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Plastic strain relaxation and alloy instability in epitaxial corundum-phase (Al,Ga)₂O₃ thin films on *r*-plane Al₂O₃

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The growth of (Al_xGa_{1-x})₂O₃ alloy thin films in the corundum phase on *r*-plane (01.2) Al₂O₃ substrates is investigated. The growth mode changes from step flow for pseudomorphic layers to three-dimensional growth for strongly relaxed layers. Atomic force microscopy and transmission electron microscopy reveal defects due to prismatic and basal slip. An instability in the growth of the alloy $x \approx 0.6$, manifested in doubly-periodic incorporation of Al-rich slabs, is observed.

1 Introduction

Gallium oxide and related materials, which are ultrawide-bandgap semiconductor materials, have emerged as promising candidates for a new generation of high-power devices.^{1,2} These sesquioxides can be fabricated as thin films in various crystal phases.^{3,4} The focus of this paper is on the rhombohedral (or trigonal) phase, also termed the corundum- or α -phase. The growth of α -Ga₂O₃^{5,6} and α -(Al,Ga)₂O₃ alloys for buffer layers^{7–10} on sapphire has gained large interest. Also, the (Al,Ga)₂O₃-system is interesting as a barrier layer for Ga₂O₃- and (In,Ga)₂O₃-based heterostructures;^{11,12} the corundum phase offers larger band offsets compared to the monoclinic phase.¹³ Compared to the more familiar hexagonal wurtzite semiconductors (such as GaN and ZnO), the trigonal crystal structure introduces particular effects regarding the stress-strain situation.¹⁴

In this work the growth of α -(Al,Ga)₂O₃ layers on *r*-plane Al₂O₃ is investigated using techniques with high lateral resolution in order to detect and characterize individual defects arising from plastic strain relaxation. A peculiar alloy instability is found, leading to an inhomogeneous cation distribution along the growth direction.

2 Experimental methods

Selected samples¹⁵ fabricated by pulsed laser deposition (PLD)¹⁶ were investigated. For more details concerning PLD

growth, see ref. 17–19. The substrate temperature was set to about 750 °C or 1000 °C. The oxygen partial pressure was 10^{−3} mbar. The targets for our pulsed laser deposition (PLD) process were fabricated from high purity Al₂O₃ and Ga₂O₃ powders in different relative quantities. All samples were grown with 30 000 pulses on *r*-plane (01.2) Al₂O₃ substrates. Atomic force microscopy (AFM) was performed with a Park Scientific XE-150 in non-contact mode.²⁰ (Scanning) Transmission electron microscopy ([S]TEM) was performed using a Thermo Fisher Scientific TITAN³ G2 80-300 aberration-corrected (objective lens) instrument operated at 300 kV in high-resolution multi-beam interference contrast and high angle annular dark field (HAADF) modes for either TEM or STEM imaging, respectively. Energy dispersive X-ray (EDX) mappings were additionally recorded in STEM mode, using a FEI SuperX detector system in the same microscope. Prior to inspection, cross-sectioned samples were prepared and thinned to electron transparency using the wedge polishing approach explained in more detail in ref. 21. Static charging of samples upon TEM inspection was avoided by selective carbon coating.²²

3 Experimental results

3.1 Strain relaxation

In Fig. 1a, a TEM cross-sectional micrograph of the interface region of a pseudomorphic (Al_xGa_{1-x})₂O₃ layer ($x = 0.91$) is shown; a flat and abrupt interface is visible without defects. For a smaller Al cation fraction, in a plastically relaxed sample, the interface looks more disordered (Fig. 1b for $x = 0.61$) and defects appear that apparently also extend back into the substrate. The slight stripes parallel to the interface will be discussed below in more detail.

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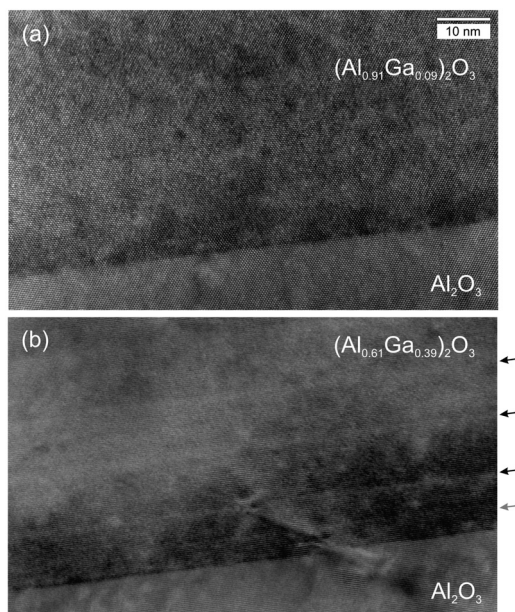


