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# Microstructure–mechanical properties of Ag<sup>0</sup>/Au<sup>0</sup> doped K–Mg–Al–Si–O–F glass-ceramics

Mrinmoy Garai, <sup>a</sup> Arianit A. Reka, <sup>b</sup> Basudeb Karmakar<sup>a</sup> and Atiar R. Molla<sup>a</sup>

In understanding the catalytic efficacy of silver (Ag<sup>0</sup>) and gold (Au<sup>0</sup>) nanoparticles (NPs) on glass-ceramic (GC) crystallization, the microstructure–machinability correlation of a SiO<sub>2</sub>–MgO–Al<sub>2</sub>O<sub>3</sub>–B<sub>2</sub>O<sub>3</sub>–K<sub>2</sub>O–MgF<sub>2</sub> system is studied. The thermal parameters viz., glass transition temperature (*T*<sub>g</sub>) and crystallization temperature (*T*<sub>c</sub>) were extensively changed by varying NPs (*in situ* or *ex situ*). *T*<sub>c</sub> was found to be increased (*T*<sub>c</sub> = 870–875 °C) by 90–110 °C when *ex situ* NPs were present in the glass system. Under controlled heat-treatment at 950 ± 10 °C, the glasses were converted into glass-ceramics with the predominant presence of crystalline phase (XRD) fluorophlogopite mica, [KMg<sub>3</sub>(AlSi<sub>3</sub>O<sub>10</sub>)F<sub>2</sub>]. Along with the secondary phase enstatite (MgSiO<sub>3</sub>), the presence of Ag and Au particles (FCC system) were identified by XRD. A microstructure containing spherical crystallite precipitates (~50–400 nm) has been observed through FESEM in *in situ* doped GCs. An *ex situ* Ag doped GC matrix composed of rock-like and plate-like crystallites mostly of size 1–3 μm ensured its superior machinability. Vicker's and Knoop microhardness of *in situ* doped GCs were estimated within the range 4.45–4.61 GPa which is reduced to 4.21–4.34 GPa in the *ex situ* Ag system. Machinability of GCs was found to be in the order, *ex situ* Ag > *ex situ* Au ~ *in situ* Ag > *in situ* Au. Thus, the *ex situ* Ag/Au doped SiO<sub>2</sub>–MgO–Al<sub>2</sub>O<sub>3</sub>–B<sub>2</sub>O<sub>3</sub>–K<sub>2</sub>O–MgF<sub>2</sub> GC has potential for use as a machinable glass-ceramic.

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## 1. Introduction

Fluormica glass-ceramics are polycrystalline materials containing a residual silicate (Si–O–Si) glass matrix with a dispersed crystalline phase.<sup>1–3</sup> They are considered machinable as they can be readily milled, drilled, turned or cut without resorting to diamond tipped tools.<sup>2–4</sup> The superior machinability of such fluormica glass-ceramics is due to their unique microstructure consisting of plate-like fluorophlogopite [KMg<sub>3</sub>(AlSi<sub>3</sub>O<sub>10</sub>)F<sub>2</sub>] crystals that impinge on one another.<sup>4,5</sup> This type of microstructure possesses enough capability to prevent fracture by offering preferential cleavage along the [001] crystalline plane.<sup>5,6</sup> Moreover, the layered structure of [KMg<sub>3</sub>(AlSi<sub>3</sub>O<sub>10</sub>)F<sub>2</sub>] crystallites allows easy splitting along the planes of the flat structural network, while splitting across the flat crystal network is hard due to the possibility of bending and shifting along the splitting planes.<sup>7,8</sup>

There is increasing interest in [KMg<sub>3</sub>(AlSi<sub>3</sub>O<sub>10</sub>)F<sub>2</sub>] based glass-ceramics for dental crowns, onlays and inlays, particularly with the widespread usage of CAD–CAM within dental surgery.<sup>9–12</sup> These applications using mica based glass-ceramics are directly dependent on their machinability which is strongly influenced by hardness of the GC.<sup>13,14</sup> The following equation<sup>14</sup>

indicates the relationship between Hardness (*H*) and machinability parameter (*m*):

$$m = 0.643 - 0.122H \quad (1)$$

The mechanical properties like microhardness of mica glass-ceramics are strongly affected by crystallite particle size, amount of precipitated mica crystals, their strength and volume fraction of the crystalline matrix.<sup>15–18</sup> Behraznia *et al.*<sup>14</sup> argued that machinability of mica glass-ceramics is widely varied with effective crystallinity which is a combining parameter of aspect ratio of crystals and the volume fraction.<sup>4</sup> They<sup>14</sup> explicated that, as the mica volume fraction increases there is a reducing need to have a high aspect ratio in order to achieve a high effective crystallinity. In case of lower volume fraction mica glass-ceramics, a high aspect ratio (>10) is required in order to achieve better machinability.<sup>4,5,14</sup> The commercial glass-ceramic Macor® possess the aspect ratio >20 and a relatively low crystal volume fraction.<sup>5,14</sup>

Thus, the microstructural parameters *i.e.* crystallinity, aspect ratio and volume fraction altogether control machinable properties of [KMg<sub>3</sub>(AlSi<sub>3</sub>O<sub>10</sub>)F<sub>2</sub>] glass-ceramics. Crystallization (or devitrification) in vitreous systems like SiO<sub>2</sub>–MgO–Al<sub>2</sub>O<sub>3</sub>–K<sub>2</sub>O–B<sub>2</sub>O<sub>3</sub>–F (with highly viscous nature) process is generally leaded by two kinetic processes: (i) phase separation by nucleation and growth and (ii) spinodal decomposition.<sup>1,7</sup> To obtain the fine-grained microstructures, it is essential to ensure that

<sup>a</sup>Specialty Glass Division, CSIR-Central Glass & Ceramic Research Institute (CGCRI), Kolkata, India. E-mail: mrinmoygarai@yahoo.in

<sup>b</sup>Department of Chemistry, Faculty of Natural Sciences and Mathematics, University of Tetova, Blvd Ilinden n. n., 1200 Tetovo, Republic of North Macedonia

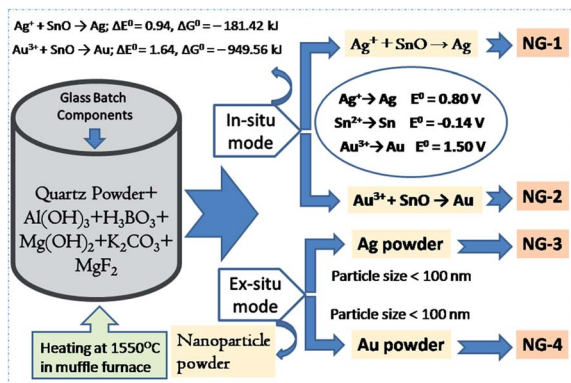



Fig. 1 Schematic diagram showing the synthesis of *in situ* and *ex situ* nanoparticle doped  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glasses.

