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# Temperature assistance of electric field-controlled spin–orbit torque-based magnetization switching in PMN–PT/FePt heterostructures†

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We report the temperature assistance of electric field (E-field)-controlled spin–orbit torque (SOT)-based magnetization switching of  $L1_0$ -FePt films grown on a  $PbMg_{1/3}Nb_{2/3}O_3$ – $PbTiO_3$  (PMN–PT) (011) substrate, which generates considerable strain *via* piezoelectric effects of the PMN–PT substrate under E-field. Owing to large strain-induced effective field and weak perpendicular magnetic anisotropy (PMA) at a high temperature, E-field controls the PMA- and SOT-based magnetization switching more effectively. Driven by E-field, magnetization switching is detected by a magnetic optical Kerr (MOKE) microscope under a fixed perpendicular magnetic field. Furthermore, E-field modulates change of anomalous Hall resistance regularly, which enables us to achieve the bidirectional transmission of data by designing an E-field controlled SOT-based logical circuit. This study indicates an efficient way to fabricate potential E-field-controlled spintronic applications at high temperatures.

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## Introduction

Spin–orbit torque (SOT)-based current-induced magnetization switching has drawn considerable interest due to its prospective utility in low energy consuming spintronic devices.<sup>1–3</sup> SOT is in a dominant position in research field of spintronics for magnetization switching, which makes it an aplenty and energy efficient physical phenomenon.<sup>4</sup> The technical significance of SOT for the promotion of future magnetic random access memories has been introduced, which records information *via* SOT-based magnetization switching.<sup>5</sup> FePt with  $L1_0$ -ordered is an ideal magnetic alloy for information recording with high perpendicular magnetic anisotropy (PMA), the source of which comes from hybridization between Fe 3d and Pt 5d electrons and spin–orbit coupling (SOC). SOC is a precondition of SOT effects.<sup>6–8</sup>

Electric field (E-field)-controlled magnetic and electric properties, which is known as the magnetoelectric (ME) coupling, also have been investigated in ferromagnetic/ferroelectric (FM/FE) heterostructures owing to the advantages of reduced energy consuming, high efficiency and high storage density.<sup>9,10</sup> Strains generated *via* the piezoelectric effects of a ferroelectric substrate under E-field-controlled magnetic and electric properties is one of the most extensively used methods of ME coupling.<sup>11,12</sup> The  $PbMg_{1/3}Nb_{2/3}O_3$ – $PbTiO_3$  (PMN–PT) substrate attracted considerable attention due to its high

piezoelectric activity in FM/FE heterostructures, which is an ideal strain source.<sup>13</sup> The PMN–PT(011) substrate has largest ferroelastic domain switching and piezoelectric coefficients  $d_{33}$  along the [01–1] direction,<sup>14</sup> which means E-field along the [01–1] direction controls ME coupling in FM/PMN–PT(011) heterostructures more efficiently. E-field-controlled SOT switching and SOT switching logic operations on the PMN–PT substrate also have been demonstrated.<sup>15,16</sup> In addition, few researches on temperature assistance of SOT-based magnetization switching are reported.<sup>17,18</sup> Thus, it is rational to explore the mechanism of temperature assistance of E-field controlled SOT-based magnetization switching in PMN–PT/FePt heterostructures.

In this study, we explore the temperature assistance of E-field-controlled SOT-based magnetization switching. E-field has an improved manipulating effect on PMA- and SOT-based magnetization switching of PMN–PT/FePt heterostructures at 350 K. E-field controlled magnetization switching is detected by a magnetic optical Kerr (MOKE) microscope. Then, an E-field controlled SOT-based logical circuit is designed, which is based on the reversible change of anomalous Hall resistance regulated by E-field and realizes the bidirectional transmission of data.

## Experimental method

2.5 nm-FePt films were grown on the PMN–PT(011) substrate by magnetron sputtering at 400 °C with a base pressure less than  $2 \times 10^{-6}$  Pa. Continuously, FePt films were fabricated into Hall bar *via* standard lithography and Ar ion milling, the size of which is  $20 \times 120 \mu\text{m}$ , as shown in Fig. 1(a). The Pt

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electrodes are used to apply uniform E-field. Before each measurement, PMN-PT substrates were polarized by E-field of  $15 \text{ kV cm}^{-1}$ .

The surface roughness of the PMN-PT(011) substrates was measured by an atomic force microscope (AFM) and the magnetic

properties of FePt films were obtained on a vibrating sample magnetometer (VSM). The crystal structure of the FePt films was analyzed *via* grazing incidence X-ray diffraction (GIXRD). Magnetization switching is detected by the MOKE microscope.  $R_{\text{H}}-H$  and

