


Cite this: *RSC Adv.*, 2021, 11, 18187

# Thermodynamic assessment of the stability of bulk and nanoparticulate cobalt and nickel during dry and steam reforming of methane†

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The high reaction temperatures during steam and dry reforming of methane inevitably entail catalyst deactivation. Evaluation of the feasibility or potentially relevant mechanisms at play is of utmost importance to develop highly active and stable catalysts. Herein, various oxidation reactions of bulk-sized nickel and cobalt to the corresponding metal oxide or in the presence of a metal oxide carrier are evaluated thermodynamically and linked to approximated conditions during methane reforming. In particular cobalt aluminate, as well as cobalt or nickel titanates are likely to form. As oxidation to bulk-sized metal oxide is unlikely, a thermodynamic analysis of metallic nanoparticles was performed to calculate the size dependent stability against oxidation to nickel oxide or cobalt oxide in water and carbon dioxide-rich environments. The calculations indicate that nickel nanoparticles >3 nm and cobalt nanoparticles >10 nm are expected to withstand oxidation during steam and dry reforming of methane with stoichiometric feed compositions and methane conversion levels >10% at temperatures up to 1100 and 900 °C, respectively. Lastly, the reduced thermal stability of nanoparticles due to melting point suppression was assessed, leading to similar recommendations concerning minimum particle sizes.

Received 9th March 2021

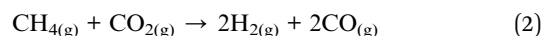
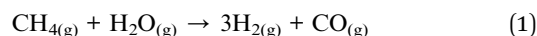
Accepted 15th April 2021

DOI: 10.1039/d1ra01856f

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## Introduction

Steam reforming of methane (SRM, eqn (1)) is the state-of-the-art process for the production of a large amount of synthesis gas from methane due to superior economical features and process performance. SRM is a well-established technology for the production of hydrogen-rich synthesis gas covering approximately 80–85% of the global H<sub>2</sub> production.<sup>1–4</sup> An upcoming alternative of great potential in regard to sustainability and valorisation of less abundant methane sources is dry reforming of methane (DRM, eqn (2)). Here, steam is replaced by CO<sub>2</sub> as the oxidative molecule for methane. Incorporation of this greenhouse gas into the value chain of chemical sites makes DRM ecologically attractive as it further provides great potential to mitigate environmental challenges associated with GHG emissions.<sup>4–9</sup> In addition, the absence of steam decreases the energy requirements of DRM regarding heat-up of the reactants, which results in approximately 20% lower operating costs and a lower carbon footprint in comparison to SRM.<sup>6,8</sup>



The major difference between DRM, SRM, and alternative reforming processes of methane for the production of synthesis gas, such as partial oxidation (POX), is the oxidising agent.<sup>6,8</sup> The oxidants H<sub>2</sub>O in SRM and CO<sub>2</sub> in DRM are required due to the strong saturated C–H bonds in the methane molecule. As CO<sub>2</sub> is a weaker oxidant, DRM is even more endothermic than SRM and consequentially requires elevated operation temperatures in the range of 700–1000 °C for industrial application.<sup>7</sup> Nevertheless, thermocatalytic low temperature reforming (≤500 °C) has been successfully demonstrated in the literature for SRM and DRM,<sup>10–12</sup> but an efficient conversion to synthesis gas is strongly limited by thermodynamic constraints.<sup>1</sup> The typically elevated operation temperatures in combination with an oxidising reaction mixture including hydrocarbons may cause rapid catalyst deactivation *via* coking and sintering, which are typically accelerated at elevated temperatures.<sup>8,13</sup> In addition, the oxidants in the feed may induce deactivation by oxidation of the active metallic phase (eqn (3) and (4)) exemplary for the common reforming catalyst Ni<sup>0</sup>. While oxidation of the active phase for methane reforming, such as Ni<sup>0</sup> and Co<sup>0</sup>, is thermodynamically not feasible for bulk-sized structures,<sup>14–18</sup> it has been suggested as a deactivation pathway of catalysts with small crystallite sizes of the active metallic phase for Ni-based catalysts in DRM<sup>19</sup> or SRM,<sup>10,20–22</sup> as well as Co-based catalysts in the

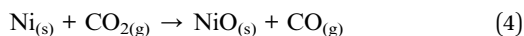
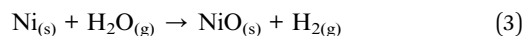
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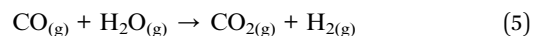
† Electronic supplementary information (ESI) available. See DOI: 10.1039/d1ra01856f



Fischer–Tropsch synthesis.<sup>16,23–25</sup> Noteworthy, oxidation may also enable additional conversion of carbon from CH<sub>4</sub> decomposition *via* a Mars–van–Krevelen type mechanism, *i.e.* an oxidised phase may be re-reduced forming CO. Hence, such a conversion pathway may not only result in an enhanced coking resistance, but also boost the catalyst activity.<sup>18,26</sup>



The high temperatures and the oxidising atmosphere present the major challenges in the commercialisation of DRM. During commercial SRM, coking of the catalysts may be mostly suppressed by co-feeding an excess of oxidising H<sub>2</sub>O in the reformer, *i.e.* by increasing the steam-to-carbon ratio (S/C) in the inlet stream.<sup>13,27,28</sup> S/C ratios exceeding the stoichiometry of the reforming reaction (eqn (1)) render SRM a combination of methane reforming and water–gas shift (WGS) reaction (eqn (5)),<sup>4</sup> which also results in a typically desired increased H<sub>2</sub>/CO ratio in the product gas. The suppression of excessive coking and increased H<sub>2</sub> content in the produced synthesis gas are also the reason for co-feeding steam and CO<sub>2</sub> in the first commercialisation attempts of DRM in industry, which renders the processes a combination of DRM and SRM. This beneficial effect on suppression of coking in lab-scaled DRM is also reported in the literature, but co-feeding of steam generally mitigates the advantage regarding energy requirements of the reforming process.<sup>28,29</sup> Hence, recent advances in catalyst research for DRM mostly focus on concepts on prevention of excessive sintering and carbon deposition to boost the catalysts' stability.<sup>30</sup> For example, perovskite-based catalysts were employed in various studies and displayed suppressed coking and phase transformation of the active Ni<sup>0</sup> phase.<sup>19,31,32</sup> Further, novel mixed-metal oxide support materials were developed to hinder the solid-state reaction of active Ni<sup>0</sup> nanoparticles with classical support materials, such as Al<sub>2</sub>O<sub>3</sub>, resulting in an increased stability against oxidation.<sup>33,34</sup> Song *et al.* recently deliberately allowed for sintering of 2.9 nm Ni nanoparticles, supported on highly ordered single-crystals of MgO, up to an average size of 17.3 nm to obtain a heat resistant catalyst.<sup>9</sup> As a result, coking was significantly suppressed as Ni<sup>0</sup> accumulated at the high energy step edges of the MgO crystals during the sintering process and physically blocked centres for coking.



