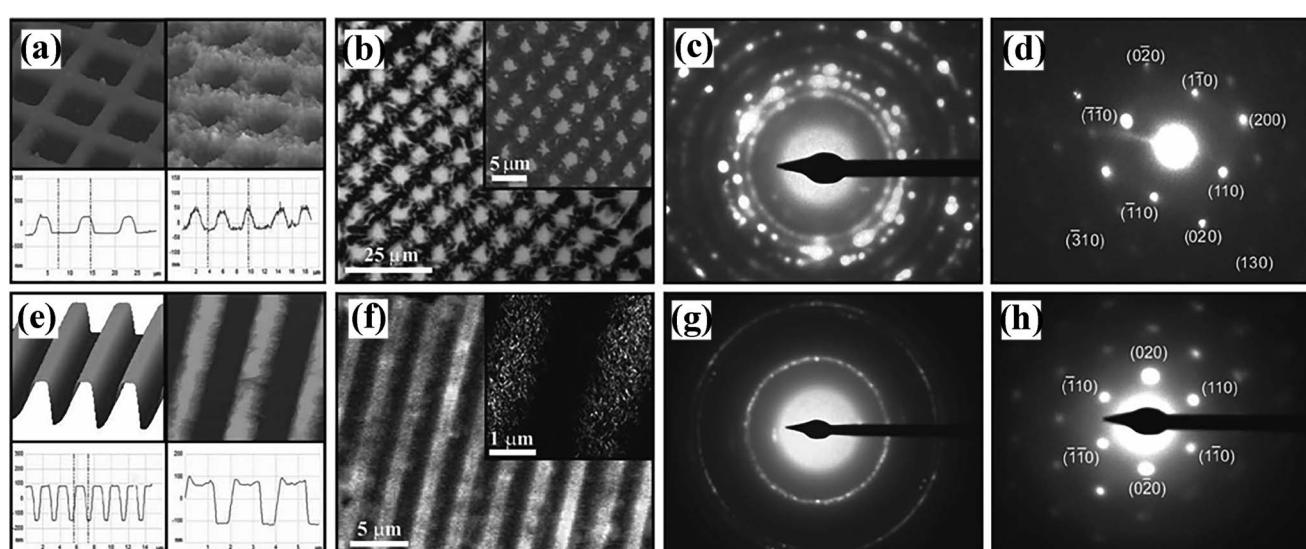


Fig. 13 AFM images of a (left) template electrode and (right) the patterns of (a) PCL and (e) PDHA with corresponding cross-sections. Optical micrographs of well-defined crystalline EHDP patterns of (b) PCL and of (f) PDHA. Diffraction patterns for a large area of (c) the PCL and (g) PDHA patterns. Selected area diffraction pattern obtained with an aperture of 3.0  $\mu\text{m}$  of a single PCL crystal in (d) and with a 1.0  $\mu\text{m}$  aperture diameter of a single PDHA crystal in (h). Reproduced with permission.<sup>129</sup> Copyright 2012, WILEY-VCH.