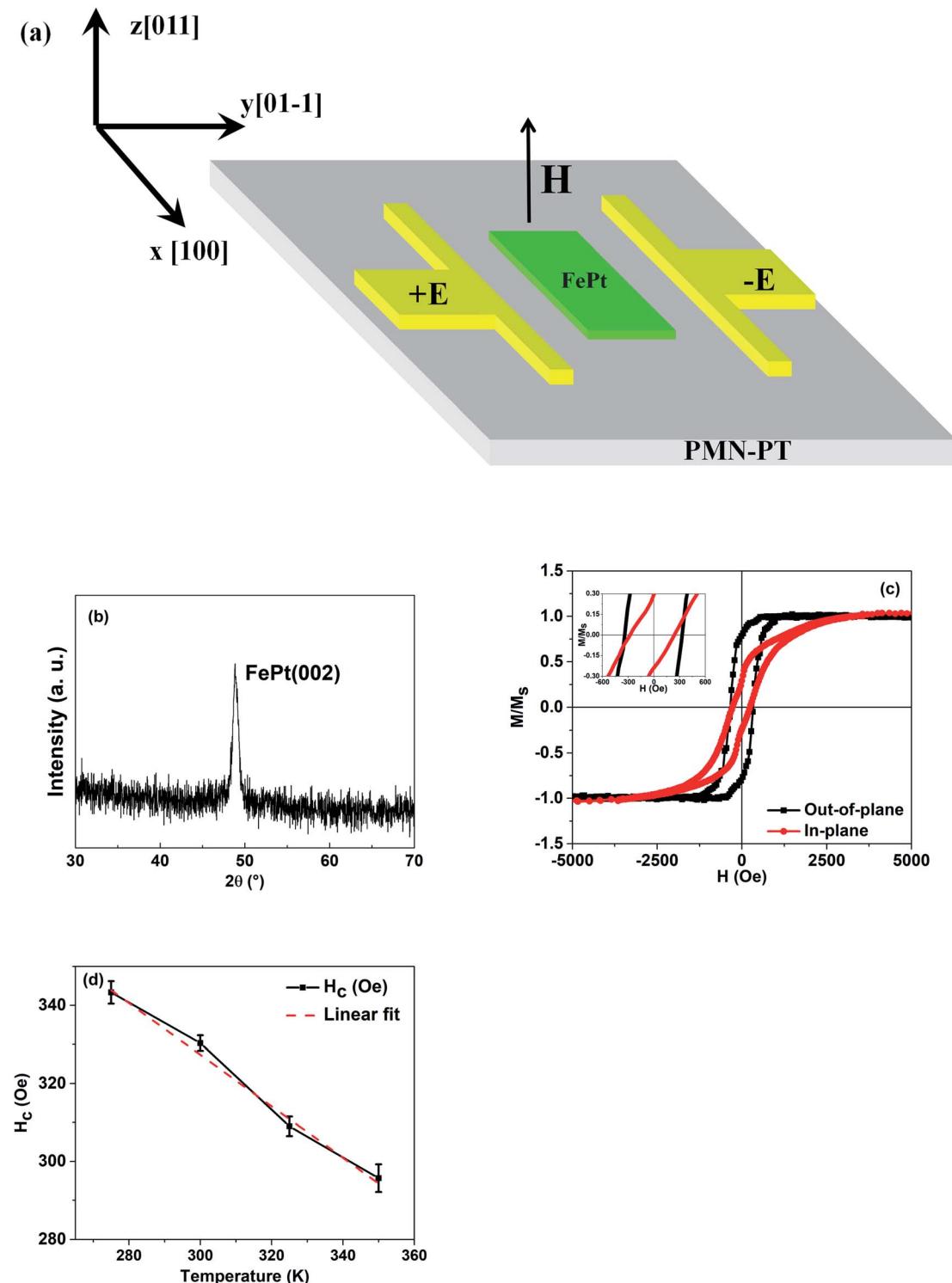


Fig. 1 (a) Schematic of the Hall bar used in this study. (b) The GIXRD pattern of FePt films deposited on the PMN-PT substrate. (c) In-plane and out-of-plane  $M-H$  loops of the PMN-PT/FePt heterostructure. The inset shows the enlarged  $M-H$  loops. (d) Out-of-plane coercivity as a function of varying temperatures.

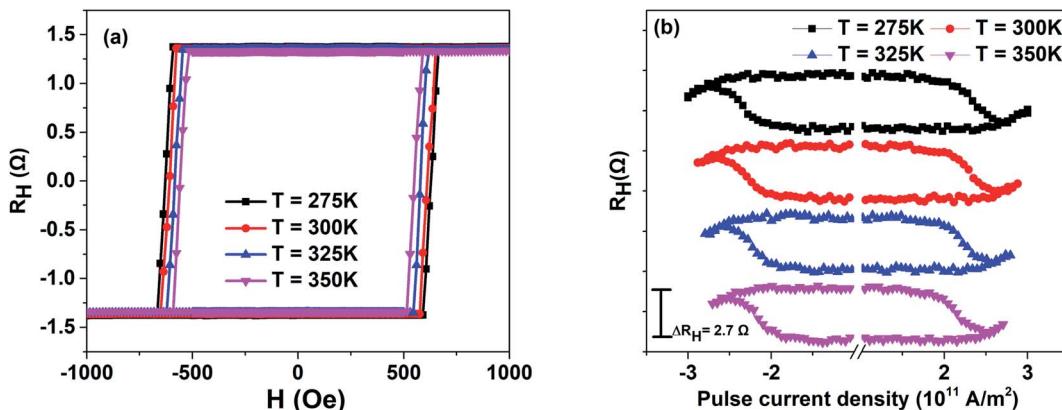


Fig. 2 (a)  $R_H$ - $H$  loops of  $L1_0$ -FePt films under different temperatures. (b)  $R_H$ - $I$  loops of  $L1_0$ -FePt films with  $H_x = 500$  Oe under different temperatures.

