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## Dynamic stabilisation during the drainage of thin film polymer solutions†

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The drainage and rupture of polymer solutions was investigated using a dynamic thin film balance. The polymeric nature of the dissolved molecules leads to significant resistance to the deformation of the thin liquid films. The influence of concentration, molecular weight, and molecular weight distribution of the dissolved polymer on the lifetime of the films was systematically examined for varying hydrodynamic conditions. Depending on the value of the capillary number and the degree of confinement, different stabilisation mechanisms were observed. For low capillary numbers, the lifetime of the films was the highest for the highly concentrated, narrowly-distributed, low molecular weight polymers. In contrast, at high capillary numbers, the flow-induced concentration differences in the film resulted in lateral osmotic stresses, which caused a dynamic stabilisation of the films and the dependency on molecular weight distribution in particular becomes important. Phenomena such as cyclic dimple formation, vortices, and dimple recoil were observed, the occurrence of which depended on the relative magnitude of the lateral osmotic and the hydrodynamic stresses. The factors which lead to enhanced lifetime of the films as a consequence of these flow instabilities can be used to either stabilise foams or, conversely, prevent foam formation.

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## 1 Introduction

When bubbles or droplets come into close proximity, a thin liquid film (TLF) usually forms between them. The dynamics of this TLF control both the equilibrium<sup>1</sup> and non-equilibrium<sup>2</sup> properties of various multiphase systems, such as foams, emulsions, antibubbles, and immiscible polymer blends.<sup>3–7</sup> A body of work related to the dynamics of TLFs has focused on the influence of the interaction forces and surface stresses on film stability.<sup>8–10</sup> For example, the effects of DLVO forces acting across the film have been quantified,<sup>11,12</sup> and effects of surface rheology,<sup>13,14</sup> and Marangoni stresses<sup>15–17</sup> on the drainage have been studied for a wide range of surface-active systems. Yet, properties of the bulk fluids in confinement have also been identified as possibly playing an important role.<sup>18–21</sup> The most known effect is the occurrence of oscillatory structural forces normal to the interface due the confinement of finite sized structural elements, such as micelles,<sup>22</sup> nanoparticles<sup>18</sup> or polyelectrolytes.<sup>23</sup> The local structuring causes a difference in the osmotic pressure between the film and the surrounding plateau border which can balance the Laplace pressure difference and stabilises the film.<sup>18</sup> However, the expulsion of a

structured layer can also give rise to attractive depletion forces (Casimir-like forces) which accelerate drainage.<sup>24</sup>

These effects have some common characteristics among different systems, like micelles, nanoparticles, and polyelectrolytes. First, the magnitude of structural forces increases with the concentration.<sup>18,22,25–27</sup> Moreover, smaller sizes lead to larger structural forces,<sup>26,28</sup> with size polydispersity adversely impacting film stability.<sup>18,29–31</sup> For films at equilibrium, this reduction in film stability is attributed to the weakening of the layering in the TLF,<sup>32</sup> while for draining films the different depletion layer lengths play a role.<sup>29</sup> Finally, there have been some reports on polyelectrolytes and micelles, which indicate that structural forces depend on the deformability of the confined species,<sup>27,33</sup> and on their charge density.<sup>33,34</sup>

Structural and depletion forces do not depend only on the intrinsic properties of the confined species and concentration. Rather, the observation of oscillatory forces, as measured in colloidal-probe AFM, was found to depend on the employed approach speed,<sup>27</sup> with the importance of structural forces becoming negligible as hydrodynamics become important.<sup>29</sup> At high drainage speeds, the deformability of the confining film surfaces also plays a role, as it results in a less constrained organisation of the confined species.<sup>35,36</sup>

One common feature is that these forces, either repulsive or attractive, act normal to the film's surface. However, lateral forces can also be induced, *e.g.* as the concentration of confined species in the film becomes increasingly inhomogeneous at

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faster thinning rates, corresponding to high Péclet numbers. This effect can be expected to occur especially in films containing poly-disperse species. In contrast to Marangoni surface stresses,<sup>16</sup> such dynamic osmotic stresses are bulk stresses. The utilisation of such stresses to influence film drainage has not yet been explored. However, there are indications in literature that this is a worthwhile avenue. For example, it has been observed that concentration differences between the inner TLF and the surrounding Plateau border can give rise to an “osmotic swelling” of the dimple, caused by the inflow of liquid towards the centre of the film.<sup>37,38</sup> Moreover, looking back at the pioneering work of Nikolov and Wasan,<sup>18</sup> one can observe that the surfaces of draining films containing nanoparticles show thickness corrugations. This is another indication that apart from the normal contribution of osmotic pressure, there might be a lateral ones too, when concentration gradients are induced by the flow.

Most of the studies mentioned so far involved either the approach of bubbles or particles at constant speed and the measurement of the static oscillatory forces<sup>29,39,40</sup> or planar films draining with very low thinning velocities.<sup>18,30</sup> In such experimental conditions it would be impossible to detect dynamic effects such as the “osmotic swelling of the dimple”,<sup>37,41</sup> similarly to the inability to detect using colloidal-probe AFM<sup>27</sup> the spontaneously growing dimple due to Marangoni counterflows.<sup>42–44</sup> Such effects can only be observed in (i) constant pressure experiments, and (ii) at realistically high capillary numbers, at which the film is dimpled.

The present work aims to investigate the conditions under which such stresses because of concentration fluctuations, which we will term dynamic osmotic stresses, come into play. This bears relevance as polymers in solution are used as viscosity modifiers, *e.g.* in lubricants<sup>45</sup> where undesired foaming can be an issue<sup>46</sup> or in emulsion stability.<sup>47</sup> Browne<sup>48</sup> studied the collision of two air bubbles in aqueous polyvinylpyrrolidone solutions using AFM. No structural or depletion forces were observed. Starting from such a reference case for which osmotic stresses are negligible, we then explore how and when these come into play, specifically interrogating the effect of polymer molecular weight, molecular weight polydispersity, and thinning velocity on their magnitude. We study neutral polymers, which in contrast to ref. 48 have no surface activity. We can thus decouple the effects related to the dynamic osmotic stresses from those related to Marangoni stresses and surface rheology. A good solvent for the dissolved polymer is chosen to ensure that phase separation does not occur at rest.

Using the dynamic thin film balance<sup>49</sup> we study the behaviour of dilute and semi-dilute polymer solutions in a broad range of hydrodynamic conditions. The visualisation capabilities of this technique provides insight into the phenomena occurring in these confined environments, and provide clear guidelines for optimising the formulations of various polymer-containing industrial products, such as foams, emulsions, and lubricants.

## 2 Theoretical background

The dynamics of TLFs containing non-surface active polymer solutions are controlled by an interplay between hydrodynamics, capillarity, and osmotic effects. Here, we provide a brief description of these effects, specifically focusing on how osmotic stresses can arise both in the normal, as well in the lateral direction.

The drainage of TLFs with deformable surfaces is usually described by the generalised Stokes–Laplace–Reynolds equation<sup>50,51</sup> which describes the evolution of the changes in film thickness  $h$ , as a function of radial position relative to the center ( $r$ ) and time ( $t$ ):

$$\frac{\partial h(r, t)}{\partial t} = \frac{1}{12\eta r} \frac{\partial}{\partial r} \left( rh^3 \frac{\partial P_H}{\partial r} \right) - \frac{1}{r} \frac{\partial}{\partial r} (rhU_s), \quad (1)$$

where  $\eta$  is the bulk viscosity of the liquid,  $h$  is the film's thickness, and  $U_s(h, r)$  is the surface velocity, which is equal to zero for highly stress-carrying surfaces.<sup>10</sup> The hydrodynamic pressure  $P_H(h, r)$  is given by a local pressure balance:<sup>52</sup>

$$P_a + \frac{2\sigma}{R} = P_H(h, r) + P_\infty - \Pi_d(h, r) + \frac{\sigma}{2r} \frac{\partial}{\partial r} \left( r \frac{\partial h}{\partial r} \right), \quad (2)$$

where  $P_a$  is the externally applied pressure across the film (driving drainage),  $2\sigma/R$  is the Laplace pressure due to the curvature of the Plateau border ( $\sigma$  being the surface tension, and  $R$  the radius of the bike-wheel's hole),  $P_\infty$  is the pressure at the meniscus,  $\Pi_d$  is the disjoining pressure, and the last term is the local “Laplace” pressure contribution due to curvature differences in the film. As it will be discussed in Section 3.2, the total applied pressure in our setup is equal to  $P_a = P_{c,i} + \Delta P$ , where  $P_{c,i}$  is an initial pressure that is applied to equilibrate the film at a given thickness, and  $\Delta P$  is an additional pressure drop applied on top of this initial pressure to cause film drainage.

