Continuous dimethyldioxirane generation for polymer epoxidation†

Grace P. Ahlqvist, † Eileen G. Burke,‡ Jeremiah A. Johnson †* and Timothy F. Jamison †*

Post-polymerization modification of commodity polymers yields new applications for materials already produced industrially. Incorporation of small amounts of epoxides into unsaturated polymers such as polybutadiene expands their use for grafting and compatibilization applications, but controlled epoxidation of these polymers in a safe, scalable manner presents a challenge. Herein we describe the development of a reactor for the continuous flow generation and use of dimethyldioxirane (DMDO) and its application to the low-level epoxidation of unsaturated polymers. A continuous stirred tank reactor (CSTR) prevents reactor clogging by allowing solid precipitates to settle, enabling the pumping of a homogeneous solution of oxidant. Modification of relative concentrations, flow rates, and temperatures achieves variable epoxidation levels. This method has been demonstrated on gram scale.

Post-polymerization modification vastly expands the properties and applications of simple commodity polymers such as polyolefins.1,2 Polymer epoxidation can alter properties such as solubility, aggregation, and thermal stability, as well as providing functional handles for further modification.3–5 Low epoxidation levels are particularly useful for compatibilization and grafting applications, as minimal backbone alteration preserves polymer properties while providing functional handles for novel modifications. For example, pure poly(lactic acid) (PLA) is brittle at room temperature, but can be strengthened by blending with rubber. However, since PLA is immiscible with common rubbers like polybutadiene (PBD), modifications allowing reactive compatibilization improve the properties of the resultant polymer blend.6 Sun et al. report PLA toughening from acrylonitrile-butadiene-styrene (ABS) rubber containing a small (1%) amount of glycidyl methacrylate (GMA), which contains epoxides that react with PLA end groups.7 Similar effects have been observed for PLA toughened with methyl methacrylate-butadiene block copolymers with added GMA.8

Direct use of epoxidized PBD removes the need for copolymerization with a compatibilizer like GMA, and low-level epoxidation of polybutadiene is particularly valuable, as high epoxidation levels cause an increase in glass transition temperature that negatively impact the toughness of the resulting PLA blends.9 Unfortunately, typical peracid epoxidation methods7,4 necessitate storage and use of hydrogen peroxide or an organic peroxide reagent, which is costly and hazardous on scale.10 Safe, sustainable epoxidation methods are desirable for the large-scale production of polymer with low-level epoxide incorporation.

To circumvent the issues of storing hydrogen peroxide solutions, dimethyldioxirane (DMDO) can be employed. DMDO epoxidation has been demonstrated for unsaturated polymers in batch.11–14 DMDO is generated from acetone and solid, commercially available Oxone® (active ingredient potassium monoperoxysulfate) in a buffered aqueous solution.15 Due to the inherent instability and hazards of storage and use of organic peroxides, DMDO is typically prepared in situ or immediately before use. Its preparation is low-yielding and requires a hazardous distillation procedure to isolate it as a solution in acetone.16,17 On-demand generation of DMDO is desirable for large-scale applications, such as polymer oxidation at industrial scale, to avoid the hazards of using large amounts of organic peroxides.

Reports of dioxirane generation in continuous flow are promising, as synthesis in flow is ideally suited for on-demand generation and use of hazardous reagents.18,19 The first use of DMDO continuous flow was reported in 2018 by McCluskey et al., who epoxidized a variety of alkenes in 60–98% yield.20 However, the use of acetone as solvent limits the generality of this method for substrates such as higher olefin polymers that are insoluble in acetone. Methyl[trifluoromethyl]dioxirane (TFDO) has also been generated in continuous flow and used for aliphatic C–H oxidation.21 Unfortunately, the use of acetone to replace trifluoroacetonitrile in the system reportedly
caused precipitation. A robust, scalable protocol for DMDO generation and use in continuous flow for epoxidation of non-polar polymers has yet to be developed.

