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Ultra-low voltage bipolar hydrogen production from biomass-derived aldehydes and water in membrane-less electrolyzers[†]

Hengzhou Liu,^{‡,a} Naveen Agrawal,^{‡,b} Arna Ganguly,^{‡,c} Yifu Chen,^{‡,a} Jungkuk Lee,^{‡,a} Jiaqi Yu,^d Wenyu Huang,^{‡,d} Mark Mba Wright,^{‡,c} Michael J. Janik^{*b} and Wenzhen Li^{‡,a}

Water electrolysis using renewable energy inputs is being actively pursued as a green route for hydrogen production. However, it is limited by the high energy consumption due to the sluggish anodic oxygen evolution reaction (OER) and safety issues associated with H₂ and O₂ mixing. Here, we replaced the OER with an electrocatalytic oxidative dehydrogenation (EOD) of aldehydes for bipolar H₂ production and achieved industrial-level current densities at cell voltages much lower than during water electrolysis. Experimental and computational studies suggest a reasonable barrier for C–H dissociation on Cu surfaces, mainly through a diol intermediate, with a potential-dependent competition with the solution-phase Cannizzaro reaction. The kinetics of the EOD reaction was further enhanced using a porous CuAg catalyst prepared from a galvanic replacement method. Through Ag incorporation and its modification on the Cu surface, the geometric current density and electrocatalyst durability were significantly improved. Finally, we engineered a bipolar H₂ production system in membrane–electrode assembly-based flow cells to facilitate mass transport, achieving maximum current densities of 248 and 390 mA cm⁻² at cell voltages of 0.4 V and 0.6 V, respectively. The faradaic efficiency of H₂ from both the cathode and anode reactions attained ~100%. Taking advantage of the bipolar H₂ production without the issues associated with H₂/O₂ mixing, an inexpensive, easy-to-manufacture dialysis porous membrane was demonstrated to substitute the costly anion exchange membrane, achieving an energy-efficient and cost-effective process in a simple reactor for H₂ production. An estimated H₂ price of \$2.51/kg from an initial technoeconomic assessment is competitive with US DoE's "Green H₂" targets.

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Broader context

It is critical to combat against global warming and stabilize global temperature to the manageable level of +1.5 °C by curbing CO₂ emissions, eventually achieving zero net emissions by 2050. This target requires the significant deployment of renewable energy and clean hydrogen in all industry sectors. Particularly, hydrogen produced from water electrolysis provides a promising route to decarbonation of industry and transportation. However, the dominant energy loss in traditional water electrolyzers is the unfavorable thermodynamics and slow kinetics of oxygen evolution reaction at the anode. In this work, an efficient bipolar hydrogen production system was demonstrated by combining cathodic hydrogen evolution from water and anodic hydrogen generation from aldehyde oxidation. Unlike conventional combined systems for hydrogen production that require high voltage (>1.0 V) and are limited by mass transport (<100 mA cm⁻²) of reactants, this study doubled the hydrogen production rate to achieve industrial-level current density with economic viability. Biorenewable furfural (a model aldehyde) with a large production scale suggests another green hydrogen source of biomass. The successful implementation of such an energy-efficient process will seamlessly integrate renewable electricity (from wind, solar) and renewable carbon sources, thus impacting future distributed manufacturing of green hydrogen and carbon chemicals with low-energy consumption and low-carbon footprint.

^a Department of Chemical and Biological Engineering, Iowa State University, 618 Bissell Road, Ames, IA 50011, USA. E-mail: wzli@iastate.edu, mij13@psu.edu, markmw@iastate.edu

^b Department of Chemical Engineering, Pennsylvania State University, State College, PA 16801, USA

^c Department of Mechanical Engineering, Iowa State University, Ames, IA 50011, USA

^d Department of Chemistry, Iowa State University, 618 Bissell Road, Ames, IA 50011, USA

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‡ These authors contributed equally to this work.

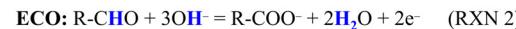
1. Introduction

Hydrogen can serve as an energy carrier in clean, efficient, sustainable, and cost-attractive energy systems.¹ The full environmental benefit of moving toward a hydrogen society is to realize its production from renewable resources including water or biomass.^{2,3} “Green H₂” produced from renewable energy sources can then be used in fuel cells to supply electricity for stationary and transportation applications.¹

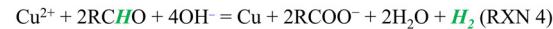
Water electrolysis is the most attractive and sustainable approach for future H₂ generations;^{1,4} however, the current water electrolyzers are limited by their high cost, largely due to the thermodynamically and kinetically sluggish oxygen evolution reaction (OER).^{5,6} In addition, a gas crossover, between unbalanced gas pressures of cathodic H₂ (two-electron transfer) and anodic O₂ (four-electron transfer), can induce explosive H₂/O₂ mixtures, and the produced reactive oxygen species could damage the membranes, leading to safety concerns.^{7,8} Expensive ion-exchange membranes are commonly used to separate gaseous products,⁹ and developing suitable low-cost, easy-to-manufacture membrane materials is still in need.^{9,10} One strategy to address the above-mentioned problems is to replace the OER with anodic reactions that are thermodynamically more favorable and economically more attractive, with potential to produce valuable products rather than O₂.¹¹ Despite the significant progress on developing paired electrolyzers for H₂ production, an electrolytic voltage of >1.0 V on non-noble metal catalysts is still required.^{12–16} Moreover, limited by the mass transport of reactants in the aqueous phase, the current density is usually <100 mA cm⁻²,^{11,15} severely restricting their industrial-relevant applications.

Rather than producing H₂ from water electrolysis, biomass-derived aldehydes are excellent alternative candidates to water as the energy and H-source for H₂ production.² The effectiveness of aldehyde conversion to H₂ depends on the discovery of catalytic/electrocatalytic processes, and catalytic materials to enable such processes. Catalytic H₂ generation from bio-based aldehydes can also be accompanied by the production of valuable by-products, such as carboxylic acids. In past years, the transformation of aldehydes to carboxylic acids along with H₂ evolution was reported from several non-faradaic reactions, including base-,^{17,18} heterogeneous-,^{19–21} and homogeneous^{22–25} -catalyzed processes (RXN 3). However, these reactions generally require a high concentration of base (>1 M OH⁻) or an elevated temperature (>100 °C) with both aldehyde and H₂O as proton sources in the formation of H₂. The condition of high alkalinity/temperature is prone to favor aldehyde degradation toward humin-based polymers, largely suppressing the selectivity towards desirable acid and H₂.^{25,26} Another aldehyde-based chemical process, namely, electroless deposition (ELD) of metals (e.g., Cu, Scheme 1, RXN 4) onto conductive or nonconductive substrates, has been applied to recycle metals or develop flexible printed circuits.^{27–29} This non-faradaic process occurs by reducing metal salts in solutions where the electrons are supplied from the reducing agents, e.g., formaldehyde (HCHO), and H₂ is co-produced through aldehyde oxidation catalyzed by *in situ* reduced

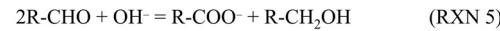
Electrochemical, Faradaic half-reactions:



Thermocatalytic, non-Faradaic overall reactions:



Disproportionation reaction (Cannizzaro reaction):



Scheme 1 Comparison of reactions of aldehydes.

metallic Cu.³⁰ More importantly, due to the non-faradaic nature of the above reactions, they are unsuitable to replace the anodic OER for bipolar H₂ generation in the electrolytic cell.

Alternatively, Wang *et al.* recently reported an electrocatalytic oxidative dehydrogenation (EOD) pathway on the Cu electrode, in which the aldehyde oxidation cogenerated H₂ and carboxylic acid (Scheme 1, RXN 1) at anodic potentials near 0 V (vs. RHE).^{31,32} The EOD process is fundamentally distinct from the conventional electrochemical oxidation (ECO, Scheme 1, RXN 2) of aldehydes, which requires higher anodic potentials and forms acid and protons.^{15,33–37} The facile kinetics of the EOD reaction enable pairing with the hydrogen evolution reaction (HER) at low cell voltages, evolving gaseous H₂ from both electrodes while producing carboxylic acids in the anode effluent. Despite the successful demonstration of EOD on Cu, detailed mechanistic questions remain. Why is Cu unique for EOD, compared to high overpotentials for furfural ECO on Pt and Au? In strong alkaline solutions, the non-faradaic Cannizzaro transformation from aldehydes (Scheme 1, RXN 5) is a major side reaction that cannot be ignored.³⁸ The competition between this non-faradaic path and the EOD reaction is not well explored, leaving open questions that must be answered to enable effective reaction engineering for this process.

In this work, we elucidated the mechanism for the EOD reaction, and combined it with the cathodic HER for bipolar “green H₂” production at cell voltages well below those needed for water electrolysis. Biomass-derived furfural was selected as the model aldehyde for the EOD reaction because the conversion of inedible lignocellulose to furfural is well established, currently conducted industrially on a scale of 0.43 million tons/year.^{39–41} The oxidative carboxylic acid product [e.g., 2-furoic acid (2-FA)] is a crucial precursor for the renewable polymer polyethylene furanoate (PEF) in the manufacturing of drinking bottles.⁴²

Our experimental and computational results reveal a common gem-diol intermediate with a reasonable barrier for catalyst mediated C-H dissociation to make 2-FA and H₂ on the Cu surface, competing with the solution phase Cannizzaro reaction and showing potential-dependent kinetics. Through combined electrokinetic observations and DFT calculations, we demonstrate that Cu optimally balances the ability to activate the gem-diol C-H bond, form the C-O(H) bond, avoid CO poisoning, and be stable in a metallic form at desired operating potentials. Since the EOD reaction on a Cu electrode is driven



by anodic potentials with onsets as low as ~ 0.1 V_{RHE} , we further used a galvanic replacement method to etch Cu foam to create a CuAg catalyst with higher roughness for the facile EOD kinetics. Protected by Ag layers, the stability of this Cu-based catalyst is significantly improved under electrolysis conditions of high alkalinity and anodic biasing. Moreover, we developed a membrane-electrode assembly (MEA)-based electrolysis system for bipolar H_2 production with faradaic efficiencies (FEs) from both the cathode and anode near $\sim 100\%$. Taking advantage of the facile kinetics on CuAg catalysts and increased mass transport resulting from the porous substrate and rough catalyst layer, we demonstrated a maximum current density of H_2 ($j_{\text{A-H}_2}$) of 248 mA cm^{-2} at a cell voltage of 0.4 V . Considering that H_2 was co-produced from the cathode and the anode without H_2/O_2 mixing issues, an inexpensive, easy-to-manufacture dialysis filter membrane as a porous separator was employed to separate organic reactants and replace the costly anion exchange membrane (AEM). The techno-economic analysis (TEA) of a commercial process based on the bipolar H_2 production exhibited potential economic viability with the co-generation of value-added carboxylic acids.

