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## Dynamical time scales of friction dynamics in active microrheology of a model glass

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Owing to the local/heterogeneous structures in supercooled liquids, after several decades of research, it is now clear that supercooled liquids are structurally different from their conventional liquid counterparts. Accordingly, an approach based on a local probe should provide a better understanding about the local mechanical properties as well as heterogeneous structures. Recently, the superiority of active microrheology over global rheology has been demonstrated [Yu *et al.*, *Sci. Adv.*, 2020, **6**, 8766]. Here, we elaborate this new avenue of research and provide more evidence for such superiority. We report on the results of an extensive molecular dynamics simulation of active microrheology of a model glass. We identify several time scales in time series of friction, and detect a transition in dynamical behavior of friction. We discuss the possible relation to structural heterogeneities—a subject of considerable interest in glass physics.

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### 1 Introduction

When a liquid is cooled rapidly below its melting temperature, its dynamics drastically slows down, and its viscosity increases more than fifteen orders of magnitude.<sup>1</sup> The structure of a supercooled liquid, explored by conventional measures such as structure factor or two-point density correlation function, shows no dramatic change upon the transition into the glass phase. As a result, it was believed that liquids and glasses are structurally equivalent. Two main key discoveries proved that there exist intimate, previously unnoticed, structural differences between glasses and liquids: (1) dynamic heterogeneities (DH),<sup>1</sup> and (2) hierarchical static structures—Tanaka *et al.* provide an excellent recent review of this subject.<sup>2</sup>

In a supercooled liquid, particles transiently trap in cages formed by their neighbors. The dynamics of a supercooled liquid is thus described by two main relaxation processes, which is mathematically described by a two-step relaxation function  $C(t)$ , (1) a fast exponential relaxation, known as  $\beta$  process with  $C(t) \sim e^{-(t/\tau_\beta)}$ , and (2) a slow stretched-exponential relaxation, known as  $\alpha$  process with  $C(t) \sim e^{-(t/\tau_\alpha)^b}$  where  $b < 1$ . In the  $\beta$  process, a particle rattles within the cage created by its

neighbors. This back and forth movement terminates when the particle eventually escapes the cage, and this results in the final  $\alpha$  relaxation. Below the melting temperature, cages become permanent and the  $\alpha$  process, within accessible laboratory time scales, becomes unattainable. This picture may suggest a homogeneous relaxation dynamics in a supercooled liquid. In contrast, it was revealed that in a supercooled liquid, particles displaced, let's say longer than the average particle displacement, form clusters; This is known as DH. As a result of DH, the dynamics in a supercooled liquid is heterogeneous.<sup>1,3</sup> This is in contrast to liquids that are widely considered homogeneous. Even though its name suggests a dynamic scenario, it is not clear whether the origin of DH is static or dynamic. Unveiling the origin of DH is important, because it will help to understand whether glass transition is a phase transition (the static origin) or a dynamic phenomenon (the dynamic origin). There are conflicting reports regarding the origin of DHs: some researchers advocate a static origin,<sup>4–7</sup> while others suggest a dynamic origin.<sup>8</sup> For example, Kawasaki and Tanaka identified clusters of medium-range crystalline order (MCRO), and demonstrated that MCROs are slower than the rest of the particles. The size of these clusters grows upon approaching the glass transition temperature. This suggests a possible link between MCRO and DH, and the authors concluded that MCRO may be the origin of DHs. Tanaka and co-workers pioneered this line of research and identified many other static structures;<sup>2</sup> These results demonstrate the existence of a hierarchical order in supercooled liquids. Most of these structures provide length scales that grow upon cooling. However, these length scales never become macroscopic. This is perhaps because

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of the the dramatic slowing down of the dynamics near the glass transition temperature.

Interestingly, the mechanical properties of a glass are very different from those of liquids, and share many similarities with conventional solids; though glasses have some special features such as the existence of excess vibrations, known as the boson peak. These similarities can be summarized into one main feature: both glasses and solids are rigid. These mechanical properties are investigated *via* global deformations, or shearing. However, a global deformation would only render an average response, and the local properties due to typical structural heterogeneities of supercooled liquids cannot be explored by a global deformation. A remedy for this problem is an approach based on local deformation: active microrheology. In this technique, local mechanical and transport properties can be obtained *via* the investigation of dynamics of a single-out probe particle driven into host medium.<sup>9</sup> This technique, active microrheology, has been widely used for investigations on biological materials, complex fluids,<sup>10</sup> and hard spheres as model systems for colloids.<sup>11–14</sup>

Three of us have previously investigated active microrheology of model glasses in a recent paper.<sup>15</sup> In this paper, a probe particle moves with a constant velocity,  $U$ , and the local response of the medium is obtained *via* friction force experienced by the probe particle. It was revealed that the time series of friction contains blueprints of the structural relaxations of the host medium. The study had three major outcomes:

First, the probe particle exhibited a second-order delocalization transition when the temperature was varied across the glass transition temperature. As a result, the friction,  $F$ , satisfied a scaling ansatz of the form:

$$F(U, T) = |T - T_{\text{mc}}|^{\Gamma} \mathbb{F}\left(\frac{U}{|T - T_{\text{mc}}|^{\Delta}}\right), \quad (1)$$

in which  $\delta T = |T - T_{\text{mc}}|$  is the distance from a critical delocalization temperature  $T_{\text{mc}}$ ,  $U$  is the probe velocity,  $\mathbb{F}(\dots)$  is a scaling function,  $\Gamma$  is a parameter-dependent exponent, and  $\Delta$  is a universal gap exponent. At  $T = T_{\text{mc}}$ , scale invariance requires  $F \propto U^q$ , in which  $q$  is a critical exponent, and eqn (1) grants  $q = \Gamma/\Delta$ . *Via* a systematic critical scaling analysis, we found out that the critical delocalization temperature was  $T_{\text{mc}} = 0.36875 \pm 0.0062$ , which was approximately 23% higher than the thermodynamic glass transition temperature, at  $T_{\text{K}} = 0.3$ , and the critical exponents associated with this transition were  $q = 0.17303 \pm 0.0248$ , with the crossover exponents  $\Gamma = 0.475 \pm 0.068$  and  $\Delta = 2.75$ .

Second, auto-correlation of the friction showed a two-step relaxation, described by a compressed exponential  $C(t) \sim e^{-(t/\tau_c)^b}$  where  $b > 1$ . Third, the study provided the first glance into the spatial distribution of micro-viscosity,  $\eta_{\text{m}}$ . The distribution was bell-shaped, and the skewness of the distribution function of  $\eta_{\text{m}}$  increased as the temperature was lowered. A possible connection to DH was discussed in ref. 15. We further elaborate this in the current manuscript and provide more clues about the dynamical behavior of the friction in this system.

We notice that the delocalization transition is related to a larger class of far-from equilibrium phase transitions of driven particles over random or periodic substrates; dubbed depinning transition. At low temperatures, where the thermal motion of the medium is seized, active microrheology resembles a probe particle driven over a random substrate. The depinning transition has far more ramifications in a much broader context of vortices in type-II superconductors, and skyrmions, and many other examples are given in a recent review at ref. 16.

In this work, we look at more clues in time series of friction. We will follow a usual practice in time series analysis to investigate fluctuations and the corresponding scaling behaviors across all characteristic time scales. We will ask whether time series of friction are stationary. By stationarity, we mean a time series in which two point correlation function decays as a function of the time lag, similar to the behavior of a correlation function in an equilibrium system. Another possibility is a reverse behavior in which the correlation increases as a function of time lag; this is similar to fractional Brownian Motion (fBM). This corresponds to a non-stationary time series, and results in the persistency of the underlying fluctuations. For this purpose, we will not directly use correlation functions owing to the inadequacy of the correlation functions for non-stationary processes. Instead, we will use a standard method, known as multifractal detrended fluctuation analysis,<sup>17</sup> for the time series of friction. We will show a transition in time series from stationary to non-stationary in the dynamics of friction. This will help us to identify a length scale that grows by lowering the temperature.

## 2 Method

We performed large scale Molecular Dynamics (MD) simulations using LAMMPS. We simulated a singled-out probe particle moving with constant velocity  $U$  embedded in a host medium at temperature  $T$ . A Nose-Hoover thermostat is used for constant-temperature molecular dynamics. The host is a binary mixture widely used as a model glass. For each  $U$  and  $T$ , we obtained an ensemble of 500 different independent realizations by starting from different initial conditions. We recorded the force acting on the probe particle, friction, and each simulation provided a time series of friction. Below, we describe details of simulations; more details can be found in our previous work.<sup>15</sup>

### 2.1 Kob-Andersen mixture

We used a binary system known as the Kob-Andersen (KA) mixture.<sup>18,19</sup> In KA model, atoms interact *via* a Lennard-Jones potential, and there are atoms of type-A and -B. The interaction potential between a pair is given by

$$U_{ij}(r) = \begin{cases} 4\epsilon_{ij} \left[ \left(\frac{\sigma_{ij}}{r}\right)^{12} - \left(\frac{\sigma_{ij}}{r}\right)^6 \right] + 4\epsilon_{ij} \left[ c_{ij}^{(0)} + c_{ij}^{(2)} \left(\frac{r}{\sigma_{ij}}\right)^2 \right], & r < r_{cij} \\ 0, & r > r_{cij} \end{cases} \quad (2)$$

where  $c_{ij}^{(0)}$  and  $c_{ij}^{(2)}$  ensure a smooth behavior of  $U_{ij}$  at a type-dependent cut off value  $r_{ij}^c = 2.5\sigma_{ij}$  *via*  $U_{ij}(r_{ij}^c) = 0$  and

$dU_{ij}/dr|_{r=r_{ij}^c} = 0$ . These parameters are invariant under a swap of subscripts  $i$  and  $j$ . The  $\varepsilon_{ij}$  and  $\sigma_{ij}$  parameters are given by  $\varepsilon_{AA} = 1.0\varepsilon$ ,  $\varepsilon_{AB} = 1.5\varepsilon$ ,  $\varepsilon_{BB} = 0.5\varepsilon$ , and  $\sigma_{AA} = 1.0\sigma$ ,  $\sigma_{AB} = 0.88\sigma$ ,  $\sigma_{BB} = 0.8\sigma$ . For all particles we set mass to unity. For the simplicity, length, energy, mass and time are represented in dimensionless unit  $\sigma$ ,  $\varepsilon$ ,  $m$ ,  $\tau = \sqrt{\sigma^2 m/\varepsilon}$  respectively. The number density  $\rho = 1.20\sigma^{-3}$ , and in all simulations, the time step,  $\Delta t$ , is  $0.01\tau$ . The simulation box is a cube. Two parallel hard walls are placed along the vertical axis, and periodic boundary conditions are applied to otherwise directions. Particles in the medium interact with walls via a Weeks–Chandler–Andersen (WCA) potential,  $U_{\text{wall}}(d) = 4\varepsilon[(\sigma/d)^{12} - (\sigma/d)^6 + 1/4]$ ,  $d \leq d_c = 2^{1/6}\sigma$  where  $d$  is the shortest distance between wall and a particle.