We envisioned a modular continuous flow reactor in which DMDO would be generated, reacted with a polymer dissolved in organic solvent, and then quenched at the output. This system design both minimizes the amount of DMDO present at any one time in the system, and allows tuning of experimental variables such as temperature and residence time so different levels of epoxide incorporation can be targeted. In particular, we focused on low (<20%) levels of epoxide incorporation for the purposes of this investigation, due to the compatibilization and grafting applications mentioned above.

Our initial design plan combined three inputs (Oxone® solution, base solution, and acetone solution) in a cross-mixer to make DMDO, and then added the polymer solution at a T-mixer (Fig. S1, ESI†). However, we observed rapid formation of white solids that led to clogging in this system. We hypothesized that the solid precipitation was due to the high concentrations of inorganic salts combined with acetone at the cross-mixer. Oxone® is a triple salt, and it contains one mole of less soluble, inactive salts (KHSO₄, K₂SO₄) for every one mole of active salt (KHSO₅). We sought a method to mix the reagents for DMDO formation that would allow a homogeneous oxidant solution to be pumped forward without clogging due to the precipitation of undesired salts.

Handling solid–liquid mixtures in continuous flow is an ongoing challenge in the field.22 To address this challenge in our system, we designed a simple continuous stirred tank reactor (CSTR) that would pre-mix the reagents to produce DMDO while allowing the undesired solids to settle to the bottom (Fig. 1).

Reagents were pumped via syringe pump into a small tank (a flask, stoppered syringe, test tube, or other vessel of similar size). Under slow stirring, the undesired solids settled to the bottom of the reactor. The liquid phase of the mixture, containing a solution of water, acetone, base, Oxone®, and DMDO, could then be pumped forward to react with the polymers. We quickly learned that filtration was necessary to ensure that finely divided solids did not clog the tubing; a simple piece of filter paper tied to the tubing using Teflon tape was sufficient for this purpose (see Fig. S2 in ESI†). Using common materials (flasks, filter paper, Teflon tape), a simple CSTR efficiently pre-mixed the reagents for DMDO formation while preventing solids from clogging narrow-diameter tubing and fittings.

DMDO is typically generated using NaHCO₃ as a base to buffer the aqueous solution, as DMDO is formed most efficiently at neutral or slightly alkaline pH.15 However, we observed that using sodium bicarbonate to generate DMDO in flow caused precipitation of sodium salts and evolution of carbon dioxide gas. Excess precipitation of salts caused clogging, while gas evolution and cavitation from clogging caused inconsistencies in residence time due to the formation of gas slugs in the plug flow reactor. While the CSTR improves solid handling, generating less solid overall aids in the performance of the system over long runs and avoids wasting reagents that are added but precipitate out due to solubility issues. Thus, we sought to identify a superior base for the generation of DMDO in continuous flow (Table 1).

### Table 1 Base screening for DMDO generation

<table>
<thead>
<tr>
<th>Entry</th>
<th>Base</th>
<th>pH</th>
<th>Gas evolution</th>
<th>Solid formation</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.7 M Na₃CO₃</td>
<td>5.0</td>
<td>High</td>
<td>High</td>
</tr>
<tr>
<td>2</td>
<td>0.5 M K₂HPO₄</td>
<td>5.5</td>
<td>Low</td>
<td>Low</td>
</tr>
<tr>
<td>3</td>
<td>1.0 M K₂HPO₄</td>
<td>6.0</td>
<td>Medium</td>
<td>Medium</td>
</tr>
<tr>
<td>4</td>
<td>0.5 M K₃PO₄</td>
<td>6.0</td>
<td>Low</td>
<td>Low</td>
</tr>
<tr>
<td>5</td>
<td>1.0 M K₃PO₄</td>
<td>7.0</td>
<td>Medium</td>
<td>Medium</td>
</tr>
</tbody>
</table>

* *pH in CSTR tested by pH strip after system equilibration. * Solid and gas observed and compared qualitatively.

