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Prediction of pH in multiphase multicomponent systems with ePC-SAFT advanced†

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Proton activity, which is usually expressed as a pH value, is among the most important properties in the design of chemical and biochemical processes as it determines the dissociation of species in aqueous mixtures. This article addresses the prediction of pH values in multiphase systems based on the IUPAC definition via proton activity. The required proton activity coefficients were predicted using the thermodynamic equation of state ePC-SAFT advanced. The developed framework considers reaction equilibria and phase equilibria (vapor-liquid and liquid-liquid) to predict pH in the equilibrated liquid phases.

Designing unit operations for chemical and biochemical processes requires incorporating predictive computational technologies. These reduce the experimental effort, ultimately leading to a model-supported decision for process optimization.¹ For this, molecular thermodynamics, especially equations of state and activity-coefficient models, have been emerging as a vital tool in the industry.² Still, these models have been mainly applied in a correlative way, although many among them have a high predictive power, as shown recently for pharmaceuticals, polymers, biofuels, and electrolytes.³ In many of these research areas, species distribution plays an essential role for the behavior of the mixtures, and pH is the primary quantitative indicator of the degree of dissociation of ionizable components, given that their pK_a values are known. The pH definition has recently been revised by IUPAC, cf. ref. 4, and it is a single ion quantity that accounts for the proton activity on a molality scale. Thus, pH is accessible from molecular thermodynamic models that are capable of calculating activity coefficients, providing a helpful approach towards phase-equilibrium relations in reactive systems that contain electrolytes.⁵ pH plays a vital role in different areas, e.g.,

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reaction kinetics, the activity of biomolecules, or salting-out effects, and thus, pH is important to know in applications such as seawater desalination, amino-acid purification, fermentation, CO2 capture, or injection of CO2 into groundwater with large amounts of salts.6 However, pH measurements are challenging, especially for in situ processes where applicationspecific sensors are needed, for geological applications where access is limited, or for water-poor media where pH is not welldefined.1 The characterization of electrolyte mixtures has been considered in the literature. Austgen and coworkers applied an electrolyte non-random two-liquid model (eNRTL) to the vaporliquid equilibrium of H₂S and CO₂ aqueous solutions in monoethanolamine. A significant drawback of eNRTL and other models is the high number of adjustable parameters, and most of the models are highly correlative. To overcome these issues, equations of state based on statistical associating fluid theory (SAFT) have been used extensively to model electrolyte systems.8 Recently, Kohns and coworkers used variable range SAFT to successfully model vapor-liquid equilibria in nitric acid, sulfuric acid, and carbonic acid reactive systems and other properties such as osmotic coefficients.9 That approach includes Coulombic ion-ion interactions and electrostatic ion-solvent interactions to describe correctly free energies of solvation. Dufal et al. applied the same framework using SAFT-γ-Mie to model phase equilibria in aqueous solutions of CO2 and NH3.10 Electrolyte Perturbed-Chain SAFT (ePC-SAFT) has followed a similar development. It is based on PC-SAFT¹¹ and an extended Debye-Hückel term for electrolytes,8 and it can be applied up to high salt concentrations.12 The most recent development includes a concentration-dependent dielectric constant within Debye-Hückel and Born terms. 13 It was validated by sour gas solubility in reactive systems, 14 salt solubility in organic solvents, 15 and prediction of the saltingout in liquid-liquid two-phase systems. 16 In this work, this newest ePC-SAFT development ('ePC-SAFT advanced') was used to predict pH values for aqueous systems CO2 + water (+ salt) and carboxylic acid + water + organic solvents. The considered systems form two phases (one liquid and one vapor L-V, or one

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liquid aqueous and one liquid organic phase L-L), and they involve dissociation of the present electrolytes. Both, phase equilibria and dissociation were considered in this work, and the pH was predicted at V-L or L-L phase equilibrium of the respective systems with ePC-SAFT advanced.