$R_H$ - $I$  loops were measured on a physical property measurement system (PPMS) with Keithley 6221, 2400 and 2182A.

## Results and discussion

The root mean square roughness value of the PMN-PT(011) substrate was measured by AFM, which is  $0.51\text{ nm}$  (Fig. S1, ESI†). High quality surface of the PMN-PT(011) substrate guarantees the strain transfer efficiency from PMN-PT(011) to

FePt films. The GIXRD pattern of the FePt films is shown in Fig. 1(b). The (002) peak of FePt can be observed at about  $48.9^\circ$ , which indicates the  $L1_0$  phase and the [001] orientation of the FePt films. Fig. 1(c) demonstrates the  $M$ - $H$  loops of FePt films at  $275\text{ K}$  and Fig. 1(d) displays the out-of-plane coercivity as a function of varying temperatures for FePt films. The coercivity of FePt films has an obvious change, which decreases from  $343\text{ Oe}$  to  $295\text{ Oe}$  with the increase in temperature. The reduction of coercivity results from both the increase in thermal fluctuation

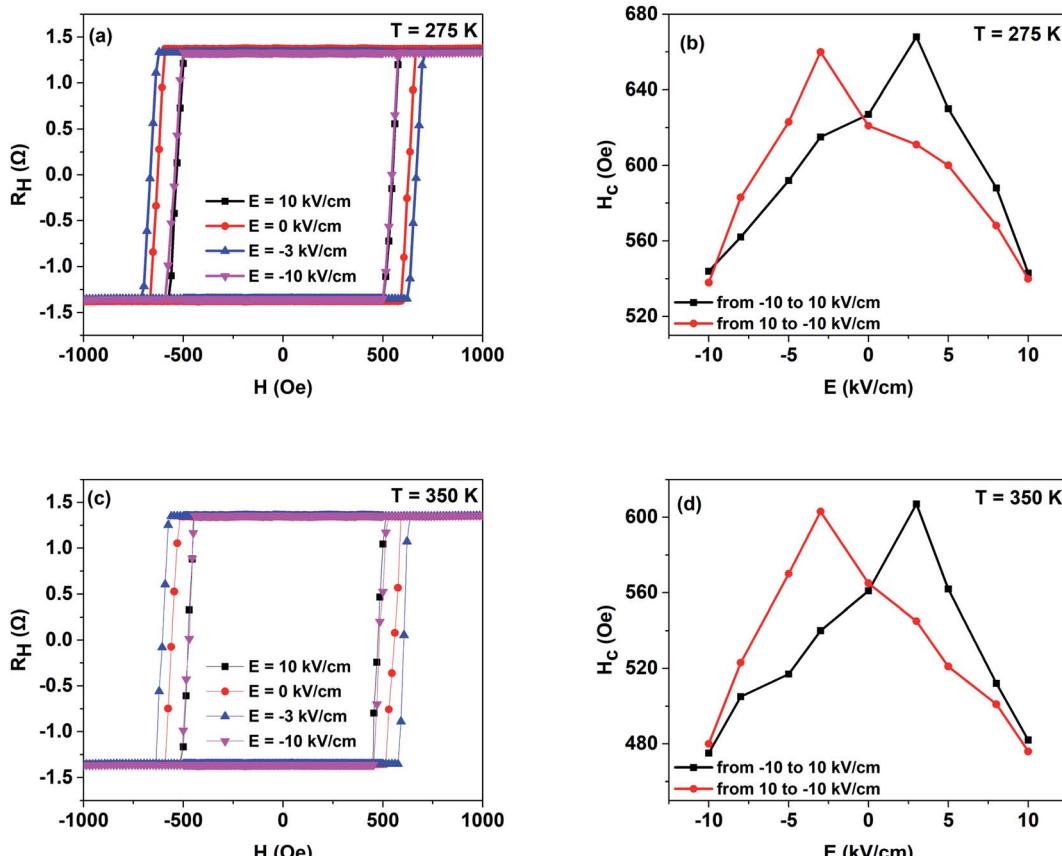


Fig. 3 (a)  $R_H$ - $H$  loops under varying  $E$ -fields at  $275\text{ K}$ . (b) Dependence of coercivity  $H_c$  on the applied  $E$ -field at  $275\text{ K}$ . (c)  $R_H$ - $H$  loops under varying  $E$ -fields at  $350\text{ K}$ . (d) Dependence of coercivity  $H_c$  on the applied  $E$ -field at  $350\text{ K}$ .

and decrease in magnetic anisotropy energy with an increase in temperature.<sup>19</sup> We can draw a conclusion that the L1<sub>0</sub>-FePt films are obtained.