maximum number of nuclei is formed which are homogeneously distributed throughout the glass matrix.<sup>7-9</sup> Thus, the crystallization can be induced to commence from abundant centers, so that the final product contains a large number smaller crystalline phases rather than a smaller number of relatively coarse grained crystallite particles.<sup>6-9</sup> The nucleation catalysts, selected by a critical prediction on the glass system, can greatly help in controlling the crystallization process and furthermore allows the glass-composition to be converted into desired glass-ceramics with desired crystallinity, aspect ratio and volume fraction.<sup>4,7</sup> The tuning of crystallization and microstructure in  $\text{SiO}_2\text{-MgO-Al}_2\text{O}_3\text{-K}_2\text{O}$  based glasses is extensively studied using several nucleating agents *viz.* (a) Metal oxides like  $\text{TiO}_2$ ,  $\text{ZrO}_2$ ,  $\text{CeO}_2$ ,  $\text{Nd}_2\text{O}_3$ ,  $\text{Sm}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{V}_2\text{O}_5$ ,  $\text{Nb}_2\text{O}_5$ ,  $\text{Ta}_2\text{O}_5$ ,  $\text{MoO}_3$ ,  $\text{WO}_3$ ,  $\text{Cr}_2\text{O}_3$ ,  $\text{Fe}_2\text{O}_3$  *etc.* (b) Metals like Ru, Rh, Pd, Os, Ir, Cu, Ag, Au, Pt, Mo, Ni, W *etc.* and (c) other compounds like  $\text{P}_2\text{O}_5$ ,  $\text{MgF}_2$ ,  $\text{CaF}_2$ , mixture of oxide like  $\text{V}_2\text{O}_5 + \text{MoO}_3$ ,  $\text{CaF}_2 + \text{MoO}_3$  *etc.*<sup>19-26</sup> However, the specific criteria for selecting the nucleating agent is mainly concerned for controlled crystallization so that they ensure high nucleation frequency uniformly distributed throughout the entire glass phase, uniform crystal size and smaller crystallite dimensions (usually only a few micrometers or nanometers) for desired mechanical properties, particularly the machinability.<sup>21,22</sup> The metals like copper (Cu), silver (Ag), gold (Au), platinum (Pt), molybdenum (Mo), tungsten (W) *etc.* are relatively insoluble in

silicate (Si-O-Si) glass and thus the heterogeneous nucleating sites are contentedly initiated by addition of a small amount of such metals.<sup>21,25,26</sup> Stookey<sup>21</sup> reported those metallic colloidal particles precipitated within the glass matrix, as nucleation sites for phase separation to initiate controlled crystallization followed by growth of various types of crystalline phases within the glass body.<sup>27</sup> Maeda and his co-author<sup>27</sup> investigated the effects of molybdenum and tungsten oxides on crystallization behavior of  $\text{MgO-Al}_2\text{O}_3\text{-SiO}_2$  glass. As they<sup>27</sup> pointed out, some fraction of  $\text{MoO}_3$  and  $\text{WO}_3$  was reduced to the metallic NPs (precipitating as small particles) by reacting with the carbon or reducing atmosphere during melting (at 1550 °C); and those nanoparticle provided heterogeneous nucleating sites for initiating the crystallization.

The present work is focused on study of influence of Ag- and Au-NPs on the crystallization of fluorophlogopite ( $\text{KMg}_3\text{AlSi}_3\text{O}_{10}\text{F}_2$ ) mica glass-ceramics. The effectiveness of NPs in their doping mechanism *i.e.* *ex situ* or *in situ* mode in  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glass is established by comparing their mechanical properties, with special reference to machinability of the glass-ceramics. The microstructure-property correlations have been done to understand the influence of Ag and Au NPs on crystallization and mechanical properties of Si-O-Si/B/Al glass-ceramics.

## 2. Materials and methods

### 2.1 Thermodynamic consideration on nanoparticle doping in glass

In order to synthesize the *in situ* Ag- and Au-nanoparticle (NP) doped glasses (NG-1 & NG-2, Fig. 1),  $\text{AgNO}_3$  (source of  $\text{Ag}^+$ ) and  $\text{HAuCl}_4$  (source of  $\text{Au}^{3+}$ ) were added as precursor for Ag and Au, respectively in  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  composition (Table 1). SnO was added as the reducing agent for  $\text{Ag}^+ \rightarrow \text{Ag}$  and  $\text{Au}^{3+} \rightarrow \text{Au}$  conversion (Fig. 1). The way of the redox reactions is different in glasses solely doped with a polyvalent element (like  $\text{Sn}^{2+}$ ) and co-doped with a second polyvalent element (like  $\text{Sn}^{4+}$ ) due to the mutual interaction between the two polyvalent elements during heating and cooling. The  $\text{Sn}^{2+}$  ions has common tendency to be converted into  $\text{Sn}^{4+}$  ions because the  $\text{Sn}^{4+}$  oxidation state (full-filled electronic configuration) is more stable than  $\text{Sn}^{2+}$ .

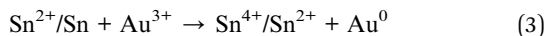
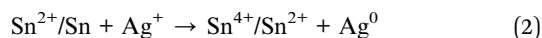
In present case, 0.3 wt% SnO was added into  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  composition. During initial heating (in melting), SnO was disproportionated into  $\text{Sn}^0$  and  $\text{Sn}^{4+}$  ions.

