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## Mechanically stable structured porous boron nitride with high volumetric adsorption capacity†

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The development of adsorbents into structured and robust forms remains a challenge for emerging porous materials. In the context of porous boron nitride (BN), studies point to a tradeoff between mechanical stability, porosity, density, and adsorption kinetics. Approaches towards shaping and densification of porous BN have been mostly empirical since a detailed understanding of its formation mechanism, and how it impacts mechanical strength and porosity, is lacking. Here, we demonstrate a synthesis method that can directly produce a mechanically robust structured BN from an easily scalable polymeric precursor, which results in the highest volumetric surface area among porous BN samples to date. Structured BN exhibits a high bulk density (ca.  $0.3\text{ cm}^3\text{ g}^{-1}$ ), 50% higher than BN powders and over ten times higher than the structured BN aerogel, while maintaining fast sorption kinetics. Structured BN presents good mechanical strength, with hardness of  $66.4 \pm 4.5\text{ MPa}$  determined *via* microindentation, *i.e.* one to two orders of magnitude higher than reported structured aerogels. Using a range of material characterisation techniques, we propose a formation mechanism for structured BN. This formation mechanism reveals that the crosslinked intermediates are responsible for the high mechanical strength of the final material. Our approach produces a form of BN that addresses the limitations of other BN- and non BN-based adsorbents, and facilitates their application in gas separation and storage technologies.

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## 1. Introduction

Owing to their high surface area, large porosity and rich surface functionalities, porous materials (*e.g.* zeolites, activated carbon, and metal-organic frameworks) can be used in a range of applications from catalysis to gas separation, and storage.<sup>1–3</sup> Processing these materials from powders to robust densified structures (*e.g.* pellets, beads, and monoliths) represents a necessary step towards their industrial deployment. Indeed, powders suffer from limited mass transfer and poor mechanical strength and they are difficult to handle at scale.<sup>4,5</sup> The large amount of interparticle space in powders also causes low bulk density and low volumetric adsorption/storage capacity,<sup>6,7</sup> which in turn, leads to an increased footprint.<sup>8,9</sup>

Shaping and densifying powders into mechanically robust structures can be done as follows: (i) mechanical compaction, (ii) application of binders, or (iii) growth on monolithic supports.<sup>7</sup> These approaches usually result in decreased performance due to pore collapse from high-pressure, pore blockage from binders, or 'dead' volume from the support. Recently, Tian *et al.* developed a methodology towards the densification of metal-organic frameworks *via* a sol-gel method without using high-pressure compaction or binders, providing scope for the development of monolithic porous materials.<sup>9</sup> However, the advances of producing other robust porous materials is still lacking, particularly for ceramics.<sup>10</sup>

Amorphous boron nitride (BN) represents a relatively new addition to the porous materials family,<sup>11–16</sup> with recent studies demonstrating its use in molecular separation,<sup>13,17–22</sup> catalysis,<sup>23</sup> and drug delivery.<sup>24</sup> Like other porous materials, identifying a way to shape and densify BN without compromising the porosity is needed. We note increasing focus towards producing structured BN in the recent literature. For example, BN aerogel, the most common form of structured BN, has been synthesised using various methods such as direct chemical reaction,<sup>25,26</sup> carbonaceous template assisted method,<sup>27–29</sup> or molecular substitution.<sup>30</sup> Yet, all structured BN aerogels exhibit low density and mechanical strength, preventing their upscaling for practical adsorption applications. Sintering, another important method to synthesise structured BN, usually leads to a low

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surface area, albeit with high mechanical strength.<sup>31</sup> Overall, these studies lead to two main observations: (i) a tradeoff persists between mechanical stability, porosity, density and adsorption kinetics; (ii) approaches towards shaping and densification of porous BN have been mostly empirical since a detailed understanding of porous BN formation mechanism and how it impacts mechanical strength and porosity is lacking. We hypothesise that higher bonding densities within BN will allow good resistance to deformation and loading. Hence, monitoring the formation mechanism of porous BN and linking it to mechanical strength will be important towards developing robust densified porous BN structures.

Herein, we present a method to synthesise structured BN, which exhibits high surface area, mechanical strength and enhanced volumetric adsorption capacity compared to powder BN. Structured BN also shows enhanced hydrolytic stability compared to BN powders, owing to a reduced oxygen content. Our method does not involve any compaction, binding or supporting step but instead relies on the use of a mechanically stable polymer precursor, a melamine-formaldehyde (MF) resin. MF resins have been well-developed at industry scale, making the current synthesis method suitable for upscaling. Through in-depth XPS and FTIR analyses, we determine the formation mechanism of structured BN starting from this polymer and how it influences the resulting mechanical stability.