We used a state-of-the-art method, known as shear annealing, to stabilize the host medium.<sup>20,21</sup> In this method, the system is periodically sheared, and below a threshold yielding amplitude, the system settles down into deeper basins in the energy landscape. The more the system is annealed, the more stable it becomes, and the fewer fluctuations happen. This step is crucial to reduce the fluctuations of the system when we perform active microrheology.

## 2.2 Active microrheology

A probe particle with a prescribed constant velocity is driven into the host medium. The interaction potential of the probe particle with the host medium is given by

$$U(r) = \begin{cases} \infty, & r \leq \Delta \\ 4\varepsilon \left[ \left( \frac{\sigma}{r-\Delta} \right)^{12} - \left( \frac{\sigma}{r-\Delta} \right)^6 + \frac{1}{4} \right], & \Delta < r \leq \Delta + r_c \\ 0, & r > \Delta + r_c \end{cases} \quad (3)$$

where  $\Delta = 2.0\sigma$  and  $r_c = 2^{1/6}\sigma$ . The particle is propelled in the direction perpendicular to the confining walls.

## 2.3 Methodology of analysis

Apart from the auto-correlation function and power spectrum of friction fluctuations, we will analyse the corresponding time series using detrended fluctuation analysis (DFA). Here, we provide a brief summary of this methodology, which we have used to investigate the scaling properties of fluctuations of the friction time series. This method enables us to eliminate possible biases due to trends in the time series, therefore will provide precise scaling exponents. Below, we describe the steps for DFA and its connection to the stationary and non-stationary behavior of friction time series.<sup>17</sup>

For the given time series  $x(t_i) \equiv x(i)$  (here friction time series) for  $\{I = 1, \dots, N\}$ , we define the mean of  $x$  series as:

$$\langle x \rangle = \frac{1}{N} \sum_{i=1}^N x_i. \quad (4)$$

The zero mean time series,  $\bar{x}_i$ , is defined as

$$\bar{x}_i = x_i - \langle x \rangle. \quad (5)$$

For a stationary time-series, the correlation function,  $C(s)$ , is given by,

$$C(s) = \langle \bar{x}_i \bar{x}_{i+s} \rangle = \frac{1}{N-s} \sum_{i=1}^{N-s} \bar{x}_i \bar{x}_{i+s}. \quad (6)$$

If  $x(i)$  is uncorrelated, then  $C(s) = \delta(s)$ : for  $s > 0$ ,  $C(s)$  will be zero. The short-range correlations is given by an exponentially decaying function<sup>22</sup>

$$C(s) \sim \exp\left(-\frac{s}{s_{\text{max}}}\right), \quad (7)$$

with a characteristic decay time scale  $s_{\text{max}}$ . For long-range correlation,  $C(s)$  is given by an algebraic decaying function of form

$$C(s) \sim s^{-\gamma}, \quad (8)$$

with the exponent typically  $0 < \gamma < 1$ .

**2.3.1 Detrended and multifractal detrended fluctuation analyses.** It is known that the presence of trends in a time-series can result in fictitious correlations.<sup>17</sup> Therefore, it is important to eliminate all possible trends in a time-series prior to any statistical computation. For this purpose, a technique, dubbed detrended fluctuation analysis (DFA), has been developed<sup>17</sup> and has already been applied to various time series analyses.<sup>23–27</sup> For a given time-series  $x(t_i) \equiv x_i$ , DFA is performed in these consecutive steps:

(i) Integration: compute integral of the original time series

$$Y(i) = \sum_{k=1}^i x_k \quad (9)$$

(ii) Division: the time series (with the length of  $N$ ) is then divided into  $N_s = \frac{N}{s}$  non-overlapping segments, where  $s$  is the box size. Because  $N/s$  has normally a non-zero remainder, especially when  $s$  is large, the remaining part of the time series is discarded. To prevent any bias as a result of division, the time-series is first divided from the beginning to end, and the remaining part is left, and second time the division is performed in the opposite direction. As a result  $2N_s$  segments are produced. Now, one can perform the detrending step.

(iii) Detrending: for each segment  $s$ , a linear, or higher-order, regression is performed using least square algorithm. For a linear dependence, the resulting function is  $P_s(i) = a_s + b_s i$ , where  $a_s$  and  $b_s$  are constants obtained from the regression, and  $i$  is time. The detrending is performed by a simple subtraction from each data point within the interval:

$$Y_s^{\text{det.}}(i) = Y(i) - P_s(i). \quad (10)$$

For simplicity from now on, we will refer to  $Y_s^{\text{det.}}$  without the superscript det. After the detrending step, we can proceed to the final step for the investigation of fluctuations. For this purpose, we will measure mean variance (fluctuation function) of data averaged over all segments.