Thermodynamic modeling of equilibrated multiphase aqueous electrolyte solutions requires simultaneously solving phase equilibria and reaction equilibria. The reactions that may take place in the liquid phases of the systems under consideration (CO2 + water + salt and carboxylic acid HA + water + organic solvents) are summarized in eqn (1)-(3).

$$2H_2O \rightleftharpoons OH^- + H_3O^+ \tag{1}$$

$$2H_2O + CO_2 \rightleftharpoons HCO_3^- + H_3O^+ \tag{2}$$

$$HA + H_2O \rightleftharpoons A^- + H_3O^+ \tag{3}$$

These reactions (1)–(3) are highly affected by a change in pH and by the amount of dissolved CO2. Thus, knowledge of pH is crucial for the dissociation degree of the acids and whether chemical equilibria take place besides physical interactions. pH is defined based on the thermodynamic activity of the proton in solution according to eqn (4).17

$$pH = -\log_{10}(a_{H^{+}}) = -\log_{10}\left(\frac{\tilde{m}_{H^{+}}\gamma_{H^{+}}^{*,\tilde{m}}}{\tilde{m}^{0}}\right). \tag{4}$$

In eqn (4) the quantity a_{H^+} is the molality-based activity of the proton, which can be calculated from the molality-based activity coefficient $\gamma_{\mathrm{H}^+}^{*,\tilde{m}}$ (accessible using a thermodynamic model) at the given composition and the molality \tilde{m}_{H^+} of the proton in the investigated system and $\tilde{m}^0 = 1 \text{ mol kg}^{-1}$. Please note, that H₃O⁺ exists in aqueous solution as the proton does not exist without hydration water. Therefore, by H⁺ we refer to H₃O⁺ in this manuscript; a differentiation between H⁺ and ${\rm H_3O}^{\scriptscriptstyle +}$ was not considered. $\gamma_{\rm H^+}^{*,\bar{m}}$ was calculated using eqn (5) according to Thomsen et al.18

$$\gamma_{\mathrm{H}^{+}}^{*,\tilde{m}} = \gamma_{\mathrm{H}^{+}}^{*,x} x_{\mathrm{w}} = \frac{\varphi_{H^{+}}(T,p,\bar{x})}{\varphi_{\mathrm{H}^{+}}^{\infty,\mathrm{w}}(T,p,x_{\mathrm{w}} \to 1)} x_{\mathrm{w}}$$
 (5)

Here $\phi_{\mathrm{H}^+}^{\infty,\mathrm{w}}$ denotes the proton fugacity coefficient at infinite dilution in water. Eqn (5) was used then in eqn (4) for the proton activity coefficient. Please note that eqn (5) was also used for all other charged reaction participants in the systems

under study
$$K_{\gamma,k} = \prod_{i=1}^{N_c} \gamma_i^{\nu_i}$$
 (see ESI†).

The required fugacity coefficients and activity coefficients were predicted with ePC-SAFT advanced, which expresses the residual Helmholtz energy ares as the sum of energy contributions caused by repulsion and attraction. It is important to state that ion-solvent interactions are captured by electrostatic iondipolar forces within a modified Born term and by nonelectrostatic ion-solvent effects (van der Waals dispersion), while Coulombic interactions between point charges are accounted for by the Debye-Hückel theory, which ignores solvent effects (primitive theory). Based on the so-obtained a^{res} ,

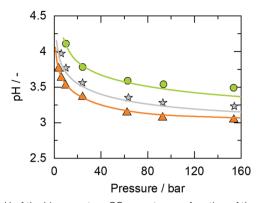


Fig. 1 pH of the binary system CO₂ + water as a function of the pressure at equilibrium CO₂ concentrations. Experimental data from Peng et al. 19 (circles: 432 K, stars: 368 K, and triangles: 323 K), Lines are modeling results obtained with ePC-SAFT advanced using the parameters listed in Tables S1-S3 in the ESI.† The underlying CO2 solubilities were modeled using the same approach, cf. ref. 20

the residual chemical potential μ_i^{res} can be accessed by derivations of ares with respect to density and mole fraction. This allows modeling fugacity coefficients and thus, modeling pH and phase equilibria using the φ - φ concept. More details on the modeling procedure and parameters used can be found in the ESI.† For technical details regarding the multiphase equilibria calculations, please refer to ref. 26.