For the sake of understanding the temperature assistance of PMA and SOT-based magnetization switching, the  $R_H$ - $H$  loops of L1<sub>0</sub>-FePt films under different temperatures were measured, as shown in Fig. 2(a). Rectangular  $R_H$ - $H$  loops reconfirm FePt films have strong PMA in the whole temperature range. The coercivity  $H_c$  of  $R_H$ - $H$  loops decreases monotonically while temperature increases from 275 K to 350 K, which is the same as the coercivity change of Fig. 1(c) and indicates weak PMA at high temperatures. It is noteworthy to notice that there is a slight reduction in the change of the anomalous Hall resistance  $\Delta R_H$  with an increase in temperature (Fig. S2, ESI†),  $\Delta R_H$  is the out-of-plane magnetization of L1<sub>0</sub>-FePt films,<sup>20</sup> which decreases with the increase in temperature due to the increasing of thermal fluctuation and decreasing of magnetic anisotropy energy.<sup>19</sup> Therefore, the corresponding  $\Delta R_H$  decreases with the increase in temperature. However, the temperature varies in a small range from 275 K to 350 K, which results in a slight reduction of  $\Delta R_H$ . For  $R_H$ - $I$  measurements, the external magnetic field  $H_x$  of 500 Oe and pulse current are applied along the [100] direction. The external magnetic field  $H_x$  is applied to overcome the Dzyaloshinskii–Moriya interaction (DMI) effective field  $H_{DMI}$ , which leads to current-induced magnetization switching.<sup>21,22</sup> The  $R_H$ - $I$  loops of L1<sub>0</sub>-FePt films under different temperatures are presented in Fig. 2(b). While

the temperature increases, the critical current density  $J_c$  reduces from  $2.35 \times 10^{11}$  A m<sup>-2</sup> to  $2.12 \times 10^{11}$  A m<sup>-2</sup>, which can be explained by formula (1):<sup>21</sup>

$$J_c = J_{c0} \left[ 1 - \frac{k_b T}{U} \ln \left( \frac{t_{pulse}}{\tau_0} \right) \right] \quad (1)$$

where  $J_c$  is the critical current density,  $J_{c0}$  is the zero thermal critical current density,  $U$  is the energy barrier between two magnetization states,  $k_b$  is the Boltzmann constant,  $T$  is the temperature,  $t_{pulse}$  is the pulse width,  $\tau_0 = 1$  ns. It is clear that the critical current density is inversely proportional to temperature.

To survey the temperature assistance of the E-field controlled PMA of PMN-PT/FePt heterostructures,  $R_H$ - $H$  loops under varying E-field at 275 K were obtained, as shown in Fig. 3(a). E-field generates an apparent change in coercivity and  $\Delta R_H$  keeps still. Dependence of coercivity  $H_c$  on the applied E-field at 275 K is summarized in Fig. 3(b). Coercivity  $H_c$  varies along a butterfly shape loop, which presents a coercivity  $H_c$  change of 22.2% from 540 Oe ( $E = 10$  kV cm<sup>-1</sup>) to 660 Oe ( $E = -3$  kV cm<sup>-1</sup>) and indicates E-field controls PMA of PMN-PT/FePt heterostructures reversibly at 275 K. PMA of L1<sub>0</sub>-FePt originates from both hybridization between Fe 3d and Pt 5d electrons and SOC.<sup>23</sup> According to the piezoelectric properties under E-field reported by Peng and Li,<sup>13,24</sup> when the E-field decreases from 10 kV cm<sup>-1</sup> to  $-10$  kV cm<sup>-1</sup>, L1<sub>0</sub>-FePt films suffer compressive strain along the [01-1] direction at  $E = -3$  kV cm<sup>-1</sup>.

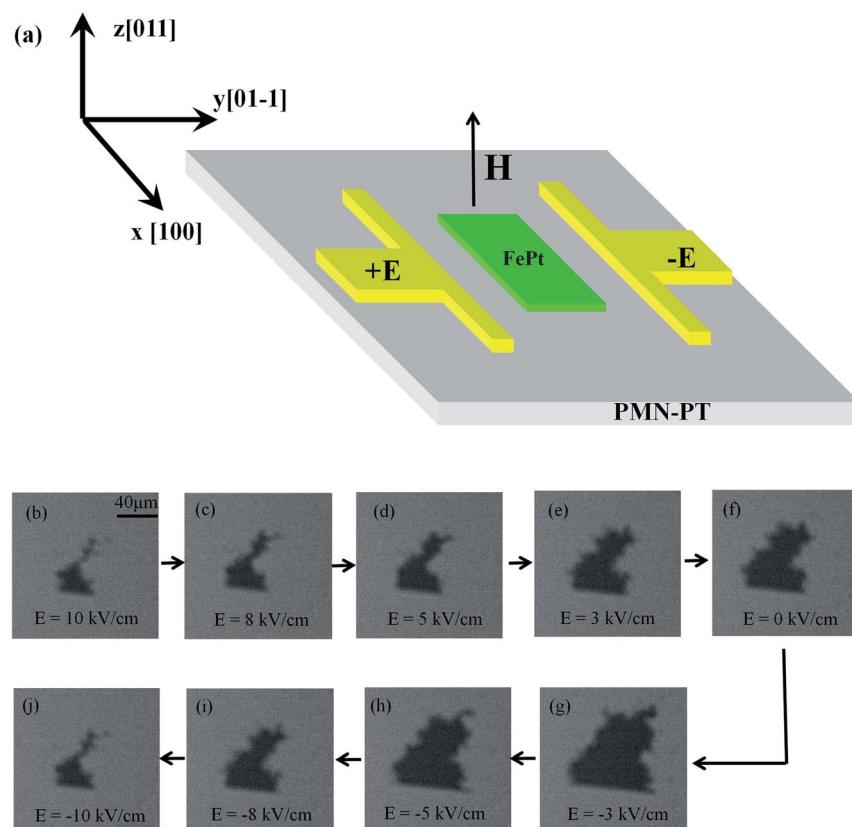


Fig. 4 (a) Schematic of the MOKE measurement. (b–j) present MOKE images of E-field controlled magnetization switching of the PMN-PT/FePt heterostructure. The white and black areas of MOKE images stand for the magnetization up and down, respectively.