Pronounced sintering of nano-sized materials is, like most structural effects, a result of the increased contribution of the surface energy ( $\gamma_{\text{surf}}$ ) to the overall energy of nanoparticles when compared to bulk-sized material. The surface energy of a crystal is given by half the required energy to cut the crystal into two equal halves.<sup>35</sup> The fundamental principle of minimisation of surface energy also applies to nanoparticles. While this driving force typically results in a minimisation of the surface area, crystalline particles form facets resulting in smaller surface energies than for spherical structures with a corresponding number of atoms. In turn, the thermodynamically stable phase of nanoparticles may differ from the one in larger particles.<sup>36</sup> For example, the fcc-Co structure (Fig. 1) is the preferential phase for nanoparticles below 20 nm (ref. 37–39) while hcp-Co is the stable phases in larger structures.<sup>40</sup> Such a behaviour becomes particularly important for structure sensitive reactions. In the case of the two Co<sup>0</sup> allotropes, hcp-Co has been suggested to lower the activation energy for CO dissociation due to the presence of unique active sites and may consequentially enable higher turn-over rates, *e.g.* in the Fischer–Tropsch synthesis.<sup>41,42</sup>

Fundamental statistics on the geometry of nanoparticles were developed by van Hardeveld and Hartog<sup>44</sup> allowing for the approximation of the surface energy by the broken bond model.<sup>15,35,45</sup> Surface atoms are coordinatively unsaturated and hence surfaces have a potential for additional coordination. The number of broken bonds describes the difference in coordination number of such surface atoms compared to a bulk atom when cutting a crystal along certain crystallographic planes.<sup>35,45</sup> The incomplete coordination of surface atoms binds energy, which in turn results in an increased surface energy. The surface energy of transition metal particles has been reported to correlate with the number of broken bonds,<sup>15,46,47</sup> which increases for smaller crystallite sizes and depends on the morphology of the nanoparticle. Based on such theoretical statistics, the surface energy of nanoparticles can be estimated as a function of the size according to eqn (6) and drastically increases for crystallite sizes below 10 nm (Fig. 2).<sup>15</sup> In turn, nanoparticles below 10 nm have an amplified drive to minimise their surface energy.

$$\gamma_{\text{surf}} = \gamma_{\text{surf,bulk}} \left( 1 + \frac{A}{d} + \frac{B}{d^2} \right) \quad (6)$$

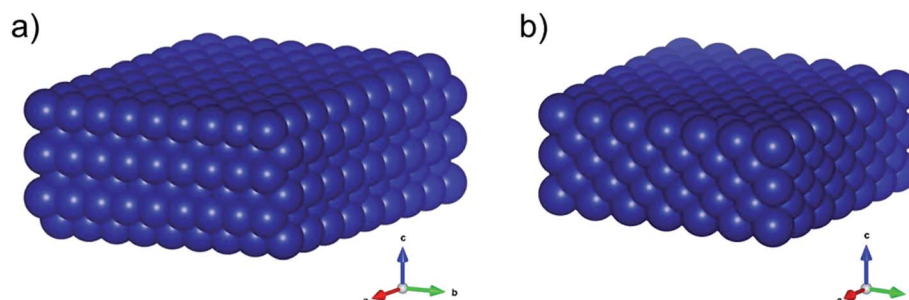


Fig. 1 Three-dimensional schematics of the main allotropes of cobalt with (a) hexagonal-close-packed (hcp) and (b) face-centered-cubic (fcc) crystal structure. The graphics were produced in VESTA.<sup>43</sup>



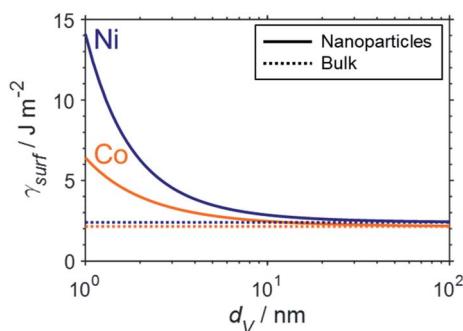


Fig. 2 Empirical approximation of the surface energy of fcc-cobalt (orange) and nickel (blue) nanoparticles (solid) as a function of crystallite size based on the number of broken bonds according to the methodology by van Steen *et al.*<sup>15</sup> and compared to the particular bulk-sized metals (dotted).

where  $\gamma_{\text{surf,bulk}}$  is the surface energy of the metal in the bulk phase,  $A$  and  $B$  are metal specific parameters describing the size dependency according to the broken bond model, and  $d$  is the particle size.

The increased ratio of surface to bulk atoms in nanoparticles also affects their thermal stability.<sup>48</sup> According to the Lindemann criterion, the melting point ( $T_M$ ) of a crystal is reached when the mean thermal displacement of the atoms equals a certain fraction of the actual interatomic distance.<sup>35</sup> The large fraction of surface atoms in nanoparticles increases the atomic displacement when compared to larger particles and hence nanoparticles melt at lower temperatures.<sup>35</sup> A structural melting point suppression of nano-sized metal particles has firstly been reported by Thomson *et al.* describing a size dependency of the melting point ( $T_M$ ) of solid particles.<sup>49</sup> The structural dependency can be predicted by the Gibbs–Thomson correlation (eqn (7)) and becomes significant for particle sizes below 100 nm, *i.e.* for nanoparticles.<sup>48,49</sup> Couchman *et al.* proposed a more complex thermodynamic approach providing similar predictions, which are in agreement with experimental results for various metals.<sup>50</sup> Smaller particle sizes are generally reported to display a higher susceptibility towards sintering.<sup>39,51–54</sup> Aside from the temperature, the composition of the gas phase,<sup>54–56</sup> the dispersion of the active phase over the support,<sup>39,51</sup> the morphology and physico-chemical properties of the support,<sup>54,57–59</sup> as well as promoters<sup>51</sup> have been identified as parameters for sintering. Lastly, several studies report a dependency of the sintering tendency on the particle size distribution with the size difference being the driving force.<sup>58,60,61</sup>

$$T_M = T_{M,\text{bulk}} \left( 1 - \frac{4\varepsilon_{\text{sl}}}{\Delta H_f \rho d} \right) \quad (7)$$

where  $\varepsilon_{\text{sl}}$  is the solid–liquid interfacial energy,  $\Delta H_f$  is the latent heat of fusion, and  $\rho$  is the density of the bulk phase.

In this study, potential phase transformations of nickel and cobalt resulting in deactivation during reforming of methane, namely oxidation to metal oxides or metal–support compounds, are evaluated thermodynamically for various conditions and a wide temperature range. Both metals may be employed in

reforming of methane. In addition, structural dependent deactivation *via* size dependent oxidation of nano-sized  $\text{Ni}^0$  and  $\text{Co}^0$  by  $\text{H}_2\text{O}$  or  $\text{CO}_2$ , as well as enhanced sintering due to melting point suppression in metallic nanoparticles are investigated theoretically. Hence, the study aims to contribute fundamental understanding of various potential processes of catalyst deactivation during reforming of methane.