Fig. 1 Cross-sectional TEM images of the substrate/film interface region of two α -($\text{Al}_x\text{Ga}_{1-x}$) $_2\text{O}_3$ thin films on (01.2) Al_2O_3 with (a) $x = 0.91$ ([01.1] viewing direction) and (b) $x = 0.61$ ([$\bar{2}$ 1.0] viewing direction). The arrows in panel (b) indicate anomalies in the cation ratio.

It should be emphasized that the quality of our pseudomorphic epitaxial layers (with sufficiently large Al-concentration) is very high as no structural defects can be identified with transmission electron microscopy or atomic force microscopy. X-ray diffraction shows clearly defined layers and substrate peaks similar to results previously published and discussed for similar samples.^{18,19}

Plastic strain relaxation in the corundum phase occurs preferentially *via* twinning and prismatic and basal slip.^{23–26} The nature of plastic relaxation in the thin films on an *r*-plane corundum has been investigated previously using X-ray diffraction and detailed analysis.^{17–19} The plastic relaxation is anisotropic at first and starts through prismatic slip *via* the *a*-plane glide system and subsequently *via* basal slip (*c*-plane glide system).^{18,19} The prismatic slip lines were identified first in ref. 19 and an example is shown in Fig. 2, where the surface morphology of a slightly relaxed thin film ($x = 0.88$) is imaged *via* AFM. The average surface step height is determined as $h = 0.36(3)$ nm, close to the *r*-plane lattice spacing $d_{(01.2)} = 0.348$ nm (for Al_2O_3) and in agreement with previous reports, *e.g.* ref. 27, where $h = 0.33(5)$ nm was found. In the following, the step height is also termed a ‘monolayer’; the atomic arrangement of the *r*-plane is discussed in ref. 28. Two types of slip-lines are visible. They form a mutual angle of $2\alpha = 86.0(3)^\circ$, matching our expectation of an angle $\alpha = \pm 42.9^\circ$ (for Al_2O_3 lattice parameters), which the two types form with the [$\bar{0}$ 111]-direction.^{18,29}

The two types are related to the (11.0) and ($\bar{1}$ 2.0) *a*-planes. As detailed in ref. 18, the $b_1 = 1/3[\bar{1}101]$ Burgers vector for the (11.0)-plane and $b_2 = 1/3[\bar{1}01\bar{1}]$ Burgers vector for the ($\bar{1}$ 2.0)-plane have the same length of their edge component but opposite tilt components. The sum of the two vectors is

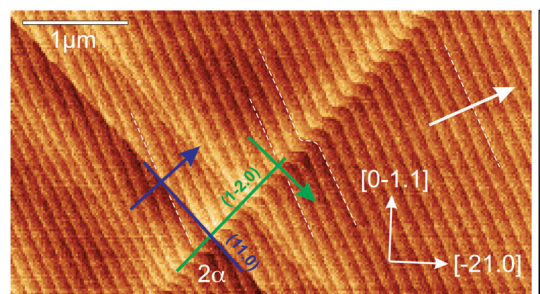


Fig. 2 AFM image of the surface of an approximately 600 nm thick (just above the critical thickness for plastic strain relaxation) α -($\text{Al}_{0.88}\text{Ga}_{0.12}$) $_2\text{O}_3$ thin film on (01.2) Al_2O_3 grown at 1000 °C showing regular surface terraces. Some step edges are highlighted with thin dashed white lines; the white arrow denotes the direction of the substrate off-cut from the *r*-plane. Two types of slip-lines from prismatic glide stem from (11.0) (blue line) and ($\bar{1}$ 2.0) (green line) *a*-plane glide systems. The associated arrows denote the direction of the step component of their Burgers vectors. The angle formed by the slip-lines is $2\alpha = 86.0(3)^\circ$. The height scale is 0–2.5 nm.

$b_s = 1/3[\bar{2}110]$, $|b_s| = a$, leading to strain relaxation in this direction. The tilt components for $b_{1,2}$ are $b_p = \pm d_{(01.2)}$. This means that when crossing the slip-line in the direction of the (in-plane projection of the) Burgers vector b_1 (*i.e.* the (11.0) slip-line) the next higher terrace is reached, and accordingly for b_2 (*i.e.* the ($\bar{1}$ 2.0) slip-line) the next lower terrace is reached.