2. Results and discussion

2.1 Evaluating transition-metal catalysts for the EOD reaction

The EOD of furfural was first studied in an H-type reactor with various commercially available metallic foams or foils as catalysts (Fig. S1 and S2, ESI[†]). Linear sweep voltammetry (LSV) was performed with and without furfural in 1 M KOH . As shown in Fig. 1a, LSV curves on Cu foam with 200 mM furfural showed an apparent current density in a potential range of $0.1\text{--}0.5 \text{ V}_{\text{RHE}}$, corresponding to the EOD reaction. Half-hour chronoamperometry (CA, Fig. 1b) tests at 0.2 and $0.4 \text{ V}_{\text{RHE}}$ (V_{RHE} : potential *versus* reversible hydrogen electrode) showed that the production rate ratio of 2-FA-to- H_2 is close to $2:1$, which is in line with the stoichiometry of the EOD equation (Scheme 1, RXN 1). The FEs of

2-FA and H_2 , defined as the moles of 2-FA or 2 times of the moles of H_2 produced at the Cu electrode divided by the total moles of electrons applied, are both $\sim 100\%$.

The EOD current density increases initially as the potential is shifted anodically until the onset of Cu oxidation. The optimum potential range of $0.1\text{--}0.4 \text{ V}_{\text{RHE}}$ for EOD is below the thermodynamic potential of Cu oxidation toward Cu_2O ($0.46 \text{ V}_{\text{RHE}}$, $\text{pH} = 14$, Table S5, ESI[†]). An additional control experiment on a Cu_2O coated catalyst showed a negative current density at $0.4 \text{ V}_{\text{RHE}}$, indicating that no Cu oxidation occurs at this potential (Fig. S3, ESI[†]). The current density was gradually approached zero suggesting the reduction of Cu_2O to Cu. These observations align with the previous experimental (using *in situ* grazing incidence XRD^{43,44}) and computational⁴⁵ works that the surface Cu oxide layer is fully reduced to metallic Cu at anodic potentials below $0.4 \text{ V}_{\text{RHE}}$. These results all suggested that metallic Cu is the active phase for EOD catalysis. The detailed physical characterization of our self-prepared Cu-based catalysts for EOD was shown in Section 2.4.

A similar EOD reaction was observed on Ag foil with an onset potential of $\sim 0.3 \text{ V}_{\text{RHE}}$ (Fig. S4, ESI[†]), positively shifting $\sim 200 \text{ mV}$ compared to the Cu foam. Interestingly, the occurrence of the EOD reaction was not observed on other transition metals (Fig. S5, ESI[†]). For Pd, Pt, Au and Ni electrodes, no apparent current density was observed in the relatively low anodic potential regions, and no detectable H_2 was obtained from our online-gas chromatography (GC). These results suggested that Cu and Ag are unique metal catalysts for the EOD reaction, with Cu demonstrating a higher current density and a lower overpotential.

Furfuryl alcohol detected in the electrolyte is hypothesized to be generated from the competing, non-faradaic Cannizzaro pathway. The reported FE and production rate of 2-FA from the EOD pathway is calculated after subtracting 2-FA co-produced from the Cannizzaro reaction (quantified from the amount of furfuryl alcohol produced). Fig. 1c shows that the Cannizzaro reaction is the only reaction occurring at an open circuit voltage

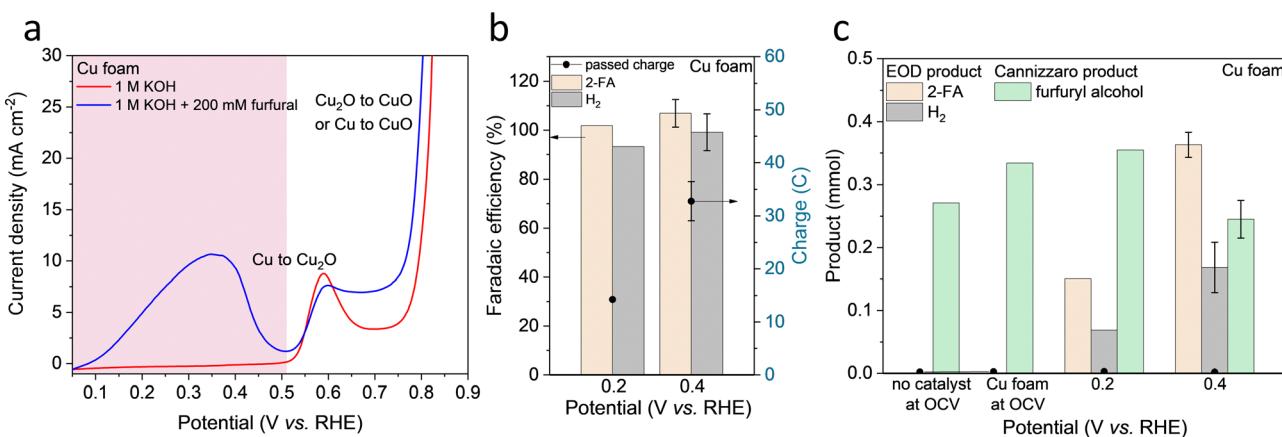


Fig. 1 EOD reaction on Cu foam. (a) LSV curves (2nd cycle) on Cu foam (1 cm^2) with or without 200 mM furfural in the 1 M KOH electrolyte. (b) Faradaic efficiency (left y-axis) and passed charge (right y-axis), and (c) product for half-hour electrolysis in 1 M KOH with 200 mM furfural at an open circuit voltage or different applied potentials.



(OCV) without a catalyst. Interestingly, the presence of a catalyst (*i.e.*, Cu foam at the OCV) promoted this non-faradaic reaction. The results with Ag foil, and Cu and Ag nanoparticles at an OCV also showed the elevated Cannizzaro reaction rates (Table S1, ESI†). When the applied potential increased from 0.2 to 0.4 V_{RHE} (Fig. 1c), the EOD pathway became more favorable, suppressing the Cannizzaro reaction. This potential dependent competition suggests that these two reactions share a common intermediate, which could be a deprotonated form of gem-diol. We then used NMR to estimate the equilibrium ratio of aldehyde to gem-diols. Fig. S6 (ESI†) shows that 68% of furfural existed as its diol form in the 0.1 M KOH solution, and this value approached ~100% when the base concentration increased to ≥ 0.5 M. Thus, the diol species, produced from a chemical (or solution-mediated) step with OH^- attacking the aldehyde, is the common intermediate involved in both the EOD and Cannizzaro reactions. The EOD reaction could involve the adsorption of this diol species on the electrode surface followed by the C–H bond cleavage to produce H_2 .

2.2 DFT calculations

The proposed reaction mechanisms for aldehyde EOD, ECO, and Cannizzaro reactions are shown in Scheme 2. As per molecule of furfural consumed, the ECO, EOD, and Cannizaro are 2, 1, and 0 electron transfer reactions. The equilibrium conversion between the shared gem-diol intermediate ($\text{R}-\text{CH}(\text{OH})_2$) for the Cannizaro or EOD (diol route) and the reactant aldehyde is noted with a black arrow signifying the connection between these paths. In the alkaline medium, this gem-diol intermediate might preferentially deprotonate to the gem-diol anion.

Our electrochemical results in Section 2.1 above show that the oxidation of furfural to furoic acid can occur on Cu at significantly lower potentials (0.1 V_{RHE}) than that on Au or Pt (0.9 V_{RHE}), and revealed an alternative low overpotential reaction (EOD) with H_2 co-generation or alcohol co-generation through the Cannizzaro reaction. We rationalize the experimental findings through DFT calculated intermediate species binding energies and elementary reaction energetics.

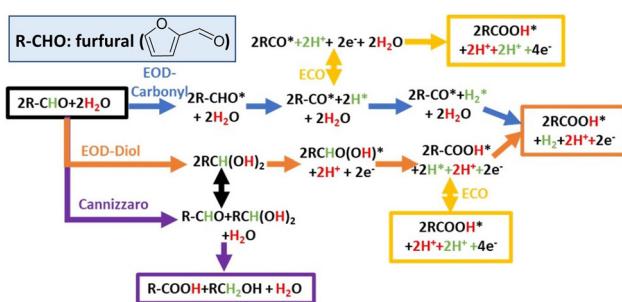
Earlier studies on furfural electro-oxidation (ECO) on transition metal surfaces suggest that the binding of CO^* is a key activity descriptor for catalytic activity.⁴⁶ At low potentials, a

high coverage of strongly bound CO^* could be formed through the thermal decarbonylation of furfural. This has long been recognized for formaldehyde electro-oxidation on Pt electrodes.⁴⁷ Due to strong CO^* binding (~1.63 eV), Pt requires an anode potential of ~0.9 V_{RHE} to observe a noticeable furfural oxidation current. The binding of CO^* on Cu (~0.63 eV) is substantially weaker than that on Pt, allowing Cu to avoid the CO^* poisoning issues observed on Pt catalysts (Table S2, ESI†). Au surfaces also bind CO^* weakly (0.15 eV), though large overpotentials are still observed experimentally due to inherently low activity for C–H bond dissociations (as discussed below).