Table 1 Raw materials and corresponding purity for synthesizing the nanoparticle doped  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glasses

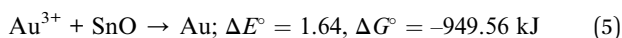
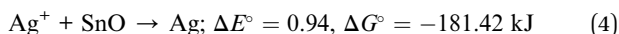
Glass component	Precursor material	Purity (%)	Source/company
$\text{SiO}_2$	Quartz powder	99.8	Sipur A1 Bremtheler Quarzitwerk, Usingen, Germany
$\text{Al}_2\text{O}_3$	$\text{Al(OH)}_3$	97	Loba Chemie, India
MgO	$\text{Mg(OH)}_2$	97	Loba Chemie, India
$\text{K}_2\text{O}$	$\text{K}_2\text{CO}_3$	98	Loba Chemie, India
$\text{B}_2\text{O}_3$	$\text{H}_3\text{BO}_3$	99.5	Loba Chemie, India
$\text{MgF}_2$	$\text{MgF}_2$	99.9	Loba Chemie, India
SnO	SnO	99.9	Alfa Aesar, India
<i>In situ</i> Ag	$\text{AgNO}_3$	99.9	Exceller, Qualigens fine Chemicals, India
<i>In situ</i> Au	$\text{HAuCl}_4 \cdot x\text{H}_2\text{O}$	49% Au	Loba Chemie, India
<i>Ex situ</i> Ag	Ag powder size <100 nm	99.5	Sigma-Aldrich fine Chemicals, India
<i>Ex situ</i> Au	Au powder size <100 nm	99.9	Sigma-Aldrich fine Chemicals, India



Reduction of  $\text{Ag}^+$  into Ag and  $\text{Au}^{3+}$  into Au were then happened during final heating to cooling time through the following mechanism:



The free energy change ( $\Delta G^\circ$ ) for those reductions is calculated from respective cell potential ( $\Delta E^\circ$ ).<sup>22</sup>



For a reaction to occur spontaneously, the free energy change ( $\Delta G^\circ$ ) should be negative. From the above two eqn (4) and (5), it is seen that  $\Delta G^\circ$  value for reduction of silver ( $\text{Ag}^+ \rightarrow \text{Ag}$ ) and gold ( $\text{Au}^{3+} \rightarrow \text{Au}$ ) is strongly negative. In this way the *in situ* NPs were doped in  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass.

For *ex situ* nanoparticle doping (NG-3 & NG-4), the Ag- and Au-nanometal powder (particle size <100 nm) were directly mixed (Fig. 1) into  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass batch mixture (Table 1).

## 2.2 Melt-quenching of glasses

About 100 g raw materials were used (details about raw materials presented in Table 1), for synthesis of various nanoparticle doped precursor glasses (*i.e.* NG-1 to NG-4) based on the component system  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  (composition shown in Table 2), were weighed, thoroughly mixed and melted in a platinum (Pt) crucible at  $1550 (\pm 10)^\circ\text{C}$  for 2 h with intermittent stirring for 15 s using a silica glass rod. Finally, each glass melt was poured onto a pre-heated steel mold to obtain the quenched glass block. Fig. 1 depicts the schematic diagram for synthesis of nanoparticle doped glasses. The quenched NG glass blocks were annealed in a muffle furnace at  $620 (\pm 10)^\circ\text{C}$  for 2 h to remove the internal thermal stresses developed in the glass followed by natural cooling to room temperature.

## 2.3 Controlled crystallization

The as-annealed  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glasses were cut into pieces for necessary characterizations as well as heat-treatment for crystallization. The glass pieces were allowed to heat-treatment at temperature  $950 (\pm 10)^\circ\text{C}$  for  $\sim 4$  h duration so that sufficient time is attained for crystallization. The as-annealed and heat-treated glass blocks were cut, grinded on

silicon carbide and polished with cerium oxide powders into required dimensions to carry out the necessary characterizations.

## 2.4 Characterization of glasses and glass-ceramics

In order to estimate the glass transition temperature ( $T_g$ ) and crystallization temperature ( $T_c$ ), differential scanning calorimetry (DSC) experiment using precursor  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass powders (particle size < 60  $\mu\text{m}$ ) was carried out in the temperature range  $30\text{--}1200^\circ\text{C}$  in nitrogen atmosphere at heating rate  $20^\circ\text{C min}^{-1}$  with a NETZSCH instrument (Model STA 449 Jupiter F3, NETZSCH-Gerätebau GmbH, Selb, Germany).

The densities ( $\rho$ ) of the glass samples were determined by the standard Archimedes principle. The measurements were done using single pan balance and distilled water ( $\text{H}_2\text{O}$ ) as an immersion liquid. The density ( $\rho$ ) was obtained from the relation:

$$\rho = \frac{ad}{(a-b)} \quad (6)$$

where 'a' is the weight of the glass sample in air, 'b' is the weight of the glass sample when suspended in distilled water (considering density of water,  $d = 0.997604 \text{ g cm}^{-3}$  at  $25^\circ\text{C}$ ).

The X-ray diffraction (XRD) of the glasses and heat-treated glass-ceramics were investigated using an XPERTPRO MPD diffractometer (PANalytical, Almelo, Netherlands) operating with Ni-filtered  $\text{CuK}\alpha$  ( $\lambda = 1.5406 \text{ \AA}$ ) radiation as the X-ray source irradiated at 40 kV and 40 mA. The scan range was  $5^\circ\text{--}90^\circ$  with a step size of  $0.05^\circ$  at room temperature ( $\sim 25^\circ\text{C}$ ).

The crystallization characteristics and microstructural morphology of  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass-ceramics was examined with a field-emission scanning electron microscope (FESEM model S430i, LEO, CEA, USA). Prior to the FESEM investigations, the glass-ceramic samples were polished and chemically etched by immersion into 2 vol% aqueous HF solution for 7 min. To dictate the existing elements (K, Mg, Al, Si, O and F) in the glass-ceramic matrix, qualitative elemental composition analysis was performed using energy dispersive X-ray (EDX) analysis using the EDX detector attached with FESEM microscope.

The micro hardness of all the polished  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass-ceramics were determined using micro indentation hardness testing systems (Clemex CMT, Longueuil, Canada) equipped with a conical Vickers indenter. Average of ten indentations was taken for each sample applying 200 gf load for dwell time = 5 s. The diagonals of the different indents were measured using the optical microscope attached with the instrument and consequently the hardness values were calculated using the standard eqn (7) and (8) for the Vickers and Knoop geometries respectively.

$$H_V = \frac{1.854P}{d^2} \quad (7)$$

$$H_K = \frac{1.854P}{C_p L^2} \quad (8)$$

**Table 2** Composition (wt%) of different precursor nanoparticle doped  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glasses

Glass	$\text{SiO}_2$	$\text{Al}_2\text{O}_3$	MgO	$\text{K}_2\text{O}$	$\text{B}_2\text{O}_3$	$\text{MgF}_2$	SnO	Excess
NG-1	39	16	12	10	11	12	0.3	Ag = 0.2 ( <i>in situ</i> )
NG-2	39	16	12	10	11	12	0.3	Au = 0.2 ( <i>in situ</i> )
NG-3	39	16	12	10	11	12	—	Ag = 0.2 ( <i>ex situ</i> )
NG-4	39	16	12	10	11	12	—	Au = 0.2 ( <i>ex situ</i> )