The directions of the edge components of the two Burgers vectors are shown as blue (green) arrows for b_1 (b_2). Indeed, when following b_1 (b_2), the next higher (lower) terrace is reached, confirming the sign and magnitude of the expected tilt components of the Burgers vector. It should be noted that for ensuring the correct orientation of the AFM image, the direction of the (projection of the) *c*-axis was confirmed using a X-ray diffraction (using a PANalytical X'Pert PRO materials research diffractometer) ϕ -scan around the (01.2) normal of the (00.6) reflex.

Structural defects were investigated by cross-sectional TEM investigations. In Fig. 3, various defects are found, with the most prominent being features parallel to the *a*-plane glide planes. These are indicated by red lines in the lower panel of Fig. 3. Also basal defects are visible as expected for this already strongly relaxed sample (blue lines). Some other defects seem to stem from ($\bar{0}$ 1.1)-planes (orange lines); another set of lines with an angle of about 103° against the [$\bar{0}$ 1.1]-direction, for which no simple plane was found, is shown as dashed lines.

The comparison of the AFM-derived surface morphologies of layers with different Al cation fractions, fabricated under identical growth conditions (1000 °C, 30 000 PLD pulses), shows significant changes in correlation with the strain relaxation. In the plot of Fig. 4, the average relaxation in the two perpendicular in-plane directions, $\rho = (\rho_x + \rho_y)/2$, is shown, where $\rho_x = \rho_y = 1$ (0) means a pseudomorphic (fully relaxed) film. For $x > 0.8$, for the given layer thicknesses, anisotropic relaxation *via* prismatic slip is present, while for $x < 0.8$ strong relaxation *via* basal slip sets in and also the rms surface roughness increases strongly. More details can be seen from the AFM scans.



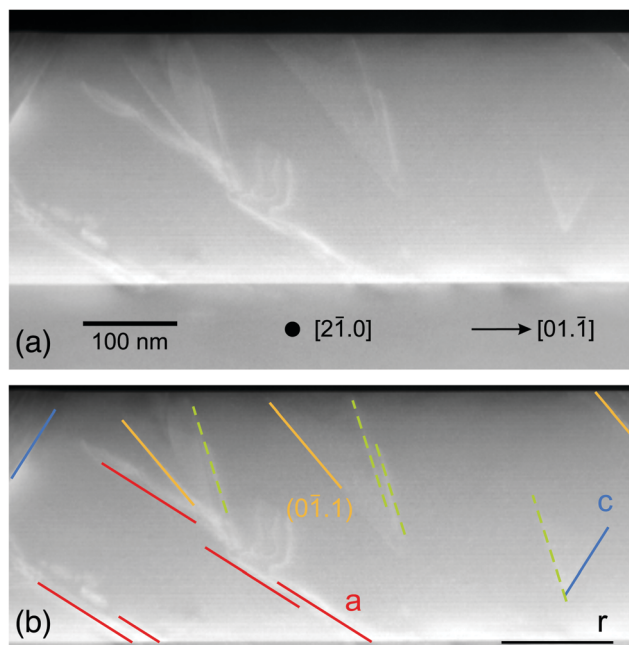


Fig. 3 (a) Cross-sectional TEM image (STEM-HAADF contrast at a camera length of 230 mm, emphasizing diffraction contrast at the expense of compositional contrast) of an α -($\text{Al}_{0.61}\text{Ga}_{0.39}$) $_2\text{O}_3$ thin film on (01.2) Al_2O_3 . Panel (b) depicts the same image as in panel (a), superimposed with the positions of a- (red) and c-plane (blue) defects from prismatic and basal glide. Also features belonging to {01.1}-planes (orange) are visible. Another set of line features is shown (green, dashed).

Fig. 4a depicts a pseudomorphic (Al,Ga) $_2\text{O}_3$ thin film with a surface that looks very much like the typical morphology of the Al_2O_3 *r*-plane annealed at 1000 °C for 1 h, exhibiting 'comb-shaped chemical domains' as reported for example in ref. 27. The growth occurs *via* the step-flow mode. Fig. 4b shows the surface of a film just above the critical thickness for plastic strain relaxation (same sample as in Fig. 2). The terrace structure is regular and the slip-lines have already been discussed above. With decreasing Al cation fraction and thus increasing lattice mismatch, more defects develop. In Fig. 4c it becomes visible that the slip-lines exhibit endings, hinting at defect interaction and annihilation. Also, the terrace structure becomes more irregular and the surface appears a bit wobbly. For even stronger relaxation (Fig. 4d) defects cluster and lead to stronger modulation of the surface height. Eventually (Fig. 4e), terraces cannot be distinguished anymore and the growth has changed from the step-flow to 3D growth mode.