(iv) Scaling of fluctuations: variance of an interval of length  $s$  is defined as

$$F_s^2 = \langle (Y_s(i))^2 \rangle = \frac{1}{s} \sum_{i=1}^s (Y(i) - P_s(i))^2. \quad (11)$$

The standard fluctuation function,  $F(s)$ , is obtained by

$$F(s) = \left( \frac{1}{2N_s} \sum_{s=1}^{2N_s} F_s^2 \right)^{1/2}. \quad (12)$$

The superiority of DFA becomes clear upon a re-inspection of eqn (11). Usually, a variance is defined as  $F_s^2 = \langle (Y_s(i))^2 \rangle - \langle Y_s(i) \rangle^2$ , where the last term on the right-hand-side (rhs) of this equation can cause numerical instabilities during a scaling analysis. This hinders the detection of genuine scaling properties of the data. For clear reasons, in DFA that term is not required. To investigate the underlying scaling properties, we seek the following scaling relation

$$F(s) \sim s^h, \quad (13)$$

where the index  $h$  has the following relationship with exponent of the correlation function  $C(s)$  of eqn (8):

$$\gamma = 2 - 2h. \quad (14)$$

If  $h < 1$ , then  $\gamma > 0$ , and thus, the correlation function  $C(t)$  will decay as a function of the time lag,  $s$ . As a result, a time series with  $h < 1$  is called stationary. However, if  $h > 1$ , then  $\gamma < 0$  and  $C(s) \sim s^{|\gamma|}$ : the correlation will grow as a function of time  $s$ , akin to fBM, and as a result a time series with a positive correlation is considered non-stationary:

$$\begin{cases} \text{stationary} & h < 1 \\ \text{non-stationary} & h > 1. \end{cases} \quad (15)$$

For a stationary process,  $h < 1$ , the exponent  $h$  is identical to the well-known Hurst exponent  $H$ .<sup>28,29</sup> For this reason,  $h$  is called generalized Hurst exponent. Depending on the value of  $H$ , the time series may have various dynamical states:

$$\begin{cases} \text{short-term anti-persistent} & 0 < H < \frac{1}{2} \\ \text{white-noise} & H = \frac{1}{2} \\ \text{long-term persistent} & \frac{1}{2} < H < 1 \end{cases} \quad (16)$$

The implementation of DFA has been done by the MF DFA package in python provided by L Rydin/MF DFA.

### 3 Results

In Fig. 1, time series of friction for three different probe velocities  $U = 1, 0.223$  and  $0.018$  are depicted versus the probe displacement,  $t \times U$ . The temperature is  $T = 0.45$ , which is above the delocalization temperature,  $T_{mc} = 0.36875$ .<sup>15</sup> We will show that the corresponding generalized Hurst exponent for  $U = 1$  is  $h < 1$  at all time scales, indicating that the time series is

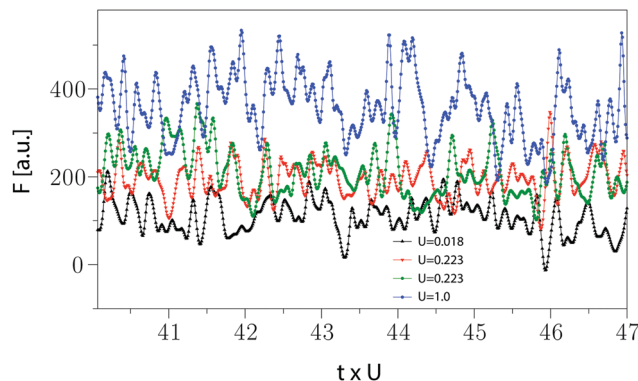


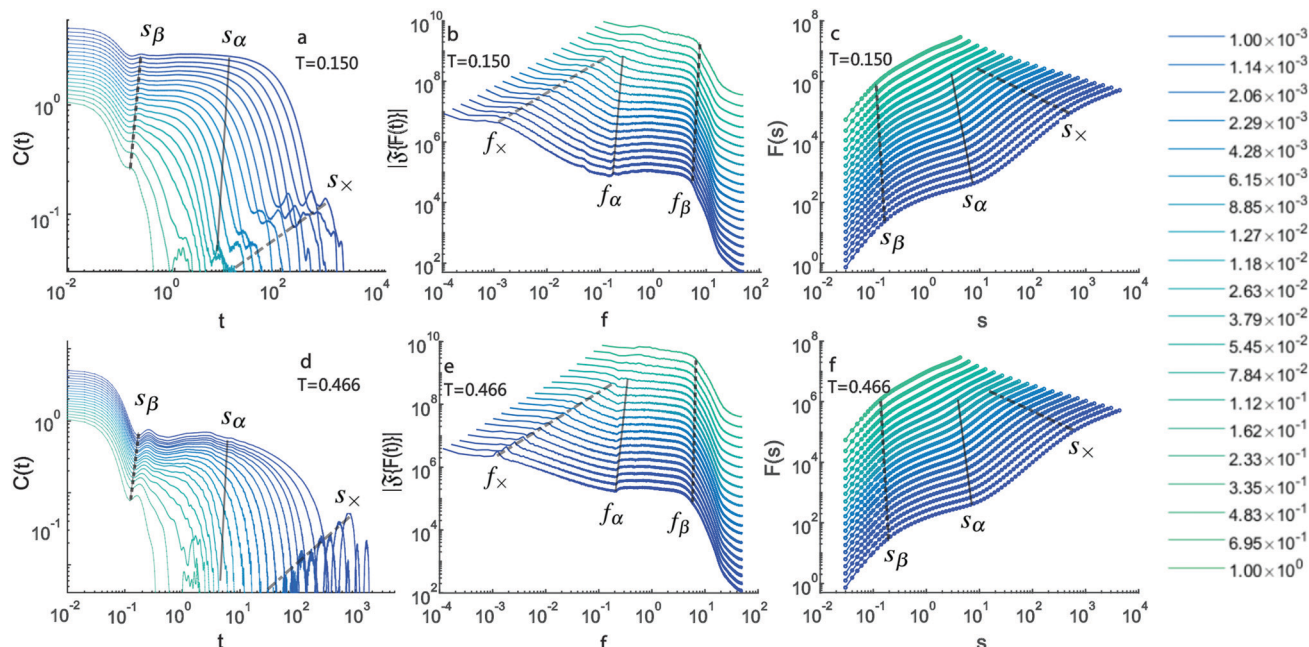
Fig. 1 Friction time series. The magnitude of the total force exerted by the medium to the probe particle, friction, is depicted versus the probe displacement,  $t \times U$ , for different probe velocities. The medium is in the liquid state with temperature  $T = 0.45$ , which is above the delocalization transition temperature  $T_{mc} = 0.36875$ .<sup>15</sup> The stochastic characteristics of the time series of friction depends on temperature and velocity. We will show that for  $U = 1$  and  $0.018$ , the corresponding generalized Hurst exponents are  $h < 1$  and  $h > 1$ , respectively. However, for  $U = 0.223$ , some of simulated time series are stationary and some others are non-stationary. This represents a transition as a function of the control parameter  $U$  in the behavior of time series.