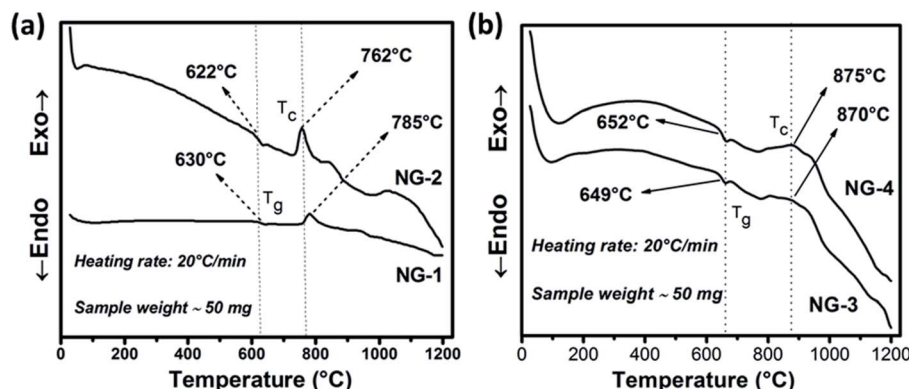


Fig. 2 DSC curves of *in situ* (a) and *ex situ* (b) Ag/Au nanoparticle doped  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glasses.

Table 3 DSC thermal properties ( $^{\circ}\text{C}$ ) of different precursor nanoparticle doped  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glasses<sup>a</sup>

Glass	$T_g$	$T_x$	$T_c$
NG-1	$630 \pm 2$	$748 \pm 2$	$785 \pm 2$
NG-2	$622 \pm 2$	$732 \pm 2$	$762 \pm 2$
NG-3	$649 \pm 2$	$780 \pm 2$	$870 \pm 2$
NG-4	$652 \pm 2$	$763 \pm 2$	$875 \pm 2$

<sup>a</sup>  $T_g$  = glass transition temperature;  $T_x$  = crystallization onset temperature;  $T_c$  = crystallization temperature.

where,  $H_V$  and  $H_K$  are the Vickers and Knoop hardness numbers in  $\text{kg mm}^{-2}$ .  $P$  is the normal load in kg,  $d$  is the average diagonal length of the indentation in mm,  $L$  is length of indentation along its long axis and  $C_p$  is the correction factor related to the shape of the indenter ( $=0.070279$ ). Here, the hardness value obtained/ $100.1$  = hardness ( $H$ ) in GPa. The machinability parameter ( $m$ ) was determined using the eqn (1) i.e.  $m = 0.643 - 0.122H$ .<sup>14</sup> The machinability parameter ' $m$ ' is important to characterize the machinable mica glass-ceramics.

### 3. Results and discussion

#### 3.1. DSC thermal properties of $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$ glasses

Controlled heat-treatment facilitated the glass to glass-ceramic phase transformation with containing the desired crystalline phase. From differential scanning calorimetry (DSC) experiment the optimum heat-treatment temperature was selected. The DSC thermograms of the investigated nanoparticle doped  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glasses are shown in Fig. 2. Glass transition ( $T_g$ ) temperature is the characteristic feature of the first endothermic minima in DSC thermogram whereas the exothermic peaks correspond to the crystallization temperatures ( $T_c$ ). As is evident from Fig. 2a, in the DSC thermogram of NG-1 glass, a slight endothermic peak is started to at  $\sim 617^{\circ}\text{C}$  and ends at  $\sim 645^{\circ}\text{C}$ . For the other glasses containing *in situ* generated Au (NG-2 in Fig. 2a), *ex situ* doped Ag (NG-3 in Fig. 2b) and *ex situ* doped Au (NG-4 in Fig. 2b); the first endothermic peak starts to appear at about  $\sim 628$ ,  $\sim 644$  and  $\sim 642^{\circ}\text{C}$  and reached the bottom at approximately  $\sim 638$ ,  $\sim 668$  and  $\sim 665^{\circ}\text{C}$ , respectively. From the onset of endothermic hump  $T_g$  value was estimated  $630 \pm 2$  and  $622 \pm 2^{\circ}\text{C}$  for NG-1 and NG-2 glasses, respectively. As is seen from Table 3,  $T_g$  value increased in NG-3

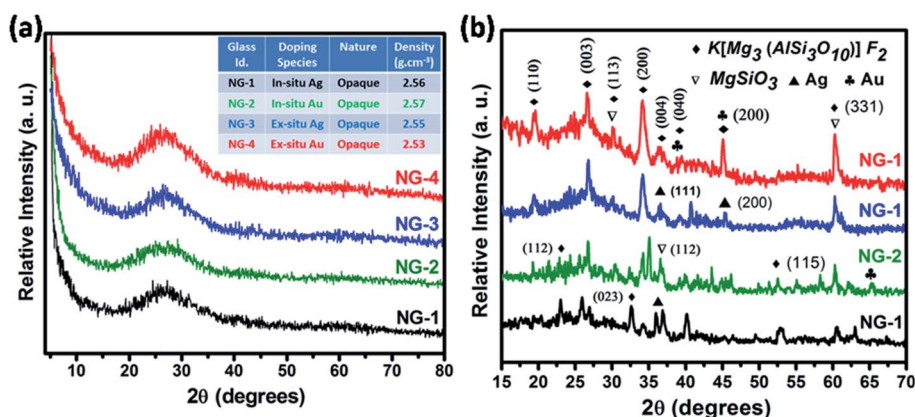


Fig. 3 X-ray diffraction (XRD) pattern of (a)  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glasses and (b) corresponding glass-ceramics heat-treated at  $950^{\circ}\text{C}$ .

and NG-4 glasses because of more stable glass network in presence of *ex situ* doped Ag and Au nanoparticles.

The exothermic peak starts to appear in the DSC thermogram (Fig. 1a), at  $\sim 748$  and  $\sim 732$  °C ( $T_x$ ) for NG-1 and NG-2 glasses, respectively, indicating onset of crystallization. For *ex situ* coinage nanometal doped glasses *i.e.*, NG-3 and NG-4, this exotherm is started at  $\sim 780$  and  $\sim 763$  °C ( $T_x$ ), respectively. Difference between the  $T_x$  and  $T_g$  describe thermal stability (TS) of glass phase.<sup>20–23</sup>

$$TS = T_x - T_g \quad (9)$$

For NG-1, NG-2, NG-3 and NG-4 glasses, TS is calculated as 111, 110, 131 and 114 °C, respectively. Such TS value is rather low for a glass to be thermally stable, also it indicates that the nucleation and growth process may be initiated well before the crystallization peaks obtained in DSC studies. Ag-Being the 4d transition metal has lower atomic size than Au-(5d) and hence it can accommodate itself in the glass matrix more comfortably. So, the glass stability of NG-1 and NG-3 glasses (*in situ* and *ex situ* silver) is more than that of NG-2 and NG-4 glasses (*in situ* and *ex situ* gold). For NG-1, NG-2, NG-3 and NG-4 glasses, the

first exothermic peak *i.e.*  $T_c$  (Fig. 2) is observed at 785, 762, 870 and 875 °C, respectively. So, the primary crystallization temperature increased  $\sim 80$ – $110$  °C on doping of *ex situ* silver and gold nanoparticle instead of *in situ* generated silver and gold (Table 2). Moreover, the first exothermic peak obtained NG-1 and NG-2 glasses is sharper than that of NG-2/NG-3 glasses that signifies that *in situ* nanoparticles doped glass-ceramics are formed because of either single-phase crystallization or an almost simultaneous precipitation of different crystalline phases after heat treatment.