## 2. Experimental section

### 2.1 Materials

Melamine (99%), urea ( $\geq 99.5\%$ ) and boric acid ( $\geq 99.5\%$ ) were purchased from Sigma-Aldrich; dicyandiamide (99.5%), and formaldehyde solution (37%) were purchased from Fisher. All chemicals were used as received. The gases used in this study, namely NH<sub>3</sub> (99.98%), CH<sub>4</sub> (99.5%), N<sub>2</sub> (99.9995%), and Ar (99.999%) were purchased from BOC.

### 2.2 Synthesis of structured and powder BN

A mechanically robust melamine-formaldehyde resin, referred to as MF resin, was used as the precursor to synthesise structured BN. The overall synthesis procedure is shown in Scheme 1 and described below.



**Scheme 1** Schematic representation of structured BN synthesis via the formation of a melamine-formaldehyde resin (MF resin). A = melamine + formaldehyde; B = dicyandiamide, C = boric acid.

**2.2.1 Synthesis of MF resin.** Formaldehyde (5 mL), NaOH (1 M, 0.15 mL) and melamine (2.08 g) were mixed in a 50 mL round bottom flask and stirred at 90 °C for 1 h. 1.5 g dicyandiamide (DCD) was then added to the transparent solution and stirred for 5 min. Boric acid (1 g) was added to the transparent solution and vigorously stirred for 2 min, followed by a curing step at 80 °C overnight. The collected transparent solid was further dried at 120 °C under vacuum overnight and is referred to as MF resin. The MF resin 'slab' broke into small pieces after vacuum treatment.

**2.2.2 Synthesis of structured BN.** The MF resin was placed in an alumina boat crucible and transferred to a tubular furnace. The resin was first degassed at room temperature under Ar flow (250 mL min<sup>-1</sup>). Upon completion of the degassing, the sample was heated to 1000 °C (10 °C min<sup>-1</sup>) under pure NH<sub>3</sub> gas flow (100 mL min<sup>-1</sup>) and held isothermally for 3 h, unless otherwise specified. The furnace was cooled naturally under NH<sub>3</sub> to 600 °C and then to room temperature under Ar. A light yellow structured material was collected after the synthesis and further dried at 120 °C under vacuum overnight.

**2.2.3 Synthesis of powder BN.** Powder porous BN was synthesised based on the method reported previously by our group.<sup>20</sup> Boric acid (0.618 g), melamine (0.126 g), and urea (3 g) were mechanically mixed and ground for 5 min in an agate mortar. The mixture was placed in an alumina boat crucible and transferred to a tubular furnace. The resin was first degassed at room temperature under N<sub>2</sub> flow (250 mL min<sup>-1</sup>). Upon completion of the degassing, the sample was heated to 1050 °C (10 °C min<sup>-1</sup>) under N<sub>2</sub> gas flow (50 mL min<sup>-1</sup>) and held isothermally for 3.5 h. The furnace was cooled to room temperature naturally and white powder sample was collected and further dried at 120 °C under vacuum overnight. This powder sample was selected because it has the highest surface area among all powder samples we have made.

**2.2.4 Formation of BN pellets.** ~150 mg of BN powder was ground with an agate pestle and mortar and was placed into a 13 mm pellet die (Specac, 13 mm). The die was positioned into a manual press and 5 tonnes of load was applied and held for ~60 s to form a pellet.

### 2.3 Material characterisation

**2.3.1 Chemical properties.** Infrared (IR) spectra were collected using a PerkinElmer Spectrum 100 spectrometer equipped with an attenuated total reflectance accessory. The samples were first ground using an agate mortar and spectra were collected in the range of 650–4000 cm<sup>-1</sup>. X-ray photoelectron spectroscopy (XPS) was performed on a Thermo Scientific K-Alpha<sup>+</sup> X-ray photoelectron spectrometer equipped with a MXR3 Al K $\alpha$  monochromated X-ray source ( $h\nu = 1486.6$  eV). The samples were initially ground and mounted onto an XPS sample holder using a small piece of conductive carbon tape. The X-ray gun power was set to 72 W (6 mA and 12 kV). The high-resolution spectra were obtained using 20 eV pass energy and 0.1 eV step size. Thermo Avantage software was used to analyse the data.