Eqn (1) describes the thickness profile that develops in the TLF because of flow. A dimple typically occurs as a result of an interplay between hydrodynamics and capillarity,<sup>51</sup> which can be described by the dimensionless Capillary number,<sup>10,53</sup> defined here based on the film characteristics:

$$Ca = \frac{\eta u R^2}{2\sigma h^2} \sim \frac{\Delta P}{2\sigma/R}, \quad (3)$$

where  $u$  is the characteristic velocity of drainage. Although this interplay between capillarity and hydrodynamics is important in the coalescence of droplets, with typical  $Ca > 10^{-2}$ ,<sup>54</sup> only a few studies in the literature involve the direct visualisation of freestanding films draining at such relatively high values of  $Ca$ .<sup>49,55–57</sup>

In the polymer solution films,  $\Pi_d$  is equal to the sum of attractive the van der Waals interactions ( $\Pi_{vdw}$ ), and the osmotic forces ( $\Pi_{osm}$ ).  $\Pi_d(h)$  is equal to the first derivative of the total excess Gibbs free energy with respect to  $h$ .<sup>58</sup> The stability of films with stress-free surfaces can be improved not only by increasing their bulk viscosity (based on eqn (1)), but also by changing their free energy. In that respect, solutions of non-adsorbing polymers allow independent variations in



their viscosity and free energy by changing the molecular weight or the concentration of the polymer, without modifying the surface properties of the films.

One way to describe the free energy of polymer solutions with spatially inhomogeneous concentration is using the two-fluid model of Brochard and DeGennes,<sup>59</sup> in which the polymer and solvent are modeled as two independently moving, superimposed fluids. Using this model we expect that the free energy will be controlled by the intermolecular interactions between the two opposing surfaces, and additionally have osmotic, confinement, and elastic effects as well:<sup>60</sup>

$$G = G_{\text{osm}} + G_{\text{el}} + G_{\text{u}} + G_{\text{vw}}, \quad (4)$$

where  $G_{\text{osm}}$  is the osmotic free energy (energy of mixing),  $G_{\text{el}}$  the elastic free energy which is negligible for the concentration and molecular weight range employed in our study,<sup>61,62</sup>  $G_{\text{u}}$  the kinetic free energy, which for creeping flow is also negligible, and  $G_{\text{vw}}$  the contribution of van der Waals interactions. In this expression the total free energy  $G$  depends on the film thickness, the drainage velocity, and the polymer concentration.

For polymer solutions, the osmotic contribution can be estimated as:<sup>63</sup>

$$G_{\text{osm}} \sim \chi^{-1}(\phi^2 + \xi^2 |\nabla\phi|^2), \quad (5)$$

where  $\phi$  is the volume fraction of the polymer,  $\chi$  is the susceptibility and  $\xi$  is the correlation length. The susceptibility, which is an indication of the solvent quality, depends non trivially on concentration, molecular weight and its distribution, and temperature.<sup>64</sup> Moreover,  $\chi$  includes a small entropic contribution that depends on polymer chain architecture and conformation.<sup>65</sup>

Based on eqn (5) and following Van Egmond and Fuller,<sup>66</sup> we define two dimensionless osmotic numbers that describe the static and dynamic contribution of osmotic stresses to the total pressure drop across the film. A *static* osmotic number is defined as:

$$\text{Os}_{\text{st}} = \frac{k_{\text{B}} T \phi}{R_{\text{H}}^3 \Delta P} \sim \frac{\Pi_{\text{osm}}(h)}{\Delta P} \quad (6)$$

where  $k_{\text{B}}$  is the Boltzmann constant and  $R_{\text{H}}$  is the hydrodynamic radius of the polymer. The static contribution of osmotic stresses has a similar contribution to the forces normal to the interfaces (and hence to the disjoining pressure), as the structural forces arising in particle- and micelle-containing films.<sup>67</sup> However, in polymer-solutions, such effects are more complicated given the deformability of polymer chains, and the existence of polymer-polymer and polymer-solvent interactions. In our experiments we studied polymers dissolved in a good solvent at concentrations close to  $c^*$ . We can thus assume that  $\chi$  remains constant during drainage and does not significantly differ among samples. Therefore, we can specifically interrogate the influence of  $R_{\text{H}}$  and  $\phi$  on the static osmotic stresses by changing the molecular weight and the concentration of the polymer.

Similarly, we define a dynamic osmotic number,  $\text{Os}_{\text{d}}$  that describes the relative importance of lateral osmotic stresses

because of concentration gradients with respect to the viscous ones arising because of drainage:

$$\text{Os}_{\text{d}} = \frac{k_{\text{B}} T \frac{\partial\phi}{\partial r}}{\xi^2 P_{\text{H}}(h, r)} \sim \frac{\Delta\Pi_{\text{osm}}}{\Delta P} \quad (7)$$

For concentrations close to the overlap concentration  $c^*$ , as those employed in our study, it can be assumed that  $\xi \approx R_{\text{H}}$ .<sup>68</sup> Although for monodisperse polymers differences in osmotic pressure  $\Delta\Pi_{\text{osm}}$  and thus osmotic stresses arise only because of concentration gradients in bulk, in solutions containing polydisperse polymers, like those studied here, differences in the molecular weight,  $\Delta M_{\text{w}}$ , also contribute to  $\Delta\Pi_{\text{osm}}$ . Therefore, as mentioned above for  $\text{Os}_{\text{st}}$ , by changing the size (or molecular weight) distribution and the initial concentration (which will also affect  $\partial\phi/\partial r$ ) we can tune the magnitude of the *lateral* osmotic stresses.

Using a virial expansion, the osmotic pressure of polymer solutions can be approximated as:<sup>69</sup>

$$\Pi_{\text{osm}} = \frac{\bar{R} T c}{M_{\text{n}}} \left( 1 + A_2^* \frac{M_{\text{n}} c}{2} \right)^2, \quad (8)$$

where  $c$  is the concentration,  $M_{\text{n}}$  is the number-average molecular weight,  $\bar{R}$  is the gas constant, and  $A_2^*$  is an effective virial coefficient (ESI<sup>†</sup>). Eqn (8) can qualitatively describe the increase in the osmotic pressure that is expected for polymer solutions above  $c^*$ .<sup>68</sup> As mentioned above, when concentration differences  $\Delta c$  are present, these will result in osmotic pressure differences  $\Delta\Pi_{\text{osm}}$ . Eqn (8) indicates that the magnitude of the lateral osmotic stresses between a depleted and a concentrated region will be different for a given  $\Delta c$  when the initial concentration is close to  $c^*$ . The calculated static and dynamic osmotic numbers can be found in the ESI.<sup>†</sup>

Finally, concentration gradients in bulk are expected to depend on the Péclet number:

$$\text{Pe} = \frac{v R_{\text{f}}}{D} \quad (9)$$

where  $R_{\text{f}}$  is the film's radius,  $v$  is the characteristic velocity of thinning, assumed to be approximately equal the rate of radial expansion  $dR_{\text{f}}/dt$  (ESI<sup>†</sup>), and  $D$  the diffusion coefficient.  $v$  is controlled by applied pressure. At very high  $\Delta P$ , the motion of polymer molecules will be convection-dominated with negligible concentration differences, and the outflow of the polymer solution will be described by the bulk viscosity.<sup>63</sup> On the other hand, at quasi-static conditions, *i.e.* for low  $\Delta P$ ,  $\partial\phi/\partial r \rightarrow 0$  as the motion of polymer molecules is diffusion-dominated. Therefore, the  $\text{Os}_{\text{d}}$  is expected to have a non-monotonic behaviour with the applied pressure drop, showing a maximum at a certain  $\Delta P$ . The static osmotic effects (normal direction) will be relevant to the low Pe regime, as the absence of concentration gradients ensures a homogeneous packing of polymer molecules in the film. Lateral dynamic osmotic stresses will occur at intermediate Pe, at which bulk diffusion can no longer suppress the concentration differences. Increasing the Pe even more, can be expected to result in the suppression of the



concentration gradients again. In the following sections we will study the effect of each dimensionless number on drainage and discuss in particular how the osmotic stresses can be tuned in such a way to promote film stability.