Our prior DFT results, in collaboration with experimental efforts of Holewinski and co-workers, concluded that the ECO of furfural can proceed through either a carbonyl or a solution-assisted diol route on transition metal catalysts.⁴⁸ On Au catalysts, the diol route is preferred due to the weaker binding of the furanic ring and requires a significant oxidative overpotential due to the poor activity of Au for the C–H dissociation step inside the diol route.⁴⁸ Cu better balances weak CO^* binding and C–H activation, as well as H^* and OH^* binding, to enable the low potential EOD process (albeit, requiring alkaline conditions for stability, whereas Au and Pt can be used in acid as well).

The key distinction between the EOD and ECO through the perspective of elementary steps is the only step involving the surface bound H^* derived from C–H cleavage (Scheme 2), which either converts to a proton through a reverse-Volmer step (yellow arrow) or a half mole of hydrogen through a Tafel step (orange and blue arrows). The preference between the EOD and ECO mechanisms is indirectly dictated by a combination of thermodynamic (CO^* , H^* , OH^* , and FCOOH^* binding energies) and kinetic descriptors (C–H and C–OH activation). Table S2 (ESI†) shows the comparison of key thermodynamic descriptors. Fig. 2a shows the reaction free energy diagram for the EOD reaction at 0.2 V_{RHE} through the carbonyl route on Pt(111), Cu(111), and Au(111) surfaces. The desorption energy of 2-FA(FCOOH) is likely overestimated on all metals due to solvation effects, as discussed in our prior work.⁴⁸ Ignoring the desorption of furoic acid, C–H cleavage for the EOD mechanism is the limiting step on all three metals. Among the three metals, Pt has the lowest C–H barrier (0.39 eV) for the EOD mechanism. However, EOD has not been observed on Pt despite it being a great HER catalyst. This is because Pt requires a significant overpotential (0.9 V_{RHE}) to become electrocatalytically active for furfural oxidation due to CO^* poisoning. At such high potentials, the reverse Volmer step is highly favorable, and the ECO process occurs instead of EOD. In contrast, Au binds H^* quite weakly (+0.38 eV) but is limited by slow C–H activation (1.54 eV barrier), which still requiring significant oxidative overpotentials beyond the EOD feasibility region where H^* remains bound to the surface. Cu has a moderate barrier for C–H cleavage (0.72 eV) and intermediate H binding (+0.31 eV), suggesting that, at low potentials, a Tafel step might be preferable over the reverse-Volmer step, leading to the EOD mechanism.

The H^* in an EOD/ECO reaction is produced from the non-electrochemical C–H cleavage of either the adsorbed aldehyde



Scheme 2 Proposed reaction mechanisms for EOD, ECO, and Cannizzaro reactions.



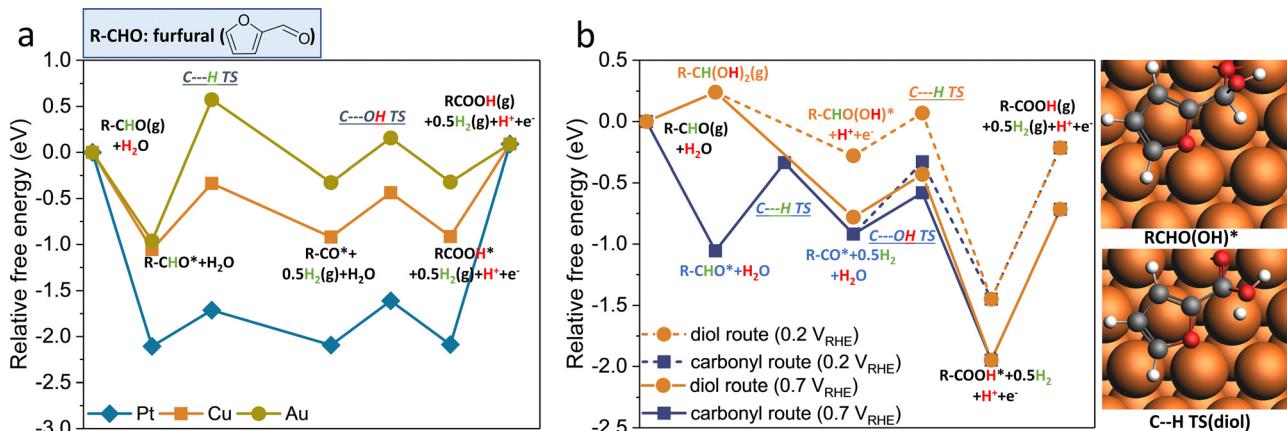


Fig. 2 Reaction free energy diagrams for EOD paths on late transition metal (111) surfaces. (a) Comparison of the relative free energy on Pt/Cu/Au (111) surfaces for the EOD of furfural using the carbonyl route. (b) Potential dependent relative free energies for carbonyl and diol routes on the Cu(111) surface. Inset figures in (b) show the adsorbed RCHO(OH)* optimized structure and C–H dissociation transition state in the diol mechanism, both on the Cu(111) surface.

(R-CHO*) in the “carbonyl route” or the hydrolyzed form of the aldehyde (R-CH(OH)₂) in the “diol route”. The preference between the carbonyl and diol routes for EOD is dependent on the concentration ratio of diol to furfural in the solution and the applied potential. Experiments in this study show that the concentration of the diol increases as the concentration of the base increases. Fig. 2b compares the reaction free energy diagram for the carbonyl (blue) and diol routes (orange) on Cu(111) at 0.2 and 0.7 V_{RHE}. At 0.2 V_{RHE}, there is no clear preference between the two routes, but as the potential is made more positive (0.7 V_{RHE}), the adsorption (with an electron transfer) of the deprotonated diol (R-CHO(OH)) becomes more favorable by 0.5 eV. Determining the exact potential at which the diol route dominates is challenging, as it requires comparing the adsorption and surface reaction energies, and determining the adsorption thermodynamics in the solvated system is challenging. However, the diol route appears viable on Cu electrodes, with its dominance increasing over the carbonyl route as the potential increases.

The experimentally observed suppression of the Cannizzaro reaction relative to the EOD reaction at higher potentials can be explained by the potential dependent free energy diagram of EOD vs. the non-faradaic Cannizzaro reaction in Fig. S7, ESI[†]. The common intermediate between the two pathways is the diol (RCH(OH)₂) or its deprotonated form in a basic medium (RCHO(OH⁻)). The energetics in Fig. S7 (ESI[†]) show that the formation of the adsorbed deprotonated ion becomes more favorable at more positive potentials due to the involvement of electron transfer during adsorption. The more favorable adsorption promotes the rate of surface mediated C–H cleavage, and therefore, the EOD reaction becomes more competitive with the Cannizzaro reaction as the potential is increased. The precise potential at which EOD becomes competitive with the solution phase Cannizzaro reaction is challenging to determine using DFT, due to the imprecision in the evaluation of solution phase energetics and approximations of using a single crystal Cu surface and a single surface coverage.

It is challenging for DFT methods to examine the relative rates of H^{*} oxidation (reverse Volmer step) and H₂ evolution, which will depend on the relative activation barriers for these two steps, as well as the surface coverage of H^{*} and effective concentration of OH⁻ near the surface. The rapid C–H dissociation from the aldehyde/diol would allow establishing a high coverage of H^{*} species, and a higher coverage would promote H₂ evolution relative to H^{*} oxidation.

2.3 Unifying the EOD reaction with CuO_x reduction by aldehydes within a chemical looping scheme

In addition to the occurrence of the EOD reaction on the metallic Cu electrode (faradaic half-reaction), we examined the chemical reaction of copper oxide with furfural, as half of an overall chemical looping reaction in which copper is oxidized, then reduced by furfural while producing furoic acid and hydrogen products. As we discuss here, the copper oxide reduction step is analogous to the EOD reaction, in that the chemical reaction can be considered as a coupling of a copper oxide reduction half-reaction, with the copper metal produced by this reaction and then catalyzing the EOD reaction as the oxidation half-reaction.

When an oxidized Cu foam was immersed in the electrolyte, H₂ spontaneously evolved. The H₂ production rate increased and then decreased with the progressing time (Fig. S9, ESI[†]). Further experiments were performed in a batch reactor with 1 M KOH + 200 mM furfural, and 50 mg of Cu₂O or CuO nanoparticles (NPs) under an Ar atmosphere (Fig. S10a and b, ESI[†]). H₂ production shows a similar volcano-type production rate with time, as the initial copper oxide reduction produces the Cu metal that accelerates the EOD reaction, until the consumption of copper oxide slows the reduction half-reaction. No H₂ was detected in the control experiments with Cu NPs, as H₂ is only detected when the Cu NPs were intentionally oxidized prior to the reaction with the aldehyde. XRD confirmed that oxidized Cu was reduced back to its metallic state after the reaction (Fig. S10c, ESI[†]), indicating that Cu



oxides were indeed consumed during H_2 evolution. In addition, the ratio of the production rate of 2-FA and H_2 on all oxidized Cu is close to 2:1, which is consistent with the stoichiometry of the EOD reaction. Furthermore, when fully deuterated (D_2O with 1 M NaOD) solution was used, differential electrochemical mass spectroscopy (DEMS) showed only the *m/z* signal of 2, confirming that both H atoms in H_2 are from the aldehyde group (Fig. S10d, ESI[†]), which is in line with the EOD reaction. The chemical reduction of CuO_x nanoparticles

effectively behaves as a “short-circuited” combination of CuO_x reduction (the equilibrium potential of CuO_x reduction is 0.3–0.4 V_{SHE} , Table S4 and S5, ESI[†]) and the EOD reaction (Fig. 3c), with the effective mixed potential presumably varying between the two potentials based on the relative rates of the two half-reactions as the reaction progresses to equilibrium.^{49,50}