### 3.2 Crystalline phases in $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$ glass-ceramics

The glassy nature of precursor glasses and crystalline nature of corresponding glass-ceramics after heat-treatment at 950 °C was identified by XRD study depicted in Fig. 3. No crystalline phase developed in melt-quenched (1550 °C)  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass was confirmed from Fig. 3a. As provided in the inset of Fig. 3a, the density of nanoparticle doped glasses have been found 2.53–2.57 g cm<sup>−3</sup>. The XRD pattern of GCs heat-treated at 950 °C is presented in Fig. 3b. Three major

Table 4 XRD peaks and corresponding planes of different crystalline phases developed in studied machineable glass-ceramic

Peak position (2 $\theta$ ) (degree)	Corresponding planes	Crystalline phase (chemical formula)	JCPDS file no.
19.4, 23.3, 26.6, 30.3, 32.7, 34.3, 36.6, 39.3, 45.1, 52.5, 60.5, 62.9	(110), (112), (003), (113), (023), (200), (004), (040), (111), (115), (331), (261)	Fluorophlogopite ( $\text{KMg}_3\text{AlSi}_3\text{O}_{10}\text{F}_2$ )	71-1542
30.1, 36.7, 60.4	(321), (112), (650)	Enstatite ( $\text{MgSiO}_3$ )	83-2057
36.5, 44.8, 64.7	(111), (200), (220)	Silver particle (Ag)	01-1164
38.8, 45.1, 65.2	(111), (200), (220)	Gold particle (Au)	02-1095

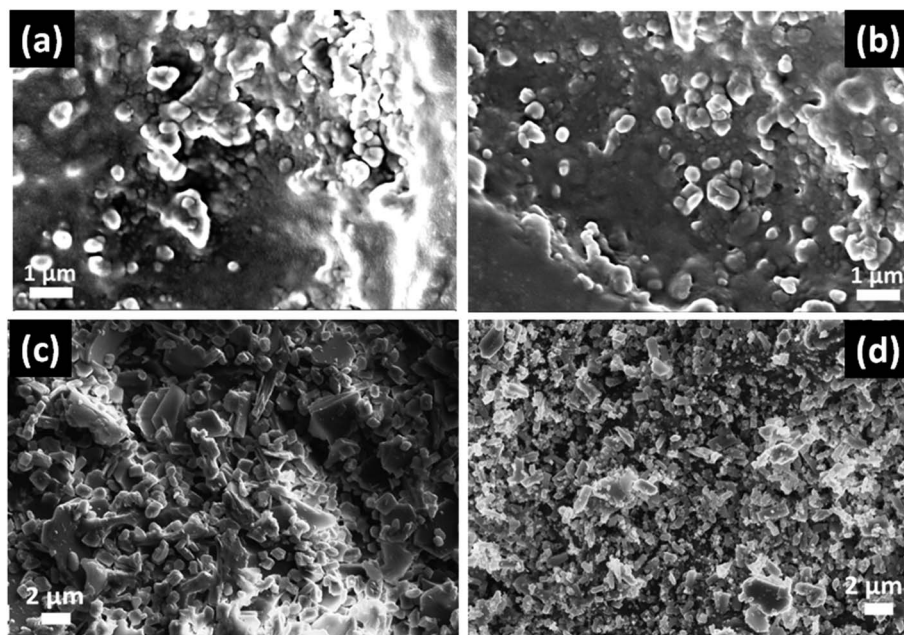


Fig. 4 FESEM photomicrograph of (a) NG-1, (b) NG-2, (c) NG-3 and (d) NG-4 glass-ceramics heat-treated at 950 °C ( $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  samples polished and chemically etched by 2 vol% aqueous HF solution for 7 min).



crystalline peaks appeared at  $(2\theta) \sim 26.6^\circ$ ,  $32.7^\circ$  and  $60.5^\circ$  is almost similar for NG-1 to NG-4 glass-ceramics. As summarized in Table 4, that three major peaks correspond to the crystalline planes (003), (023) and (331) of fluorophlogopite mica  $[\text{KMg}_3(\text{AlSi}_3\text{O}_{10})\text{F}_2]$ , JCPDS file number 71-1542 (molecular weight = 421.24, monoclinic system (end-centered) with lattice parameter:  $a = 5.299$ ,  $b = 9.188$  and  $c = 10.13$ ). Other crystalline planes *i.e.* (110), (112), (113), (200), (004), (040), (111), (115) and (261) indexed at  $(2\theta)$   $19.4^\circ$ ,  $23.3^\circ$ ,  $30.3^\circ$ ,  $34.3^\circ$ ,  $36.6^\circ$ ,  $39.3^\circ$ ,  $45.1^\circ$ ,  $52.5^\circ$  and  $62.9^\circ$  are also observed due to the formation of fluorophlogopite phase where large 12-coordinated  $\text{K}^+$  ions are electrovalent bonded with strongly bound alumino-silicate sheets  $[\text{Mg}_3(\text{AlSi}_3\text{O}_{10})\text{F}_2]^-$ . From Fig. 3b it is clearly observed that more intense crystalline planes for fluorophlogopite are obtained in NG-3 and NG-4 glass-ceramics, and that is attributed to the presence of *ex situ* doped nanoparticles. Efficient nucleation by heterogeneous phase

separation with the aid of such metallic nuclei was first achieved by Stookey<sup>21</sup> in precipitating the metallic nuclei throughout the glass. Since those metals are relatively insoluble in silicate (Si–O–Si) glass, heterogeneous nucleating sites are contentedly initiated by addition of a small amount of the metal.<sup>21,26,27</sup> In the studied  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass the Ag- and Au-nanoparticles catalyzed the formation of  $[\text{KMg}_3(\text{AlSi}_3\text{O}_{10})\text{F}_2]$  during the heat-treatment. However, a secondary crystalline phase was identified by the XRD peaks positioned at  $(2\theta)$   $30.1^\circ$ ,  $36.7^\circ$  and  $60.4^\circ$  corresponding to (321), (112) and (650), respectively for the development of enstatite ( $\text{MgSiO}_3$ ), JCPDS file no. 83-2057 (orthorhombic, primitive).