stationary. However, for  $U = 0.018$ , in some time scales we obtain  $h > 1$ , which indicates that the time series is non-stationary. The case for  $U = 0.223$ , depicted by green and red curves, exhibits a mixed nature; for one case  $h > 1$  and for the other  $h < 1$ . Therefore,  $U = 0.223$  presents the boundary between the stationary and non-stationary dynamics in the detected time intervals.

In order to gain more insight about the dynamical nature of friction time series, similar to our previous work,<sup>15</sup> we present auto-correlation of time series of friction,  $C(t) = \langle F(0)F(t) \rangle$ , in Fig. 2a and d, for  $T = 0.15$  and  $0.466$ , respectively. Each curve has a different color which corresponds to different probe velocity  $U$  whose values are given in the legend. One can see that  $C(t)$  faithfully represents the typical two-step structural relaxation of a supercooled liquid: (1) an exponential decay as a result of ballistic motion, followed by a plateau representing the cage effect akin to the  $\beta$  relaxation with time scale  $\tau_\beta$ , and (2) final relaxation due to escape of a particle from the surrounding cage akin to the  $\alpha$  relaxation with  $\tau_\alpha$ . These time scales can be obtained by a model-fitting function of the form:

$$C(t) = (1 - A)e^{-(t/\tau_\beta)} + Ae^{-(t/\tau_\alpha)^b} \quad (17)$$

where  $A$  is a fitting parameter.<sup>7,30</sup> We will show that active microrheology combined with time series analysis provide an alternative direct way to obtain these time scales. We note that the two-step relaxation function of the friction time series may be confused with the standard two step relaxation of a supercooled liquid; the latter being discussed in the introduction. In standard glass literature, the two step relaxation behavior is obtained using intermediate scattering function.<sup>1</sup> This function is the Fourier transform of displacement of particles over a wave number whose magnitude equals to the inverse of a typical cage size;



**Fig. 2**  $C(t)$ ,  $\mathfrak{F}\{F(t)\}$  and DFA. Various properties of friction time series are plotted for two different temperatures  $T = 0.150$  and  $T = 0.466$  in the first and second rows, respectively. Each color corresponds to a different probe velocity,  $U$ , whose magnitude is given in the legend. (a and b) Auto-correlation function of friction time series,  $C(t)$ , exhibits two-step relaxation as well as more intimate details about the dynamics of the medium. More description can be found in the text. For clarity, curves are shifted upwards. (b and d) The magnitude of Fourier transforms of time series,  $\mathfrak{F}\{F(t)\}$ , versus frequency,  $f = 1/t$ , clearly shows many different cross overs. These cross overs are marked by dashed lines labeled by  $f_x$ ,  $f_\alpha$  and  $f_\beta$ . (c–f) The generalized fluctuation function,  $F(s)$ , also shows various time scales and cross overs.

this is normally the position of first peak of the pair correlation function. This function gives rise to a two-step relaxation curve in the liquid phase; however, in the glass phase the final  $\alpha$  relaxation cannot be observed in the usual laboratory time scales. This is in contrast to the behavior of friction correlation function, which exhibits  $\alpha$ -like relaxation deep in the glass phase. The reason for this difference originates from the fact that our probe particle is active and can escape cages in the glass phase. Despite this difference, our approach has one very important technical benefit for simulations: the computation of  $C(t)$  of friction requires only trajectory of the probe particle, however, intermediate scattering function requires trajectories of all particles. The latter becomes challenging when it comes down into the technical aspect of work such as the data storage. Especially if one is interested in short term dynamics which requires more finer trajectories, and thus a larger data storage.

We have previously shown that by rescaling  $C(t)$  versus  $x = t \times U^\nu$ , where  $\nu = 1 - q = 0.95$  being the force-thinning exponent, all curves collapse into a master curve given by a compressed exponential function  $e^{-(x/\tau_x)^b}$  with  $b > 1$ , resembling a time-force superposition similar to time-shear superposition principle predicted by mode-coupling theory<sup>31</sup> and spin glass theory.<sup>32</sup> These results established the fact that friction time series contains blueprint of structural relaxations in supercooled liquids.