**2.3.2 Textural properties and morphology.** Powder X-ray diffraction (PXRD) patterns were recorded using a PANalytical X'Pert PRO diffractometer using Cu K $\alpha$  radiation ( $\lambda = 1.54178 \text{ \AA}$ ) with a step of  $0.01^\circ$  at a scanning speed of 10 s per step. An anode voltage of 40 kV and emission current of 20 mA were chosen as the operating conditions. Scanning electron microscope (SEM) images were taken using a Zeiss Auriga microscope with an accelerating voltage of 5 kV. The samples were placed on the carbon tape without grinding and coated with 15 nm of gold. Transmission electron microscope (TEM) images were taken using a FEI Titan 80-300 Cs image-corrected microscope. The sample was dispersed in ethanol and drop-depositing the supernatant on a holey carbon copper grid. N<sub>2</sub> adsorption isotherms were undertaken at 77 K, using a Micromeritics 3Flex instrument. The samples were initially degassed overnight at 120 °C at approximately 0.2 mbar pressure. Prior to the sorption isotherm measurement, the samples were further degassed *in situ* for 4 h at 120 °C. The equivalent specific surface areas of the samples were determined using the Brunauer–Emmett–Teller (BET) method.<sup>32</sup> The total pore volume was evaluated from the volume of N<sub>2</sub> adsorbed at a relative pressure ( $P/P_0$ ) of 0.97. The micropore volume was determined using the Dubinin–Radushkevich model.<sup>33</sup> The pore size distribution was derived from the built-in software from Micromeritics, using DFT model for carbon slit shape pores. Rate of adsorption data was logged by intercepting the raw 3Flex data output using PuTTy. Mercury porosimetry was employed up to a final pressure of 2300 bar using an AutoPore IV 9500 instrument from Micromeritics to measure the bulk density. Prior to the analysis, the samples were activated overnight at 120 °C under vacuum.

**2.3.3 Moisture stability test.** A vial with 20 mL of DI water was placed in a 1 L sealed container until the relative humidity reached >99%, which was measured by a hygrometer. Structured BN was kept in the container for different durations before it was collected and dried at 120 °C under vacuum.

**2.3.4 Mechanical stability test.** The hardness of structured BN was measured using a Struers Duramin -1/2 Micro-Vickers hardness tester, following the Vickers method. A load of 0.025 kgf (1 kgf = 9.8 N) was applied with a dwell time of 12 s. For each sample, at least 10 indentations were performed at different points. The samples were polished on 2000 grit sandpaper with a Struers TegraPol-31 polisher before the measurement.

**2.3.5 Methane adsorption isotherms.** High-pressure CH<sub>4</sub> adsorption isotherms were carried out at 298 K in the pressure range of 0–70 bar using the equipment and method reported before.<sup>34</sup> In brief, CH<sub>4</sub> uptake was measured gravimetrically using a Rubotherm Magnetic Suspension Balance (MSB) with an equilibration time of at least 90 min for each pressure point. The samples were initially degassed in a vacuum oven overnight at 393 K and approximately 0.2 mbar pressure. Prior to the sorption isotherm measurement, the samples were further degassed *in situ* for 12 h at 393 K and a Helium gravimetry experiment was carried out at 298 K to estimate the adsorbent skeletal density.

### 3. Results and discussion

#### 3.1 Synthesis of structured BN

We used a macroporous melamine-formaldehyde (MF) resin as the precursor to produce structured BN (Scheme 1). To synthesise the porous MF resin, we employed dicyandiamide (DCD) as a foaming agent<sup>35</sup> and boric acid as the curing agent. The pore density in the MF resin was controlled by the DCD content and appears to impact the final morphology of the porous BN (Fig. 1). DCD acts as a porogen for the MF resin. Indeed, on the one hand, a low DCD content results in a non- or poorly porous MF resin, as indicated by the low ‘bubbles’ density observed on the microscope images (Fig. S1†). We attribute this behavior to the fact that gases generated during pyrolysis could not easily ‘escape’ through the tight resin, thus leading to pressure build-up and eventually structure collapse (Fig. 1a and b). On the other hand, a high DCD content formed a highly porous resin (Fig. S1†). We speculate that the low crosslink density (*i.e.* high porosity) of the resin meant that it was too fragile to withstand the chemical decomposition and gas release during pyrolysis, leading to the formation of powder (Fig. 1e). Overall, we have found that a DCD/melamine weight ratio of 0.72 resulted in a precursor with moderate pore density and high mechanical strength. In this case, the pores act as channels for the porogen to escape while the good crosslink density prevents the collapse of the macrostructure upon pyrolysis. As a result, we obtain a structured BN sample (Fig. 1c and d).