### 3 Materials and methods

#### 3.1 Materials

Three different grades of polyisobutylene (PIB) were used in this study. Oppanol B10SFN, and B50SFN were provided by BASF (Ludwigshafen, Germany), and P500 was purchased from Polysciences Inc. (Warrington, USA). The weight-average molecular weight and the polydispersity index of each polymer as determined by Gel Permeation Chromatography is shown in Table 1 (average of two measurements). The full molecular weight distribution (ESI<sup>†</sup>) was determined using an Agilent GPC 1260 Iso at 35 °C with a refractive index and a UV-VIS (254 nm) detector. THF was used as a solvent.

The critical molecular weight for the onset of entanglements is  $M_c = 13\,100\text{ g mol}^{-1}$ .<sup>70</sup> All grades are stabiliser-free and IR spectroscopy showed no presence of heteroatoms. *n*-Hexadecane was purchased from Acros Organics and has a purity of 99%. Hexadecane is a good solvent for PIB, with a Flory interaction parameter  $\chi_F$  in the range of 0.3–0.43.<sup>71</sup> In the case of B10SFN, four different solutions were prepared, with concentrations of 1, 5, 10, and 15 wt%. The solutions of the B10SFN act as the reference case for which lateral osmotic stresses are negligible. The concentrations of the two other PIB grades were chosen so that the bulk viscosities of the prepared solutions are equal to the 10 wt% B10SFN solution. We were thus able to study the effect that the osmotic stresses have on drainage, while keeping the hydrodynamic conditions constant. All solutions were filtered with a 0.2  $\mu\text{m}$  PTFE filter before usage.

For each polymer, the critical overlap concentrations was calculated following Graessley:<sup>72</sup>

$$c^* = \frac{3M_w}{4\pi R_G^3 N_A} \quad (10)$$

where  $M_w$  is the weight-average molecular weight,  $N_A$  is the Avogadro number, and  $R_G$  is the radius of gyration. The last is equal to  $R_G = \sqrt{[(b^2 C_\infty M_w)/(3M_u)]}$ , where  $b$  is the C–C bond length,  $C_\infty$  is the characteristic ratio, and  $M_u$  the molecular weight of the repeating unit.<sup>73</sup> For polyisobutylene  $b = 0.1505\text{ nm}$ ,<sup>74</sup> and  $C_\infty = 6.7$ .<sup>75</sup> Given the wide molecular weight distributions of the polymers in our study,  $c^*$  was estimated using the average of the weight- and number-average molecular weights (ESI<sup>†</sup>). The values of  $c^*$  shown in Table 1 can vary up to ~20% depending on the choice of the  $M_w$ , given the broad PDI

of the polymer. The calculated  $R_G$  (Table 1) results in  $R_G/R_H$  ratios in the range of 0.75–0.8, as expected for linear polymers dissolved in good solvents.<sup>76</sup>

#### 3.2 Methods

**3.2.1 Dynamic light scattering.** The hydrodynamic radius,  $R_H$  of the B10SFN and B50SFN grades in hexadecane was determined with dynamic light scattering (DLS) using an ALV CGS3 compact goniometer with 22 mW HeNe laser light source at 25.0 °C and an angle of 90°. The  $R_H$  of all polymers are shown in Table 1 (average of 3 measurements) and agree with previous results on polyisobutylene in good solvents.<sup>77</sup> For P500 (lowest  $M_w$ ),  $R_H$  is below 1 nm and for sub-nanometer particles the poor signal-to-noise ratio results in low correlation functions of ~0.1–0.2,<sup>78</sup> so the value reported here is only apparent with great uncertainty. No aggregation was found to occur in bulk even after 3 months after the first dissolution.

**3.2.2 Viscosimetry.** The bulk viscosity of all solutions was measured using an Anton Paar MCR302 rheometer with a double-gap Couette-cell geometry. The flow curves of all polymer solutions were Newtonian in a shear rate range of 10–100  $\text{s}^{-1}$  at 25 °C. At least three measurements were done for each solution. The measured viscosities are shown in Table 2.

**3.2.3 Tensiometry.** The surface tension of all samples was measured at room temperature using a Wilhelmy plate with a width of 19.62 mm and a thickness of 0.1 mm mounted on a balance (KSV Nima). Three measurements were conducted for each solution. The obtained values of the viscosity and surface tension are shown in Table 2. In general, when the surface tension of the pure polymer is higher than that of the solvent, then no surface adsorption is observed.<sup>79</sup> For our systems, polyisobutylene is not surface active, and in our range of molecular weights has a surface energy higher than hexadecane's.<sup>80,81</sup>

**3.2.4 Dynamic thin film balance.** The dynamic thin film balance (DTFB, Fig. 1a) technique consists of four main components: (i) an upright fixed-stage microscope, (ii) a pressure control system, (iii) an in-house fabricated aluminium pressure chamber, in which the (iv) bike-wheel microfluidic device is

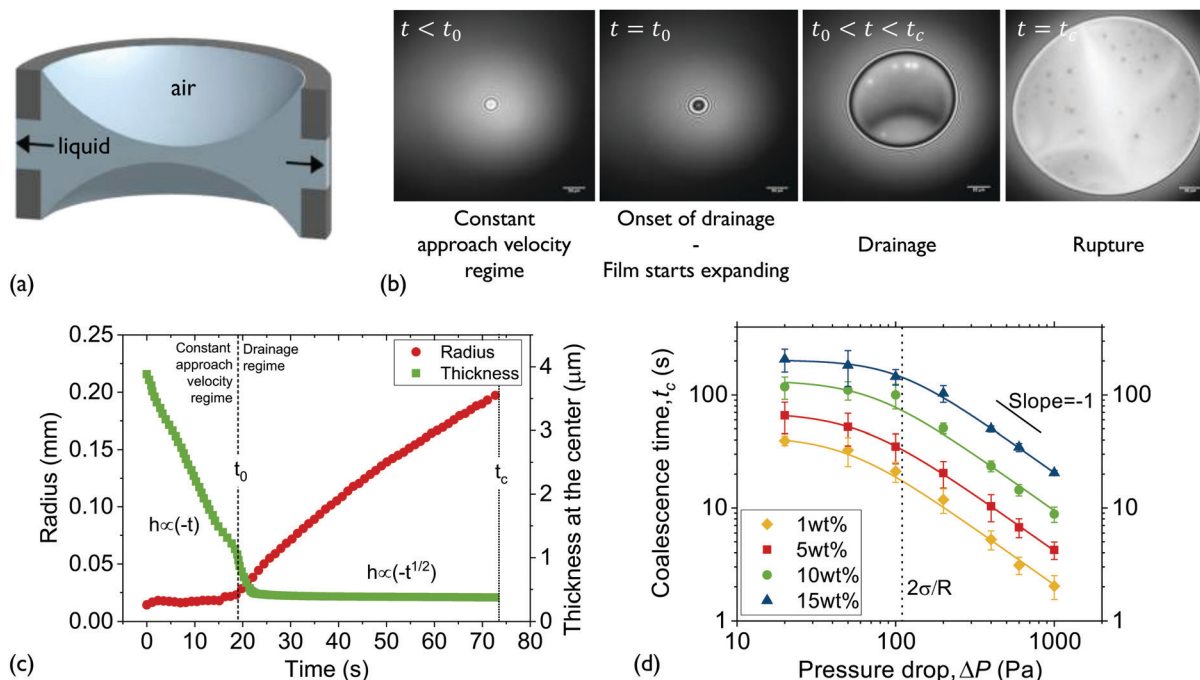
Table 2 Properties of the polyisobutylene-in-hexadecane solutions

Polymer (tradename)	Concentration wt%	Viscosity (mPa s)	Surface tension (mN m <sup>-1</sup> )
P500	52	19.8 ± 0.1	27.5 ± 0.1
B10SFN	1	3.5 ± 0.1	27.3 ± 0.1
	5	7.7 ± 0.1	27.3 ± 0.1
	10	18.3 ± 0.2	27.4 ± 0.1
	15	37.7 ± 0.3	27.4 ± 0.1
B50SFN	2.5	18.9 ± 0.5	27.4 ± 0.1
<i>n</i> -Hexadecane	0	3.1 ± 0.1 <sup>82,83</sup>	27.4 ± 0.1

Table 1 Properties of the polyisobutylene grades

Polymer (tradename)	Weight-average molecular weight, $M_w$ (g mol <sup>-1</sup> )	Polydispersity index, PDI (–)	$R_H$ (nm)	$R_G$ (nm)	$c^*$ (wt%)
P500	1273	2.1	0.83 ± 0.06	1.1	62.2
B10SFN	57 635	2.8	5.5 ± 0.1	7.2	9.7
B50SFN	327 079	1.5	14.3 ± 0.2	17.2	3.7