In addition, as shown in Fig. S11 and Table S4, S5, (ESI[†]) the reduction of Ag_2O with aldehydes also leads to H_2 production, whereas reductions of Pt(II) and Pd(II) do not evolve H_2 .⁵¹ This is

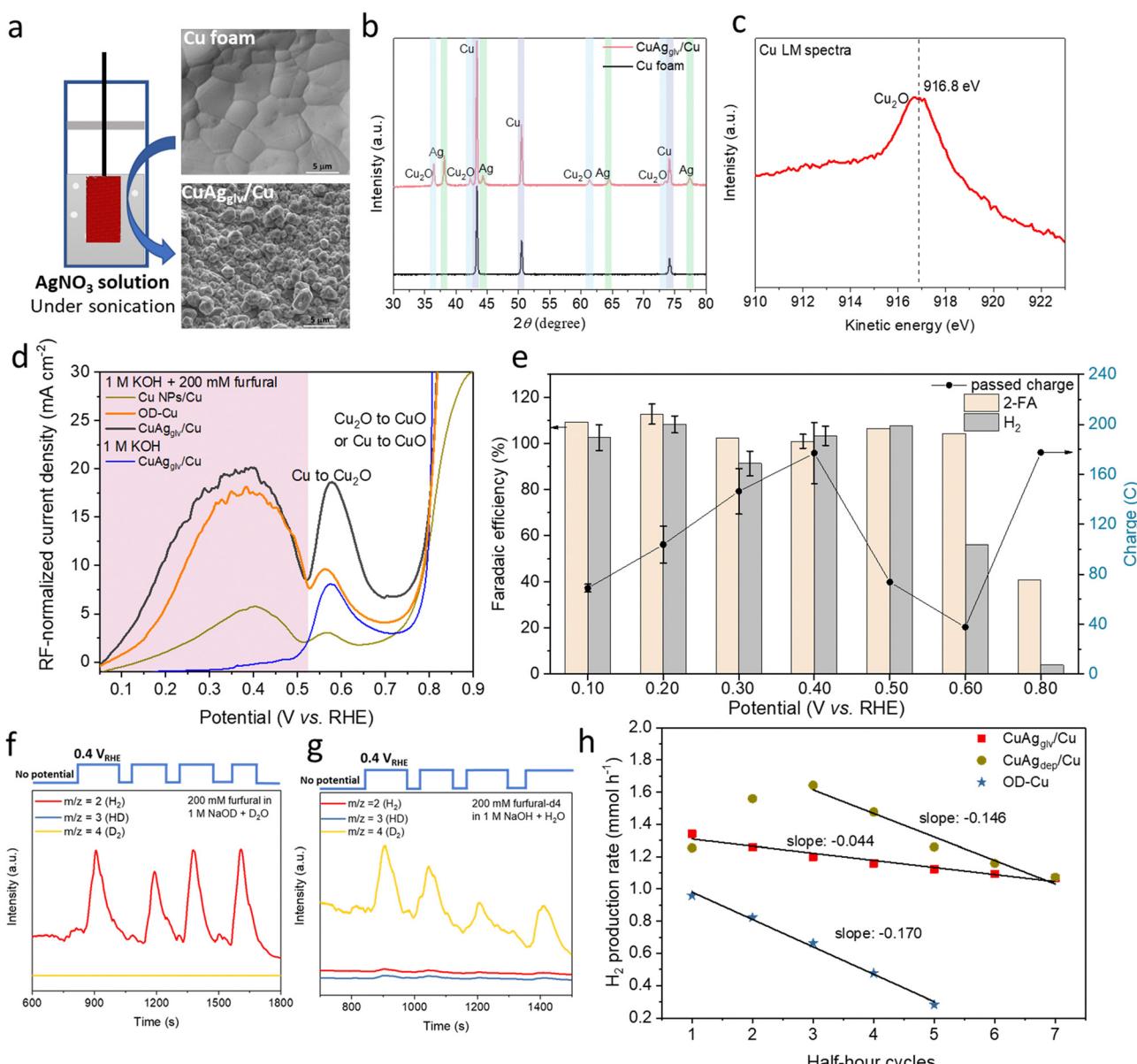


Fig. 3 EOD reaction on $CuAg_{gl}/Cu$ in the H-type cell. (a) Scheme of the galvanic replacement method and SEM images of Cu foam and as-synthesized $CuAg_{gl}/Cu$. (b) XRD patterns of Cu foam and as-synthesized $CuAg_{gl}/Cu$. (c) Auger Cu LM spectrum of as-synthesized $CuAg_{gl}/Cu$. (d) Linear sweep voltammetry (2nd cycle) on Cu-based electrodes, including Cu NPs/Cu, OD-Cu, $CuAg_{gl}/Cu$, with or without 200 mM furfural in the 1 M KOH electrolyte. The current density was normalized to the roughness factor (RF). (e) Faradaic efficiency (left y-axis) and passed charge (right y-axis) in 1 M KOH with 200 mM furfural at different applied potentials on $CuAg_{gl}/Cu$ for half-hour electrolysis. The geometric area for the electrode was 1 cm^2 . (f) and (g) DEMS signals at *m/z* = 2, 3, and 4 at a pulsed potential of 0.4 V_{RHE} on the $CuAg_{gl}/Cu$ electrode. Measurements in two deuterated electrolytes were performed: (f) 200 mM furfural in D_2O with 1 M NaOD and (g) furfural-d4 in H_2O with 1 M NaOH. (h) H_2 production rate at different numbers of cycle for independent half-hour electrolysis with different Cu-based electrodes: OD-Cu, $CuAg_{gl}/Cu$, and $CuAg_{dep}/Cu$. A fresh electrolyte was replaced after each half-hour electrolysis. The slopes in (h) show their degradation rate.



in agreement with the electrochemical furfural oxidation studies discussed above, in which furfural ECO will occur rather than EOD once Pt and Pd metals are formed.

Overall, we reported EOD and Cu/CuO_x chemical looping reactions showing H₂ generation (Fig. S12c, ESI[†]) that is distinct to the previously reported ECO of aldehyde toward acid without H₂ production on high oxidation states of Cu (Fig. S12a, ESI[†])^{33,52} or through Cu(i)/Cu(ii) redox cycling (Fig. S12b, ESI[†]).^{16,53} The major reason is that Cu(0) is active for the EOD reaction, but Cu(i)/Cu(ii) is not. The EOD reaction is shown to occur as the oxidation half reaction during the simultaneous chemical reduction of CuO_x by aldehydes. The metallic Cu is required for EOD due to both higher activity for C–H dissociation and the Tafel H–H formation step.

2.4 Demonstrating an active and stable CuAg catalyst for the EOD reaction

To further improve the EOD kinetics on metallic Cu, we prepared an oxide-derived Cu (OD–Cu) electrode *via* an electro-oxidation–thermal treatment method (details in Methods section). In addition to its high surface area, oxide-derived catalysts are highly active for various electrochemical reactions because of their unique features such as low coordinated sites, grain boundaries, and subsurface oxygen.^{54–57} However, under steady-state electrolysis (EOD reaction) at 0.2 V_{RHE}, a fast decay was observed during five continuous half-hour electrolysis periods (Fig. 3h), resulting in a 71% decrease of the H₂ production rate, along with a loss of the Cu nano-sized morphology and surface roughness (Fig. S13, ESI[†]).

Inspired by the approaches of using noble metals (*e.g.*, Pd and Rh) to induce surface reconstruction and stabilize Cu substrates,^{58–60} we prepared bimetallic CuAg catalysts (through galvanic replacement and electrodeposition methods). We chose Ag as the second metal to add to Cu because Ag is expected to be more durable⁶¹ and Ag was also observed to catalyze the EOD reaction. A Cu-rich, nano-sized CuAg catalyst prepared from the galvanic replacement method (denoted as CuAg_{glv}/Cu) facilitates the EOD reaction with higher intrinsic activity and stability. The as-synthesized CuAg_{glv}/Cu catalyst was prepared by immersing the pre-cleaned Cu foam in the AgNO₃ solution under sonication to create an oxidized porous Cu surface with large area (Fig. 3a) and well-dispersed Ag on and underneath the Cu-rich surface (as shown in EDS, Fig. S14, ESI[†]). The roughening of the surface is a result of rapid Cu crystal deformation that started from the grain boundaries and defects.⁶² XRD analysis indicated that both metals are polycrystalline with Cu₂O, Cu, and Ag phases (Fig. 3b). The Auger electron spectra of Cu LM (Fig. 3c) with a kinetic energy peak at ~916.8 eV suggested that the surface is dominated by Cu₂O species, while the Ag 2p spectra showed its metallic state (Fig. S15, ESI[†]). HRTEM and EDS mapping also suggested the uniform distribution of Ag on Cu and a clear phase separation between Ag and Cu₂O (Fig. S16, ESI[†]).

Extensive measurements were conducted on the CuAg_{glv}/Cu anode in the three-electrode H-type cell to test its performance for the EOD reaction. The as-synthesized CuAg_{glv}/Cu was first

held *in situ* at –0.1 V_{RHE} for 3 min to reduce the surface Cu₂O back to the metallic Cu in the furfural-containing electrolyte. XRD and Auger Cu LM spectra showed a significant decrease in the Cu₂O intensity after this treatment (Fig. S17, ESI[†]). We further compared the intrinsic activity of various Cu-based electrodes [CuAg_{glv}/Cu, OD–Cu, and commercial Cu NPs coated on Cu foam (Cu NPs/Cu)], normalizing their activity by quantitatively determining their surface areas. The double-layer capacitance was measured to assess the roughness of each material and then normalized to the plain Cu foam (Fig. S18, ESI[†]). LSV curves with the roughness factor (RF)-normalized current density showed a similar trend among those Cu-based catalysts (Fig. 3d). Typically, CuAg_{glv}/Cu exhibited four times higher intrinsic activity (in the RF-normalized current density) than Cu NPs/Cu at 0.4 V_{RHE}. In addition, we observed a slightly higher RF-normalized current density of oxide-derived CuAg_{glv}/Cu than that of OD–Cu (20.2 vs. 17.7 mA cm^{–2} at 0.4 V_{RHE}), suggesting that an active oxide-derived Cu-rich surface was obtained by a simple galvanic replacement method, which effectively improved the EOD reaction performance.