The use of a high growth temperature of 1000 °C leads to a promotion of strain relaxation but reduced gallium incorporation. The crystal quality is high and comparable with growth at lower temperatures in the range of 700–800 °C.¹⁹ However, only a high-temperature annealing step prior to growth can ensure a terraced surface like in Fig. 4a.

3.2 Alloy instability

In Fig. 1b, a stripe-like modulation along the growth direction is visible which shall be discussed in more detail in the following. It is related to a modulation of the cation ratio.

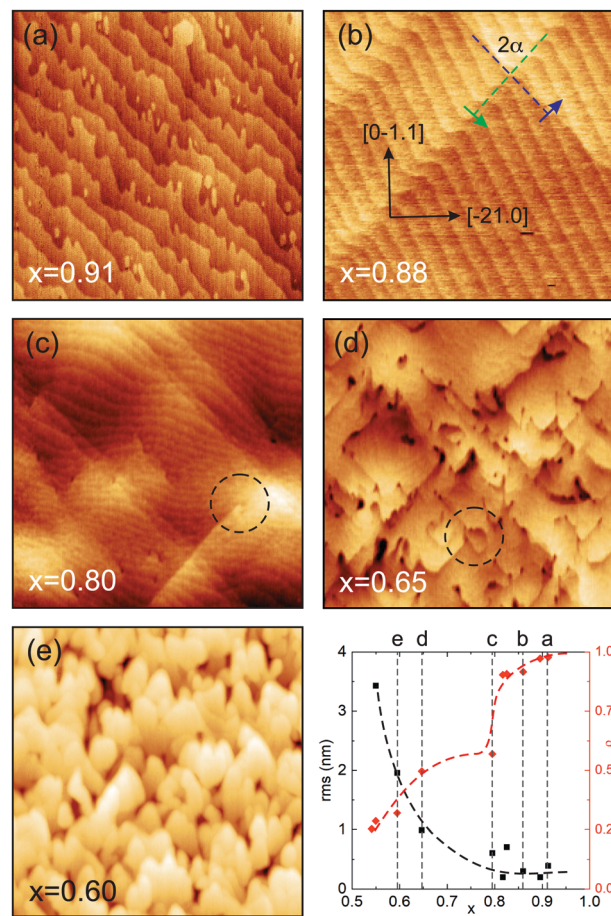


Fig. 4 (a)–(e) AFM images ($2\ \mu\text{m} \times 2\ \mu\text{m}$) of α -($\text{Al}_x\text{Ga}_{1-x}$) $_2\text{O}_3$ thin films on (01.2) Al_2O_3 with 5 different Al cation fractions as labeled. In panel (b) the crystallographic directions are shown. The slip-lines from prismatic glide are shown for (11.0) in blue and for (12.0) in green. The circle in panel (c) highlights the end of a slip-line. The circle in panel (d) highlights a dislocation loop. The line graph shows the rms roughness (black, left scale) from the $5\ \mu\text{m} \times 5\ \mu\text{m}$ AFM scans and the strain relaxation $\rho = (\rho_x + \rho_y)/2$ (red, right scale); the black and red dashed lines are guides to the eye, and the grey vertical dashed lines indicate the Al cation fraction for the samples from panels (a)–(e).

For a more specific analysis, EDX maps were recorded in STEM mode and linescans of the Al- and Ga-fractions in the growth direction were extracted. It should be noted that for the sample with $x = 0.91$, such a modulation is absent in EDX measurements. Also, sample and target rotations as possible sources of the modulation³⁰ (or PLD target inhomogeneities) can be technically excluded. The target rotation was 0.5 Hz (*i.e.* one full rotation in 2 s), the substrate rotation was $2/29 \approx 0.069$ rounds per second, and the laser pulse frequency was 15 Hz. The growth rate was about 1.75(5) nm/100 pulses.¹⁸ Thus for the vertical period of about 10.1 nm (see analysis below), 575(15) pulses were made, *i.e.* 38(1) s of growth. In that time the target rotated about 19 times and the substrate rotated 2.64(7) times.