**Fig. 1** Experimental setup and experimental approach: (a) a thin liquid film is formed in the hole of the bikewheel (cross section shown). Upon application of an extra  $\Delta P$  at the air-side results in liquid being pushed out through the side-channels. The presence of multiple side-channels allows the symmetric drainage of films of relatively high viscosities. (b) Interferometric images during the various thinning regimes. The coalescence time is defined as the interval between the onset of film expansion ( $t = t_0$ ) and film rupture ( $t = t_c$ ). (c) The expansion of the film and its thinning as a function of time. The definitions of the various regimes and times during a drainage experiment are also shown. (d) The coalescence times of solutions of medium  $M_w$  PIB B10SFN at four different concentrations as a function of pressure. Adapted from ref. 57.

placed. A sketch of the setup can be found in ref. 49. The bike-wheel chip is a custom-designed microfluidic device based on the initial design of Cascão-Pereira *et al.*<sup>84</sup> It is fabricated using photolithography on borosilicate glass (by Micronit Microfluidics). It consists of: (i) a diamond-drilled hole with a diameter of 1 mm and a thickness of 400  $\mu\text{m}$ , (ii) 25 channels (width of 45  $\mu\text{m}$  and depth of 20  $\mu\text{m}$ ) connected to the hole, all leading to a circular channel of larger dimensions. The chip is glued onto a titanium holder using two-component epoxy. To ensure that the contact line between the liquid and the glass is pinned, the bike-wheel's outer surface is first hydrophilised by immersing it in a saturated NaOH ethanol solution and leaving it under microsonication for 20 min, and then hydrophobised with octadecyltrichlorosilane. More details regarding the bike-wheel microfluidic device and its fabrication can be found elsewhere.<sup>85</sup>

The pressure inside the chamber is controlled by an Elveflow MK3+ piezoelectric pressure control system which has a resolution of 1 Pa and a maximum pressure of 20 kPa. The response time was independently measured by coupling the control system to a Baratron 120AD differential pressure transducer, and was found to be  $O(10^{-2}$  s). The application of the desired pressure step was followed by an initial pressure overshoot (of a maximum relative magnitude of  $\sim 20\%$  for low  $\Delta P$ ) that settled after  $O(10^{-1}$  s). The control system is connected to the pressure chamber by rigid PTFE tubing with an inner diameter of 0.1 mm.

The film visualisation is done with a Nikon Eclipse FN1 fixed-stage upright microscope (to minimise vibrations) and a  $10\times$  long working distance objective with a numerical aperture of 0.30. The entire setup being mounted onto an active noise cancelling table. The film is monitored by a Hamamatsu ORCA-Flash4.0 CMOS camera. A monochromatic wavelength of 508 nm was used for imaging in reflection. A sequence of images is saved (with a maximum of 10 ms temporal resolution) and is then converted to thickness using the Sheludko equation:<sup>1</sup>

$$h_{\text{eq}} = \left( \frac{\lambda}{2\pi n_f} \right) \left[ m\pi \pm \arcsin \sqrt{\frac{\Delta}{1 + 4Q(1 - \Delta)/(1 - Q)^2}} \right], \quad (11)$$

where  $h_{\text{eq}}$  is the equivalent thickness,  $\lambda$  is the wavelength of the monochromatic light,  $n_f = 1.434$ <sup>86</sup> and  $n_c = 1$  are the refractive indices of the film (hexadecane) and continuous phase (air), respectively, and  $m$  is the order of interference.  $Q = [(n_f - n_c)/(n_f + n_c)]^2$  and  $\Delta = (I - I_{\text{min}})/(I_{\text{max}} - I_{\text{min}})$ .  $I$  is the intensity of a pixel of the image, and  $I_{\text{min}}$  and  $I_{\text{max}}$  the minimum and maximum intensities measured in the film during its drainage, equal to the values corresponding to the destructive and constructive interference of light. For planar films, this methodology results in a thickness resolution of  $\pm 2$  nm, with the error increasing as the film becomes more dimpled. The thickness can be monitored in the whole film area, allowing us to obtain the 3D thickness profiles of the films as done in



ref. 87 and 88. The already negligible effect of evaporation was further minimised by adding excess solution in the pressure chamber.

The experimental procedure and an example of the resulting evolution of the radius and the thickness of a 5 wt% polymer film are shown in Fig. 1c for a 50 Pa pressure drop. Initially a thick film is created and its equilibrium pressure is determined by applying a pressure equal to  $P_{c,i}$  at the gas phase. The equilibrium point can be easily determined by varying the pressure in steps of 1 Pa until the first interference fringes that appear when the thickness of the TLF is in the order of a few  $\mu\text{m}$  are stable. More information regarding the experimental method and the involved pressures can be found in ref. 57. Subsequently, the pressure inside the film is lowered using pressure drops,  $\Delta P$ , in the range of 20 to 1000 Pa. When the pressure drop is applied, the film begins to drain at a constant speed. This corresponds to a constant approach velocity regime, where  $h \sim (-t)$ . At a thickness of  $O(10^2 \text{ nm})$  the hydrodynamic pressure inside the film builds up, causing its expansion. This initial thickness depends on the applied pressure step.<sup>89,90</sup> The pressure balance in the thin film is given by eqn (2).

The onset of film's expansion (when the first interference fringes are observed) is identified as the beginning of drainage,  $t_0$  (Fig. 1b and c). In the drainage regime,  $h \sim (-t^{0.5})$ , in agreement to the integrated form of the Reynolds equation (eqn (1)) (Fig. 1c and ESI<sup>†</sup>). As these polymer films are thermodynamically unstable, the end of drainage is set by the rupture of the film (Fig. 1b and c). A similar definition of coalescence time has been used by Kannan *et al.*<sup>91</sup> At least 5 measurements were done for each combination of  $\Delta P$  and polymer concentration for the B10SFN solutions, while at least 3 measurements were done for the P500 and B50SFN solutions.

## 4 Results and discussion

The simplest observable from the DTFB experiments is the coalescence time as defined in Section 3.2.4 for a given applied pressure drop (and hence  $Ca$ ). In this section we will discuss (i) how the imposed  $\Delta P$  affects the dynamics of films of different concentrations when osmotic stresses are negligible, and (ii) the effect of the polymer molecular weight and (iii) molecular weight distribution on the magnitude of osmotic stresses and the resulting film dynamics.

### 4.1 Drainage dynamics of polymer solution films

**4.1.1 Effect of the Capillary number,  $Ca$ .** First we study the effect of applied pressure on solutions of B10SFN at different polymer concentrations. By keeping the  $M_w$  of the dissolved polymer constant, we are able to specifically interrogate the effect of bulk viscosity on film drainage by changing concentration. The coalescence times,  $t_c$ , of four solutions of the medium  $M_w$  polymer as a function of applied  $\Delta P$  are shown in Fig. 1d.

For this  $M_w$ , the same trend is observed for all concentrations. A change in the slope of the coalescence time is observed at a pressure of the same magnitude as the Laplace pressure due to the film's curvature in the bikewheel ( $2\sigma/R$ ). This critical pressure marks the gradual transition from a regime where drainage is slow<sup>92</sup> to a hydrodynamically-dominated regime in which the coalescence time is inversely proportional to the applied pressure drop.<sup>57</sup> The differences between the coalescence times of the various solutions were found to be proportional to their bulk viscosity, as expected from eqn (1). More details on drainage, and specifically on the temporal evolution of the thickness, radius, and volume of the films for the employed range of  $Ca$  can be found in the ESI.<sup>†</sup>

**4.1.2 Influence of osmotic stresses at low  $Ca$ .** The relatively long drainage times observed despite the expected absence of surface stresses, are a first indication that static osmotic stresses may play a role. For example, stress-free films of pure water, with a viscosity not much smaller than the 1 wt% solution studied here, rupture within  $\sim \text{ms}$ <sup>93</sup> compared to the tens of seconds here.

Although the coalescence times of all solutions were proportional to the viscosity (within experimental accuracy), the microscopically observed behaviour was quite complex. The various patterns that were observed during drainage of the medium  $M_w$  solutions are shown in Fig. 2. The probability for asymmetric drainage accompanied by flow instabilities, as well as the type of the latter, depended non-trivially on polymer concentration and the applied  $Ca$ .