## Theoretical methods

Gibbs free energies ( $\Delta G_{\text{rxn}}$ ) of selected chemical reactions were calculated for the temperature range 500–1100 °C employing the Gibbs–Helmholtz equation. Accordingly, the calculation depends on the temperature ( $T$ ), the reaction specific constants standard enthalpy of reaction ( $\Delta H_{\text{rxn}}^0$ ) and standard Gibbs free energy of reaction ( $\Delta G_{\text{rxn}}^0$ ), as well as a mathematical description of the temperature dependency of the heat capacities ( $C_p$ ) of reactants and products (eqn (8)). All thermodynamic calculations are conducted with data provided by Knacke *et al.*<sup>62–64</sup>

$$\Delta G_{\text{rxn}}(T) = T \left( \frac{\Delta G_{\text{rxn}}^0}{T^0} - \int_{T^0}^T \frac{\Delta H_{\text{rxn}}^0 + \int_{T^0}^T \Delta C_p(T) dT}{T^2} dT \right) \quad (8)$$

The feasibility of oxidation of a metal (eqn (9)) changes with the ratio of oxidant over reductant. Combination of eqn (8) and the definition of the Gibbs free energy with the equilibrium constant of reaction ( $K_c$ ) (eqn (10) and (11)) results in a thermodynamic description of the partial pressure ratio of reactants over products (eqn (12)). Assuming that the oxidant and reductant are the only gaseous compounds present, the phase equilibrium of metal *vs.* metal oxide can be described by the partial pressure ratio of oxidising over reducing agent.



$$\Delta G_{\text{rxn}}(T) = -RT \ln K_c \quad (10)$$

$$K_c = \left( \frac{p_{\text{oxidant}}}{p_{\text{reductant}}} \right)^b \quad (11)$$

$$\frac{p_{\text{oxidant}}}{p_{\text{reductant}}} = \exp \left\{ \frac{1}{bR} \left( \frac{\Delta G_{\text{rxn}}^0}{T^0} - \int_{T^0}^T \frac{\Delta H_{\text{rxn}}^0 + \int_{T^0}^T \Delta C_p(T) dT}{T^2} dT \right) \right\} \quad (12)$$

The significantly increased contribution of the surface energy to the overall energy of nano-sized materials can be considered in thermodynamic predictions on the size dependent stability of nickel and cobalt nanoparticles under oxidising atmosphere according to van Steen *et al.*<sup>15</sup> The oxidation of spherical nickel or cobalt crystallites by either  $\text{H}_2\text{O}$  or  $\text{CO}_2$  to  $\text{NiO}$  and  $\text{CoO}$  (eqn (9);  $a = b = 1$ ), respectively, is thermodynamically favoured if the Gibbs free energy of reaction considering structural dependency according to eqn (13) is negative,



i.e. if the metallic state plus oxidant has a lower energy level then the corresponding oxide plus reductant.

$$\Delta G_{\text{rxn}}(T, d) = \mu_{\text{MeO(s)}}(T) + \mu_{\text{reductant(g)}}(T) - \mu_{\text{Me(s)}}(T) - \mu_{\text{oxidant(g)}}(T) + RT \ln \left( \frac{p_{\text{reductant}}}{p_{\text{oxidant}}} \right) + \frac{6\gamma_{\text{Me}}(d)M_{\text{Me}}}{\rho_{\text{Me}}d_{\text{Me}}} \left( \gamma_{\text{MeO/Me}}(d) \left( \frac{\rho_{\text{Me}}M_{\text{MeO}}}{\rho_{\text{MeO}}M_{\text{Me}}} \right)^{\frac{2}{3}} - 1 \right) \quad (13)$$

where  $\mu_i(T)$  is the chemical potential of compound  $i$  at temperature  $T$  and 1.013 bar,  $\gamma_{\text{Me}}(d)$  is the surface energy of the metal for crystallite size  $d$ ,  $\gamma_{\text{MeO/Me}}(d)$  is the ratio of the surface energy of metal oxide over metal for crystallite size  $d$ , and  $M_i$  is the molar mass of compound  $i$ .

The size dependency of the surface energy of metallic Ni and Co nanoparticles was estimated using eqn (6) with a surface energy of the metallic bulk phase of 2.39 and 2.14 J m<sup>-2</sup>, respectively. While the surface energy of Co was adapted from van Steen *et al.*,<sup>15</sup> an average value was calculated for Ni based on various publication.<sup>65–72</sup> Parameters  $A_{\text{Co}} = 2.14$  and  $B_{\text{Co}} = 0.55$  were also adapted from van Steen *et al.*, who correlated the average amount of broken bonds per surface atom in various crystal structures to the surface energy of Co nanoparticles.<sup>15</sup> In a similar manner, the average amount of broken bonds per surface atom was calculated for Ni nanoparticles with an fcc octahedral crystal structure (Fig. S1†) by employing statistical and mathematical descriptors for atoms in nanoclusters.<sup>44,73</sup> Correlation with the surface energy of bulk-sized Ni resulted in  $A_{\text{Ni}} = 1.60$  and  $B_{\text{Ni}} = 3.30$  for eqn (6). The ratio of the surface energy of bulk CoO and Co of 0.2167 was adapted from van Steen *et al.*<sup>15</sup> For the system NiO/Ni, a larger ratio of 0.4705 was calculated based on several studies in literature.<sup>74–76</sup> Even though a mild structural dependency of  $\gamma_{\text{MeO/Me}}$  has been reported for bulk CoO and Co,<sup>15</sup> the ratio is herein simplified to be considered constant for both systems.

Calculation of the melting point suppression of nano-sized nickel and cobalt (eqn (7)) was conducted with a melting point of the bulk phase of 1455 (Ni) and 1480 °C (Co), a specific gravity of 8908 (Ni) and 8860 kg m<sup>-3</sup> (Co), a specific latent heat of melting of 299 401.97 (Ni) and 259 844.91 J kg<sup>-1</sup> (Co), as well as with an interfacial tension between the solid and liquid interface of 0.306 (Ni) and 0.306 N m<sup>-1</sup> (Co).<sup>16,45,77</sup>

## Results and discussion

### Thermodynamic predictions on oxidation of bulk metal

Calculation of the Gibbs free energies (eqn (8)) for various oxidation reactions of the active metallic phase during dry or steam reforming indicates the feasibility of such deactivation reactions for bulk-sized structures in the considered temperature range. Calculation of the required partial pressure ratio of oxidant (H<sub>2</sub>O or CO<sub>2</sub>) over reductant (H<sub>2</sub> or CO) puts the Gibbs free energy in perspective to required conditions during SRM and DRM to initiate oxidation. In fact, these partial pressure ratios are the driving force and have been previously identified

as a good descriptor for such an oxidation reaction.<sup>15,16,19</sup> The oxidant : reductant ratios are decreasing with increasing conversion levels for both reforming reactions (Fig. 3). For SRM with a stoichiometric feed and methane conversion levels in the range of 9–50%, a partial pressure ratio of H<sub>2</sub>O to H<sub>2</sub> ( $p_{\text{H}_2\text{O}}/p_{\text{H}_2}$ ) between 10 and 1 may be approximated (Fig. 3a). High conversions exceeding 91% represent ratios below 0.1. Co-feeding of steam in excess to suppress coking is a common strategy to mitigate deactivation<sup>27,28</sup> and will result in increased  $p_{\text{H}_2\text{O}}/p_{\text{H}_2}$  ratios (Fig. S1†). During DRM,  $p_{\text{CO}_2}/p_{\text{CO}}$  ratios of 10, 1, and 0.1 are expected for methane conversion levels of 5, 33, and 83%, respectively, when assuming a stoichiometric feed (Fig. 3b).