Consequently,  $L1_0$ -FePt films suffer compressive strain along the [011] direction and tensile strain along the [100] at  $E = -3$  kV cm<sup>-1</sup>. The compressive strain along the [011] direction not only improves the chemical ordering parameter  $S$  of  $L1_0$ -FePt films, which results in stronger SOC, but also increases the hybridization between Fe 3d and Pt 5d.<sup>7,23,25,26</sup> As a result, PMA and coercivity  $H_c$  are enhanced at  $E = -3$  kV cm<sup>-1</sup>. Similarly,  $L1_0$ -FePt films suffer tensile strain at  $E = \pm 10$  kV cm<sup>-1</sup> along the [011] direction, which reduces the PMA and coercivity  $H_c$ . Then, Fig. 3(c) and (d) show the  $R_H$ - $H$  loops under varying E-field at 350 K and the dependence of coercivity  $H_c$  on applied E-field at 350 K, respectively. The coercivity  $H_c$  at 350 K also varies along a butterfly shape loop. However, compared with the change in coercivity  $H_c$  at 275 K, the coercivity  $H_c$  has a larger change of 32.3% from 476 Oe ( $E = 10$  kV cm<sup>-1</sup>) to 603 Oe ( $E = -3$  kV cm<sup>-1</sup>) at 350 K. Higher temperature enhances the piezoelectric coefficient of the PMN-PT(011) substrate and results in a large strain-induced effective field  $H_s$  under E-field, which is given by formula (2):<sup>27</sup>

$$H_s = \frac{3\lambda Y}{M_s(1+v)} E(d_{33} - d_{31}) \quad (2)$$

where  $M_s$  is the saturated magnetization (1000 emu cm<sup>-3</sup>),  $Y$  is the Young's modulus (180 GPa),  $v$  is the Poisson's ratio (0.3),  $E$  is the E-field,  $d_{33}$  and  $d_{31}$  is the piezoelectric coefficients, and  $\lambda$  is the saturation magnetostriction coefficient (34 ppm for  $L1_0$ -FePt films).<sup>28,29</sup> The  $d_{33}$  and  $d_{31}$  under different temperatures are given by Peng and Li,<sup>13,24</sup> and we set  $E = 10$  kV cm<sup>-1</sup>, and then the strain induced effective field  $H_s$  was calculated to be 999.47 Oe at 350 K, which is higher than  $H_s$  of 809.28 Oe at 275 K. Because of the large strain induced effective field  $H_s$  and weak PMA of  $L1_0$ -FePt films at 350 K,<sup>19</sup> coercivity  $H_c$  has a larger change, which reveals E-field has an improved regulating effect on PMA of PMN-PT/FePt heterostructures at higher temperature.

For verifying the E-field controlled PMA of PMN-PT/FePt heterostructures, we observe the magnetization switching of  $L1_0$ -FePt films under different E-fields directly by the MOKE microscope. Due to the restriction of the MOKE microscope, we can only observe the magnetization switching on rectangular