At low  $Ca$ , small thickness corrugations and dark spots were observed, in agreement with the results of Nikolov and Wasan<sup>18</sup> on films containing nanoparticles. In the latter case, the occurrence of thickness fluctuations was observed in the regions in the film where particles are present. The thickness of the dark spots at low  $\Delta P$  just before rupture is  $30 \pm 9 \text{ nm}$ . The thickness of these dark domains did not depend on the  $R_H$  of the polymer, with the films of P500 (with  $R_H \simeq 1 \text{ nm}$ ) having similar minimum thickness values (ESI<sup>†</sup>). The critical thickness measured just before rupture is always located in such a dark spot, and can be predicted by simple rupture models that neglect osmotic effects.<sup>57</sup> Therefore, this suggests that these regions contain no polymer molecules, in agreement with earlier results on nanoparticle-containing films.<sup>94</sup>

Interestingly, at the highest concentration some films showed thickness steps in the radial direction, observed as abrupt grayscale variations in the 15 wt% films at  $\Delta P = 20 \text{ Pa}$  (Fig. 2a). The obtained thickness profile (ESI<sup>†</sup>), suggests that a lateral organisation exists within the film. This effect, which has been predicted by Klapp *et al.*<sup>95</sup> and reported for wetting films,<sup>96</sup> has not been previously observed in freestanding films with deformable surfaces.

**4.1.3 Influence of osmotic stresses at medium and high  $Ca$**   
*Effect of concentration.* Upon increasing the applied pressure, the behaviour of the films depended significantly on concentration. The drainage could proceed either axisymmetrically, with the formation of a dimple at the centre of the film<sup>97</sup> or asymmetrically, accompanied by dimple wash-outs which in



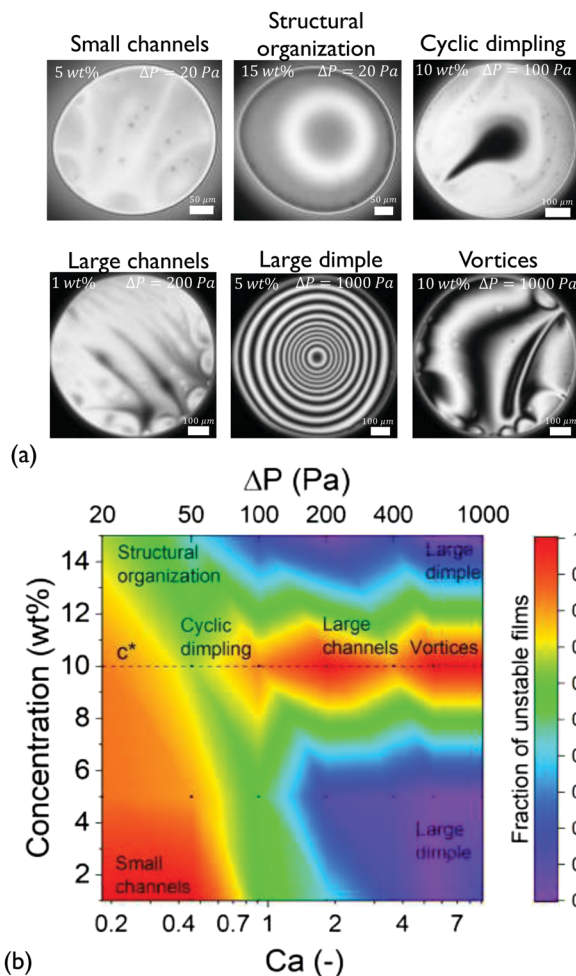


Fig. 2 Thin film dynamics of the medium  $M_w$  solutions: (a) microinterferometric images of selected snapshots highlighting characteristic patterns. A variation of drainage type with polymer concentration and applied  $\Delta P$  was observed. (b) State diagram describing the propensity of films of different concentrations to show asymmetric drainage. Films become distinctly unstable at  $c^*$ . The black points correspond to conditions at which detailed experimental observations were performed.

certain cases were followed by the dimple reforming,<sup>41</sup> the formation of channels of higher thickness,<sup>37</sup> and even the formation of vortices close to the edge of the film (Fig. 2a). The observed drainage modes depend non-trivially on the concentration of the dissolved polymer and the applied Ca. The cause of these instabilities are lateral osmotic stresses that will be discussed further below.

Because of the stochastic character of the asymmetric drainage, we plot the fraction of films that were unstable (*i.e.* not showing an axisymmetric dimple) as a function of Ca in a state diagram (Fig. 2b). In general, capillarity will tend to stabilise the film's shape. The probability for symmetric drainage hence increases with Ca, following a normal cumulative distribution function (ESI†). The exact prediction of the conditions at which instabilities occur would require a linear stability analysis, similar to that conducted for instabilities caused by Marangoni stresses.<sup>98,99</sup> Organising the observed instabilities in a state

diagram can provide some insight on the involved processes. For  $c < c^*$  (1 and 5 wt%) the behaviour of the films was quite similar. Increasing Ca results in a gradual stabilisation of the dimple and a transition from slightly asymmetric drainage observed at low Ca to a fully axisymmetric drainage. The origin of the unstable regime at low Ca is related to the weak stabilising effect of capillary forces. At this regime small thickness corrugations are observed despite the relatively small expected magnitude of lateral osmotic stresses.

The dimple size increases with the applied Ca and the thickness at the centre scales as  $h_{\text{cent}} \propto \text{Ca}$  (ESI†). The linear dependence is slightly lower than the  $3/2$  exponent predicted by simulations,<sup>100,101</sup> which could be attributed to the complexity of the phenomena taking place during the drainage of the polymer solutions and to the standard deviation of the measurements. The same gradual transition to the dimpled configuration was also observed for the 15 wt% film, with the exception of the lateral structural organisation at low Ca that was described above. Apart from the stabilising effect of Ca, the re-stabilisation of the film's dimpled shape with increasing  $\Delta P$  is in agreement with the Pe-dependent transport of polymer molecules. As discussed in Section 2, when the thinning rate of the film is high, the transport of the polymer molecules becomes convection-dominated. Such large drag forces are known to equalise the relative velocities of the polymer and solvent,<sup>63</sup> thus minimising any concentration and osmotic pressure differences.

*Propensity for instabilities close to  $c^*$ .* The drainage sequences of the films with a concentration close to the critical concentration ( $c = 10 \text{ wt}\% \simeq c^*$ ) show highly unstable, asymmetric patterns for all values of Ca (Fig. 2b and ESI†). These instabilities actually become more pronounced with Ca, changing gradually from small channels, over cyclic dimples, to large channels and vortices.

This propensity for instabilities close to  $c^*$  is an indication that lateral osmotic stresses develop in the films. At  $c^*$ , as we move from the dilute to the semi-dilute regime, polymer-polymer interactions result in a change in the concentration dependence of osmotic pressure from a linear to a non-linear one.<sup>64,68</sup> Hence, when the initial concentration is close to  $c^*$ , as in the case of the 10 wt% solution, an induced concentration difference results in a strong pressure imbalance between the concentrated and the depleted region, with the polymer molecules interacting only in the former. Thus, the resulting unequal osmotic stresses will cause an inhomogeneous bulk stress distribution in the film, destabilising the outflow of the liquid.

The occurrence of these instabilities did not have a significant effect on the coalescence time (within the experimental limits of our technique). However, the volume of the film just before rupture was more strongly affected (ESI†). The 10 wt% solution, which is the most prone to asymmetric drainage, had the lowest estimated volume at rupture. This is an indication that the instabilities mentioned above have a strong effect on the liquid entrained inside the film. The dimple wash-outs and



the formation of channels can be expected to accelerate the outflow of liquid.<sup>102</sup> On the other hand, the overall enhanced viscous dissipation in the films due to the complex flow may slow down drainage globally. The net effect on coalescence time is still limited.

**Characteristic timescale of instabilities.** To prove that lateral osmotic stresses cause the instabilities, the characteristic timescales of the latter were determined from the time evolution of the thickness fluctuations, as in Fig. 3a. The local thinning velocity is obtained by differentiation  $dh_{\text{cent}}/dt$  (Fig. 3b). The strong thickness peaks are caused by the dimple wash-out events, while the small peaks are caused by smaller scale instabilities, such as channels (Fig. 3c). The period for all instabilities,  $T_f$ , is taken to be equal to the time between two consecutive local minima, which correspond to the onset and end of each instability, respectively. Fig. 4 shows that  $T_f$  for different concentrations collapse onto a master curve and the determining variable is  $Os_d$ , as defined in eqn (7). As the actual concentration difference in the film is unknown, we assumed that  $\Delta c \sim c$  and calculated the expected  $\Delta\Pi_{\text{osm}}$  from eqn (8).