The pH of the binary system CO₂ + water for temperatures up to 423 K and pressures up to 150 bar was found to be in the range 3.0 < pH < 4.0 depending on the amount of dissolved CO₂ and thus, on temperature and pressure. ²⁰ Fig. 1 represents pH values in the system CO₂ + water at various temperatures.

Fig. 1 shows that ePC-SAFT advanced is able to predict the pH of the binary system CO₂ + water over a broad temperature range and pressure range with an excellent agreement with available data from the literature. The dependence of pH on temperature and pressure is interrelated to CO2 solubility. The higher the pressure, the more CO2 is soluble in water, which makes the aqueous solution more acidic and decreases the pH. In addition, the pH increases with an increase in temperature. This is again caused by CO2 solubility that decreases with increasing temperature and produces a less acidic solution. The underlying CO₂ solubility was predicted as well, cf. ref. 20.

Fig. 2 shows the pH in the pseudo-ternary system CO₂ + water + salt as a function of the salt molality $\tilde{m}_{\rm salt}$ for the salts KCl, NaCl, and NaHCO3. Fig. 2 illustrates that predictions obtained with ePC-SAFT advanced are in excellent agreement with the available literature data. This is an outstanding result since the ePC-SAFT parameters for all ionic species were used from the literature, and binary fitting parameters between CO2 and ions were not used. Note, the binary fitting parameters within SAFT models are a correction for the short-range forces and thus, not related to electrostatics (the electrostatic potentials as applied by us do not include adjustable parameters). As no binary dispersion parameters between CO2 and ions were applied, the shown results are fully predictive. This also applies to the CO2 solubilities that were predicted as well and the

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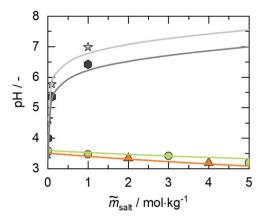


Fig. 2 pH of the ternary system CO_2 + water + salt as a function of salt molality $\tilde{m}_{\rm salt}$ at equilibrium CO_2 concentrations. Symbols are experimental data from the literature (stars:²¹ NaHCO₃ at T=308 K and p=9.2 bar, hexagons:²¹ NaHCO₃ at T=308 K and p=43 bar, circles:²¹ NaCl T=343 K and p=10 bar, and triangles:²² KCl at T=298 K and p=9 bar). Lines are modeling results obtained with ePC-SAFT advanced using the parameters listed in Tables S1–S3 in the ESI.† The underlying CO_2 solubilities were modeled using the same approach, see ESI† Fig. S1 and S2. A low-concentration regime is shown in ESI† Fig. S3.

corresponding results are shown in Fig. S1, S2 and S4 in the ESI.† A strong increase in pH is visible in Fig. 2 for the system CO_2 + water upon the addition of NaHCO₃.

The addition of bicarbonate (HCO₃⁻) salts drastically shifts the dissociation equilibrium of eqn (2) to the left-hand side, which explains the subsequent shift of pH. Thus, ePC-SAFT advanced is able to predict the influence of salts containing a reactive species on the pH. Furthermore, Fig. 2 shows that the pH stays almost constant upon addition of NaCl or KCl. The chloride salts are not involved directly in the dissociation equilibrium. However, the presence of ions (e.g., Na⁺ or Cl⁻) indirectly affects the dissociation equilibrium via salting-out effects. Thus, a small effect of such salts on the resulting pH might have been expected. As the chloride salts cause a decrease in CO2 solubility (see Fig. S2 and S4 in ESI†), the pH is expected to increase upon chloride addition. However, according to experimental measurements shown in Fig. 2, the pH slightly decreases upon adding NaCl or KCl. ePC-SAFT advanced is able to account for these effects and is able to correctly predict the resulting pH. This effect is caused by the proton activity that decreases upon chloride addition. Anyway, this effect is not pronounced and the pH of CO2 + water + chloride salt remains in the range of 3.0 < pH < 4.0 as already found for the binary system CO₂ + water. This observation has already been stated in previous works (cf. ref. 20) where the influence of dissociated carbonic acid was found to be negligible in the systems CO₂ + water + chloride salts.