In Fig. 5 the HAADF contrast shows a periodic modulation across the entire layer thickness. A linescan, averaged perpendicular to the direction of the linescan, shows the modulation of the Al-concentration. The separation of the maxima is doubly-periodic



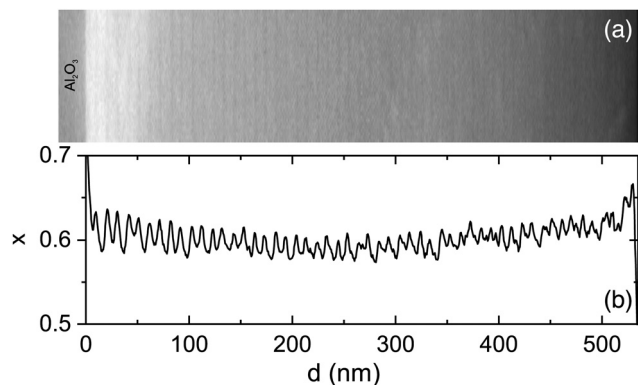


Fig. 5 (a) STEM micrograph (HAADF contrast) of the Al cation fraction x of an α -($\text{Al}_x\text{Ga}_{1-x}$) $_2\text{O}_3$ thin film on (01.2) Al_2O_3 . In (b) the averaged corresponding STEM-EDX linescan is shown, with the average Al cation fraction being $\bar{x} \approx 0.6$.

as shown in Fig. 6. Up to about 300 nm layer thickness, the periods are quite regular with alternating separations of 11.2(4) nm (about 32 monolayers) and 9.1(3) nm (about 26 monolayers), as indicated by dashed lines. On average, the periodicity is $p = 10.2$ nm. For larger distances from the interface, the modulation becomes weaker and less regular (possibly due to the slight bending of the cross-sectional and wedge-shaped sample).

In the higher resolution EDX maps depicted in Fig. 7, the stripe-like modulation of the Al- and Ga-contents is also obvious. The oxygen signal intensity changes slightly between the substrate and the film, possibly due to the slightly decreasing TEM sample thickness from the substrate to the top of the film. In the substrate, the (non-calibrated) Al-signal $x_{\text{EDX,Al}}$ correlates with 100% of the cations. For the film, the (non-calibrated) Ga-signal $x_{\text{EDX,Ga}}$ is multiplied by a factor f such that $x_{\text{EDX,Al}} + f x_{\text{EDX,Ga}}$ divided by the oxygen signal is constant throughout the film. The Al cation fraction x is then calculated as $x_{\text{EDX,Al}} / (x_{\text{EDX,Al}} + f x_{\text{EDX,Ga}})$. This procedure yields an Al cation fraction x close to the average concentration of $x = 0.608$ determined for this film from the X-ray diffraction analysis.¹⁸ It should be noted

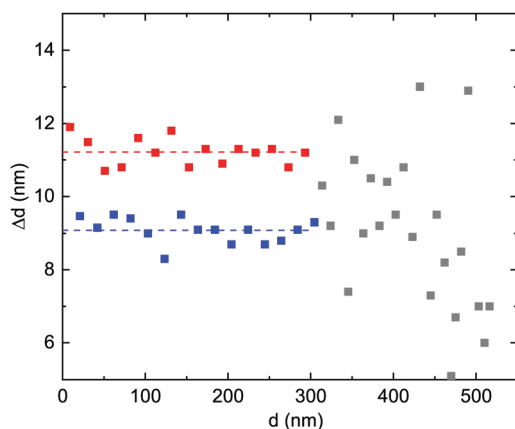


Fig. 6 Distances of maxima of the Al cation fraction along the linescan shown in Fig. 5. Up to $d = 300$ nm, the two different separations are shown in blue and red symbols, with their averages indicated as dashed lines. The less regular separations for $d > 300$ nm are shown as grey symbols.

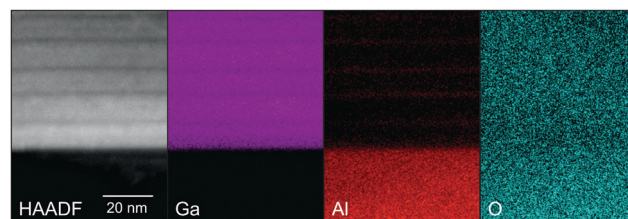


Fig. 7 STEM images of an α -($\text{Al}_{0.61}\text{Ga}_{0.39}$) $_2\text{O}_3$ thin film on (01.2) Al_2O_3 (bottom part) with HAADF contrast and maps of gallium, aluminum and oxygen signals as labeled.

that in Fig. 8 also the gallium fraction is shown for comparison, but this is given by $1 - x$ in our procedure and does not provide further information.