The conducted thermodynamic calculations for the oxidation of bulk Ni<sup>0</sup> and Co<sup>0</sup> to the corresponding metal oxide during SRM and DRM result in high Gibbs free energies (Fig. 4 and 5), which indicates an unlikely oxidation of the metals by CO<sub>2</sub> or H<sub>2</sub>O at reasonable conversion levels. This trend has been previously reported for bulk-sized materials.<sup>14–18</sup> For fcc-Ni and temperatures below 900 °C, H<sub>2</sub>O/H<sub>2</sub> and CO<sub>2</sub>/CO ratios exceeding 60 are required for oxidation to NiO (Fig. 4b and d), which corresponds to low to zero level of conversion in SRM and DRM (Fig. 3). Even though the required ratios are lower for the formation of CoO from hcp-Co (Fig. 5b and d), oxidation by CO<sub>2</sub> or H<sub>2</sub>O of bulk-sized cobalt is also unlikely. For example,  $p_{\text{CO}_2}/p_{\text{CO}}$  ratios exceeding 10 are required for oxidation of bulk-sized Co<sup>0</sup> during DRM at 1100 °C. Considering the typically lower operation temperatures for DRM and the strong temperature dependency of the feasibility of this reaction, oxidation of bulk Co<sup>0</sup> can also be considered as highly unlikely unless operation at CH<sub>4</sub> conversion levels <5%. However, the active metal of the first fraction of a fixed-bed catalyst bed may undergo a certain degree of oxidation as the reducing H<sub>2</sub> and CO are generated

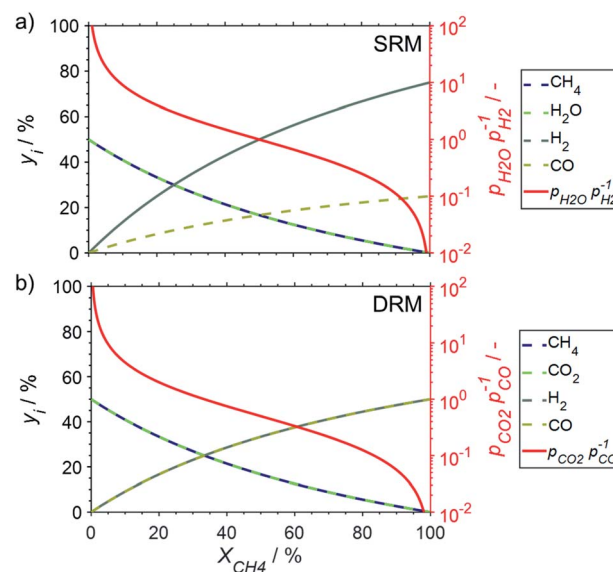


Fig. 3 Gas phase composition during (a) steam reforming and (b) dry reforming of methane together with the partial pressure ratio of the corresponding oxidant–reductant couple of reactant to product. The calculations neglect side reactions and assume a stoichiometric feed composition.





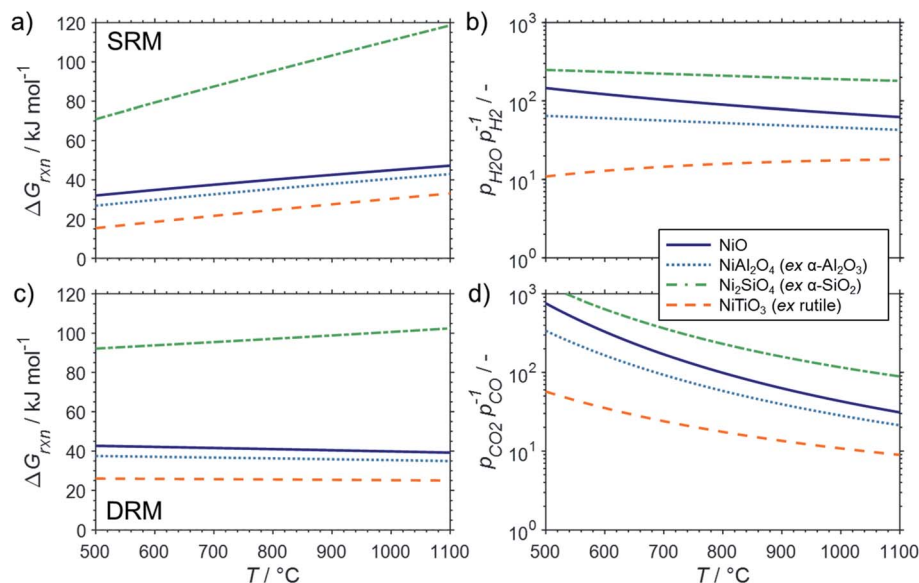


Fig. 4 (a and c) Gibbs free energies and (b and d) thermodynamic equilibria, represented by the ratio of oxidant over reductant, for selected oxidation reactions of bulk fcc-Ni with (a and b) gaseous  $\text{H}_2\text{O}$  or (c and d)  $\text{CO}_2$  forming nickel oxide or metal-support compounds. Calculations are based on thermodynamic data by Knacke *et al.*<sup>62–64</sup>

gradually along the catalyst bed. This may become relevant and result in strong deactivation if an oxidation front slowly moves along the catalyst bed during prolonged operation. Noteworthy, oxidation of  $\text{Co}^0$  by  $\text{CO}_2$  has previously been demonstrated to be absent during exposure of a reduced Co-based catalyst to 90%  $\text{CO}_2/\text{Ar}$  at 150  $^\circ\text{C}$  demonstrating the kinetical hindrance of this oxidation reaction at lower temperatures.<sup>78</sup>