Fig. 4 shows how the period of fluctuations is constant for low  $Os_d$  and then increases with  $T_f \propto \sqrt{Os_d}$ . This can be rationalized by considering the relative magnitudes of hydrodynamic ( $\Delta P$ ) and osmotic pressure differences ( $\Delta\Pi_{\text{osm}}$ ). We can assume that  $\Delta P \propto \Delta c$ , as in ref. 98. Concerning  $\Delta\Pi_{\text{osm}}$ , for small values of  $\Delta c$ , the second order term in eqn (8) can be neglected and the differences in osmotic pressure are also

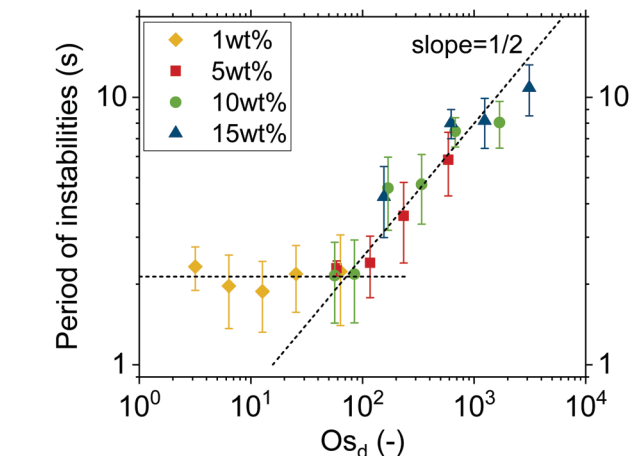


Fig. 4 Dynamic  $Os_d$  scaling: a master-curve is obtained for all concentrations of the medium  $M_w$  polymer solutions when plotting the characteristic timescale of the instabilities versus  $Os_d$ . The two regimes are related to differences in the magnitude of  $\Delta c$ .

simply proportional to the applied pressure drop. As both  $\Delta P$  and  $\Delta\Pi_{\text{osm}}$  are proportional to the applied pressure drop,  $T_f$  is constant. In contrast, for higher  $\Delta c$ , the  $c^2$  term in eqn (8) can no longer be neglected, and the relation between  $\Delta\Pi_{\text{osm}}$  and  $\Delta P$  becomes non-linear. A  $T_f \propto \sqrt{Os_d}$  dependence, indicative of the occurrence of lateral osmotic forces, is observed experimentally over the experimentally accessible range in Fig. 4. For very high  $\Delta c$ , at which the  $c^2$  term in eqn (8) becomes dominant, one

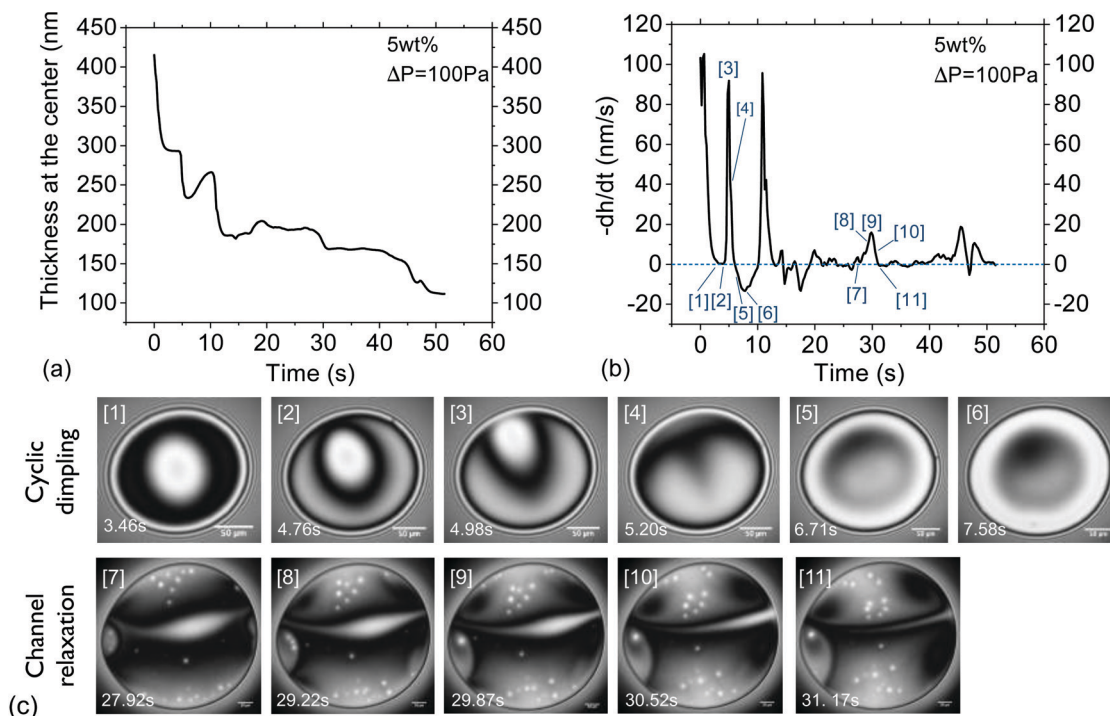


Fig. 3 Characteristic timescale of instabilities of the medium  $M_w$  solutions: (a) The drainage curve of a 5 wt% solution at  $\Delta P = 100$  Pa. (b) The corresponding thinning velocity. The temporal evolution of the two instabilities is shown with numbers. (c) Microinterferometry images of the same film, showing two instabilities, namely cyclic dimple formation and channel relaxation. The numbers of each image correspond to distinct times of the thinning velocity curve shown above.





would expect that  $T_f$  becomes proportional to  $Os_d$ . The period of instabilities of the low  $M_w$  polymer solution (see ESI†) studied at  $c = 52$  wt%, indicates that a gradual transition to a linear dependency might indeed occur for higher values of  $Os_d$ .

Concluding, there are so far three different observations that support the argument that the dynamics of the polymer solution films are controlled by osmotic effects. First, the long coalescence times of  $O(10^0-10^2)$  s, which are observed despite the absence of surface stresses. Second, the occurrence of strong instabilities during the drainage of films, in particular for those solutions with concentrations close to  $c^*$ . Finally, the fact that the time scale of the instabilities, as characterized by  $T_f$ , is controlled by  $Os_d$  (Fig. 4). It can be noted that the procedure of determining the period of the instabilities could potentially be applied to surfactant micellar-containing foam films as well, thus enabling the separation of the osmotic effects from other contributions like Marangoni<sup>103</sup> or even viscoelastic stresses.<sup>104</sup>

Despite the existence of osmotic stresses, it is evident that increasing just the concentration of the polymer in the solution is not a powerful method to exploit such effects. In the investigated concentration range, the coalescence times of all solutions were found to be proportional to the viscosity (Fig. 1d). Thus, the lateral dynamic osmotic stresses ( $Os_d$ ), and the increase in the normal  $Os_{st}$  because of the increased concentration (calculated to be of  $O(10)$ , ESI†) had only a small to negligible effect on the lifetime of the films. As it will be discussed in the next sections, changing the molecular weight and the molecular weight distribution of the dissolved polymer provide more effective means to further tune film dynamics.

#### 4.2 Controlling the lifetime of thin films of polymer solutions

There are two ways by which osmotic stresses can affect the lifetime of the films. One way would be through  $Os_{st}$ , which controls the static osmotic stresses that act normal to the film's surface and influence the disjoining pressure. The second way is more subtle, through  $Os_d$ , which controls the magnitude of

the osmotic stresses that act in the direction of flow, *i.e.* laterally.

**4.2.1 Compositional control over static osmotic stresses,  $Os_{st}$ .** To assess the effect of the molecular weight on film dynamics we investigated solutions of three different polymer grades with  $M_w$  equal to 1.3, 57.6, and 327.1 kg mol<sup>-1</sup>. The concentrations of the dissolved polymer were chosen in a way such to achieve the same bulk viscosity for all solutions, allowing us to study all films at the same hydrodynamic conditions. Concentrations close to  $c^*$  were employed in order to achieve the maximum possible  $\Delta\Pi_{osm}$ , as discussed in Section 2. Any small differences on the distance from  $c^*$  (Table 1) can be attributed to the different polydispersity of the polymers. The solutions also have the same surface tension (Table 2).

The coalescence times as a function of  $\Delta P$  are shown in Fig. 5. As in Fig. 1d two distinct regimes are observed, separated at approximately  $2\sigma/R$ . The significant differences in drainage times at low  $\Delta P$  are directly related to the contribution of  $Os_{st}$  to the disjoining pressure. The calculated  $Os_{st}$  (eqn (6) and (8)) of the various solutions were found to be orders of magnitude different (ESI†). At  $\Delta P = 50$  Pa, the  $Os_{st}$  of the low  $M_w$  can be estimated to be  $O(10^4)$ , while for the medium  $M_w$  was of  $O(10^1)$ , and for the high  $M_w$  was of  $O(10^{-1})$ . As a result the coalescence times of the various solutions, differ at the low  $\Delta P$  regime by almost an order of magnitude. Experimentally, a relation  $t_c \propto M_n^{-1/3}$  was observed.