The Al-fraction is modulated between about $x = 0.58$ and $x = 0.66$ (for the given spatial resolution) with maxima about 10 nm (about 29 lattice constants) apart on average. This leads to the conclusion that, at least for the given growth parameters, the growth exhibits an instability, with aluminum segregating on the surface up to a certain amount which is then incorporated within a thin, Al-rich slab.

The EDX linescan has a finite spatial resolution as can be seen from the smooth transition of the Al/Ga ratio at the interface that is assumed to be atomically sharp. A Gaussian broadening³¹ cannot model this lineshape. It can be modeled, however, rather well using a sigmoidal broadening function $g(d)$ of the type (we restrict to $\gamma > 0$ in the following),

$$g(d) = \frac{\gamma^2}{2(d^2 + \gamma^2)^{3/2}}. \quad (1)$$

All lengths are measured here in nm. The maximum is $g(d = 0) = 1/(2\gamma)$ and the full width at half maximum (FWHM)

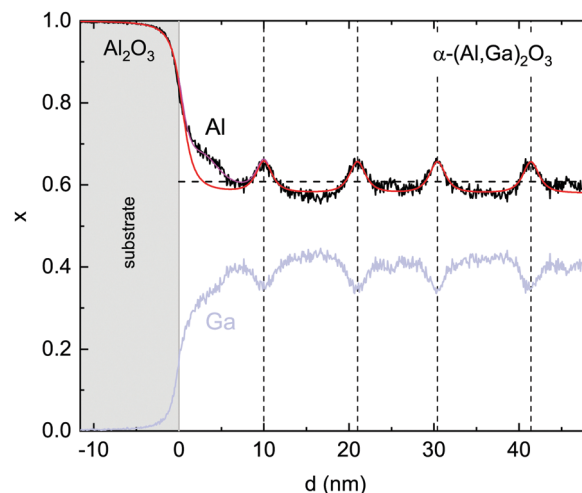


Fig. 8 STEM-EDX linescans (averaged laterally over 53 nm) of the Al-fraction x (black) extracted from Fig. 7. The gallium content $1 - x$ is shown in light blue. The light grey area indicates the substrate. The vertical dashed lines mark the maxima. The horizontal dashed line denotes the average Al cation fraction $\bar{x} = 0.608$ as determined by X-ray diffraction. The red and purple lines represent fits as discussed in the text.

is $2\gamma\chi$ ($\chi = \sqrt{2^{2/3} - 1} \approx 0.77$). The integral of g over all d is unity. Using this function, the EDX linescan can be fitted rather closely (red line in Fig. 8). The gradual interface is well reproduced by a step function (positioned at linescan coordinate $d = 0$) from 1 to $x' = 0.58$ convoluted with g using $\gamma = 1.4$ nm. The periodic Al enrichments were fitted with delta-like additional aluminum convoluted by βg with the same γ -value as for the interface and $\beta = 0.22$. The lineshape of the Al-rich slabs is mimicked rather well; it has the same broadening γ as found for the substrate/film interface, meaning that the actual width d' of the Al-distribution is much smaller than the FWHM of the broadening, about 2.2 nm.³²

β represents the integrated extra aluminum; it could correspond to a pure Al_2O_3 layer of thickness $s = (1 - x')/\beta = 0.5$. Therefore, it can be concluded that the EDX data are compatible with the presence of thin, periodic layers with pure Al_2O_3 , with a thickness of about 0.5 nm \approx 1.5 monolayers, or for example 2 monolayers with an Al cation fraction of about 0.9. The average Al cation fraction for this model is ($p = 10.2$ nm) $\bar{x} = (px' + \beta)/p = 0.602$, which is in good agreement with the EDX area average of $x = 0.607$ and the X-ray result of $x = 0.608$.¹⁸ Another feature, a locally higher Al-concentration up to about 5 nm from the interface in the EDX linescan, can be additionally fitted with another Al-rich slab but with a larger broadening of $\gamma = 3.3$ nm and $\beta = 0.44$ (purple line); this feature is also directly visible in Fig. 1b, where it is indicated by the grey arrow.

First the situation is discussed from a total energy perspective. From a thermodynamic standpoint, the corundum-phase ($\text{Al}_x\text{Ga}_{1-x}$) $_2\text{O}_3$ alloy is metastable for $x < 0.71$ ¹³ or for $x < 0.84$ for a cation-disordered phase³³ (the stable phase is the monoclinic β -phase). Thus, our α -phase layer with $x \approx 0.6$ is expected to be in the metastable range for the bulk material. In Fig. 9 the enthalpy of formation is reproduced from ref. 13. It is zero for $x = 1$ and it is sublinear³⁴ with $1 - x$.