Aside from oxidation to the corresponding metal oxide, the formation of metal-support compounds (MSCs), such as

aluminates, silicates, or titanates, may also lower the availability of the active metallic phase resulting in deactivation.<sup>17,18,33</sup> Furthermore, the formation of these inactive mixed-metal oxides is typically associated with a drastic change of the morphology from metallic nanoparticles to highly dispersed metal atoms within the support structure.<sup>17</sup> Hence, a reductive regeneration of formed MSCs is challenging, which is also linked to the elevated reduction temperatures of these MSCs.<sup>14,79,80</sup> Nevertheless, such a regeneration at high

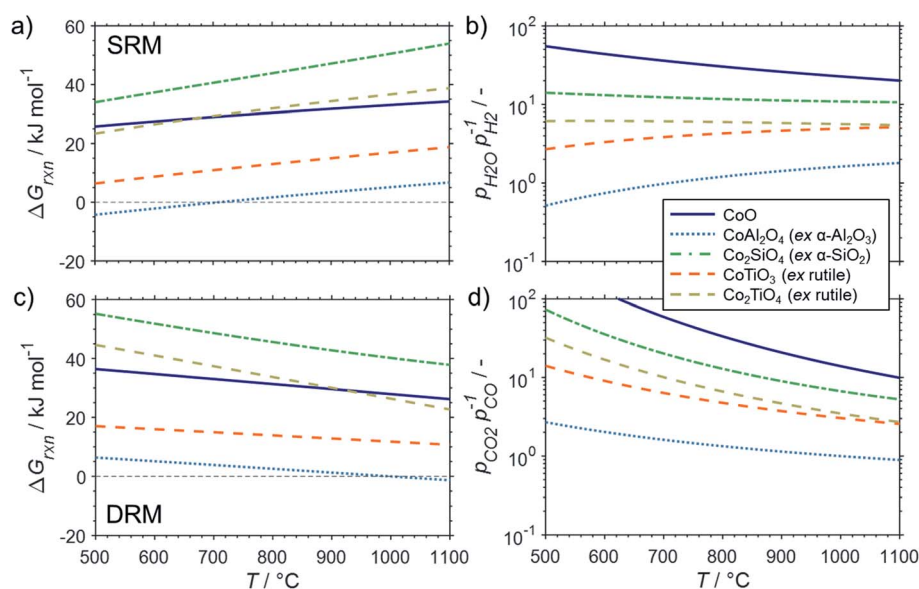


Fig. 5 (a and c) Gibbs free energies and (b and d) thermodynamic equilibria, represented by the ratio of oxidant over reductant, for selected oxidation reactions of bulk hcp-Co with (a and b) gaseous  $\text{H}_2\text{O}$  or (c and d)  $\text{CO}_2$  forming cobalt oxide or metal-support compounds. Calculations are based on thermodynamic data by Knacke *et al.*<sup>62–64</sup>

temperatures is possible and even utilised in order to create anchored metallic nanoparticles as stable catalyst for methane reforming.<sup>81,82</sup> Either way, the required conditions for potential formation of these mixed-metal oxide compounds during SRM and DRM remain important.

Similar to the oxidation to nickel oxide, the herein conducted thermodynamic calculations indicate an unfeasible formation of MSCs during SRM over Ni<sup>0</sup> on  $\alpha$ -Al<sub>2</sub>O<sub>3</sub>,  $\alpha$ -SiO<sub>2</sub> (quartz), and  $\alpha$ -TiO<sub>2</sub> (rutile), which were selected as representative common metal oxide support materials (Fig. 4a and b). For these support materials and SRM at 900 °C, nickel titanate (NiTiO<sub>3</sub>) is predicted to form at the lowest H<sub>2</sub>O/H<sub>2</sub> ratio of 17, while aluminates ( $p_{\text{H}_2\text{O}}/p_{\text{H}_2} = 49$ ) and particularly silicates ( $p_{\text{H}_2\text{O}}/p_{\text{H}_2} = 199$ ) are unlikely to form at moderate conversion levels. Even when increasing the S/C ratio in the inlet to 5, the resulting H<sub>2</sub>O/H<sub>2</sub> ratios remains below 20 for conversions levels exceeding 25% (Fig. S1†). The same order in the feasibility for the formation of MSCs was calculated for DRM over Ni-based catalysts (Fig. 4c and d), while increased reaction temperatures increase the likelihood of the formation of MSCs drastically. However, the  $p_{\text{CO}_2}/p_{\text{CO}}$  ratio of 8.9, which is required to initiate the formation of nickel titanate in a fcc-Ni/rutile catalyst at a high reaction temperature of 1100 °C, still correlates to relatively low conversion levels <6% (Fig. 3b).

The formation of MSCs in Co-based catalysts is generally more likely than for nickel (Fig. 5). Especially the formation of cobalt aluminate is highly likely from a thermodynamic point of view.<sup>18</sup> For certain temperature ranges, the Gibbs free energies for the oxidation of hcp-Co/ $\alpha$ -Al<sub>2</sub>O<sub>3</sub> by H<sub>2</sub>O during SRM ( $T < 700$  °C) or CO<sub>2</sub> during DRM ( $T > 1000$  °C) to CoAl<sub>2</sub>O<sub>4</sub> becomes negative. Hence, already a low oxidant : reductant ratio of 1 : 1 may induce the formation of this MSC. However, the formation of cobalt aluminate has previously been hypothesized to be kinetically hindered during the FTS.<sup>14</sup> A certain kinetical hindrance of this water-driven solid state reaction was recently demonstrated experimentally for a fcc-Co/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst at 220 °C.<sup>17</sup> Nevertheless, the elevated temperatures during SRM and DRM may overcome such kinetic limitations and potentially enable a rapid formation.

The formation of cobalt titanates during SRM and DRM also requires moderate oxidant : reductant ratios (Fig. 5). During SRM, the required H<sub>2</sub>O/H<sub>2</sub> ratio for the formation of CoTiO<sub>3</sub> ranges from 2.7–5.5 in the studied temperature range of 500–1000 °C. The cobalt titanate polymorph Co<sub>2</sub>TiO<sub>4</sub> is also likely to form with ratios below 6.2. Lastly, the formation of cobalt silicate (Co<sub>2</sub>SiO<sub>4</sub>) from quartz and hcp-Co is the least likely. For DRM, the required CO<sub>2</sub>/CO ratios for the formation of the cobalt titanate polymorphs is below 10 when exceeding 700 °C. As in the calculations for Ni-based catalysts, elevated reaction temperatures also drastically increase the likelihood for the formation of MSCs during DRM. At 1100 °C, the required ratios of CO<sub>2</sub>/CO for all three selected support materials is below 5.2.