Based on the observations above, we then focused our attention on the BN samples obtained using a 0.72 DCD/melamine weight ratio (Fig. 1d and S2†). We explored the effects of reaction atmosphere, reaction temperature and duration on the pyrolysis product to identify the optimal pyrolysis conditions. Looking first at the reaction atmosphere, we note significant differences between the products obtained under either NH<sub>3</sub> or N<sub>2</sub>, starting from the colour: yellowish *vs.* black, respectively. As shown in Fig. S3†, the sample obtained under NH<sub>3</sub> exhibits a higher BET specific surface area than that obtained under N<sub>2</sub> (1513 m<sup>2</sup> g<sup>-1</sup> *vs.* 216 m<sup>2</sup> g<sup>-1</sup>). These differences result from the amount of active N-containing gases (*e.g.* NH<sub>3</sub>) during the synthesis. Under N<sub>2</sub>, the reactive N source comes principally from the resin and is insufficient for complete reaction with boric acid. Therefore, carbonization is predominant resulting in a black sample with a low surface area. In contrast, the synthesis under NH<sub>3</sub> provides an excess of

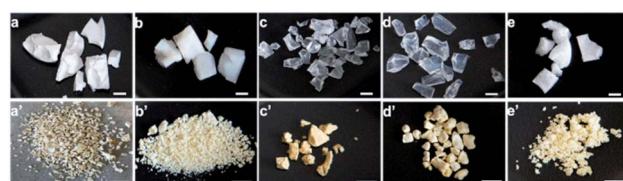


Fig. 1 Optical images of the melamine-formaldehyde (MF) resin with different amounts of foaming agent, DCD (a–e), and the derived porous BN samples (a'–e'). DCD/melamine weight ratio of (a) and (a') 0; (b) and (b') 0.24; (c) and (c') 0.48; (d) and (d') 0.72; (e) and (e') 0.96. Scale bar = 1 cm.



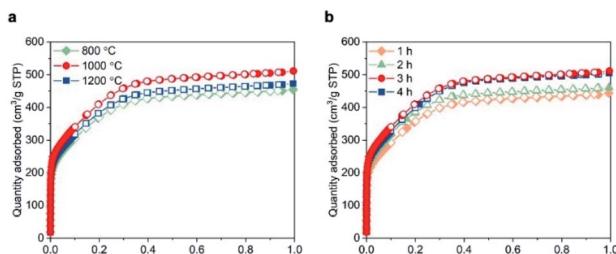


Fig. 2 Analysis of the pyrolysis conditions on the porosity of BN.  $N_2$  sorption isotherms of structured BN at 77 K. (a) Pyrolysed for 3 h at different temperatures; (b) pyrolysed at 1000 °C for increasing durations.

reactive N over a wide range of temperature, which is known to enhance the surface area of porous BN.<sup>20</sup> Consequently,  $NH_3$  was selected as the reaction atmosphere for further tests.

Next, we investigated the effects of the reaction temperature and the duration of the isothermal step. Keeping the duration at 3 h, the BET specific surface area increased from  $1349\text{ m}^2\text{ g}^{-1}$  at 800 °C to  $1513\text{ m}^2\text{ g}^{-1}$  at 1000 °C (Fig. 2a). Further increasing the reaction temperature to 1200 °C resulted in a decreased BET area ( $1397\text{ m}^2\text{ g}^{-1}$ ), possibly due to a partial crystallization of BN.<sup>13,30</sup> Furthermore, extending the duration of the isothermal step up to 3 h at 1000 °C enhanced the porosity (Fig. 2b). Beyond 3 h, the surface area reached a plateau, pointing towards a completion of the reactions leading to the gases release and porosity formation. To summarise, pyrolysing the MF resin in  $NH_3$  atmosphere at 1000 °C for 3 h appeared the most effective method in obtaining structured BN and was used in the current work.

### 3.2 Characterisation of structured BN

We now analyse in more detail the features of structured BN obtained using the optimal conditions determined above.

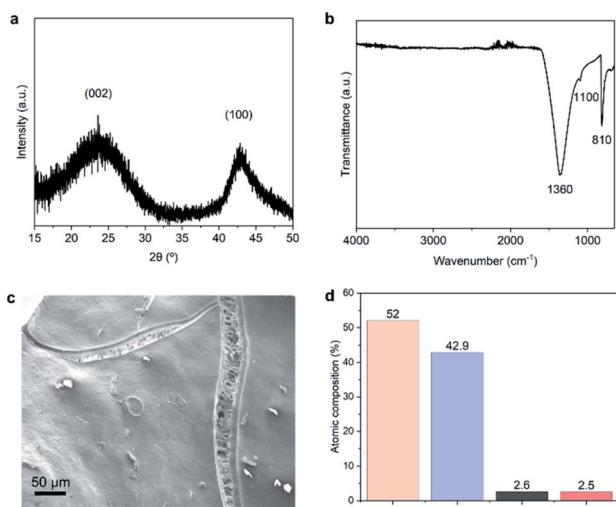


Fig. 3 Structure, morphology and surface composition of structured BN. (a) XRD patterns; (b) FTIR spectrum; (c) SEM image; (d) XPS relative atomic percentages.