EOD activity on CuAg_{glv}/Cu was further tested under static electrolysis conditions at different potentials. The online DEMS with a pulsed potential of 0.4 V_{RHE} confirmed that the proton source for H₂ in the EOD reaction is the aldehyde group rather than H₂O (Fig. 3f and g). With the constant electrolysis duration (half-hour), Fig. 3e shows a ~100% FE of both 2-FA and H₂ (the production rate ratio is ~2:1, Fig. S19, ESI[†]) in a potential range of 0.1–0.5 V_{RHE}. The passed charge (Fig. 3e, right y-axis) increased from 0.1 to 0.4 V_{RHE} followed by a decrease starting from 0.5 V_{RHE}. Specifically, the maximum current density of H₂ at the early stage of electrolysis at 0.4 V_{RHE} attained ~250 mA cm^{–2} (Fig. S19, ESI[†]), and the gradual decrease in the current density was attributed to the consumption of furfural during electrolysis. The EOD performance can be further increased by conducting electrolysis in flow cells (details are shown in Section 2.6). The decrease in the reaction activity at higher potentials is due to the gradual oxidation of Cu to Cu(i), which is unable to catalyze the EOD reaction. The decrease in the FE ratio of H₂ and 2-FA from ~1 to 0.5 at 0.6 V_{RHE} suggests the concurrent occurrence of EOD (RXN 1) and ECO (RXN 2) reactions. An additional support for Cu(i) not being active was demonstrated by the relatively low EOD activity on a drop-coated Cu₂O/Cu catalyst (Fig. S20, ESI[†]). A further increase in the anodic potential to 0.8 V_{RHE} largely increased the passing charge to a relatively high value (178 C), but with significantly suppressed H₂ formation (FE: ~4%). This could be due to the further oxidation of Cu and Cu(i) to Cu(ii) that switched the dominant pathway from the EOD reaction to the ECO reaction.^{16,33,53,63} The favorable ECO reaction on copper oxides could be due to their weak binding of surface H or low H coverage due to slow C–H activation, suggesting that the dominant pathway between the EOD and ECO reactions can be well-regulated by anodic potentials and/or chemical states of Cu.

The catalyst synthesis conditions of sonication and precursor concentrations are critical for obtaining the fully etched and oxidized Cu surface, which strongly affects the EOD activity. The concentration of AgNO₃ offers a tunable driving



force to manage the surface roughness and relative abundance of Cu_2O in the as-synthesized $\text{CuAg}_{\text{glv}}/\text{Cu}$ (Fig. S21, ESI[†]). Changing its concentration from 1 to 200 mM is equivalent to a ~ 0.14 V Nernstian shift of the redox potential (Supplementary Methods, ESI[†]). We observed that a higher concentration of AgNO_3 is needed to form a Cu_2O -dominated pre-catalyst; however, using too concentrated AgNO_3 (>100 mM) excessively dissolved the Cu surface and decreased the surface roughness (Fig. S21, ESI[†]), leading to a decrease of the EOD activity.

To further study the function of Ag and how its distribution on the Cu foam substrate affecting the EOD durability, $\text{CuAg}_{\text{glv}}/\text{Cu}$ was compared with a CuAg catalyst obtained from the electrodeposition method (*i.e.*, $\text{CuAg}_{\text{dep}}/\text{Cu}$). Different from the porous surface of $\text{CuAg}_{\text{glv}}/\text{Cu}$ created from the driving force between two metals with the spontaneous deposition of Ag and exchange with Cu, the mesoporous architectures of $\text{CuAg}_{\text{dep}}/\text{Cu}$ were generated by H_2 bubbles from the concurrent HER under strong acid conditions (1.5 M H_2SO_4).⁵⁸ The use of sufficiently large cathodic current density (2 A cm^{-2}) minimized the spontaneous galvanic replacement, and the diffusion of metal ions dominantly governed their deposition onto the electrode. Therefore, a linear relationship between the atomic percentage of the incorporated Ag in the electrode (as determined by ICP) and the molar percentage of the precursor Ag^+ in the deposition solution was established (Fig. S22– and S23, ESI[†]). From this plot, the Ag loading at 12.5 at% for $\text{CuAg}_{\text{dep}}/\text{Cu}$ (same as $\text{CuAg}_{\text{glv}}/\text{Cu}$) can be well-controlled by tuning the Ag^+ percentage in the deposition solution.

SEM showed the dendritic Ag and hexagonal Cu morphologies on the $\text{CuAg}_{\text{dep}}/\text{Cu}$ surface with a microporous high-surface-area, exhibiting a higher RF than $\text{CuAg}_{\text{glv}}/\text{Cu}$ (14.2 vs. 4.5, Fig. S22 and 23, ESI[†]). However, the durability for the EOD reaction showed a different trend between these two catalysts (Fig. 3h). At 0.2 V_{RHE}, $\text{CuAg}_{\text{dep}}/\text{Cu}$ showed an increased H_2 production rate in the first three half-hour cycles and outperformed the $\text{CuAg}_{\text{glv}}/\text{Cu}$ electrode, mainly benefiting from the higher surface area of $\text{CuAg}_{\text{dep}}/\text{Cu}$. Nevertheless, $\text{CuAg}_{\text{dep}}/\text{Cu}$ activity degraded faster than $\text{CuAg}_{\text{glv}}/\text{Cu}$ activity as shown by different slopes for the degradation rate: -0.146 vs. -0.044 . The cross-sectional SEM and EDS images (Fig. S24–S26, ESI[†]) by pre- and post-electrolysis exhibited different Ag distributions between the two electrodes. We observed that the galvanic deposited Ag layer covered the outer shell of the Cu boundary for the $\text{CuAg}_{\text{glv}}/\text{Cu}$ catalyst (Fig. S24 and 25, ESI[†]), and this cross-sectional Ag layer still existed after 7-cycle of electrolysis. Resulting from more stable Ag than Cu (as shown in Pourbaix diagrams in Fig. S28, ESI[†]), the Ag layers in the cross-section partially protected Cu and avoided its quick deactivation under harsh electrolytic conditions. This unique structure could keep a rough and active surface to maintain stability throughout electrolysis. In contrast, the cross-sectional SEM-EDS of $\text{CuAg}_{\text{dep}}/\text{Cu}$ showed the randomly distributed Ag that loosely covered the Cu substrate (Fig. S26, ESI[†]), without forming an intact Ag layer at the outer shell of the Cu surface. Furthermore, the porous structure of $\text{CuAg}_{\text{dep}}/\text{Cu}$ was very fluffy and easy to peel off, leading to the physical detachment of Cu and Ag and

the loss of the partial Cu foam substrate after long-term electrolysis (Fig. S26, ESI[†]). This distinct distribution of Ag and different dynamic surface reconstructions resulted in more durable $\text{CuAg}_{\text{glv}}/\text{Cu}$ than $\text{CuAg}_{\text{dep}}/\text{Cu}$. More detailed characterization studies and comparisons of the dynamic changes of catalysts are shown in the Notes S2 and S3, ESI[†].

The Ag-decorated Cu electrode showed similar LSV and CA behaviors as the Cu foam substrate and other Cu-based monometallic electrodes, indicating that the incorporated Ag did not directly participate in the EOD reaction to alter the product selectivity, but acted as a promoter to improve the intrinsic EOD activity and mitigate Cu degradation. In particular, $\text{CuAg}_{\text{glv}}/\text{Cu}$ was able to maintain a higher RF than monometallic Cu. After 5 continuous half-hour electrolysis, the surface of OD–Cu lost its RF (from 3.5 to 1.1) and showed minimal EOD activity, while $\text{CuAg}_{\text{glv}}/\text{Cu}$ showed only the slightly decreased activity (21%) and RF (4.5 vs. 4.1, Fig. S33, ESI[†]) after 7 successive cycles. The assessment clearly demonstrated that Cu–Ag bimetallic catalysts have a faster EOD rate than pure Cu and Ag, indicating that incorporating Ag into Cu engenders a synergistic effect that improves the activity and durability beyond either of its component metals.

With the presence of highly concentrated OH^- ions in the electrolyte, and more severely, under anodic biasing, the dynamic surface reconstructions occurred during long-term electrolysis. SEM-EDS, XRD, and XPS analyses showed an overall decrease trend in the Cu-to-Ag ratio followed by its increase to the original values. These surface reconstructions were not owing to the detachment of Cu or Ag from the electrode surface to the electrolyte (as confirmed by ICP that the Ag atomic percentage was maintained at ~ 13 at%, Table S8, ESI[†]). The mobility of Ag and Cu was significant even at room temperature, and the applied anodic bias during the EOD reaction was sufficient to drive drastic changes in their morphology.^{64,65} Although we observed the dynamic surface reconstruction of the $\text{CuAg}_{\text{glv}}/\text{Cu}$ catalysts, the dynamic surface changes did not significantly decrease the EOD durability because of its maintained high surface roughness. After sufficient long-term electrolysis, *ex situ* SEM-EDS and XPS confirmed the partial detachment of the cross-sectional Ag layer and increase in the surface oxygen content [towards $\text{Cu}(\text{OH})_2$ and CuO], which could rationalize the experimentally observed 21% drop of the reaction activity after 7 cycles of electrolysis on $\text{CuAg}_{\text{glv}}/\text{Cu}$. Designing Cu-based electrocatalysts with much longer-term durability, especially under harsh electrolytic conditions (*e.g.*, high alkalinity and anodic biasing),⁶⁶ remains a challenge that needs to be addressed in future studies.