An interesting point is the appearance of a second small plateau for low-temperature and glass phase and small enough probe velocities in panel-a, which might be related to the fBm

nature of friction dynamics in those scales and propagation of waves in the system as a result of the probe motion. This secondary plateau does not exist in the liquid state in panel-d. Therefore, active microrheology reveals many more interesting time scales that are not visible for globally averaged quantities, such as the self part of the scattering function. These time scales cannot be obtained by a simple fitting procedure using eqn (17), and more elaborate techniques should be used. To distinguish these cross overs, we compute the magnitude of Fourier transform of time series,  $\mathfrak{F}\{F(t)\}$ , depicted in Fig. 2 panel-b and -e. The existence of many cross overs at different time scales becomes much more clear in the frequency domain,  $f = 1/t$ . Below a frequency  $f_x$ , curves nearly level off at  $f \rightarrow 0$ . For  $f > f_x$ , a scaling regime is observed. In panel-f in liquid phase, we observe a ripple mode on  $f_x$  line (zoom in required).<sup>33</sup> This scaling region levels off at  $f_\alpha$ , which is followed by another plateau, similar to the corresponding plateau in the time domain in  $C(t)$ , then there is another scaling regime at the end of this region for  $f > f_\beta$ . We use these plots to identify cross over frequencies  $f_x$ ,  $f_\alpha$  and  $f_\beta$  for every curve individually. These cross overs are marked by dashed lines. The boundaries between these cross overs become blurred at large probe velocities for  $U > 2.33 \times 10^{-1}$ .

We are now ready to perform DFA. This is done in Fig. 2 panel-c and -f. One can see that each curve crosses over to various scaling regimes. Generally, DFA provides more clean scaling behavior with respect to other methods. The corresponding cross overs can be found using both DFA or power

spectrum analysis. Using the results of the Fourier transform analysis, we can determine cross overs in these curves as,  $s_\beta = 1/f_\beta$ ,  $s_\alpha = 1/f_\alpha$  and  $s_\times = 1/f_\times$ . Using linear regressions for the ranges  $s_\beta < s < s_\alpha$  and  $s_\alpha < s < s_\times$  in double logarithmic scale, we examine the following scaling behaviors

$$F(s) \sim \begin{cases} s^{h_\beta} & s_\beta < s < s_\alpha \\ s^{h_\alpha} & s_\alpha < s < s_\times, \end{cases} \quad (18)$$

and obtain  $h_\beta$  and  $h_\alpha$  for a given  $U$  and  $T$ . These exponents are related to the index of scaling of spectrum,  $\mathfrak{F}\{F(t)\} \sim f^{-\beta}$ , via Wiener–Khinchin theorem according to  $\beta = 2h - 1$ . Note that the similarity between names of exponent  $\beta$  and  $h_\beta$  is just a coincidence. We use this relationship to cross check our results, and we found plausible agreement between them. One can see that some of the curves in Fig. 2c and f have strong correction-to-scaling near the crossover region marked by  $s_\alpha$ . This means that eqn (18) cannot capture the full behavior of the data, and new terms, such as  $s^h(1 + ks^h)$ , must be added. To prevent this, we use compensated plots to compute the corresponding asymptotic exponent  $h$  for each respective region.<sup>34</sup> An example of a compensated plot is given in Appendix A.

### 3.1 Scaling behavior of the friction dynamics

We construct diagrams showing dynamics of friction in  $T$ - $U$  plane using  $h_\beta$  and  $h_\alpha$ . Fig. 3a and b show diagrams for  $\beta$  and  $\alpha$  regions, respectively. The color code is given by the corresponding exponents,  $h_\beta$  and  $h_\alpha$ . One can see that for all  $T$  and  $U$ , in  $\beta$  region of relaxation functions, we obtain  $h_\beta < 1$ , which indicates the stationarity of the process. Moreover, the exponent satisfies inequality  $0.5 < h_\beta < 1$ , which refers to the persistency of friction over this time scale. By persistency we mean that an increase of friction will be followed by an increase, and similarly, a decrease will be followed by a decrease.

More interesting behavior is found in panel-b for  $\alpha$  region. Here, we discover that  $h_\alpha$  crosses over from a region with  $h > 1$  to  $h < 1$ . A transition boundary can be drawn at  $h = 1$ ; this is marked by a dashed line. The area inside the cone represents the non-stationary regime. The non-stationary region expands as temperature is lowered. The area outside the cone represents

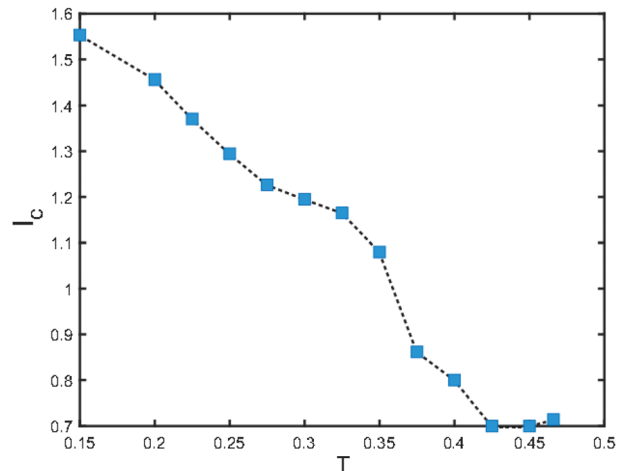


Fig. 4 Critical length scale. We define a length scale,  $l_c$ , given by  $l_c = (t_x - t_\alpha)U_c$  where  $U_c$  is the probe velocity at which we obtained a stationary to non-stationary transition. In liquid phase,  $l_c$  is almost zero, however, near  $T_{mc} = 0.36875$  it has a sharp increase, and then it monotonically increases by lowering the temperature.