Fig. 3a shows the XRD pattern of the sample. The two broad peaks corresponding to (002) and (100) planes together with the absence of other reflections point to the presence of turbostratic/amorphous BN.<sup>30</sup> The two main characteristic IR bands of BN at  $\sim 1360\text{ cm}^{-1}$  (in-plane BN stretching) and at  $\sim 810\text{ cm}^{-1}$  (out-of-plane B–N–B bending) are detected (Fig. 3b), confirming the chemical composition of structured BN.<sup>20</sup> We attribute the additional small band at  $\sim 1100\text{ cm}^{-1}$  to B–O bending mode.<sup>23</sup> The presence of oxygen is further confirmed by XPS analyses, with a quantity of 3 at% (Fig. 3d). The lower oxygen content of structured BN compared to powder BN (3 at% vs. 9 at%) leads to a significant improvement of hydrolytic stability, an important feature for industrial application, as shown in Fig. S4 and S5†.<sup>36</sup> SEM image of structured BN (Fig. 3c and S6†) reveals a continuous solid phase with slender cracks. The compact solid phase presents a relatively flat surface similar to other highly dense monolithic porous materials.<sup>8,9</sup> The morphology is different from that of powders or aerogels, which contain a large amount of interparticle space.<sup>20,29</sup> The slender cracks with macropores are distributed within the continuous flat surface and may result from the pores in the resin precursor. The pores propagated and enlarged under the stress generated during the synthesis, forming these gully-like cracks. TEM images in Fig. S7† reveal that the structured BN possesses disordered microstructure, which is supported by the fast Fourier transform (FFT) patterns. These analyses point to an amorphous nature of structured BN similar to powder BN.

### 3.3 Textural and gas adsorption properties of structured BN vs. powder BN

We evaluated the porosity of structured BN using the  $N_2$  adsorption isotherms at 77 K and compared it with a highly porous BN powder recently reported by our group (Table 1, Fig. S8†).<sup>20,23</sup> Structured BN possesses a similar specific surface area to powder BN. However, different to powder BN which exhibits type IV isotherms (*i.e.* mesoporous material), structured BN exhibits a type I(b) isotherm, typical for materials with both micropores and narrow mesopores.<sup>37</sup> The pore size distribution in Fig. S9† shows that the majority of the pores in structured BN are  $<2.5\text{ nm}$ . Furthermore,  $N_2$  sorption in structured BN plateaus for  $P/P_0 > 0.5$ . On the contrary,  $N_2$  adsorption in powder BN increases towards high  $P/P_0$  values due to  $N_2$  condensation. This is due to the compact nature of structured BN, which results in minimal interparticle porosity.

To quantify the compact nature of structured BN, we measured its bulk density using mercury porosimetry, a well-established technique that has been used to measure the bulk density of other porous materials.<sup>38</sup> Mercury is a non-wetting liquid that does not intrude small pores at ambient pressure, which facilitates the measurement of bulk volume and thus the density (Section S4.2†). Table 1 shows the bulk density of structured BN was  $0.31\text{ g cm}^{-3}$ , nearly 50% higher than that of the bulk powder, which leads to a significantly higher volumetric BET area, achieving  $473\text{ m}^2\text{ cm}^{-3}$  (vs.  $315\text{ m}^2\text{ cm}^{-3}$  for powder BN). To densify the powder, we prepared BN pellets by compressing powder BN under 5 tonnes. Even though the bulk



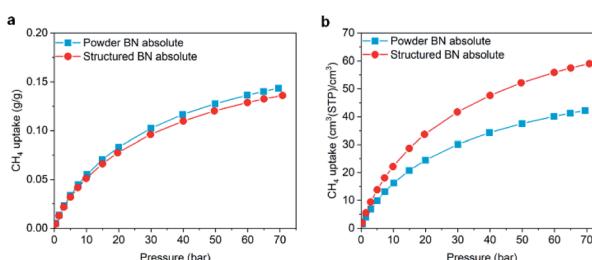
**Table 1** Comparison of gravimetric and volumetric properties of structured BN and powder BN. BET area ( $S_{\text{BET}}(\text{mass})$ ), total pore volume ( $V_{\text{tot}}$ ), micropore volume ( $V_{\text{micro}}$ ) obtained from  $N_2$  sorption isotherms at 77 K and bulk density ( $\rho$ ) and volumetric BET area ( $S_{\text{BET}}(\text{vol})$ ) derived from mercury porosimetry