This increased stability with reducing the size of the confined species has also been reported for micelles, nanoparticles<sup>26</sup> and polyelectrolytes.<sup>28</sup> However, it is usually observed as an increase in the amplitude of the structural oscillatory forces. The magnitude of the  $Os_{st}$  might depend on the polydispersity<sup>18,26,29,30,32,39,40,105</sup> and on the deformability of the confined polymer.<sup>27,33</sup> However, studying these effects would require (i) the addition of polymers of the same  $M_n$  and different PDI, or (ii) the addition of polymers of the same  $M_n$  but different persistence lengths, and are thus beyond the scope of this study.

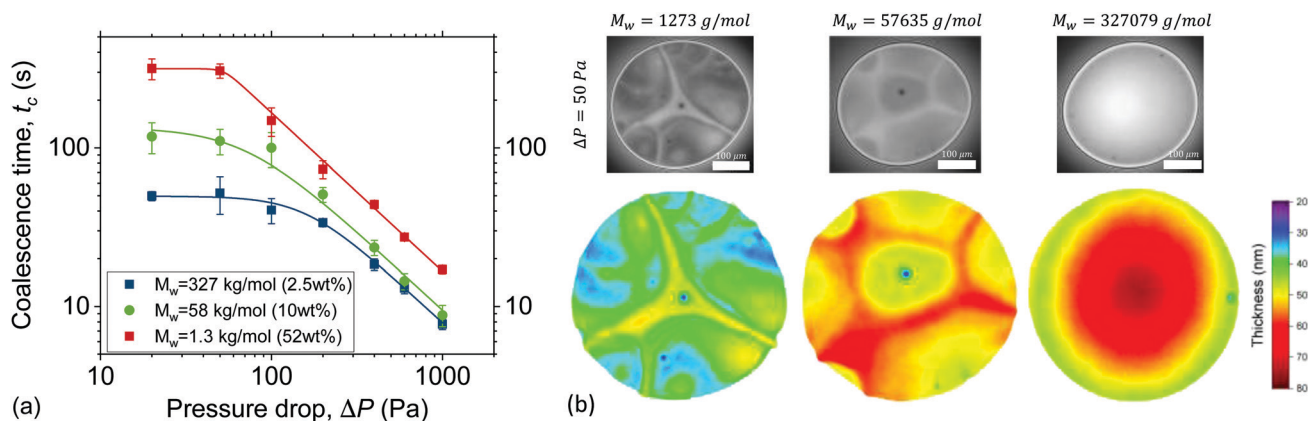


Fig. 5 Effect of molecular weight on the coalescence time and drainage dynamics for equal viscosity solutions: (a) the coalescence times for different  $M_w$  as a function of  $\Delta P$ . (b) Microinterferometry images of films of the same solutions just before rupture for  $\Delta P = 50$  Pa. The corresponding 3D thickness maps are shown below. The average thickness increases with  $M_w$ , while the radius of the film remains constant.



The contribution of static osmotic stresses can be inferred from the interferometry images of the films and their corresponding 3D thickness maps (Fig. 5b). The average thickness at rupture is found to differ, as expected based eqn (2).<sup>89</sup> According to the 3D thickness maps, the average thickness at rupture of the films at  $\Delta P = 50$  Pa increases with  $M_w$ . This means that the static osmotic contribution is higher for the polymer with the smallest  $M_w$ , as it is able to counteract the attractive vdW disjoining pressure down to thicknesses of  $\sim 30$  nm. In contrast, the  $57.6 \text{ kg mol}^{-1}$  and the  $327.1 \text{ kg mol}^{-1}$  polymer films rupture when their average thickness is  $\sim 50$  nm and  $\sim 60$  nm, respectively. The absence of pronounced osmotic effects in the case of the highest  $M_w$  polymer resulted also in the complete absence of thickness corrugations. The differences in coalescence times reduces as  $\Delta P$  increases (Fig. 5a). Previous studies with a bubble-probe AFM on air bubbles separated by polyelectrolyte-containing aqueous films also report an attenuation of the structural forces as hydrodynamics become dominant.<sup>28,29</sup>

As mentioned above, the films of the highest  $M_w$  showed no thickness corrugations and a much lower amount of dark spots (Fig. 5b), indicating that osmotic contributions are much smaller than the Laplace pressures. Interestingly, these films also showed a very small dimple or no dimple at all even at the highest applied  $\Delta P$  (ESI†). The absence of a dimple at high nominal  $Ca$  is in general considered an indication of surface stress-free drainage.<sup>106,107</sup> Films with Marangoni stresses can be planar, when axisymmetry in drainage is not maintained,<sup>10,16,108</sup> but they always exhibit some thickness corrugations, which is not the case for the high  $M_w$  polymer solutions studied here. A comparison with simulations could provide definite conclusions on the magnitude of surface stresses in the draining films. Such polymer solutions with negligible lateral but finite normal osmotic stresses are nice model systems to study the effect of surface stresses on drainage, given that despite their relatively low viscosity they exhibit long coalescence times, orders of magnitude higher than those of stress-free films of *e.g.* pure water, which are of  $O(10^0-10^1)$  ms.<sup>93</sup>

Despite the complexity of film stabilisation using static osmotic pressure  $Os_{st}$ , it is clear that for a given viscosity, monodisperse, low  $M_w$  polymers result in longer film lifetimes. This should be relevant for the design of multiphase materials containing non-adsorbing species, such as polyelectrolyte foams<sup>109</sup> and polymer-containing emulsions.<sup>47</sup> The higher stability of films containing species of small size is relevant for a wide range of (typically relevant)  $Ca$  numbers (Fig. 5a).

**4.2.2 Compositional control over dynamic osmotic stresses,  $Os_d$ .** The final way by which osmotic effects could potentially be tuned to control film dynamics, is through the molecular weight distribution of the dissolved polymer. All the polymer grades that have been employed in this study are relatively polydisperse, with PDIs in the range of 1.5–2.8. However, a clean strategy to change  $Os_d$  while keeping  $Os_{st}$  constant is to use bimodal solutions. Therefore, we mixed the solutions of the medium and the low  $M_w$  polymers of Fig. 5 at a

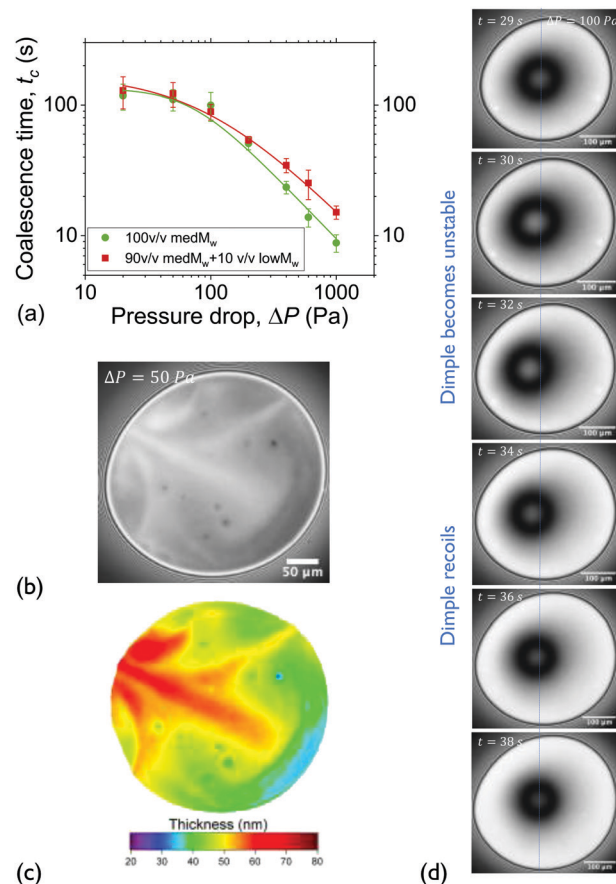


Fig. 6 Effect of the molecular weight distribution on the coalescence times and drainage dynamics: (a) the coalescence times as a function of  $\Delta P$  for two polymer films with different PDI. (b) Microinterferometry image of the bimodal film just before rupture at  $\Delta P = 50$  Pa. (c) The corresponding 3D thickness map. (d) The evolution of "dimple recoil". The dimple moves towards the Plateau border until  $t = 32$  s and then moves back towards the film's center.