the stationary region. To gain a better insight about the nature of this “stationary to non-stationary” transition, we look individually at each trajectory within our ensemble, and we calculate the ratio of cases where  $h < 1$  to the total number of trajectories, or probability  $P(h_\alpha < 1)$  in panel-c. It can be seen that deep inside the non-stationary region near the origin of the plot, almost all trajectories are non-stationary  $P(h_\alpha < 1) \simeq 0$ ; however, near the transition boundary almost half of trajectories are stationary. This may imply that the transition is second-order-type.

The transition boundary at  $h = 1$  for a given  $T$  occurs at a critical probe velocity  $U = U_c$ . We define a critical length scale,  $l_c$ , given by  $l_c = (t_x - t_\alpha)U_c$ . We plot this length scale as a function of temperature in Fig. 4. One can see that  $l_c$  increases as  $T$  is lowered. The largest gap in  $l_c$  happens near the delocalization transition temperature at  $T_{mc} = 0.36875$ . In the liquids phase,  $l_c$  is almost zero. Similar to many other length scales that are proposed for supercooled liquids, this length scale remains microscopic across all temperatures. However, to gain a better understanding of this length scale, a finite size scaling is

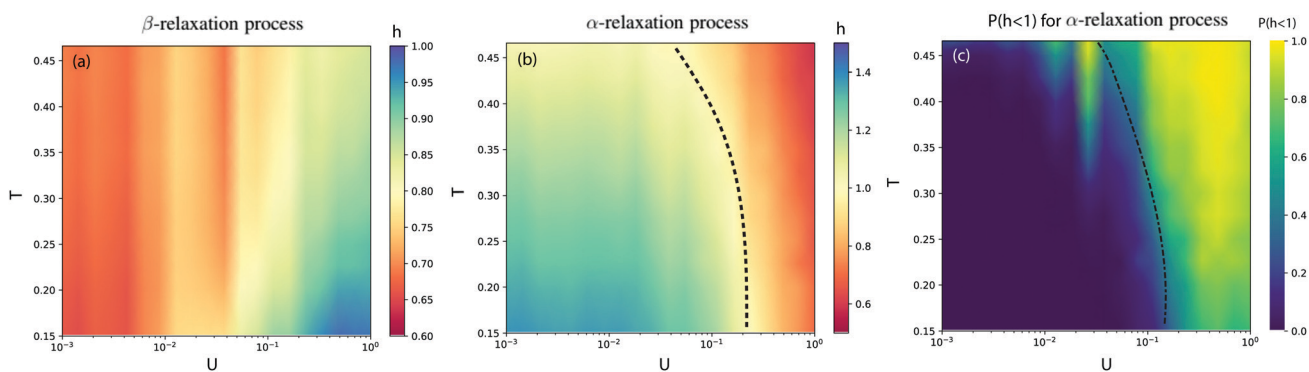


Fig. 3 Friction dynamics. Diagrams representing measured DFA exponent  $h$ , across (a)  $\beta$  and (b)  $\alpha$  regions. The dashed line in panel-b shows the phase boundary between non-stationary and stationary states. (c) The ratio of trajectories whose  $h_\alpha < 1$  is shown. Near the phase boundary, there are as much stationary trajectories as non-stationary ones, indicating possibly a second-order transition. The dashed line depicts the probability of  $P(h_\alpha < 1) \approx 0.5$ .

required to see how  $l_c$  grows with the system size. This is out of reach for the present work, but we will address it in near future.

## 4 Discussion and conclusion

In this paper, using extensive molecular dynamics simulations of active microrheology of a model glass combined with various statistical methods of time series analyses, we unveiled that friction time series undergoes a dynamical transition from stationary ( $h < 1$ ) to non-stationary ( $h > 1$ ) behavior in  $\alpha$  region. The non-stationary behavior is akin to fBM in which correlations grow as a function of time. This is in contrast to conventional equilibrium-like systems where correlations decay as a function of time. We also computed diagrams using the generalized Hurst exponent,  $h$ , in  $T$ - $U$  plane for both  $\beta$  and  $\alpha$  regions. Whereas  $\beta$  region is always stationary, we showed that the non-stationary region in  $\alpha$  domain grows as the temperature is lowered. As a result, for a given  $T$ , there exists a critical probe velocity  $U_c$  at which the dynamics crosses over.

Previous studies on the rheology of supercooled liquids by Berthier-Barrat,<sup>35</sup> and Varnik<sup>36</sup> demonstrated that, even though a supercooled liquid falls out of equilibrium near the melting temperature, however, the application of a shear flow into the system settles down the system into a dynamical stationary state akin to an equilibrium system. Here, active microrheology demonstrates that there exists a stationary state only above a critical threshold,  $U > U_c$ . Note that, we previously have shown that the probe velocity  $U$  is akin to a global flow rate  $\dot{\gamma}$  via  $\dot{\gamma} = U/D$ , where  $D$  is the probe diameter. It is possible that the onion structure in  $T$ - $U$  plane is smeared out in macrorheology. This demonstrates once again the superiority of active microrheology with respect to macrorheology.

