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#### Broader context

The product selectivity zones in gas diffusion electrodes during the electrocatalytic reduction of CO<sub>2</sub>†

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Here we report on the most prominent factors influencing the performance of a Cu-based  $CO<sub>2</sub>$ electrolyzer operating at high currents. Using a flow-electrolyzer design where  $CO<sub>2</sub>$  gas feed passes directly through the electrode interacting with the Cu catalyst layer, we observed that the selectivity of the electrochemical  $CO<sub>2</sub>$  reduction in (bulk) pH neutral media can greatly be influenced by adjusting the structure of the electrode. In this, the variations in catalyst loading and ionomer content can profoundly affect the selectivity of  $CO<sub>2</sub>RR$ . We explore the hypothesis that this originates from the overall mass transport variations within the porous catalytic layer of the gas diffusion electrode. As further evidence for this, apart from the  $CO<sub>2</sub>$  electrolysis results, we propose a special method to benchmark the reactant mass transport in flow-cells using oxygen reduction reaction (ORR) limiting current measurements. Our analysis suggests that a restriction of mass transport is highly desirable due to its connection to a local alkalization and corresponding suppression of pH-dependent reaction products, given the absence of local CO<sub>2</sub> concentration limitations. We further show how the electrode structure can be used to push the observed catalytic  $CO_2$  reduction selectivity either towards  $C_1$  or  $C_{2+}$  products, dependent on the ionomer content and catalyst loading in a cathodic current range of 50 to 700 mA cm<sup>-2</sup>. Measurements at various KHCO<sub>3</sub> electrolyte concentrations agree with the notion of the local pH dictating the overall selectivity and point towards the presence of pronounced concentration gradients within the system. Overall, our work suggests that the differences in electrocatalytic  $CO<sub>2</sub>$  reduction selectivity at high currents (in a range of pH neutral buffering electrolytes) largely originate from the local concentration gradients defined by the initial catalyst ink formulation and architecture of the catalytic layer, both of which represent a powerful tool for optimization in the production of selected value-added products. **PAPER**<br> **(a)** Check for undates<br> **EXECUTE:**<br> **CALCOMETER STATES TO CONSULT AND THE PRODUCT Selectivity zones in gas diffusion<br>
electrocastalytic reduction<br>**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and**  $\frac{1}{2}$  **and \frac{1}{2}** 

fuels by upcycling waste-CO<sub>2</sub> into value-added compounds. Over the recent years, much progress has been made by fabrication of catalysts into so-called gas diffusion electrodes (GDEs) to tackle the issue of low CO<sub>2</sub> solubility in aqueous electrolytes and to advance towards commercially viable current densities of >300 mA cm<sup>-2</sup>. Though the selectivity towards CO<sub>2</sub>RR could be largely improved over the competing HER using GDEs, the underlying factors for an efficient production of the individual CO<sub>2</sub>RR products remain elusive. In the present study, we deploy a flow-electrolyzer system to investigate structure-selectivityinterrelations of a Cu-based GDE in a buffering electrolyte. By systematic investigation of three parameters: (i) particle catalyst loading, (ii) ionomer to catalyst ratio and (iii) buffer capacity, we set out to understand the structural properties that dictate the spatial variation of the selectivity across the catalyst layer at high reaction rates. Thereby, we describe a sequence of zones of distinct selectivity within the catalyst layer (''selectivity zones''), which arise from the inhomogeneous distribution of the reactants ( $CO<sub>2</sub>$  and pH) and control the overall selectivity of the system.

The electrocatalytic CO<sub>2</sub> reduction reaction (CO<sub>2</sub>RR) on Cu-based catalysts has the potential to enable the sustainable production of commodity chemicals and

# Introduction

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The direct electrochemical  $CO_2$  reduction reaction  $(CO_2RR)$  has been emerging as a potential technology for storage of renewable energy and sustainable production of carbon-based chemicals.<sup>1</sup> In this area, the catalyst research has mainly been