Furthermore, the predictive capabilities of ePC-SAFT advanced were tested against experimental pH values in demixed aqueous/organic systems. The equilibrated aqueous phase that originates from a phase split of a two-phase liquid-liquid system formed by water and an organic solvent, with a weak organic acid dissolved into that system, was considered.

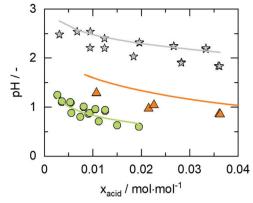


Fig. 3 pH of ternary systems carboxylic acid + water + organic solvent. pH plotted against the acid mole fraction $x_{\rm acid}$ in the aqueous phase of the biphasic aqueous/organic liquid–liquid equilibrium. Symbols are experimental data from the literature at T=298 K and p=1 bar (stars:²³ acetic acid, triangles:²⁴ citric acid, and circles:²⁵ oxalic acid). Lines are predicted results obtained with ePC-SAFT advanced. The underlying liquid–liquid equilibria were modeled using the same approach, see ESI,† Fig. S5.

ePC-SAFT advanced prediction results of pH are displayed in Fig. 3. These pH values were predicted at liquid-phase compositions of the aqueous phase that were also modeled with ePC-SAFT advanced (using the same model parameters). These are shown in Fig. S5 in the ESI.†

The considered pseudo-ternary systems carboxylic acid + water + organic solvent comprise one of the acids acetic acid, citric acid, and oxalic acid. The biphasic systems are formed by water and an organic solvent. The systems with acetic acid and oxalic acid contain toluene as the solvent, whereas the system with oxalic acid contains methyl isobutyl ketone (MIBK) as the solvent. As shown in Fig. 3, ePC-SAFT advanced is able to predict the pH value in the aqueous phase of the ternary systems carboxylic acid + water + organic solvent with an excellent agreement with the literature data. The purecomponent parameters were inherited from the literature. Binary interaction parameters k_{ij} between the acid and the organic solvent were fitted to experimental partition coefficients from the literature. 23-25 Binary interaction parameters between water and the organic solvent were fitted to the respective binary liquid-liquid equilibria, which were partly inherited from previous works. It is important to note that no binary interaction parameters were fitted for pairs that involve ionic species; such k_{ii} values were all set to zero according to experiences from previous publications. 16,26 Most importantly, no parameters were fitted to the experimental pH values considered in this work. The input data were the pK_a values and dielectric constants (Tables S4 and S5 in ESI†). All results of the considered systems (Table S6 in ESI†) are summarized by deviations between predictions and experimental data in Tables S7-S16 in ESI.† These results open the door for determining pH also in non-aqueous phases, since the isofugacity φ - φ concept requires that proton activity must be equal in the aqueous and the organic phase at phase equilibrium.

To sum up, this work suggests following the IUPAC definition for pH towards pH prediction in aqueous phases. A protonactivity-based calculation framework was developed to predict pH values in reactive phase equilibria coupled with dissociation reactions of water, CO2, or a carboxylic acid. It was suggested to use the equation of state ePC-SAFT advanced for the estimation of the required fugacity coefficients and activity coefficients of the dissolved components and especially of the proton. The studied systems were CO₂ + water + salt and carboxylic acid + water + organic solvent. All pure-component parameters for ePC-SAFT advanced were inherited from the literature. Binary interaction parameters (if any) were fitted to phase diagrams of binary systems of the molecular species present in the system, while no binary interaction parameters were used between any pair ion-molecular species. Thus, the pH values calculated in this work were obtained fully predictively. Despite this, the pH could be predicted in excellent agreement with the literature values, ultimately showing the potential of the developed

modeling approach towards accessing pH values and dissocia-

tion degrees of the dissolved components. This can be con-

sidered as an important step in reducing the experimental

effort to optimize reactive biochemical systems and processes

for CO2 capture and processing as well as for downstream

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Conflicts of interest

processing of carboxylic acids.

There are no conflicts to declare.

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