2.5 Revealing electrokinetics of the EOD reaction on the $\text{CuAg}_{\text{glv}}/\text{Cu}$ electrode

To obtain mechanistic insights into the electro-kinetics of EOD, we varied the furfural concentration and plotted $j_{\text{A}-\text{H}_2}$ against its concentration on a log-log scale. The electrolysis was conducted at 0.4 V_{RHE} with the same amount of an applied charge of 30 C. We observed a first-order dependence (slope of 0.97) of the furfural-to- H_2 reaction in the furfural concentration range

of 50 to 250 mM, and a negative reaction order at concentrations higher than 250 mM (Fig. 4a). This negative order can be attributed to the non-faradaic Cannizzaro reaction (with a reaction order of 2.2 with respect to furfural, Fig. S34a, ESI[†]) that largely outperformed the EOD reaction. As the aldehyde concentration increased, the kinetics for the Cannizzaro pathway increased more rapidly than the EOD route. The Cannizzaro reaction can be largely suppressed by positively shifting the potential from 0.2 to 0.4 V_{RHE} (Fig. 4b), which is in line with our experimentally and computationally observed potential-dependent pathway-switching behavior for the diol route. In half-hour electrolysis at 0.4 V_{RHE}, the produced 2-FA via the Cannizzaro reaction and that by the EOD reaction were 0.34 and 1.85 mmol, respectively (Fig. 4b).

The EOD reaction rate was also highly dependent on the OH⁻ concentration (Fig. S34b, ESI[†]): j_{A-H_2} linearly increased in the range of 0.1–1 M and reached a plateau at >1.0 M, which is in line with the NMR results in the formation of gem-diol (Fig. S6, ESI[†]). This high OH⁻ concentration-dependent rate agreed with our DFT calculated prediction of the more favorable diol route than the direct carbonyl route for the EOD reaction. In addition, the half-hour electrolysis of D-labeled

furfural (furfural-d4) showed a kinetic isotopic effect (KIE) of 2.06 (calculated from the partial current density ratio of 2-FA, j_{H_2}/j_D , Fig. S34c, ESI[†]). This large primary KIE suggested the involvement of C–H/D bond cleavage in the rate-determining step (RDS).⁶⁷ The electrolysis of furfuryl alcohol on CuAg_{glv}/Cu at 0.4 V_{RHE} (Fig. S35, ESI[†]) showed a minimal current density and undetectable H₂, indicating that the unique EOD reaction only occurred on the aldehyde group.

The versatility of the EOD reaction was also demonstrated by extending the substrate to acetaldehyde (CH₃CHO) and formaldehyde (HCHO), two representative aldehydes with and without α -H, respectively. It is known that the Cannizzaro reaction occurs only on the compounds without any α -H, because the formation of the critical diol intermediate cannot occur in the presence of α -H.^{38,68} The occurrence of the EOD reaction, however, did not strongly rely on the type of aldehyde (Fig. S36, ESI[†]), possibly suggesting a direct carbonyl route for the EOD reaction. The lower current density for CH₃CHO (with α -H) than the reactants without α -H indicated that the diol route is more favorable than the direct carbonyl route. These experimental results are all consistent well with the DFT calculations. Such a versatility can benefit future H₂ production from the EOD of aldehyde feedstocks from different resources.

2.6 Developing innovative flow cells for bipolar H₂ production

2.6.1 H₂ production from the EOD reaction with enhanced mass transport. Based on the facile EOD kinetics and optimized catalyst morphology and electrolysis conditions, we designed an MEA-based flow cell for bipolar H₂ production (Fig. 5a). The MEA consisted of an AEM, a Pt/C cathode, and a CuAg_{glv}/Cu anode in a zero-gap configuration. 1 M KOH with and without 250 mM furfural were used as the anolyte and catholyte, respectively.

LSV measurements (Fig. 5b) showed that the cell voltage for the HER-EOD reaction (0.21 V) was significantly lower than that of the HER-OER reaction (1.63 V with the RuO₂ anode and 1.69 V with the IrO₂ anode) at 100 mA cm⁻². The current density for the HER-EOD reaction increased to a maximum of ~500 mA cm⁻² at 0.7 V, followed by a decrease from >0.7 V, which can be attributed to the oxidation of Cu that switched the reaction pathway toward the ECO reaction, which is in line with the H-cell results.

Steady-state, half-hour electrolysis was conducted at different cell voltages (Fig. 5c). The obtained j_{A-H_2} increased when moving the cell voltage from 0.1 to 0.5 V, and then decreased from >0.6 V. The current density-time profiles (Fig. S37a, ESI[†]) showed a gradual decrease in the net current density, which is mainly attributed to the consumption of furfural, as the electrokinetic studies have confirmed the 1st order dependence of the reaction rate on the furfural concentration. To overcome the reactant starvation for half-hour electrolysis, we increased the anolyte volume from 40 to 250 ml (Fig. 5c and Fig. S37b, ESI[†]), leading to improvement in j_{A-H_2} at 248 (0.4 V) and 390 mA cm⁻² (0.6 V). The cell voltages of the HER-EOD system have outperformed the most previously reported, conventional electrolyzers for H₂ production, including the HER-OER based water

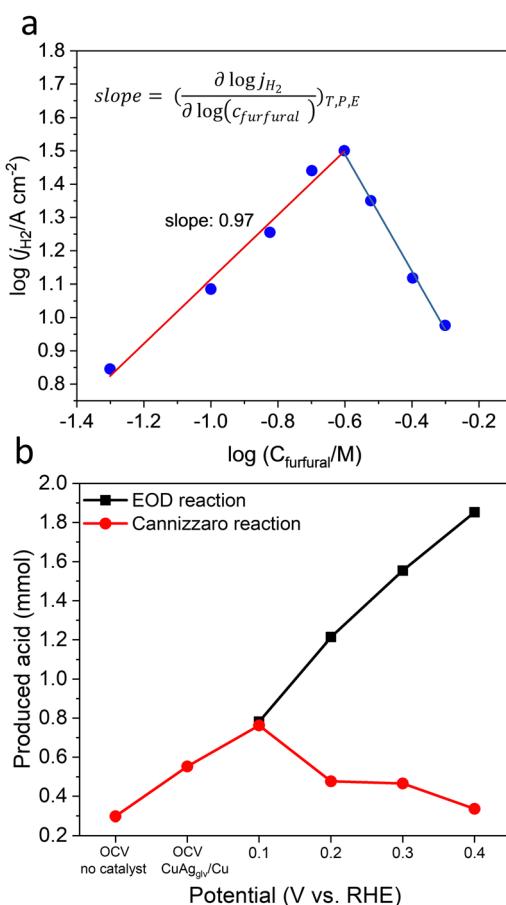


Fig. 4 Electrokinetics of EOD on CuAg_{glv}/Cu in the H-type cell. (a) Dependence of the partial current density of H₂ on the furfural concentration. (b) Produced acid from EOD and Cannizzaro reactions at OCV and different anodic potentials in the half-hour reaction.



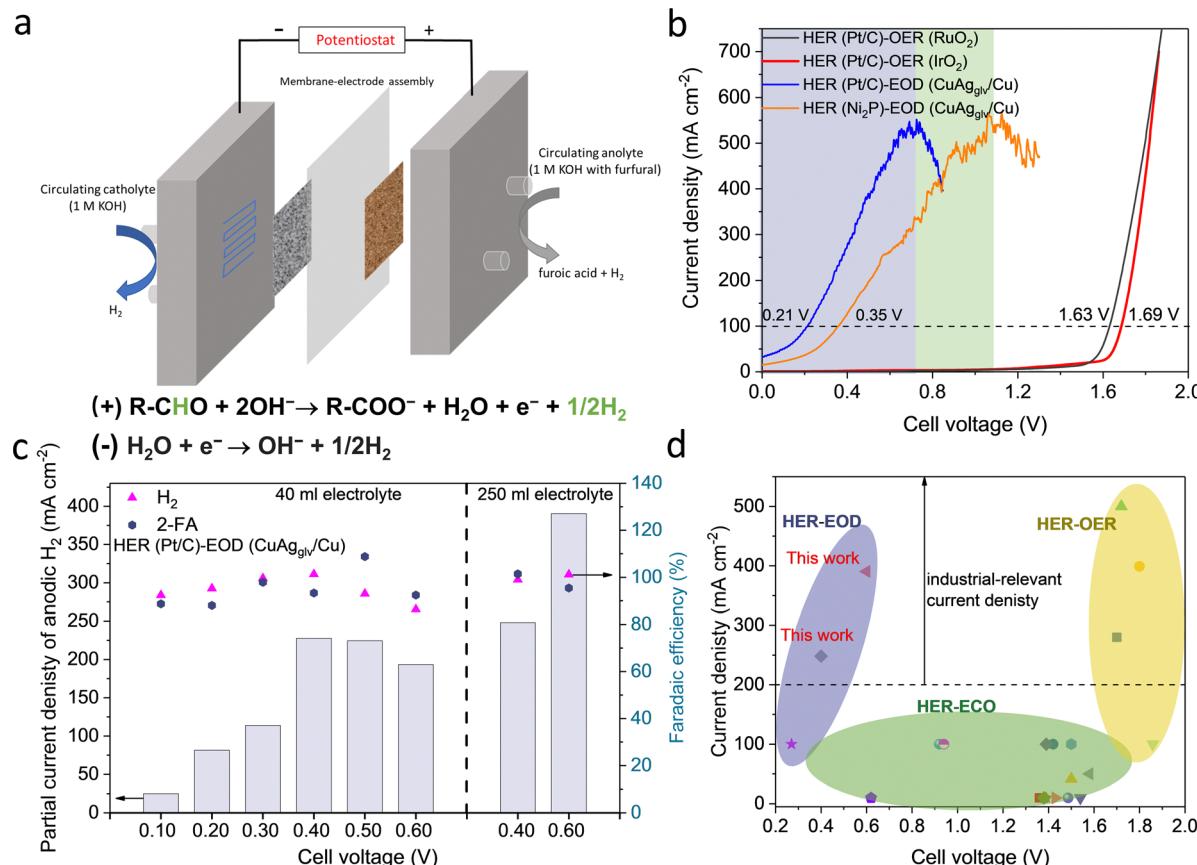


Fig. 5 Bipolar H₂ production in the MEA-based flow cells. (a) Scheme of the flow cell set-up and the reaction equations of bipolar H₂ production. The geometric area of anode was 1 cm². (b) Linear sweep voltammograms for different paired reactions on different electrodes. (c) Partial current density of H₂ at different cell voltages with 40 ml and 250 ml of the electrolyte. The HER and EOD reaction were conducted on Pt/C and CuAg_{glv}/Cu, respectively. (d) Comparison of the performance of bipolar H₂ production in this work with previous works for electrochemical H₂ production, including HER-ECO paired H₂ production, and HER-OER paired water electrolysis.

electrolyzers and HER-ECO based organic systems (Fig. 5d and Table S9, ESI†). Besides, the bipolar H₂ production system has doubled the H₂ production rate as compared to the conventional processes where H₂ is solely evolved on the cathode.