	$S_{\text{BET}}(\text{mass}) [\text{m}^2 \text{ g}^{-1}]$	$V_{\text{tot}} [\text{cm}^3 \text{ g}^{-1}]$	$V_{\text{micro}} [\text{cm}^3 \text{ g}^{-1}]$	$\rho [\text{g cm}^{-3}]$	$S_{\text{BET}}(\text{vol}) [\text{m}^2 \text{ cm}^{-3}]$
Structured BN	1523	0.79	0.56	0.31	473
Powder BN	1500	1.14	0.56	0.21	315

density improved (*i.e.* 0.43 g cm<sup>-3</sup>), the overall volumetric BET area remained lower than that of structured BN due to a lower gravimetric surface area (Fig. S8†) caused by the pore collapse. We note that structured BN aerogels usually exhibit bulk densities of 0.01–0.02 g cm<sup>-3</sup>,<sup>25,26,39–43</sup> more than one order of magnitude lower than that of structured BN, ultimately leading to a low volumetric BET area (*i.e.* 0.1–14 cm<sup>2</sup> cm<sup>-3</sup>). On the other hand, sintered structured BN typically shows high density but a low BET area (<450 m<sup>2</sup> g<sup>-1</sup>),<sup>31</sup> which results in a moderate volumetric BET area similar to the powder BN. Structured BN therefore exhibits the highest volumetric BET area for a BN sample published to date (Table S1†).

Volumetric methane storage capacity can be attractive for on board applications, where space for fuel is always a constraint. In these cases, the volumetric methane uptake is to be considered. Given the volumetric properties of structured BN, we performed CH<sub>4</sub> adsorption isotherms at 298 K up to 70 bar. Fig. 4a shows that the absolute gravimetric uptake of structured BN is comparable to that of powder BN, owing to the similar surface area and micropore volume. Remarkably, structured BN shows a significant enhancement when considering the absolute volumetric adsorption capacity (59 vs. 42 (STP) cm<sup>3</sup> cm<sup>-3</sup> at 70 bar) as a result of the higher bulk density of structured BN (Fig. 4b and S10†).

A higher material density often compromises adsorption kinetics due to the mass transfer limitation. To explore the adsorption kinetics of structured BN, we measured the adsorption equilibration time of N<sub>2</sub> adsorption at an extremely low pressure ( $2.2 \times 10^{-6}$  bar) at 77 K and compared the results likely to be the most visible, hence the selection of  $2.2 \times 10^{-6}$  bar for the measurement. Both samples show very fast adsorption kinetics, reaching equilibrium within 60 s (Fig. S11†). The small difference was mainly attributed to the lower macroporosity in structured BN, which results in a slightly lower diffusivity.



**Fig. 4** Comparison of absolute methane uptake at 298 K between powder BN (blue squares) and structured BN (red circles), (a) gravimetric capacity; (b) volumetric capacity.

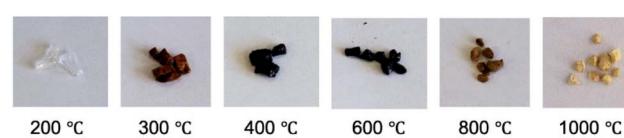
### 3.4 Mechanical stability of structured BN

Mechanical stability of adsorbents is an important property in practical applications as materials are always exposed to mechanical stress such as operational vibration and compression, *i.e.* weight of the packed adsorbent. As a preliminary and quick visual test of the mechanical robustness of structured BN, we first loaded a calibration weight onto the sample (Fig. S12†). *Ca.* 0.005 g of structured BN maintained its integral bulk structure under a 200 g calibration weight, pointing to an apparent robustness. We then evaluated quantitatively the hardness of the sample using microindentation. Our results show the hardness of structured BN is  $66.4 \pm 4.5$  MPa, which is comparable to dense binder-free graphene oxide pellets<sup>44</sup> and macroporous nickel foam.<sup>45</sup> Remarkably, the hardness is 1–2 orders of magnitude higher than that reported for BN aerogels,<sup>46,47</sup> suggesting a much higher resistance to plastic deformation, mainly attributed to the higher density.