The total strain energy density u_{el} is calculated for pseudomorphic conditions within the continuum elasticity model.^{35,36} It is expected that the energy increases roughly like $(1 - x)^2$,

$\hat{u} = u_{\text{el}}/(1 - x)^2$. In Fig. 10, $\zeta(x) = \hat{u}(x)/\hat{u}(x \rightarrow 1)$, the elastic strain energy divided by $(1 - x)^2$ and normalized to 1 for $x \rightarrow 1$ is depicted (for the r -plane). If the elastic constants and the c/a -ratio did not change between Al_2O_3 and Ga_2O_3 , ζ would be close to 1. For the given material parameters (same as in ref. 18), ζ increases³⁷ from 1 to about 1.70 for $x = 0$, meaning that the elastic energy grows slightly super-quadratically. For Ga_2O_3 , the calculation yields $u_{\text{el}} = 1.428 \times 10^9 \text{ J m}^{-3}$. The cation density ρ_c is calculated from the density of Al_2O_3 ($\rho = 3950 \text{ kg m}^{-3}$) and the molar masses ($M_{\text{Al}_2\text{O}_3} = 0.10196 \text{ kg mol}^{-1}$, $M_{\text{Ga}_2\text{O}_3} = 0.18744 \text{ kg mol}^{-1}$) as well as the lattice constants; for Al_2O_3 , $\rho_c = 3.109 \times 10^{28} \text{ m}^{-3}$ is found. In Fig. 9, the elastic strain energy is shown in units of eV per cation.

The question is whether the separation of a material with average Al cation fraction \bar{x} and thickness p into a thin Al-rich slab of concentration $x' > \bar{x}$ and thickness s and the remaining part with slightly lower Al-concentration $x' < \bar{x}$ is energetically unfavorable. First, the average concentration \bar{x} fulfills $p\bar{x} = x'(p - s) + x''s$ and second $x'' = x' + \beta/s$; therefore $x' = \bar{x} - \beta/p$. Since x'' cannot be larger than 1, s must be at least,

$$s \geq s_{\min} = \frac{\beta}{1 - x'} = \frac{\beta}{1 - \bar{x} + \beta/p}. \quad (2)$$

The difference of energies (per area) ε of the homogeneous ($\varepsilon_{\text{h}} = pu(x)$) and inhomogeneous (ε_{ih}) cases is,

$$\begin{aligned} \Delta\varepsilon &= \varepsilon_{\text{h}} - \varepsilon_{\text{ih}} = pu(x) - [(p - s)u(x') + su(x'')] \\ &= pu(x) - \left[(p - s)u\left(\bar{x} - \frac{\beta}{p}\right) + su\left(\bar{x} - \frac{\beta}{p} + \frac{\beta}{s}\right) \right]. \end{aligned} \quad (3)$$

In the case of $\Delta\varepsilon > 0$, the phase separation is energetically favorable, and also for the ratio $\hat{\varepsilon} = \varepsilon_{\text{h}}/\varepsilon_{\text{ih}} > 1$. If the total energy follows a $(1 - x)^\alpha$ -law, $\hat{\varepsilon} > 1$ for $\alpha < 1$ and $\hat{\varepsilon} < 1$ for $\alpha > 1$. Thus the enthalpy part with a sublinear slope favors phase separation and the strain energy with a (more or less) quadratic behavior stabilizes a homogeneous alloy distribution. For the actual total energy (black line in Fig. 9), which is almost linear, $\hat{\varepsilon}$ is close to

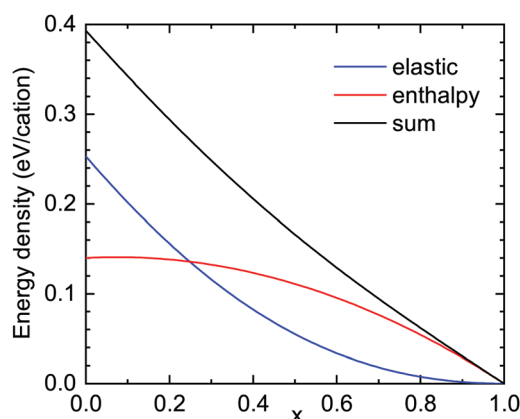


Fig. 9 Formation enthalpy (red, from ref. 13, zero for Al_2O_3) and elastic strain energy for pseudomorphic growth (blue) and their sum (black) for $(\text{Al}_x\text{Ga}_{1-x})_2\text{O}_3$ layers on r -plane Al_2O_3 .