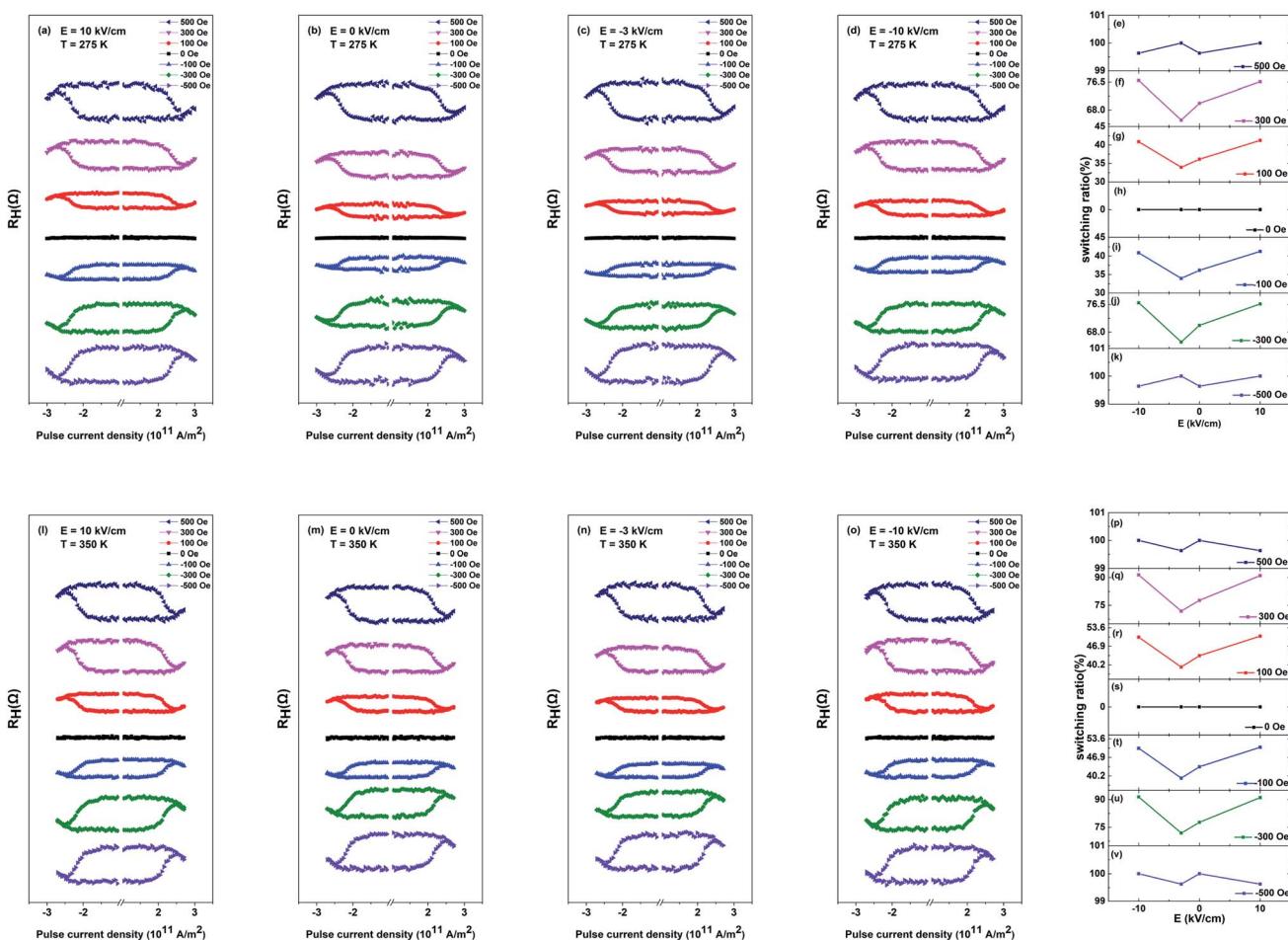


Fig. 5 (a–d)  $R_H$ - $I$  loops of  $L1_0$ -FePt films with different  $H_x$  under varying E-field ( $E = 10, 0, -3, -10$  kV cm<sup>-1</sup>) at 275 K, respectively. (e–k) The dependence of the magnetization switching ratio on the applied E-field with different  $H_x$  (500 Oe, 300 Oe, 100 Oe, 0 Oe, -100 Oe, -300 Oe, -500 Oe) at 275 K, respectively. (l–o)  $R_H$ - $I$  loops of  $L1_0$ -FePt films with different  $H_x$  under varying E-field ( $E = 10, 0, -3, -10$  kV cm<sup>-1</sup>) at 350 K, respectively. (p–v) The dependence of magnetization switching ratio on the applied E-field with different  $H_x$  (500 Oe, 300 Oe, 100 Oe, 0 Oe, -100 Oe, -300 Oe, -500 Oe) at 350 K, respectively.



$\text{L1}_0\text{-FePt}$  films instead of Hall bar at 300 K. The MOKE measurement is schematically shown in Fig. 4(a). During the measurement, a fixed magnetic field of 367 Oe with perpendicular direction is applied, where the magnetization begins to switch. Compared with other magnetic fields (Fig. S3, ESI†), the magnetic field of 367 Oe enables us to observe the electric field-controlled magnetization switching clearly. Fig. 4(b)–(j) present the MOKE images of E-field-controlled magnetization switching of  $\text{L1}_0\text{-FePt}$  films. The white and black areas of MOKE images stand for the magnetization up and down, respectively. With the E-field scanning from  $10 \text{ kV cm}^{-1}$  to  $-10 \text{ kV cm}^{-1}$ , the small black area first apparently expands to maximum and then reduces to the original state, the magnetization direction of which is opposite to external magnetic field. According to the discussion above, the  $\text{L1}_0\text{-FePt}$  films suffer the tensile strain at  $E = \pm 10 \text{ kV cm}^{-1}$  along the [011] direction, which reduces the PMA of  $\text{L1}_0\text{-FePt}$  films and makes the magnetization switch easily under the fixed magnetic field. Therefore, the area of magnetization down is small. The  $\text{L1}_0\text{-FePt}$  films suffer the compressive strain along the [011] direction at  $E = -3 \text{ kV cm}^{-1}$ . Compared with tensile strain, compressive strain exerts opposite effects on  $\text{L1}_0\text{-FePt}$  films, which enhances the PMA and expands the area of magnetization down. The magnetization switching observed by the MOKE microscope under different E-fields gives us a compelling evidence of the E-field-controlled PMA of PMN-PT/FePt heterostructures.