### 3.5 Formation mechanism of structured BN

Finally, we aimed to understand the formation mechanism of structured BN and its impact on the mechanical stability of the material by analysing the structural evolution from MF resin to structured BN. To do so, we collected samples obtained from the pyrolysis of MF resin under NH<sub>3</sub> at different temperatures: 200, 300, 400, 600, 800 and 1000 °C. We then analysed the structural and chemical properties of these intermediates. Fig. 5 presents the optical images of the intermediates and highlights significant changes in aspect as the sample subsequently turned brown (300 °C), black (400 and 600 °C), brown (800 °C) and yellow (1000 °C).

We used XPS to identify the chemical structure of the intermediates. The core level spectra of B1s, N1s and O1s are presented in Fig. 6a–c. The intermediate collected at 200 °C shows the typical melamine resin spectrum, namely two peaks located at 339.4 eV (pyrrolic N) and 398.2 eV (pyridinic N), respectively in N1s spectra and one peak at 287.6 eV assigned to triazine ring in C1s spectra.<sup>48,49</sup> The absence of C–O peak suggests the resin is crosslinked *via* methylene bridges rather than ether bridges. Only a single peak at 192.2 eV corresponding



**Fig. 5** Optical images of melamine-formaldehyde resin (MF resin) heated at increasing temperatures under NH<sub>3</sub> atmosphere.



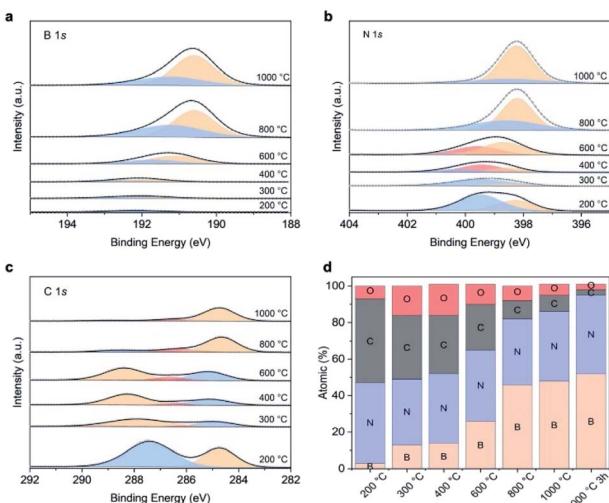


Fig. 6 Surface composition of intermediates obtained at different temperatures as determined by high resolution XPS spectra: (a) B 1s; (b) N 1s; (c) C 1s; (d) XPS relative atomic percentage of intermediates.

to B–O in boron oxide is displayed in B1s spectra, indicating that boron oxide is physically interacted with resin at this temperature but not yet interacting chemically. At 300 °C, we observe the contribution of B–O–C bonds at 192 eV in B1s spectra.<sup>50,51</sup> The appearance of this new bond is supported by

the new C–O peak (286.4 eV) in C1s spectrum, revealing that chemical interactions between boron oxide and the MF resin start at 300 °C. Further increasing the temperature to 400 °C does not alter the B1s spectra. However, the main peak in C1s shifts to a higher binding energy. This observation together with the presence of graphitic N (400.3 eV) in N1s spectrum suggests the evolution from triazine to heptazine likely from the melon-based structure, an intermediate commonly observed in carbon nitride, g-C<sub>3</sub>N<sub>4</sub>, evolution.<sup>52,53</sup> At 600 °C, we observe the formation of boronoxynitride, an important intermediate in forming porous BN, as evidenced by the new peaks at 191.2 eV (B1s) and 399.6 eV (N1s).<sup>19,47</sup> Our findings show that all the boron atoms chemically interact with the resin skeleton by either *via* B–O–C or B–O–N bond at 600 °C. BN is subsequently formed at 800 °C, as evidenced by the peaks at 190.6 eV and 398.2 eV from B1s and N1s, respectively. The majority of carbon atoms are removed at this stage as seen in Fig. 6d and as suggested by the lighter colour of the 800 °C intermediate.<sup>54,55</sup> Further increasing the temperature boosts carbon and oxygen removal and BN conversion through nitridation, resulting in a porous BN with a bright yellow colour. The structural evolution above is supported by the analysis from FTIR shown in Fig. S13.†

Based on the analysis above, we propose the structural evolution from MF resin to structured BN as shown in Fig. 7. First, methylene bridged MF resin bonds chemically to boron