The formation of the two cobalt titanate polymorphs already indicated potential effects of polymorphism on the formation of MSCs. In fact, polymorphism of the carrier materials is an important parameter affecting the formation of MSCs. For example, crystal structures for Al<sub>2</sub>O<sub>3</sub> other than the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> have

been reported to show a higher tendency towards the formation of cobalt aluminates<sup>17,25,83,84</sup> or nickel aluminate.<sup>22</sup> While thermodynamics suggest the formation of aluminate from Ni<sup>0</sup> and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> at a  $p_{\text{H}_2\text{O}}/p_{\text{H}_2}$  ratio of  $\sim 50$  for temperatures exceeding 900 °C (Fig. 4b), Sehested *et al.* reported the formation of NiAl<sub>2</sub>O<sub>3</sub> during exposure of a Ni/ $\theta$ -Al<sub>2</sub>O<sub>3</sub> catalyst to such an unreactive model atmosphere at a lower temperature of 750 °C.<sup>22</sup> Herein conducted calculations for  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> indicate a higher reactivity of other polymorphs with nickel (Fig. 6) and cobalt (Fig. 7) during SRM and DRM. For the two common TiO<sub>2</sub> polymorphs rutile and anatase, the thermodynamic calculations suggest a higher reactivity for the latter. This is in line with recently published calculations and experimental studies for Co/TiO<sub>2</sub> catalysts under water-rich conditions at lower temperatures of 220 °C.<sup>17</sup>

### Size dependent stability of metal nanoparticles

All the presented results and calculations are based on bulk properties of nickel and cobalt. As indicated in the introduction (Fig. 2), the contribution of the surface energy to the overall energy of nano-sized materials becomes important for crystallite sizes below 10 nm. Therefore, even little changes in the surface energy of nanoparticles may become driving factors for phase transformations in order to adhere to the fundamental principle of the minimisation of surface energy. This may be the case when metallic nanoparticles are exposed to oxidising atmospheres and the surface energy of the metal is higher than

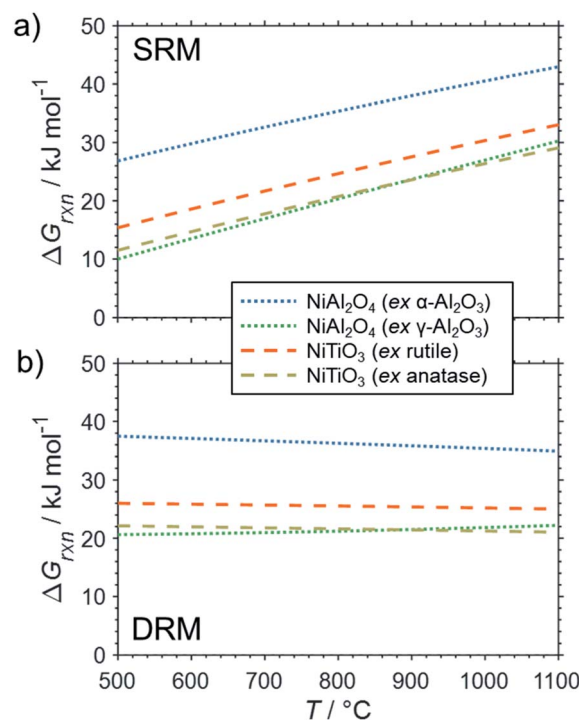


Fig. 6 Gibbs free energies for selected oxidation reactions of bulk fcc-Ni with common metal oxide carrier materials and (a) gaseous H<sub>2</sub>O or (b) CO<sub>2</sub> forming metal-support compounds demonstrating the potential impact of polymorphism of the support. Calculations are based on thermodynamic data by Knacke *et al.*<sup>62–64</sup>



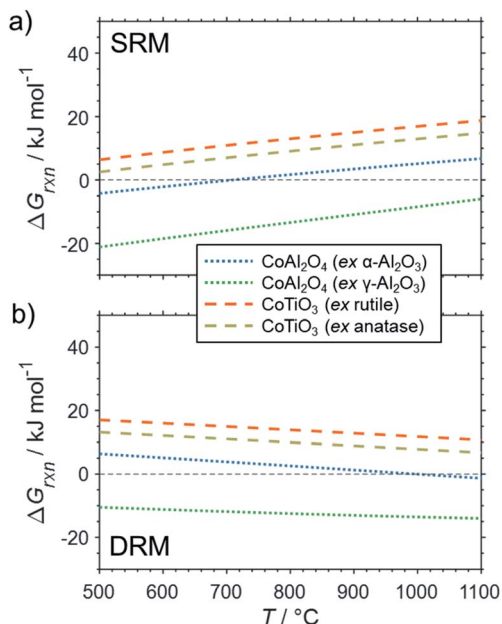


Fig. 7 Gibbs free energies for selected oxidation reactions of bulk hcp-Co with common metal oxide carrier materials and (a) gaseous  $\text{H}_2\text{O}$  or (b)  $\text{CO}_2$  forming metal-support compounds demonstrating the potential impact of polymorphism of the support. Calculations are based on thermodynamic data by Knacke *et al.*<sup>62–64</sup>

for the corresponding metal oxide.<sup>15</sup> Both metals, nickel and cobalt, fulfil this criterion and hence are expected to display an increased oxidation potential with decreasing crystallite size. This size dependent oxidation behaviour was calculated for fcc-Ni (Fig. 8), fcc-Co (Fig. 9), and hcp-Co (Fig. S2†) for the two oxidant-reductant couples during SRM ( $\text{H}_2\text{O}$  and  $\text{H}_2$ ) and DRM ( $\text{CO}_2$  and  $\text{CO}$ ), based on calculations by van Steen *et al.* for the oxidation of fcc-Co under water-rich conditions at lower temperatures.<sup>15</sup>

With a stoichiometric feed for SRM, the  $\text{H}_2\text{O}/\text{H}_2$  ratio can be expected to be below 10 for methane conversion levels exceeding 10% (Fig. 3a). For DRM, the oxidant : reductant ratio  $\text{CO}_2/\text{CO}$  is  $<5$  for this moderate conversion level (Fig. 3b). According to the thermodynamic predictions, fcc-Ni nanoparticles  $>3$  nm can be expected to display a sufficient stability against oxidation by  $\text{H}_2\text{O}$  during SRM or  $\text{CO}_2$  during DRM for  $>10\%$  conversion of methane and temperatures up to  $1100^{\circ}\text{C}$ , while the size dependent calculations suggest the rigorous formation of the stable oxidic form for fcc-Ni nanoparticles with sizes below 2 nm (Fig. 8). Hence, oxidation of  $\text{Ni}^0$  nanoparticles exceeding 3 nm in size can be expected to not play a major role during deactivation of the larger part of the catalyst bed during methane reforming. As aforementioned, only the first fraction of the catalyst bed that is contact with the fresh feed stream is exposed to severe oxidising conditions and may undergo oxidation. For example, surface oxidation of the active metal during DRM at  $600^{\circ}\text{C}$  over a  $\text{Ni}/\text{LaFeO}_3/\text{MgAl}_2\text{O}_4$  catalyst was hypothesised by Mao *et al.* due to insufficient formation of reductive environment at low conversion levels, which could be