According to the discussion above, PMA of PMN-PT/FePt heterostructures can be manipulated more effectively by E-field at high temperatures. It is rational to explore temperature assistance of E-field-controlled SOT-based current induced magnetization switching of PMN-PT/FePt heterostructures. Fig. 5(a)–(d) show the  $R_H$ -I loops of  $\text{L1}_0\text{-FePt}$  films with different  $H_x$  under varying E-field at 275 K. The  $R_H$ -I loops with  $H_x$  of  $\pm 100$  Oe and  $\pm 300$  Oe show partial magnetization switching and  $R_H$ -I loops with  $H_x$  of  $\pm 500$  Oe show fully magnetization switching. When  $H_x$  is  $\pm 100$  Oe or  $\pm 300$  Oe,  $H_x < H_{\text{DMI}}$ , the external magnetic field  $H_x$  is not sufficient to overcome the DMI effective field  $H_{\text{DMI}}$ . Therefore, the current-induced magnetization cannot be switched totally. Fig. 5(e)–(k) summarize the dependence of the magnetization switching ratio on applied E-field with different  $H_x$  at 275 K. With the E-field scanning from  $10 \text{ kV cm}^{-1}$  to  $-10 \text{ kV cm}^{-1}$ , the magnetization switching ratio first decreases from 41.8% to 33.9% and then rises back to 41.2% and has a change of 21.5% with  $H_x$  of  $\pm 100$  Oe at 275 K, and magnetization switching ratio with  $H_x$  of  $\pm 300$  Oe at 275 K shows the same trend and has a change of 18.6%. However, magnetization switching ratio with  $H_x$  of  $\pm 500$  Oe at 275 K does not change under different E-fields, which indicates the effects of strain on magnetization can be ignored with  $H_x$  of  $\pm 500$  Oe. The compressive strain along the [011] direction at  $E = -3 \text{ kV cm}^{-1}$  enhances PMA, which results in difficult

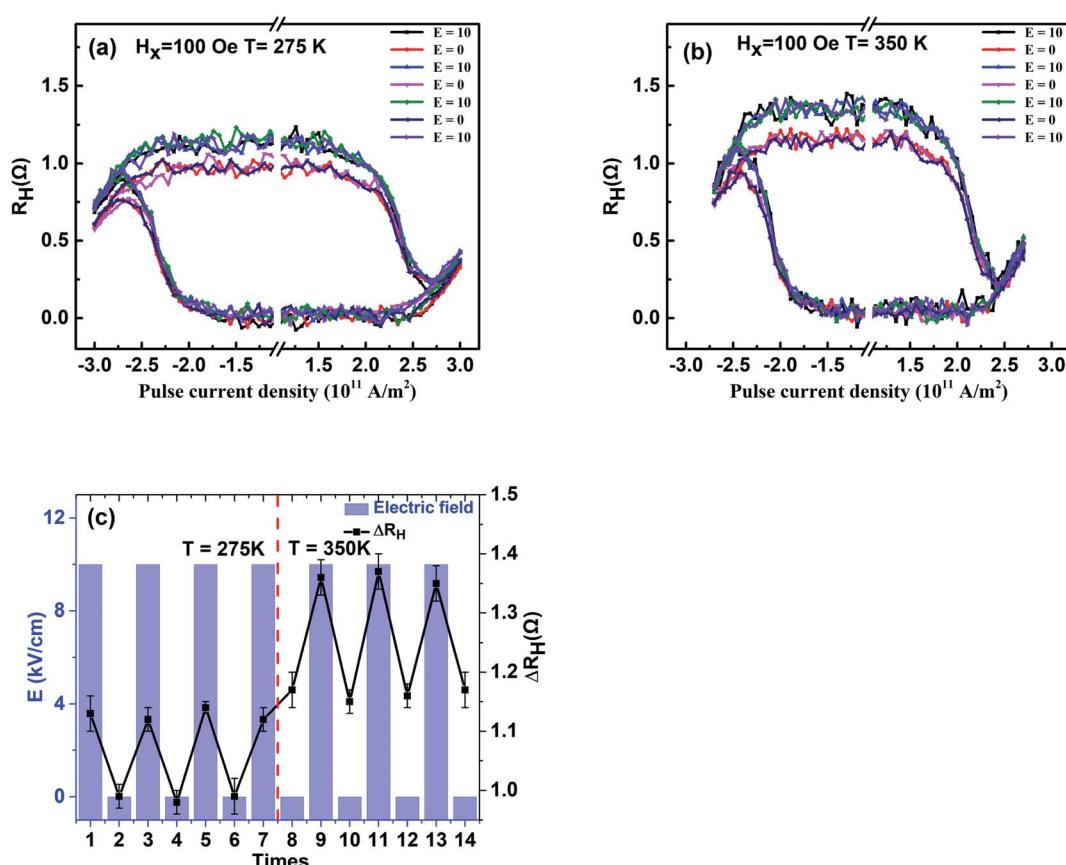


Fig. 6 (a) and (b) show the  $R_H$ -I curves under alternate E-field with  $H_x$  of 100 Oe at 275 K and 350 K, respectively. The unit of E is  $\text{kV cm}^{-1}$ . (c) Dependence of  $\Delta R_H$  on alternate E-field at 275 K and 350 K.