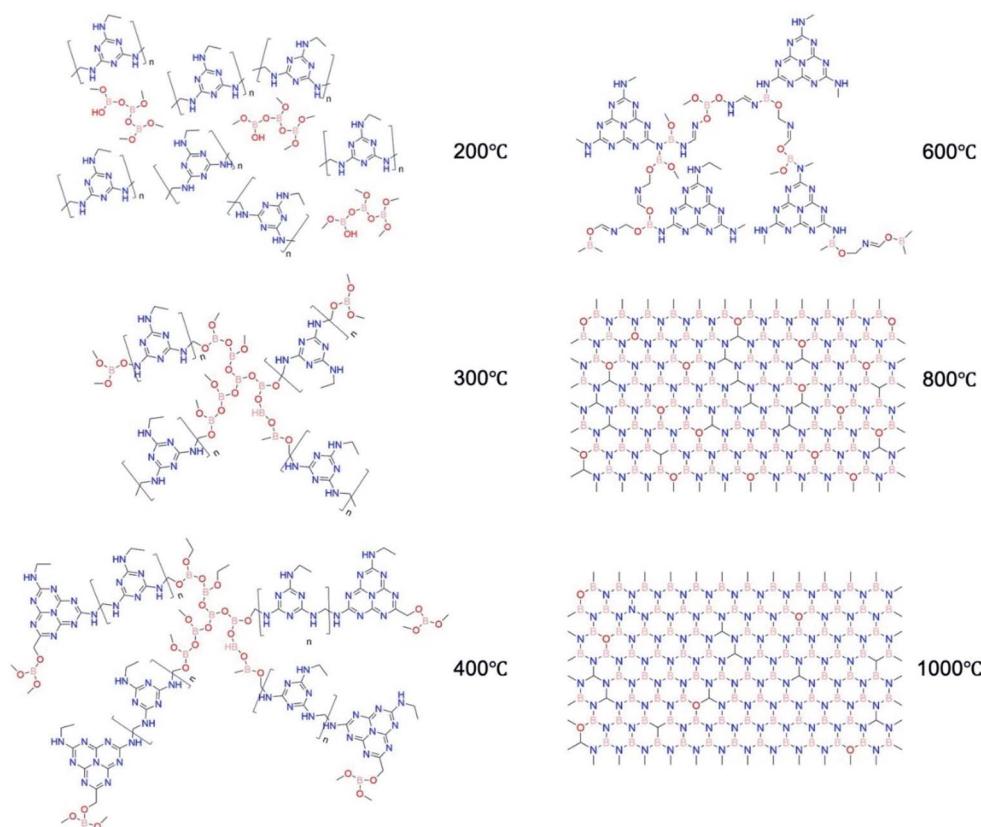


Fig. 7 Proposed structural evolution of structured BN, using melamine-formaldehyde resin (MF resin) as a precursor and NH<sub>3</sub> as the pyrolysis atmosphere.

oxide *via* B–C–O. Then, the formation of a melon-based polymer takes place. Carbon atoms are gradually removed while the remaining compounds retain the crosslinked structure *via* B–O–C and B–O–N bonds. BN is then formed *via* a nitridation process and eventually the structured BN with minimum impurities is produced. Throughout structured BN formation, a crosslinked structure is maintained. This high bonding density in turns allows mechanical robustness to be preserved in the final product. This structural evolution study paves the way for further engineering of structured BN at larger scale.

## Conclusions

We have developed a structured BN using a porous melamine-formaldehyde resin as precursor. A suitable range of pore density in the precursor and a NH<sub>3</sub> synthesis atmosphere are necessary to obtain porous structured BN. Compared to BN powders, structured BN exhibits an improved hydrolytic stability, a 50% higher bulk density and therefore an increased volumetric surface area, the highest among BN materials reported to date. As a result, structured BN displays an enhanced volumetric CH<sub>4</sub> adsorption capacity, while sorption kinetics remains fast. Structured BN shows remarkable mechanical strength (*i.e.* hardness), being one to two orders of magnitude higher than that of aerogels. Studying the structured BN formation mechanism, we found that the polymer intermediates derived from the resin crosslink with boron atoms, which impart the mechanical stability to structured BN. The promising properties support the potential of structured BN for practical molecular adsorption applications and the formation mechanism study facilitates the industrial scale production of structured BN.

## Author contributions

T. T. and C. P. designed the research. T. T. performed the synthesis and characterisation, Y. X. carried out the XRD analyses, A. L. carried out the FTIR analyses and D. D. performed the N<sub>2</sub> adsorption kinetics, all under the supervision of C. P. H. J. performed the micro-indentation. H. A. carried out the high pressure CH<sub>4</sub> adsorption under the supervision of R. P. T. T. and C. P. wrote the manuscript. All the authors contributed to the final version.

## Conflicts of interest

There are no conflicts to declare.

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