While 1.0 M K₃PO₄ yielded the highest pH at steady state (entry 5), further reactions with this base concentration showed no epoxidation, possibly due to the degradation of Oxone®. Thus, 0.5 M K₃PO₄ (entry 4) was chosen, yielding a pH of 6.0 in the CSTR and producing a minimal amount of solid and gaseous byproducts.

We then modified the setup to contain only two inputs rather than three to use fewer pumps and minimize the amount of excess salt introduced into the system. Our goal was to combine the base and acetone reagents into one solution. Due to the limited solubility of inorganic bases in acetone,
higher heat caused a decrease in epoxidation (Fig. 3a). We
variety of epoxidation yields (Fig. 3).
concentration to determine conditions that could provide a
further investigation.
and epoxidation yield favored the use of ethyl acetate for
toluene or dichloromethane, environmental considerations
rate ratio. Although PBD is less soluble in ethyl acetate than in
decreased concentration of PBD at the same DMDO : PBD flow
the epoxidation of PBD (Table 2).
solvents and concentrations to determine their influence on
superheating of the solution above the boiling point of acetone.
forward to react in a coil of perfluoroalkoxy polymer (PFA) tubing
the DMDO solution was combined with the polymer solu-
tions and section 4.1
for additional experimental data.

Table 2 Solvent Screening for PBD epoxidation

<table>
<thead>
<tr>
<th>Entry</th>
<th>Solvent</th>
<th>[PBD] (g L⁻¹)</th>
<th>Epoxidation (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Dichloromethane</td>
<td>30</td>
<td>4</td>
</tr>
<tr>
<td>2</td>
<td>Dichloromethane</td>
<td>10</td>
<td>11</td>
</tr>
<tr>
<td>3</td>
<td>Toluene</td>
<td>30</td>
<td>3</td>
</tr>
<tr>
<td>4</td>
<td>Toluene</td>
<td>10</td>
<td>5</td>
</tr>
<tr>
<td>5</td>
<td>Ethyl Acetate</td>
<td>10</td>
<td>14</td>
</tr>
</tbody>
</table>

Reaction conditions: 70 °C, tₕ 10 min, and 3 : 1 flow rate ratio of
DMDO solution to PBD solution.

high concentrations of base in acetone–water mixtures induced
phase separation in the stock solutions. After screening for
stability of the base–acetone mixture and pH of the resultant
DMDO solution, a solution of 0.33 M K₃PO₄ in a 70 : 30 mixture
of water and acetone was chosen as the ideal balance for mixing
with equal amounts of a 0.8 M Oxone® solution.

With conditions in hand to prepare DMDO in continuous
flow, we combined the DMDO stream with liquid PBD dis-
solved in an organic solvent. A flow reactor was constructed
using a peristaltic pump to pump DMDO from the CSTR to the
rest of the system (Fig. 2).
The DMDO solution was combined with the polymer solution
using a T-mixer and the biphasic mixture was pumped

Fig. 3 Effect of (a) temperature, (b) residence time, and (c) polymer concentration on epoxide incorporation. Unless otherwise noted, conditions are 25 °C, 5 min tₑ, and 10 g L⁻¹ PBD in EtOAc. Epoxide incorporation calculated by quantitative NMR, see section 3.1 in ESI† for epoxidation calculations and section 4.1† for additional experimental data.

Table 3 Epoxidation of High MW PBD

<table>
<thead>
<tr>
<th>Entry</th>
<th>[PBD] (g L⁻¹)</th>
<th>tₑ (min)</th>
<th>Epoxidation (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>30</td>
<td>1</td>
<td>1</td>
</tr>
<tr>
<td>2</td>
<td>10</td>
<td>1.25</td>
<td>3</td>
</tr>
<tr>
<td>3</td>
<td>1</td>
<td>1.25</td>
<td>22</td>
</tr>
</tbody>
</table>

Reaction conditions: Room temperature, toluene, 3 : 1 flow rate ratio of
DMDO solution to PBD solution.
Conflicts of interest

There are no conflicts to declare.

Acknowledgements

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References