In the XRD pattern of mica based glass-ceramics, the presence of several overlapping peaks becomes difficult to determine because of their low intensity.<sup>23,24</sup> In the glass-ceramics heat-treated at  $950^\circ\text{C}$ , the presence of Ag- and Au-

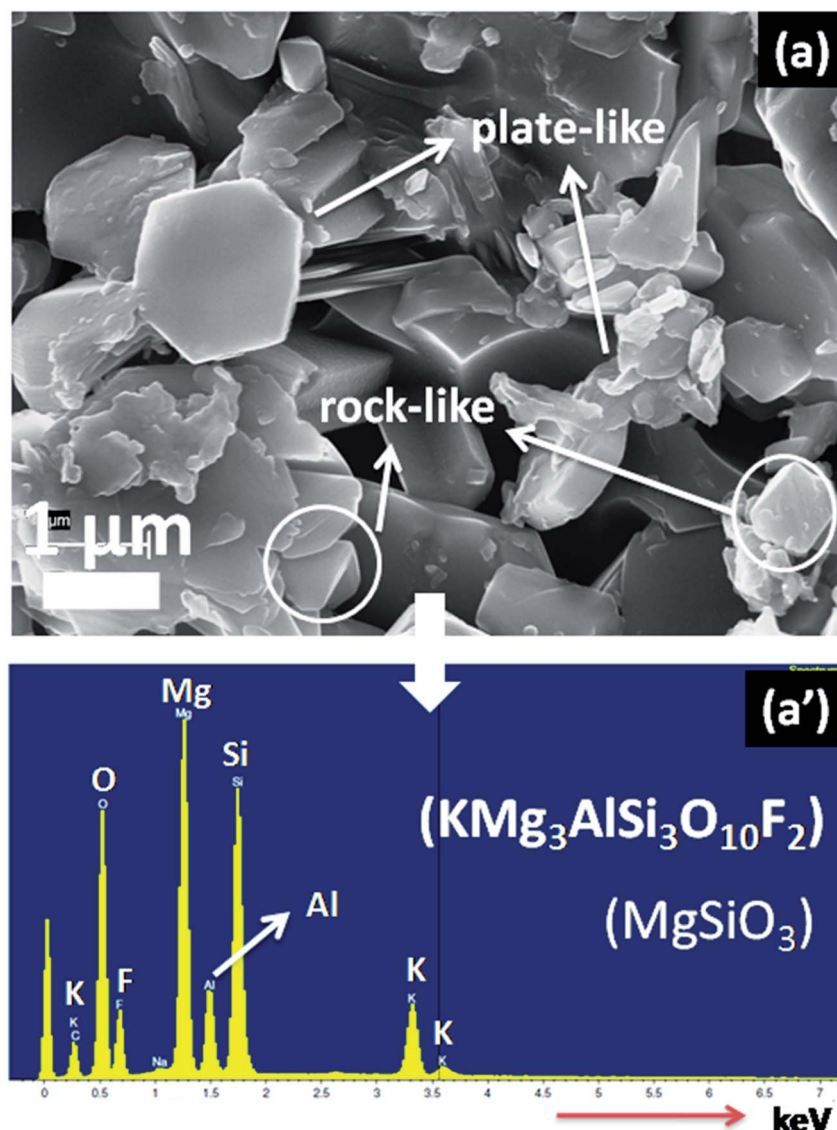


Fig. 5 Representative FESEM photomicrograph (a) and EDX pattern (a') of *ex situ* Ag-doped  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass-ceramic (NG-3) heat-treated at  $950^\circ\text{C}$  (sample is polished and chemically etched by 2 vol% aqueous HF solution for 7 min).



nanoparticles were also identified by XRD study. As seen from Fig. 3b, the Ag-nanoparticle has been identified at the characteristic peaks ( $2\theta$ ) of  $36.5^\circ$  and  $44.8^\circ$  corresponding to (111) and (200) and (220) planes (JCPDS file no. 01-1164, face centered cubic, lattice parameter  $a = 4.079$ ). The presence of Au-nanoparticle was identified at the peak positions ( $2\theta$ ) of  $38.8^\circ$ ,  $45.1^\circ$  and  $65.2^\circ$  corresponding to (111), (200) and (220) crystalline planes; JCPDS file number 02-1095, face centered cubic lattice, lattice parameter  $a = 4.068$ . Fig. 3b clearly shows the crystalline peaks corresponding to fluorophlogopite formation in NG-3 & NG-4 is more intensified compare to NG-1 & NG-2. This is due to the catalytic activity of Ag- and Au-particles as their lattice parameter is closely matched (within  $\pm 15\%$ ) with that of fluorophlogopite phase.

### 3.3 Morphology in $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$ glass-ceramics

In Fig. 4, the FESEM morphology of HF-etched surface of the  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glass-ceramics heat-treated at  $950^\circ\text{C}$  are shown. Fig. 4a and b represents the microstructure of NG-1 and NG-2 glass-ceramics which contains *in situ* generated nanoparticles whereas Fig. 4c and d depicts the microstructure of *ex situ* nanoparticle doped glass-ceramics. The crystallite particles randomly dispersed in all these microstructures are identified as fluorophlogopite mica [ $\text{KMg}_3(\text{AlSi}_3\text{O}_{10})\text{F}_2$ ] and enstatite ( $\text{MgSiO}_3$ ) by XRD study. This is furthermore confirmed from EDX pattern presented in Fig. 5. Spherical shaped crystallite particles (size  $\sim 100\text{--}500\text{ nm}$ ) are predominated in NG-1 and NG-2 glass-ceramics and those possess density value  $\sim 2.59$

and  $\sim 2.61\text{ g cm}^{-3}$ , respectively. As seen from Fig. 4c, the rock-like and plate-like crystallites are evenly distributed throughout the NG-3 glass-ceramic matrix to develop a compact microstructure. It can be seen that the rock-like particles mostly of nano size ( $\sim 300\text{--}700\text{ nm}$ ) are positioned (Fig. 4c) in fitted places between the plate shaped and card shaped crystallites of size range  $\sim 1\text{--}3\text{ }\mu\text{m}$  (Fig. 5a). Density of this glass-ceramic was estimated  $\sim 2.60\text{ g cm}^{-3}$ . The morphology of NG-4 glass-ceramic is very unique compare to other nanoparticle doped glass-ceramics. As is visual from Fig. 4d, various sized rock-like crystals are precipitated in the matrix and irregularly distributed to form a compact microstructure. Presence of hexagonal Au-nanoparticles in all over the place also increased the compactness and hence density ( $\sim 2.60\text{ g cm}^{-3}$ ). It may be pointed out here that the density of silver and gold metals are  $10.49$  and  $19.30\text{ g cm}^{-3}$  signifying that gold can fit itself in the ceramic domain with more mass in the same amount of volume rather than silver.<sup>21,22</sup> Hence, from the FESEM of NG-4 glass-ceramics, the crystallite size decreased, packing/compactness increased and density increased on small addition of Au-nanoparticles. Thus, *in situ* nanoparticle doped glass-ceramics (NG-1 & NG-2) possessed mostly spherical nanocrystallites whereas *ex situ* samples *i.e.* NG-3 and NG-4 contained rock shaped and plate shaped crystallites of micrometer range.<sup>16,22</sup>