90 : 10 v/v% ratio. As previously, the surface tension and bulk viscosity of the reference medium  $M_w$  solution and its bimodal solution are also made to be equal. The addition of such a small fraction of the low  $M_w$  polymer ensures that the normal static osmotic contribution does not vary a lot and hence any change in film dynamics is solely related to lateral dynamic effects. The experimentally obtained coalescence times of the bimodal solutions are shown together with the mono-component medium  $M_w$  polymer solution for a wide range of  $\Delta P$  in Fig. 6a. As expected the coalescence times of the two solutions at low  $\Delta P$  are the equal. This confirms that the addition of the low  $M_w$  polymer did not affect the  $Os_{st}$ , which could be explained by the partition of smaller molecules within the excluded volume of larger ones in the film.<sup>28</sup>

However, as of  $\Delta P \geq 400$  Pa the solutions with the bimodal  $M_w$  distribution started showing significantly slower coalescence, which for the highest pressure steps applied were approximately double the  $t_c$  of the pure solution. For these dynamics effects to occur,  $Pe$  should be relatively high to induce concentration differences and overcome bulk diffusion. The  $Pe$



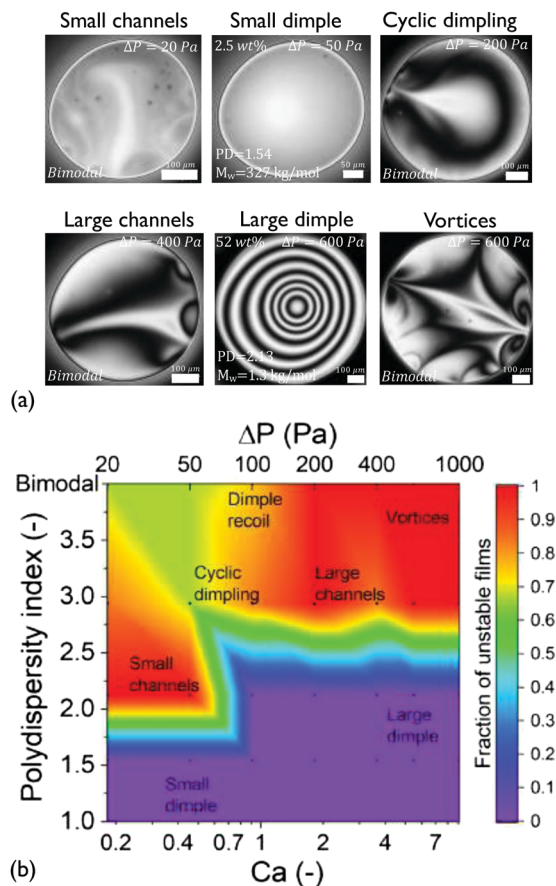


Fig. 7 Thin film dynamics influenced by dynamic osmotic stresses: (a) microinterferometric images of polymer films of different PDIs. (b) State diagram describing the propensity for asymmetric drainage as a function of  $Ca$  and  $\Delta P$  for films containing polymer of different PDIs. The black dots indicate the experimentally measured points. The bimodal mixture is separately shown at the top of the  $y$ -axis.

number in our experiments can be estimated from eqn (9) using our experimental data for the film expansion rate and the radius,<sup>49</sup> and a diffusion constant of  $10.4 \mu\text{m}^2 \text{s}^{-1}$  obtained by DLS for the medium  $M_w$  polymer. A  $Pe$  number of  $O(10^2\text{--}10^3)$  was calculated for  $\Delta P \geq 400$  Pa. Apart from the larger  $\Delta M_w$  that can be attained if bimodal solutions exhibit concentration gradients, the dynamic stabilisation could also be facilitated by the fact that larger molecules experience a stronger drag force during drainage, which could potentially result in a more pronounced depletion from the film.<sup>29,110</sup> Another estimate can be done regarding the magnitude of the concentration differences inside the film. Assuming that thickness corrugations will develop when  $\Delta\Pi_{\text{osm}} \sim 2\sigma/R$ ,<sup>37</sup> a  $\Delta c \sim 10\%$  can be estimated from eqn (8) for the solution of the medium  $M_w$  polymer (ESI<sup>†</sup>).

The addition of the small amount of low  $M_w$  fraction resulted in an intensification of the flow instabilities. Vortices were observed even at a very low  $\Delta P$  (Fig. 6b) and their occurrence strengthened with applied pressure. Moreover another flow phenomenon was observed, which has been previously termed as “dimple recoil”<sup>20</sup> (Fig. 6c and Movie).

At one point during drainage the dimple became unstable and moved towards the Plateau border ( $t = 29$  s). Then, after approximately a few seconds the dimple started recoiling and restabilised at the film’s centre. This effect was observed only at  $\Delta P = 100$  Pa  $\approx 2\sigma/R$ . The occurrence of this instability only at this specific  $\Delta P$  is probably related to the fact that at  $Ca \approx 1$  lateral osmotic stresses might locally be strong enough to destabilise the dimple, without however causing its complete collapse before hydrodynamics restabilise the flow. A similar “dimple recoil” was also recently observed in films of worm-like micelles and was attributed to bulk elasticity.<sup>20</sup> However, strong structural forces are known to develop in films with worm-like micelles,<sup>25</sup> which means that these systems also have a potential for exhibiting dynamic osmotic effects. Therefore, the origin of this effect might not necessarily be the elasticity of the film.

Overall, the polydispersity in the  $M_w$  of the dissolved polymer had a strong effect on the observed film dynamics (Fig. 7a). In the state diagram of Fig. 7b we plot the fraction of unstable films as a function of the polydispersity index of the dissolved polymer for different employed  $Ca$  numbers. The three polymers of this study are considered together with the bimodal mixture, which is independently reported on top of the polydispersity axis. It is clear that low polydispersities favour symmetric drainage and the formation of a stable dimple. In contrast, the solutions of the more polydisperse polymers exhibited mostly asymmetric drainage. For the bimodal solution, the occurrence of large channels, vortices, and dimple recoils resulted in liquid recirculation within the films, doubling their lifetime.

The increase in the lifetime of films containing polymer mixtures takes place at relatively high  $Ca$  numbers and, as such, may have gone unnoticed in earlier work. The occurrence of these dynamic osmotic stresses could have significant implications for various technological applications. For example, it is common industrial practice in lubricant technology to mix different lubricant grades to attain a certain desired viscosity.<sup>46</sup> However, both lubricants and fuels typically contain polymer additives as viscosity modifiers.<sup>111</sup> Furthermore, wide polymer molecular weight distributions are also expected to develop over time in mechanosensitive formulations.<sup>112</sup> Our results suggest that such multicomponent systems are more prone to foaming, the latter being undesirable in lubricants<sup>46</sup> and fuels.<sup>113</sup>

## 5 Conclusions

The dynamics of freestanding liquid films containing dilute and semi dilute polymer solutions were studied using a dynamic thin film balance. The effect of polymer concentration, molecular weight, and molecular weight polydispersity were examined over a wide range of capillary numbers. The viscosity of the solutions was kept constant, while the  $M_w$  and the concentration of the polymers was changed. The thinning dynamics were found to be influenced by the static osmotic



pressure that is exerted by the confined polymer molecules, in line with earlier work.<sup>26</sup>

However, osmotic stresses acted not only normal to the film surface but also laterally. At sufficiently high drainage rates, the flow induced concentration differences give rise to osmotic stresses. The drainage of the films was found to proceed either symmetrically, with the characteristic dimple formation<sup>97</sup> or asymmetrically, with thickness corrugations, channels, vortices and other flow instabilities. The type of drainage depends non-trivially on the applied pressure drop, the concentration, the molecular weight and the polydispersity of the polymer. The characteristic timescale for the evolution of the observed instabilities was found to scale with a dynamic osmotic number, which relates the magnitude of lateral osmotic stresses to the hydrodynamic ones.

It was shown that at constant bulk viscosity, the films containing the polymer with the lowest  $M_w$  were the most stable, exhibiting coalescence times as high as 300 s despite the absence of surface stresses. In contrast, the high  $M_w$  polymer films drained symmetrically and their behaviour was in line with the thinning of films with stress-free surfaces.<sup>106,107</sup> Mixing polymer grades with different  $M_w$  resulted in an intensification of the lateral osmotic pressure gradients that doubled the coalescence time in the high Ca regime. Channels, vortices, cyclic dimples and dimple recoils were observed, showing the richness of the dynamics of such films consisting of “simple” polymer solutions. These results provide new insights in the stabilisation mechanisms of films draining at realistically high Ca. The results presented contribute to a better understanding and potential optimisation of the formulation products, such as foams, emulsions, and lubricants, in which polymers are typically added as viscosity modifiers.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

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