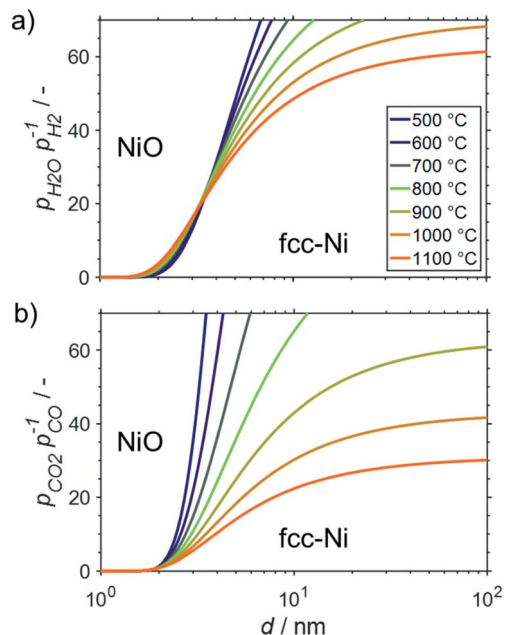


Fig. 8 Stability regions of nanometre-sized particles with required ratios of oxidant over reductant for oxidation of fcc-nickel nanoparticles to nickel(II) oxide during (a) steam reforming and (b) dry reforming of methane.

overcome by increasing the  $\text{CH}_4/\text{CO}_2$  ratio in the feed to ratios above unity.<sup>19</sup>

Aside from DRM, Mao *et al.* studied the oxidation behaviour of a  $\text{Ni}/\text{MgAl}_2\text{O}_4$  in  $\text{H}_2\text{O}/\text{H}_2$  mixtures at  $800^{\circ}\text{C}$ .<sup>19</sup> Compared to the theoretically expected oxidation potential for bulk-sized

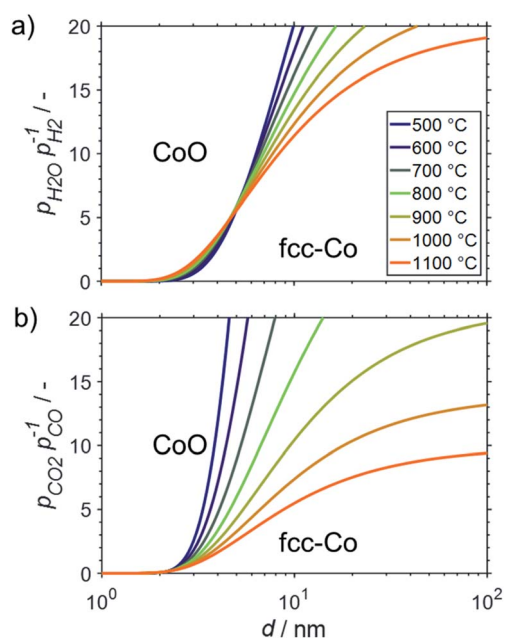


Fig. 9 Stability regions of nanometre-sized particles with required ratios of oxidant over reductant for oxidation of fcc-cobalt nanoparticles to cobalt(II) oxide during (a) steam reforming and (b) dry reforming of methane.



nickel, a small shift of the equilibrium between the metal and metal oxide phase to the oxidic side was identified. Comparison with characterisation data on other samples in said study suggests an average crystallite size of nickel in the range of 10–15 nm for the Ni/MgAl<sub>2</sub>O<sub>4</sub> catalyst with a wide size distribution. Hence, the observed lower stability of nano-sized Ni<sup>0</sup> may be linked to the herein discussed size dependent oxidation behaviour (Fig. 8a).

Strong oxidation of the metallic phase was observed when comparing X-ray diffraction (XRD) patterns of a 20 wt% Ni/SiO<sub>2</sub> after activation in 10% H<sub>2</sub>/Ar at 500 °C and after SRM with a S/C = 2 at 500 °C.<sup>10</sup> The authors linked an observed strong deactivation from ~22% conversion of CH<sub>4</sub> after 0.5 h time-on-stream to zero conversion level after 4 h to this oxidation process as carbon formation was less pronounced and sintering was not identified. However, less oxidation was observed for a 20 wt% Ni/Al<sub>2</sub>O<sub>3</sub> catalyst reduced at 700 °C, while residual NiO in a 20 wt% Ni/ZrO<sub>2</sub> after reduction at 500 °C was seemingly even reduced to Ni<sup>0</sup> during SRM.<sup>10</sup> As the average crystallite sizes of Ni<sup>0</sup> in all catalysts were estimated to be in the range of 11–17 nm, oxidation of the smaller nanoparticles may become feasible (Fig. 8a) at the observed conversion levels <25%, which corresponds to theoretical  $p_{\text{H}_2\text{O}}/p_{\text{H}_2}$  ratios >7 (Fig. S1†). However, the strong dependence of the identified phase transformation points towards a dominating effect of the support material, which may be linked to the easier formation of nickel aluminates (Fig. 4).

In another study, strong deactivation of a 8.4 wt% Ni/SiO<sub>2</sub> catalyst was observed during SRM with S/C = 2 at 500 °C.<sup>21</sup> Contrary, 8.0 wt% Ni/Al<sub>2</sub>O<sub>3</sub> as well as nickel on zinc and magnesium aluminate-like support materials displayed a stable conversion rate or even activation during SRM. The average NiO particle size after calcination of 11–13 nm in the Ni/SiO<sub>2</sub> catalyst was smaller than in the Al<sub>2</sub>O<sub>3</sub>-supported sample (19 nm).<sup>21</sup> Hence, the observed deactivation of the Ni/SiO<sub>2</sub> may indeed be linked to hypothesised oxidation of Ni<sup>0</sup>, which can be expected to be less pronounced for the Ni/Al<sub>2</sub>O<sub>3</sub> catalyst. Low levels of carbonaceous deposits were identified for both samples. The mixed oxide-supported catalysts featured the smallest particle size in the range of 3–6 nm, but strong deviation from the physicochemical properties of Ni<sup>0</sup> nanoparticles is expected due to the reduction of Ni<sup>2+</sup> ions strongly interacting with the spinel-like mixed oxide support materials during the initial activation in H<sub>2</sub>.<sup>21</sup>

The fcc structure of cobalt is the preferred allotrope in nanoparticles.<sup>37–39</sup> For fcc-Co nanoparticles, crystallite sizes >10 nm are predicted to be stable against oxidation to CoO during SRM and DRM at operation temperatures up to 1100 and 900 °C, respectively, as long as methane conversion levels exceed 10% (Fig. 9). Similar to the size dependent stability of fcc-Ni nanoparticles, fcc-Co crystallites below 2 nm are expected to oxidise rapidly. However, a strong dependency on the size is predicted for nanoparticles in the range of 2–10 nm, which is particularly pronounced for DRM due to the strong temperature dependency of the feasibility of the oxidation reaction of Co with CO<sub>2</sub>. When comparing the fcc structure to the allotrope hcp-Co, which is the thermodynamically stable structure of

cobalt in the bulk phase,<sup>64</sup> a shift to larger threshold sizes for oxidation is observed (Fig. S2†). This behaviour exhibits the higher amount of broken bonds in nano-sized hcp-Co crystallites resulting in larger surface energies and ultimately enhancing the driving force for the minimisation of energy of nanoparticles *via* oxidation.