### 3.4 Mechanical property of $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$ glass-ceramics

The mechanical property *i.e.* microhardness of four nanoparticle doped  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glass-ceramics heat-treated at  $950^\circ\text{C}$  have been evaluated by

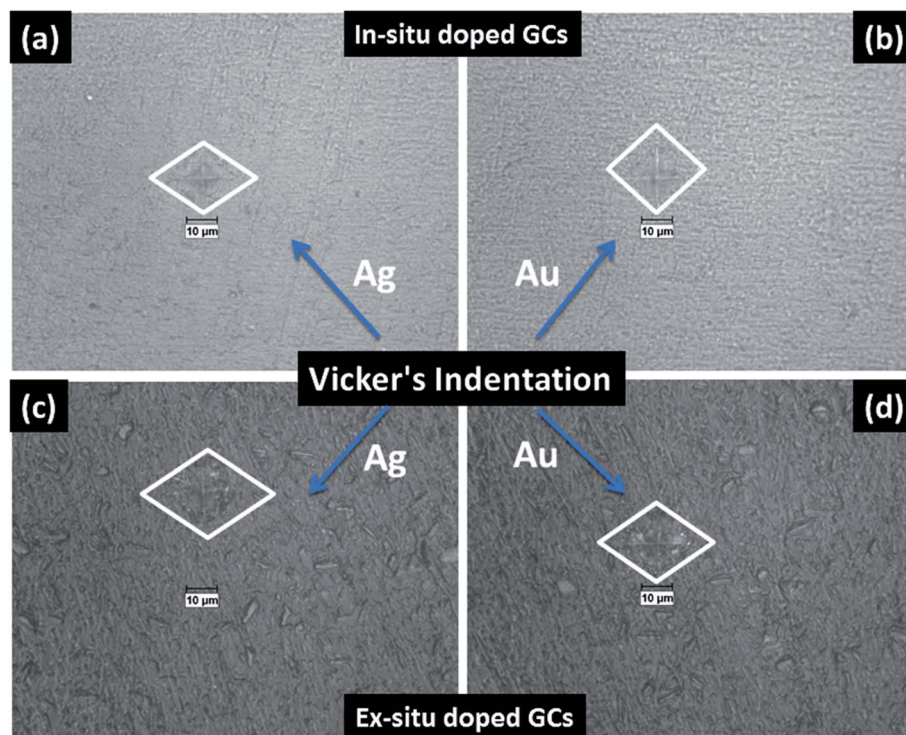


Fig. 6 Photomicrograph of Vickers indentation impression on  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glass-ceramics *i.e.* (a) NG-1, (b) NG-2, (c) NG-3 and (d) NG-4 heat-treated at  $950^\circ\text{C}$ .



Vickers and Knoop indenters. Average of ten indentations was taken under indent load of 200 g each, using the average diagonal lengths of the hardness impressions. The images of the Vickers indentation impressions on glass-ceramics are depicted in Fig. 6. Over controlled heating at 950 °C, fluorophlogopite  $[\text{KMg}_3(\text{AlSi}_3\text{O}_{10})\text{F}_2]$  crystals predominated in the ceramic matrix and for *ex situ* doped samples the crystallization is further supported. As depicted in Fig. 4a and b the spherical droplet-like nanocrystallites are precipitated predominantly in NG-1 and NG-2 glass-ceramics. The Vickers indentation impression on those two glass-ceramics is presented in Fig. 6a and b and microhardness value is estimated 4.48 ( $\pm 0.13$ ) and 4.61 ( $\pm 0.14$ ) GPa, respectively. In case of *ex situ* nanoparticle doped

samples, 1–3  $\mu\text{m}$  sized plate shaped mica crystals predominated and thus, lower microhardness is obtained as 4.34 ( $\pm 0.13$ ) and 4.46 ( $\pm 0.13$ ) GPa for NG-3 and NG-4 glass-ceramics, respectively. The Vickers indentation impression on *ex situ* samples is presented in Fig. 6c and d. It is well established that the microhardness value of glass-ceramic directly depends on crystalline packing and corresponding microstructure developed after heat-treatment.<sup>14,19</sup> As already pointed out that the catalytic activity on crystallization was supported by Ag- and Au-nanoparticles because of close matching in lattice parameter, fine grained morphology is obtained in NG-3/NG-4 glass-ceramics. Lower microhardness of NG-3 & NG-4 glass-ceramics further ensured higher machinability (*m*) which was