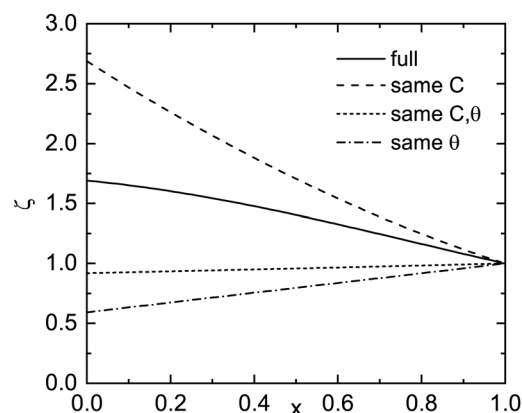


Fig. 10 Parameter $\zeta \propto$ strain energy divided by $(1 - x)^2$ for elastic strain energy for pseudomorphic $(\text{Al}_x\text{Ga}_{1-x})_2\text{O}_3$ layers on r -plane Al_2O_3 . The solid line shows the full calculation; for the other lines, the concentration dependences of the elastic constants (C), the r -plane angle θ (due to the change in the c/a -ratio) and both (C, θ), as labeled, have been neglected.



1 but slightly smaller, $\hat{\varepsilon} = 0.994$ for $s = s_{\min}$ (and approaches 1 for $s \rightarrow p$). For relaxation of 40% of the strain energy, $\hat{\varepsilon}(s_{\min}) = 1.01$ and becomes larger than 1. What can be taken from this is that the total energy situation is close to the instability point where the alloy can phase separate. If cation disorder is considered, the enthalpy term becomes smaller by approximately a factor of two,³³ favoring alloy homogeneity. However, other energies such as surface or interface energies have not been considered here.

The epitaxial growth stabilizes the corundum phase in the first place but an alloy composition instability evolves. Besides total energy arguments, certainly the kinetics of formation can also play a role. A possible growth model includes the enrichment of physi-sorbed Al on the growth surface up to one and a half extra monolayers which subsequently blocks gallium incorporation and is chemisorbed into the thin film. Possibly an extreme case of alloy ordering is observed here. Whether this happens at growth temperature or during cooling cannot be determined from the given experiments.

A well-known case of alloy ordering is the Ga/In monolayer ordering along $\langle 111 \rangle$ in $\text{Ga}_{0.5}\text{In}_{0.5}\text{P}$.³⁸ For the growth of $(\text{Ga}_{0.75}\text{Al}_{0.25})\text{As}$ on (110) GaAs, Al/Ga-cation ratio modulation along the growth direction was reported in ref. 39 and a 7 nm periodic (unquantified) change in the Al/Ga-ratio for growth on the (111)-plane was observed in ref. 40. AlAs (or Al-rich) monolayers within an $(\text{Al}_{0.3}\text{Ga}_{0.7})\text{As}$ alloy along [110] were reported in ref. 41. Since the lattice-mismatch between (Al,Ga)As and GaAs is very small, strain effects are not made responsible.

A bulk of literature has been devoted towards the theoretical treatment of lateral (in-plane) composition fluctuations^{42–44} that have been observed for several cubic and hexagonal semiconductor alloy systems, e.g. ref. 45 and 46. A microscopic model for the observed vertical segregation mechanism(s) here, however, seems missing. We therefore suggest that the observed effect, possibly due to an interplay of growth kinetics and alloy mixing effects, makes an atomistic modeling of the growth kinetics and alloy ordering necessary.

4 Summary and conclusion

In summary, direct evidence for structural defects associated with the plastic relaxation mechanisms of corundum-phase $(\text{Al}_x\text{Ga}_{1-x})_2\text{O}_3$ thin films on (01.2) r -plane Al_2O_3 has been presented. The initial relaxation *via* prismatic slip is subsequently joined by basal slip. For an epitaxial layer with a fairly low Al cation fraction ($x \approx 0.6$) which is expected to be metastable in the bulk, a peculiar alloy instability has been found, leading to the doubly-periodic inclusion of Al-rich slabs, pure Al_2O_3 or close to it. These findings may pose limits on the controllability of the growth of α -phase $(\text{Al,Ga})_2\text{O}_3$ -based heterostructures, at least for the substrate plane and growth conditions investigated here.

Conflicts of interest

There are no conflicts to declare.

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