Limited by mass transport, most previously reported partial current densities for organic electrolysis (e.g., furfural, glycerol) to target products are low (*i.e.* <100 mA cm⁻²) and cannot meet the requirement of industrial applications.^{11,36,69} Conventional ECO reactions generally need the surface reaction of adsorbed reactive oxygen or hydroxyl intermediates and organic-derived intermediates on two adjacent sites *via* the Langmuir–Hinshelwood mechanism, causing severe internal mass-transport issues and limiting the partial current density to desired products. In addition, most ECO reactions [e.g., ECO of furfural or 5-(hydroxymethyl)furfural] are particularly favorable on OER electrocatalysts (e.g., Ni- or Co-based catalysts); therefore, it is challenging to completely suppress the OER, especially at high current densities.^{11,69} Thanks to the much favorable thermodynamics (Note S1, ESI†), the EOD reaction at high current densities occurs at a low potential range of 0.1–0.5 V_{RHE}, much lower than a thermodynamic potential of 1.23 V_{RHE} for the OER, circumventing the Langmuir–Hinshelwood mechanistic sequences that involve adsorbed oxygen species formed at

higher potentials. In addition, the EOD reaction occurs through sequential chemical–electrochemical steps, and the organic species itself is the reactant whose oxidation kinetics is facilitated by single-electron transfer at the electrode–electrolyte interface without involving other complicated adsorbates. Besides, the hydrophilic porous Cu foam can facilitate the efficient transport of the liquid-phase species to the electrode surface,^{36,70} and the high porosity and high surface roughness promoted the removal of H₂ bubbles from the surface, so that they do not block the surface for the subsequent adsorption of reactants. Overall, benefiting from the favorable thermodynamics, facile kinetics, and largely facilitated external and internal mass transport, we have significantly increased the partial current density of the EOD reaction toward H₂ production.

2.6.2 Non-noble metal-based electrocatalysts for the HER.

Selecting a cathode material with much lower costs than platinum-group metals is crucial for reaching an efficient and cost-effective process. To this end, we have prepared a non-precious Ni₂P catalyst (see Methods, ESI†) with a highly roughened surface. LSV curves in a one-compartment, three-electrode cell showed a higher overpotential of ~200 mV of Ni₂P than Pt/C at 100 mA cm⁻², −0.245 V vs. −0.043 V_{RHE} (Fig. S38 and S39, ESI†),



approaching the state-of-art Ni-based catalysts prepared from various methods.⁷¹ We then employed Ni₂P in the HER ~ 200 mV EOD coupled flow system. LSV and CA measurements showed a slightly higher cell voltage (~ 200 mV shift) than the system with the Pt/C cathode (Fig. S40, ESI[†]). In addition to its lower cost, another advantage of Ni₂P is that it can suppress the electrocatalytic hydrogenation reaction (ECH, Fig. S41, ESI[†]) in the presence of aldehyde (due to the crossover from anolyte to catholyte as studied in the following section). We tested the ECH of furfural at -0.15 V_{RHE} for a half hour. The result showed a much lower FE toward furfuryl alcohol on Ni₂P than on Pt/C: 7% *vs.* 83%. Consequently, if the aldehyde crossover occurs during long-term electrolysis, the unfavorable ECH on Ni₂P would not apparently influence the H₂ evolution from the cathode.

2.6.3 Dialysis membrane as a cost-effective separator. The generation of H₂ from both the anode and cathode in the bipolar H₂ production cell can be achieved with a cheap, commercially available filter membrane, namely dialysis membrane.⁷² We selected a cellulose-based dialysis membrane with a small pore size [*i.e.*, molecular weight cut-off (MWCO) of 0.1–0.5 kD], which is appropriate for furfural (0.096 kg mol⁻¹ \approx 0.1 kD) and is stable in acid, base, and organic solutions.⁷²

The dialysis membrane was installed in the MEA-based flow cell with Pt/C cathode and CuAg_{glv}/Cu anode (Fig. 6a). The pore size allowed for the free transport of K⁺ and OH⁻ across the membrane, while the furfural crossover from anolyte to catholyte was inhibited. Prior to electrolysis, the pretreatment of the membrane in 1 M KOH is necessary for the saturation of membrane pores with ions, reducing the solution resistance across the membrane from 15.37 Ω to 0.59 Ω (Fig. S42, ESI[†]). Based on the high mobility of K⁺ and OH⁻ without any

permselectivity, we calculated the theoretical ionic conductivity for the dialysis membrane ($\kappa = 247$ mS cm⁻¹), which is much higher than a typical AEM ($\kappa = 15$ –20 mS cm⁻¹).⁷³ A slightly higher resistance of the system with the dialysis membrane (0.59 Ω) than AEM (0.3–0.4 Ω) could be due to their different thicknesses: 70 *vs.* 28 μ m. Finally, through operating this dialysis membrane in flow cells, we obtained the j_{A-H_2} values of 97 and 216 mA cm⁻² at 0.2 and 0.4 V (Fig. 6c), respectively, close to the values in the AEM-based system under the same reaction conditions with 250 ml of electrolyte.

The crossover of gas and liquid products/reactants was analyzed and compared between the systems with the AEM and dialysis membrane. Benefiting from the similar H₂ pressures on both the anode and cathode during their concurrent generation, $\sim 95\%$ FE of H₂ from both electrodes were detected with the minimal gas crossover. For half-hour electrolysis at 0.4 V with the dialysis membrane, the liquid product crossover was quantified from the catholyte (Table S10, ESI[†]), showing 0.34, 2.02, and 4.19 mM of furfural, 2-FA, and furfuryl alcohol, respectively. In comparison, these values for the AEM-based system are 0, 7.15, and 3.67 mM. The total crossover of liquid reactants and products is < 11 mM, corresponding to $< 4.5\%$ of the initial furfural concentration of 250 mM. While the furfural crossover is insignificant for both systems, the crossover of alcohol (produced from the Cannizzaro reaction) and acid (generated from the EOD reaction) is non-negligible and higher than furfural. The crossover of a negatively charged acid product (*i.e.*, C₅H₃O₃⁻ from EOD reaction) is more considerable through the AEM compared to the dialysis membrane, benefiting from the latter's non-selective characteristics for charged and uncharged species. In fact, the permeability of 2-FA [*i.e.*, 5.56×10^{-6} cm² s⁻¹, Fig. S43, ESI[†]] is one order of magnitude lower than

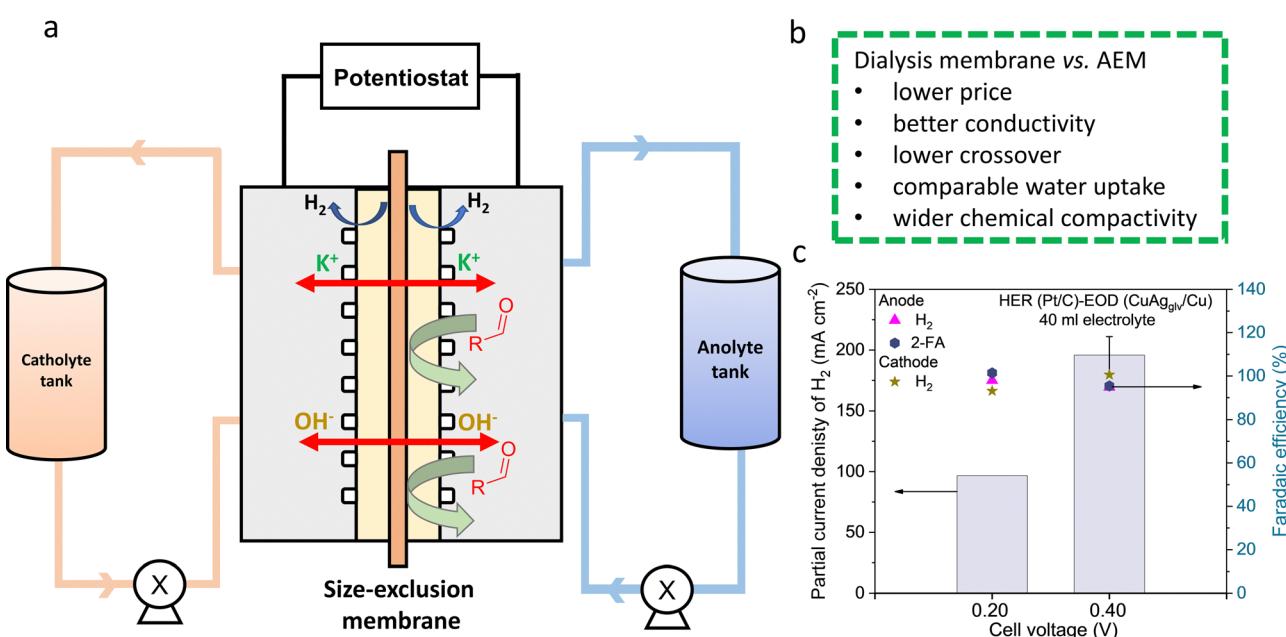


Fig. 6 Bipolar H₂ production in the system with a dialysis membrane. (a) Scheme of the flow cell with a dialysis membrane. (b) Comparison between the dialysis membrane and AEM. (c) Partial current densities of H₂ at different cell voltages with 250 ml of electrolyte.



that of the anion selective-AEM [*i.e.*, $2.80 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$]. In contrast, highly soluble neutral products (*i.e.*, alcohol) are able to crossover through sorption into and subsequent diffusion through the membrane based on the concentration gradient. The slightly higher crossover of furfural alcohol for the dialysis membrane is likely due to its higher water uptake,⁷⁴ which was determined to be 38% for the dialysis membrane and 26% for the AEM. Such a crossover could be mitigated by optimizing the properties of the dialysis membrane such as reducing the membrane thickness.