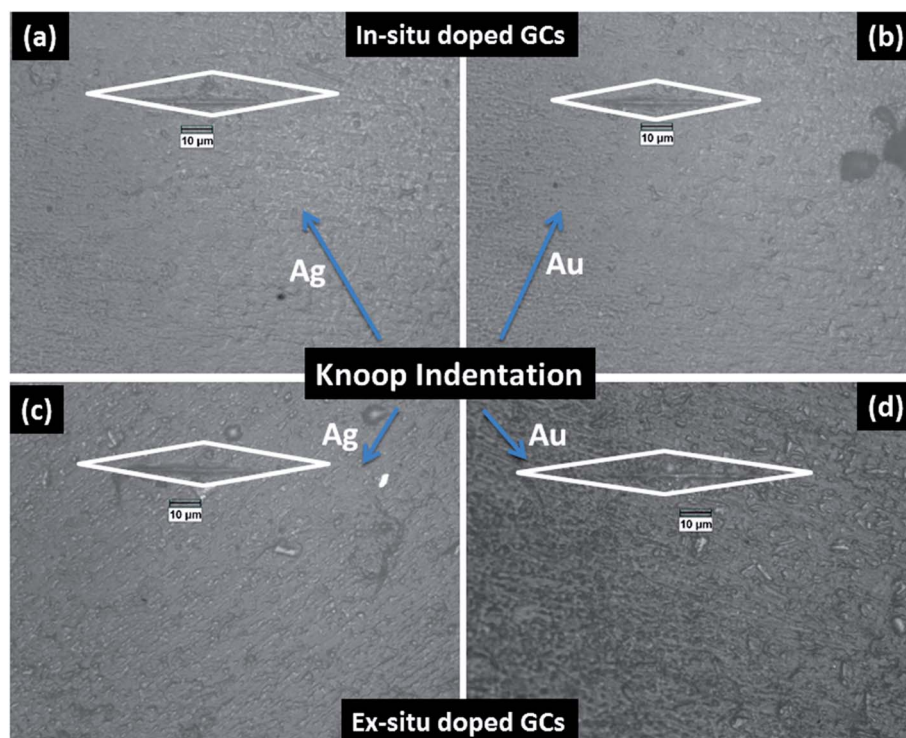


Fig. 7 Photomicrograph of Knoop indentation impression on  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  glass-ceramics i.e. (a) NG-1, (b) NG-2, (c) NG-3 and (d) NG-4 heat-treated at 950 °C.

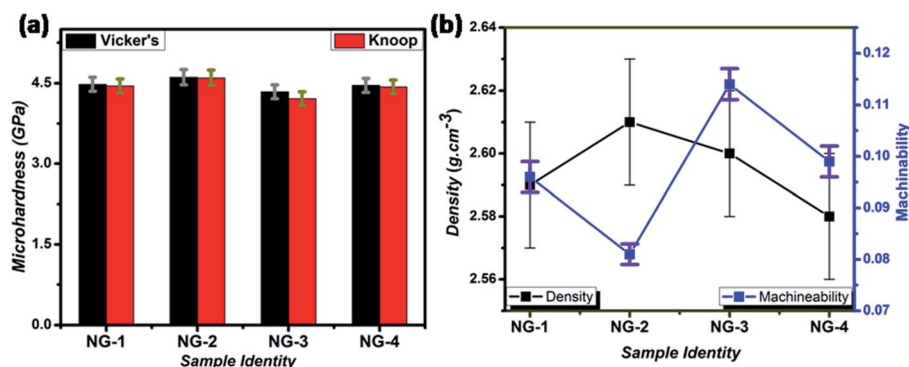


Fig. 8 Variation of Vickers & Knoop microhardness (a), and change of machinability & density (b) for different  $\text{SiO}_2\text{--Al}_2\text{O}_3\text{--MgO--K}_2\text{O--B}_2\text{O}_3\text{--MgF}_2$  samples heat-treated at 950 °C.



determined using the eqn (1) i.e.  $m = 0.643 - 0.122H$ .<sup>14</sup> For NG-1 to NG-4 glass-ceramics, the machinability was estimated 0.096 ( $\pm 0.003$ ), 0.081 ( $\pm 0.002$ ), 0.113 ( $\pm 0.003$ ) and 0.099 ( $\pm 0.003$ ), respectively. Microhardness value estimated by Knoop indentation approach using same load for NG-1 to NG-4 glass-ceramics was 4.45 ( $\pm 0.13$ ), 4.60 ( $\pm 0.14$ ), 4.21 ( $\pm 0.13$ ) and 4.43 ( $\pm 0.13$ ) GPa, respectively. The Knoop indentation impression on NG-1 to NG-4 glass-ceramics is presented in Fig. 7a–d, respectively. Here it is seen that the microhardness value evaluated for each glass-ceramic using Vickers and Knoop method are close to each other (Fig. 8a). A correlation between machinability and density for glass-ceramics is projected in Fig. 8b. Except NG-2 system, the machinability directly corresponds to density. Hence in view of Fig. 8b it can be stated that easy machining is possible for *ex situ* Ag-nanoparticle doped  $\text{SiO}_2\text{-Al}_2\text{O}_3\text{-MgO-K}_2\text{O-B}_2\text{O}_3\text{-MgF}_2$  glass-ceramics.

## 4. Conclusions

In this study, the comparative effects of *ex situ* and *in situ* generated silver and gold nanometals (0.2 wt% in excess) on crystallization behavior, thermal and mechanical properties of  $\text{SiO}_2\text{-MgO-Al}_2\text{O}_3\text{-B}_2\text{O}_3\text{-K}_2\text{O-MgF}_2$  glass system have been investigated and the major findings are summarized below:

The effectiveness of silver (Ag) and gold (Au) nanoparticles on crystallization- and evolution of microstructure of heat-treated  $\text{SiO}_2\text{-MgO-Al}_2\text{O}_3\text{-B}_2\text{O}_3\text{-K}_2\text{O-MgF}_2$  glass-ceramic and their mechanical properties is illustrated. Nanoparticles were doped *via* both *in situ* and *ex situ* mechanism and that was found to strongly affect the glass transition temperature ( $T_g$ ) and crystallization temperature ( $T_c$ ). *In situ* nanoparticle doped glasses with  $T_g$  value 622–630 °C showed similar density with *ex situ* doped glasses possessing  $T_g$  value 649–652 °C. Compare to *in situ* system, 90–110 °C increase in  $T_c$  was found for *ex situ* doped glasses ( $T_c = 870\text{--}875$  °C).

Over controlled heat-treatment at  $950 \pm 10$  °C, the glasses were converted into glass-ceramic (GC) with predominant crystalline phase (XRD) fluorophlogopite mica,  $[\text{KMg}_3(\text{AlSi}_3\text{O}_{10})\text{F}_2]$ . Along with the secondary phase enstatite ( $\text{MgSiO}_3$ ), the presence of FCC Ag and Au particles were identified by XRD study.

Spherical crystallites of size  $\sim 50\text{--}400$  nm is observed through FE-SEM in *in situ* doped GCs. Whereas, *ex situ* Ag doped GC is composed of rock-like and plate-like crystallites mostly of size 1–3  $\mu\text{m}$  ensured its superior machinability.

Vicker's and Knoop microhardness of *in situ* doped GCs were estimated within range of 4.45–4.61 GPa which reduced to 4.21–4.34 GPa in *ex situ* system. Machinability of GCs were found in the order, *ex situ* Ag > *ex situ* Au  $\sim$  *in situ* Ag > *in situ* Au. Thus, the *ex situ* Ag/Au doped  $\text{SiO}_2\text{-MgO-Al}_2\text{O}_3\text{-B}_2\text{O}_3\text{-K}_2\text{O-MgF}_2$  GC has potential for using as machinable glass-ceramic.

## Conflicts of interest

There are no conflicts to declare.

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