The oxidation behaviour of nano-sized Co<sup>0</sup> structures has been under discussion in the Fischer–Tropsch community for a long time.<sup>15,16,23,24,54,85–89</sup> Recent experimental studies employing sophisticated *in situ* characterisation techniques<sup>16,54,87,88</sup> together with insight from theoretical work<sup>89</sup> enabled a compelling understanding of the mechanisms at play during water induced oxidation.<sup>25</sup> The hypothesised size dependent oxidation behaviour of Co<sup>0</sup> to CoO, as predicted by van Steen *et al.*,<sup>15</sup> has been confirmed for 220 °C.<sup>16,25,54,87,88</sup> However, oxidation was demonstrated to rather occur due to a hindered removal of adsorbed oxygen species from the surface upon CO dissociation at high partial pressures of H<sub>2</sub>O rather than direct oxidation of Co<sup>0</sup> by water splitting.<sup>88,89</sup> The latter reaction was consequentially hypothesized to be kinetically hindered at 220 °C,<sup>16,17,25,88</sup> which is likely to change at elevated operation temperatures during reforming of methane. The elevated temperatures may also allow for oxidation of Co<sup>0</sup> by CO<sub>2</sub>, which was demonstrated to be kinetically hindered in 90% CO<sub>2</sub>/Ar at temperatures below 150 °C.<sup>78</sup>

Aside from thermodynamically favoured oxidation, nano-sized material is also expected to display a lower thermal resistance against sintering when compared to bulk structures. Sintering of the catalytically active phases typically results in deactivation due to a loss of active surface area. One of the most important drivers of sintering is the temperature.<sup>51</sup> The melting point provides a good indication of the susceptibility towards sintering of a material. The Tammann (0.5T<sub>M</sub>) and the Hüttig temperatures (0.3T<sub>M</sub>) approximate the required temperatures for an increased mobility of bulk and surface atoms of a particle, respectively, which lowers the thermal stability and may result in sintering.<sup>90</sup> Combination of the thermodynamic description of the melting point suppression for metallic nanoparticles in the nanometre range<sup>49</sup> according to Gibbs–Thomson correlation (eqn (7)) and the calculation of the Tammann and Hüttig temperature allows for a prediction of the size dependency of the particular critical temperatures (Fig. 10). Such a prediction was previously published for cobalt<sup>16</sup> and was herein calculated for nickel as well.

The strong melting point suppression for cobalt and nickel nanoparticles below 2 nm is expected to result in liquification of the active metal for temperatures within typical conditions for reforming of methane (600–1000 °C; Fig. 10). Furthermore, even lower temperatures far from the (suppressed) melting point may decrease the thermal stability of nanoparticles drastically. For example, surface atoms of cobalt and nickel particles are presumed to experience a high mobility when exceeding the Hüttig temperature, which lies below typical operation temperatures for both metals. Even the Tammann temperatures of bulk-sized Ni (581 °C) and Co (601 °C)<sup>90</sup> are easily exceeded. Hence, nano-sized material below 10 nm can be expected to require significant stabilisation by strong interaction with the





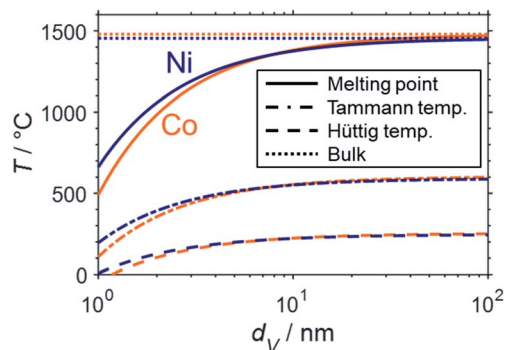


Fig. 10 Structural melting point suppression (solid), size dependent Tammann (dash-dotted), and Hüttig temperature (dashed) of cobalt (orange) and nickel (blue) spheres in the nanometre size regime according to the Gibbs–Thomson equation and compared to the melting points of the bulk-phased metals (dotted). The data for cobalt was adapted from Wolf *et al.*<sup>16</sup>

support in order to suppress sintering. The formation of anchored nanoparticles may mitigate sintering and has previously been reported, *e.g.* via the formation of the metallic phase via reduction of MSCs at elevated temperatures<sup>21,81,82</sup> or encapsulation of the supported active phase.<sup>91,92</sup> The importance of such stabilisation is emphasised by comparison of the herein presented theoretical predictions based on a fundamental thermodynamic approach with the literature data. Several studies employing supported non-stabilised Ni nanoparticles with initial sizes in the range of 2–12 nm reported drastic sintering during DRM at 700–800 °C forming particles or nanoparticle clusters in the range of 17–40 nm.<sup>91–95</sup> In this size range, the herein discussed melting point suppression is rather small, which drastically decreases the drive to further minimise the surface energy via further particle growth. Lastly, sintering may also be accelerated under hydrothermal conditions.<sup>13,22,54,96–99</sup> For example, Sehested *et al.* demonstrated the dependency of Ni<sup>0</sup> crystallite growth in various Al<sub>2</sub>O<sub>3</sub> and MgAl<sub>2</sub>O<sub>4</sub>-supported Ni-based catalysts on the temperature, exposure time, and  $p_{\text{H}_2\text{O}}/p_{\text{H}_2}$  ratio during exposure to high ratios up to 50 in the temperature range 500–825 °C.<sup>22,96,97</sup>

## Summary and conclusions

Thermodynamic calculations on the size dependent stability of metallic nickel and cobalt nanoparticles during steam and dry reforming of methane were conducted and may provide fundamental understanding of the redox properties of nano-sized Ni<sup>0</sup> and Co<sup>0</sup> under methane reforming conditions. The results suggest required particle sizes of Ni >3 nm and Co >10 nm in order to suppress oxidation by either H<sub>2</sub>O or CO<sub>2</sub> for methane conversion levels exceeding 10% and stoichiometric feed composition. Nanoparticles below 2 nm in size are thermodynamically unstable and expected to oxidise to the corresponding metal oxide. Furthermore, the melting point suppression of nano-sized materials may result in melting of cobalt and nickel nanoparticles <2 nm at typical temperatures of methane reforming. In addition to the formation of metal

oxide, the feasibility of oxidation to mixed-metal oxides with various metal oxides was evaluated for bulk structures. While the formation of metal-support compounds in supported nickel catalysts requires high oxidant-to-reductant ratios, cobalt aluminates and in particular cobalt titanates may easily form for cobalt-based catalysts. However, industrially applied increased steam-to-carbon ratios result in conditions favouring the formation of metal-support compounds.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

Financial support by the European Research Council is gratefully acknowledged (Project 786475: Engineering of Supported Catalytically Active Liquid Metal Solutions).

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