Finally, the long-term stability test in the system with the dialysis membrane was performed by conducting 7 successive cycles of 1 hour electrolysis at a cell voltage of 0.4 V (Fig. S45, ESI†). Negligible changes in the current density were observed during the first 1–4 hours, followed by a slight decrease in the performance from the 5th cycle, showing the excellent stability of both the CuAg_{giv}/Cu anode and dialysis membrane.

2.7 Techno-economic analysis (TEA)

To test the economic feasibility of the system considering capital and operation costs, we provided the TEA analysis to quantify the minimum selling price (MSP) of products (details are shown in the supplementary information). The economic performance of the system is analyzed by using the discounted cash flow rate of the return (DCFROR) method developed by the National Renewable Energy Laboratory (NREL).⁷⁵ We assumed an electrochemical plant capacity of 1500 kg per day H₂, based on the hydrogen analysis model developed by the U.S. Department of Energy for producing the same hydrogen quantity *via* water electrolysis.⁷⁶

We first focused on quantifying the MSP of H₂ (**Scenario 1**), with 2-FA as a byproduct to be sold to the market as the polyethylene 2,5-furandicarboxylate (PEF) precursor, which has been proposed to complement polyethylene terephthalate (PET) as a bio-derived plastic. The separation cost of H₂ was only considered (Fig. S46a, ESI†). In the system of AEM with the

Pt/C cathode and the CuAg_{giv}/Cu anode at a constant capacitance of H₂, the normalized installed capital costs are highly dependent on the current density, which drastically decreased by around 94% to only \$2.8/kg(H₂) when the current density was increased from 25 to 400 mA cm⁻² (Fig. S47a, ESI†). The much-decreased capital cost is mainly benefiting from the reduced electrolyzer area and electricity cost. Then, the calculated lowest net MSP of H₂ at 400 mA cm⁻² with a cell voltage of 0.6 V was \$3.2/kg (Fig. 7a), which lies within the range of DOE's target cost of H₂ from electrolyzers.^{76,77} This value is also lower than one of the industrial reported levelized costs of \$4.2/kg and \$3.7/kg for the proton exchange membrane (PEM) and AEM electrolyzer, respectively.⁷⁸ It was observed that the furfural costs contributed the most to the net MSP, and meanwhile, the earned revenue is benefited from the co-produced 2-FA from the bipolar H₂ production system. In the case of 400 mA cm⁻² and 0.6 V, sensitivity analysis (Fig. S47b, ESI†), *via* varying the factors by $\pm 20\%$, was performed to determine the key parameters influencing the MSP of H₂. The market prices of the reactant furfural and the product 2-FA (sold as PET) are two governing factors, and the separation of H₂ showed a negligible contribution.

We then quantified the economic viability of the plant by calculating the MSP of 2-FA (**Scenario 2**), with H₂ as the byproduct. In this scenario, the separation costs of both H₂ and 2-FA are considered (Fig. S46b, ESI†). The installed capital cost (Fig. S48a, ESI†) is the same with Scenario 1, and the different values is owing to the molar mass difference between H₂ and 2-FA. The lowest MSP of 2-FA (*i.e.*, \$2.51/kg) was obtained from the same condition of 400 mA cm⁻² and 0.6 V. Overall, at different voltages and current densities, the estimated MSP ranged between \$2.51 and \$2.99/kg (Fig. 7b), comparable to its market price between \$1 and \$99/kg (depend on the purity).⁷⁹ Different from Scenario 1, the fixed costs and the return on investment (ROI) were the main contributors to expenditure and revenues for the MSP of furoic acid. Moreover,

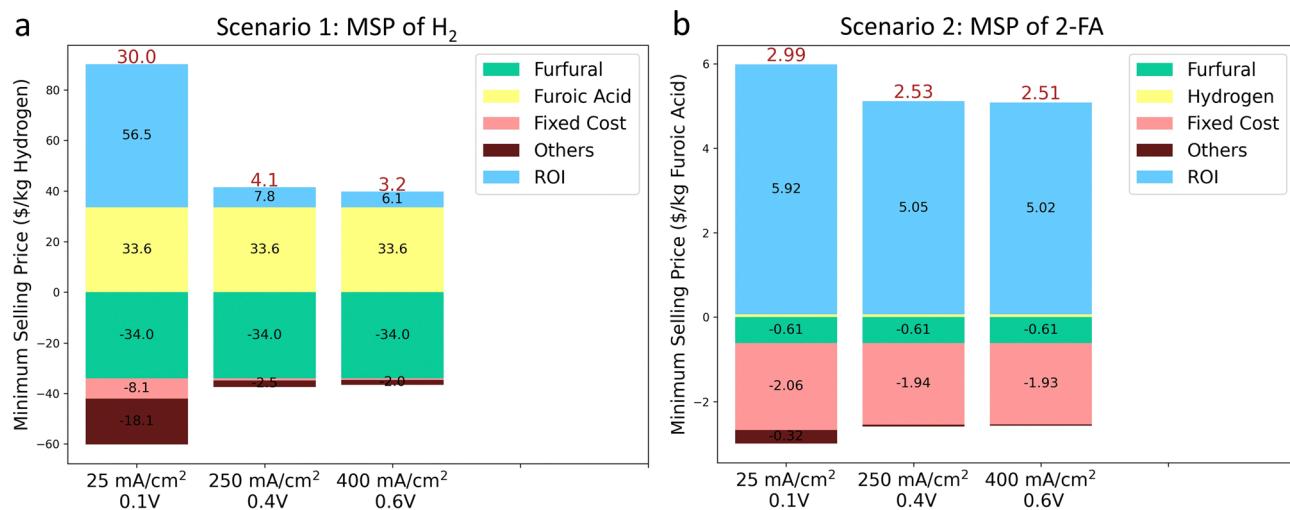


Fig. 7 Techno-economic analysis (TEA) for the bipolar H₂ production system. (a) Minimum selling price (MSP) of H₂ and (b) 2-FA at three different current densities and cell voltages. The electrochemical plant capacity is 1500 kg/day of H₂.



the most sensitive parameters that govern the MSP of 2-FA are the separation cost and the market price of furfural (Fig. S48b, ESI[†]).

Replacing the cathode catalyst from Pt/C to Ni₂P has reduced the catalyst cost by 99%. In addition, the substitution of AEM by the dialysis membrane decreased the electrolyzer cost by 50%. The total installed capital cost and the final MSP in both scenarios did not show significant differences (<5%) by these substitutions, because the major capital cost in an electrochemical plant is the balance of the plant (BOP) cost rather than the electrolyzer stacks (Fig. S49–S51, ESI[†]). Nevertheless, the development of cheap, stable, and efficient catalysts and membranes are still the major targets in the research community.

3 Conclusions

In summary, being enabled by the favorable thermodynamics and facile kinetics of the EOD reaction, we have achieved bipolar H₂ production in the flow cells with cathodic and anodic FE_s of ~100% and current densities of 248 and 390 mA cm⁻² at ultra-low cell voltages of 0.4 V and 0.6 V, respectively. These values are higher than most previously reported H₂ production rates in the HER–ECO paired systems. Experimental and DFT investigations have elucidated the reaction kinetics of the EOD reaction on Cu electrodes, and its linkage to the Cannizzaro reaction. We further explored a more efficient CuAg bimetallic catalyst synthesized on a porous Cu foam electrode, which demonstrated enhanced kinetics, mass transport, and durability. When the flow electrolyzer was engineered with a cost-effective dialysis membrane as a separator, the excellent cell performance and stability were maintained. Moreover, we linked the EOD reaction with a chemical looping reaction and highlighted the possibility of fundamentally bridged electro- and thermo-catalytic reactions, which could help in rationally designing and predicting novel electrocatalysts and processes. The present work provides a novel, robust approach toward sustainable coproduction of hydrogen and carboxylic acids from bio-derived aldehydes. Supported by the TEA study, the high efficiency, mild operating conditions, and inexpensive cell components of the approach offer potential for its future development toward a cost-effective process at an industrial scale, holding great promises for revolutionizing the renewable pathways toward clean fuels and biomass-based chemical industry.

Author contributions

H. L. and W. L. conceived the idea; W. L., M. J., and M. M. W. supervised the project; H. L. performed the electrochemical measurements and materials synthesis; N. A. and M. J. carried out the DFT calculations; Y. C. revised the manuscript and provided the constructive suggestions to this work; J. Y. and W. H. performed the HRTEM characterization; J. L. performed the XRD measurements; A. G. and M. M. W. conducted the TEA analysis. All the authors discussed the results and contributed to the manuscript writing.

Conflicts of interest

The authors declare no conflicts of interest.

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