Our analysis allowed us to extract a length scale,  $l_c$ , from our data, which is defined based on the cross over probe velocity  $U_c$ , and the corresponding time scale,  $t_x - t_z$ . We found that this length scale is almost zero in the liquid phase. Near  $T_{mc}$ , the critical delocalization temperature,  $l_c$  has a sharp increase, and then grows monotonically as the temperature is lowered. Similar growth of a length scale has been also observed in dynamic heterogeneities and hierarchal structures.<sup>2</sup> Our next goal is to find a relationship between this length scale and other known length scales in the literature. It will also be very interesting to see whether  $l_c$  will grow with the system size. This requires a systematic finite size scaling. We will address these questions in near future.

Microrheology is known to exhibit pronounced finite-size effects due to the finite size of system and the size of tracer. In its passive version, when the external drive on the tracer is switched off, results of simulations showed satisfactory quantitative agreement with continuum theories when the tracer size was about five times larger than that of the embedding medium particles.<sup>37,38</sup> A recent study on active microrheology found good agreement between the hydrodynamic theory and simulations for the dependence of viscosity as a function of system size only at intermediate system sizes,<sup>39</sup> and the the subject requires further investigation.

Our scaling approach offers a sound framework for this problem, because the system size,  $L$ , can be cast as a relevant perturbation to the scaling ansatz proposed in our previous work.<sup>15</sup> Because the delocalization transition in this system suggests a critical point at which the correlation length diverges,  $b = \xi \propto \delta T^{-\nu}$ , and the friction scales as a function of distance from the critical temperature,  $F \propto \delta T^{\beta}$ , near the critical temperature  $\delta T \rightarrow 0$  a standard critical scaling can be written as

$$F = b^{-y/\nu} \mathfrak{F}_0(Ub^z, bL^{-1}), \quad (19)$$

where  $z$  is the dynamic exponent, and  $\mathfrak{F}_0$  is a scaling function. For  $b = L$ , we obtain

$$F = L^{-y/\nu} \mathfrak{F}_1(UL^z), \quad (20)$$

which suggests that for small system sizes, when  $UL^z \ll 1$ , friction decreases as a function of the system size according to  $L^{-y/\nu}$ , and it saturates to a plateau at a cross over system size where  $L \approx \xi$ . Moreover, the size of tracer may acts as an irrelevant perturbation, which then may result in a correction-to-scaling to eqn (20). These questions merit further investigation as a future work for the comparison of predictions by critical scaling and hydrodynamics.

## Conflicts of interest

There are no conflicts to declare.

## A Appendix

Here, we explain how we carried out a compensated plot. The goal of a compensated plot is to derive an asymptotic exponent, like  $h_x$  and  $h_\beta$  in eqn (18), from the behavior of the data. For this purpose, a plot of  $s^{-h}F(s)$  versus  $s$  is depicted. Then the exponent  $h$  is varied over an interval and the genuine asymptotic exponent is the one by which the compensated plot becomes flat over the region of interest. In Fig. 5, we plot  $F(s)$  versus  $s$  for  $U = 0.001$  and  $T = 0.15$ . The original data are given by the green triangles.

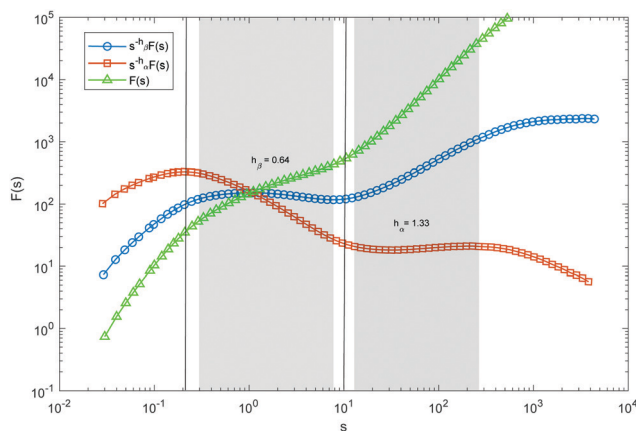


Fig. 5 Compensating plot. In this plot, we show how we derive  $h_\beta$  and  $h_x$  from original data of  $F(s)$  versus  $s$ . A compensated plot of  $s^{-h_\beta}F(s)$  versus  $s$ , the blue circles, becomes flat over  $\beta$  region for  $h_\beta = 0.64$ . Similarly, A compensated plot of  $s^{-h_x}F(s)$  versus  $s$ , the brown squares, becomes flat over  $\alpha$  region for  $h_x = 1.33$ .

We would like to derive  $h_\beta$  and  $h_\alpha$  over  $\beta$  and  $\alpha$  regions, respectively, from the original data. These regions are highlighted by two grey columns. We find that  $s^{-h_\beta}F(s)$  versus  $s$  becomes flat over the  $\beta$  region if we choose  $h_\beta = 0.64$ . This is given by the blue circles. Similarly,  $h_\alpha = 1.33$  makes  $s^{-h_\alpha}F(s)$  versus  $s$  flat over  $\alpha$  region. This is shown by the brown squares.

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