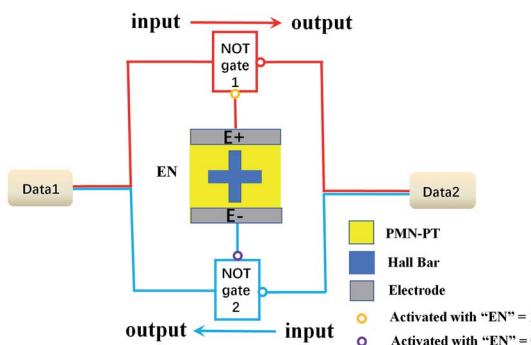


Fig. 7 Schematic designs of an SOT-based logical circuit composed by two NOT gates and an output control "EN", where the Hall bar is output control EN.

magnetization switching and a small magnetization switching ratio. The tensile strain at  $E = \pm 10 \text{ kV cm}^{-1}$  results in a large magnetization switching ratio. Fig. 5(l)–(o) show the  $R_H$ – $I$  loops of  $\text{L}_{10}\text{-FePt}$  films with different  $H_x$  under varying E-field at 350 K. Fig. 5(p)–(v) summarizes the dependence of the magnetization switching ratio on applied E-field with different  $H_x$  at 350 K. Compared with change in the magnetization switching ratio induced by E-field at 275 K, the magnetization switching ratio has an improved change of 28.2% with  $H_x$  of  $\pm 100$  Oe and an improved change of 27.2% with  $H_x$  of  $\pm 300$  Oe at 350 K under applied E-field, which is attributed to the large strain-induced effective field  $H_s$  and weak PMA of  $\text{L}_{10}\text{-FePt}$  films at 350 K. To check the stability of the Hall bar, Fig. 6(a) and (b) show the  $R_H$ – $I$  curves under alternate E-field with  $H_x$  of 100 Oe at 275 K and 300 K, respectively. Fig. 6(c) summarizes the dependence of  $\Delta R_H$  on alternate E-field with  $H_x$  of 100 Oe at 275 K and 300 K. The change of  $\Delta R_H$  is stable under alternate E-field at 275 K and 300 K, which suggests that the E-field modulated SOT-based current-induced magnetization switching of PMN-PT/FePt heterostructures is more effective and steady with small  $H_x$  at a high temperature.

An E-field controlled SOT-based logical circuit consists of two NOT gates and an output control "EN" is designed, which realize the bidirectional transmission of data, as shown in Fig. 7. Both Data1 and Data2 can be used as inputs or outputs. The Hall bar is regarded as the "EN", which is a switch for NOT gates. When "EN" = 1, the NOT gate 1 is activated and outputs of red circuit are consistent with the logic of NOT gate 1, while the NOT gate 2 is deactivated. Continuously, when "EN" = 0, the NOT gate 2 is activated and outputs of blue circuit are consistent with the logic relationship of NOT gate 2, and the NOT gate

Table 1 Truth table of an SOT-based logical circuit based on the  $R_H$ – $I$  loops shown in Fig. 6 and the design of Fig. 7, where D1 is Data1 and D2 is Data2. Data goes from input to output

EN = 1			EN = 0		
Input D1	1	0	Input D2	1	0
Output D2	0	1	Output D1	0	1

1 is deactivated. According to our studies mentioned above, when the  $H_x$  is 100 Oe and E-field is "on" ( $10 \text{ kV cm}^{-1}$ ),  $\Delta R_H$  of the Hall bar is  $1.13 \Omega$ , which stands for the high electrical level and "EN" = 1. With "EN" = 1, the NOT gate 1 is activated. The data is transmitted from left to right and we can get Data2 = −Data1. On the contrary, when the E-field is "off" ( $0 \text{ kV cm}^{-1}$ ),  $\Delta R_H$  of Hall bar is  $0.99 \Omega$ , which stands for the low electrical level and "EN" = 0. With "EN" = 0, the NOT gate 2 is activated. The data is transmitted from right to left and we can get Data1 = −Data2. Consequently, we summarize the outputs of the logical circuit, which depend on the inputs and "EN", as shown in Table 1. We realize the bidirectional transmission of data with the help of the PMN-PT/FePt heterostructure. An E-field controlled SOT-based logical circuit can be widely used in computer, digital control, communication, automation and instrument.

## Conclusions

In conclusion,  $\text{L}_{10}\text{-FePt}$  films were deposited on the PMN-PT(011) substrate. While the temperature increases, the coercivity  $H_c$  and critical current density  $J_c$  decrease monotonically because of the large strain-induced effective field  $H_s$  and weak PMA of  $\text{L}_{10}\text{-FePt}$  films at 350 K, E-field has an improved regulating effect on PMA- and SOT-based current-induced magnetization switching of PMN-PT/FePt heterostructures. Magnetization switching observed by an MOKE microscope confirms that PMA can be controlled by E-field. In addition, change in the anomalous Hall resistance  $\Delta R_H$  is modulated reversibly by alternate E-field under different temperatures, which enables us realize an E-field-controlled SOT-based logical circuit and the bidirectional transmission of data. These new discoveries offer us an avenue to manufacture potential spintronic devices and technologies by the E-field modulation of PMN-PT/FePt heterostructures at different temperatures.

## Author contributions

These authors contributed equally to this work.

## Conflicts of interest

There are no conflicts to declare.

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