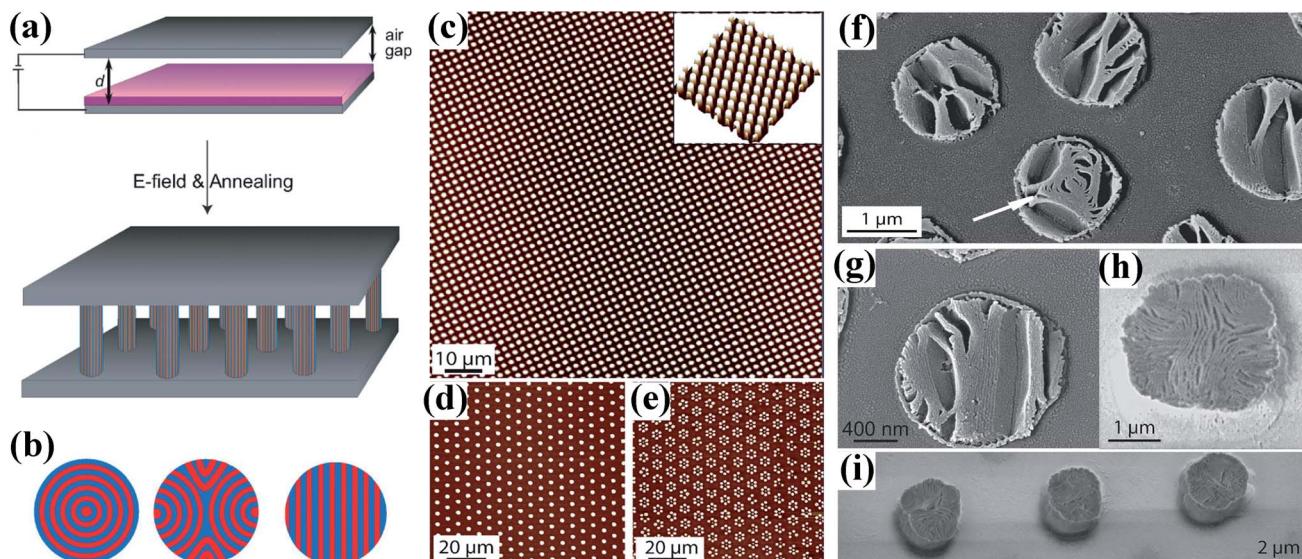


Fig. 14 (a) Schematic drawing of the experimental procedure. (b) Three possible in-plane configurations of the lamellar microdomains. (c–e) AFM images of micrometer-sized patterns of PS-*b*-PMMA films made by EHD lithography. (f–i) SEM images of the microphase morphology of PS-*b*-PMMA columns. Reproduced with permission.<sup>131</sup> Copyright 2008, WILEY-VCH.

experimental procedure was shown in Fig. 14a. The pattern formation on the micrometer scale of films with two different molecular weights was shown in Fig. 14c–e. The three different in-plane assemblies schematically was shown in Fig. 14b: onion-type concentric alignment of lamellae (Fig. 14f, arrow), parallel sheets (book sheets) (Fig. 14g) and bent lamellae pointing towards the column mantle (Fig. 14h and i). Furthermore, Goldberg-Oppenheimer *et al.* showed a functional block copolymer that contains perylene bismide (PBI) side chains which can crystallize *via*  $\pi$ - $\pi$  stacking to form an electron conducting microphase is patterned *via* EHDP. The patterned film shows a hierarchical structure with three distinct length scales: micrometer-sized polymer pillars, a 10 nm BCP microphase morphology that is aligned perpendicular to the substrate surface, and a molecular length scale (0.35–3 nm) PBI  $\pi$ - $\pi$ -stacks traverse the EHDP-generated plugs in a continuous fashion.<sup>133</sup>

## 7 Conclusions and perspective

The review provides an illustrative commentary about the progress and recent developments on EHDP. The key emphasis of the review has been to theoretically and experimentally discuss how the characteristic wavelength and the characteristic time depend on both the external conditions (such as the applied voltage, film thickness, template-substrate spacing) and the initial polymer properties (such as rheological property, electrical property and surface tension). We have theoretically and experimentally discussed various possible strategies for fabricating hierarchical patterns by combining the essential concepts of bottom-up and top-down approaches. Furthermore, we have emphasized aligning and ordering of the anisotropic polymers by EHDP.

Table 1 shows some conventional patterning methods and their characteristics of the resulting patterned surfaces

Table 1 Type of some patterning methods and characteristics of the resulting patterned surfaces

Method	Cause	Pattern	Size range	Novelty	Limitation
Photolithography	Optical diffraction	Pattern of optical diffraction	Nanometer to micrometer	High resolution High throughput	High cost Optical diffraction limit
Nanoimprint	External force	Typically negative replica of template	Nanometer to micrometer	Low cost High throughput High resolution	Large external force
EHDP	External electric field	Typically ordered arrays of pillars, positive replica of template or some hierarchical structures	Submicrometer to micrometer	Low cost High throughput High resolution Small external force	No long range order No nano-scale features



including the cause, the pattern, the size range, the novelty and the limitation. Among the conventional patterning methods, photolithography is a pattern-fabricating technique with high resolution and high throughput, but the photolithography tools are rather expensive and the feature size is limited by optical diffraction limit; nanoimprint is a pattern-transferring technique with low cost, high throughput and high resolution, however, nanoimprint typically require a comparatively large external force to press a patterned template mechanically against the substrate, possibly leading to poor geometrical integrity in the duplicated structure or even to irreversible damage of the template and substrate, making multilayer overlay alignment difficult. EHDP also is a pattern-transferring technique with low cost, high throughput and high resolution. Moreover, the most major advantage of EHDP is the capability to fast and economically create large-scale three-dimensional micro-scale structures on various kinds of materials with featureless templates, even though no long range order and no nano-scale features due to the dielectric breakdown.<sup>71</sup> In addition, EHDP just need a minimized external force to maintain a proper air gap between the liquid polymer and the template, avoiding the shortcoming of nanoimprint.

A promising direction of EHDP is the conjugation with other patterning techniques (such as dewetting, nanoimprint, and hot embossing) to fabricate extremely high-aspect-ratio or hierarchical patterns such as, cages, microlens arrays, high-aspect-ratio micropillars, mushroom-shaped micropillars with a well-controlled aspect ratio and tip diameter.<sup>134–137</sup> In addition, an attractive issue in EHDP is to extend its applicability to a larger class of materials. The benefit of exploiting new kinds of EHD materials lies in that it provides the possibility to not only improve the performance of EHDP, but also integrate functionality into final microstructures because of the interesting physical properties these materials can offer. So a promising direction in EHDP will include the structure formation in functional polymers and their various potential applications.

## Conflicts of interest

The authors declare no competing financial interest.

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