#### Paper Energy & Environmental Science

focused on Cu due to its capability to reduce  $CO<sub>2</sub>$  towards valueadded, post-CO products, such as hydrocarbons and alcohols.<sup>2</sup> The control over the electrocatalytic selectivity has been the focal point of Cu-based catalyst research, due to parallel reaction pathways and the resulting mixture of products.<sup>3</sup> Various modifications of Cu have been investigated in order to steer the selectivity towards distinct products, as for instance exposure of specific facets through nanostructuring and altered catalyst composition through oxidative treatments or addition of second metals.4–7 Apart from the catalyst itself, the reaction conditions have been repeatedly reported to influence the selectivity of the  $CO<sub>2</sub>RR$ . For instance, local pH value gradients establishing at the electrode electrolyte interface, also described as alkalization, were shown to have a decisive impact on reaction selectivity by suppression of mechanistic pathways dependent on the proton transfer as a rate-limiting step. $8-10$  Studies performed in very commonly used  $KHCO<sub>3</sub>$  electrolytes with neutral bulk pH, show that the local pH gradients near electrode surface essentially arise from a deficient mass transport unable to buffer the cathodic production of OH<sup>-11-13</sup> For H-type setups, effects of variations in the structure of the catalytic layer have been repeatedly reported to influence the mass transport, critically altering the reaction environment and therefore determining the observed selectivity of the system during electrochemical  $CO<sub>2</sub>RR$ . Here, the mass transport can be divided into a transport of reactants directed towards the surface and a transport of products leaving the surface. On the reactant side, in the aqueous electrolyte dissolved,  $CO<sub>2</sub>$  is transported towards the catalytic sites, where abundantly available water molecules supply the protons to form reduced carbon compounds under production of OH<sup>-</sup>. The generated OH $^-$  can readily react with the commonly used  $\mathrm{HCO_3}^-$  electrolyte acting as a buffer. However,  $HCO_3^-$  transport from the bulk towards the surface is not sufficiently fast to keep up with the OH<sup>-</sup> production rate, which locally shifts the pH and bicarbonateequilibrium near the reaction sites. This effect of local alkalization during  $CO<sub>2</sub>RR$  was observed experimentally at already moderate potentials by surface enhanced IR and Raman spectroscopy, simulated based on bicarbonate equilibria and often suggested to be the origin of a high selectivity for multi-carbon products during electrochemical  $CO_2RR$ .<sup>12,14-18</sup> On the products side, carbon compounds need to be transported away from the surface to allow for further reactants to fill in. However, the sustained presence of reactive intermediates such as CO have also been reported to show a beneficial effect on production of ethylene and oxygenates, and was also suggested to show a suppression for the competing HER from water reduction due to the occupation of the reactive sites. $19-23$  Generally, an increasing thickness of the catalytic layer, together with the associated electrochemically active surface area (ECSA), increases the mean path of transportation for the reactants and products. This has been proposed to impede a homogeneous through-plane mass transport within the catalytic layer, which results in more pronounced concentration gradients throughout the system.<sup>12,15,24</sup> Accordingly, it has been suggested for mesoporous Ag electrodes of various thicknesses that the  $CO<sub>2</sub>RR$  selectivity is sensitive to the concentration gradients and shows the strongest suppression of the competing **Paper**<br> **Focused on 13 October 2021. Some also are the second on 14 October 2021. The second on 14 October 2021. The second of the second of the second of the second of the second on 14 October 2022. The second of the cr** 

HER for the thickest electrode at the lowest part of the catalytic layer, where the effect of alkalization was most pronounced.<sup>25,26</sup>

Recently, the field of  $CO<sub>2</sub>RR$  has progressively moved towards studies of the high current regime in pH neutral and alkaline, gas-feed flow-electrolyzers to approach technological rates.<sup>27-29</sup> As the cathodic production of OH<sup>-</sup> is a function of the current, flow-electrolyzers in buffered electrolytes have been suggested to be particularly affected by local alkalization due to insufficient  $\mathrm{HCO_3}^-$  transport and the observed high selectivity for  $C_{2+}$  products has been, at least in part, associated to that effect.<sup>30–32</sup> Additionally, the depletion of  $CO<sub>2</sub>$  near the catalyst surface has also been reported to limit the accessible  $CO<sub>2</sub>RR$ currents and greatly influence the observed catalytic selectivity.<sup>33-35</sup> Despite those indications for the crucial role of the electrode structure for high-current  $CO<sub>2</sub>RR$ , correlations similar to the impact of mass transport in low-current H-cells remain underexplored for gas diffusion electrodes in flow-electrolyzers. It is plausible that high rate  $CO<sub>2</sub>RR$  on GDEs in flow-cell electrolyzers shows the same fundamental correlations of mass transport and catalytic selectivity as those reported for H-cell setups. We propose that the catalytic selectivity of Cu during high rate  $CO<sub>2</sub>RR$  in pH buffering KHCO<sub>3</sub> electrolyte is largely controlled by the mass transport, which can be rationalized by a discussion of  $CO_2$  transport and transport of pH buffering  $HCO_3^-$  anions.

#### Flow-cell electrolyzer setup

We employed a flow-cell electrolyzer with three distinct compartments to investigate  $CO<sub>2</sub>RR$  electrolysis at high currents and catalytic rates (Fig. 1a). Two different solutions of 1 M  $KHCO<sub>3</sub>$  were used separately as anolyte and catholyte and continuously looped through the two liquid compartments divided by an anion conducting membrane. Anodic and cathodic reaction products were transported out of the respective compartments with the flow of the electrolytes. A convective stream of  $CO<sub>2</sub>$ was fed from the third compartment through the backside of the porous cathode towards the catalytic layer, which allowed a fast supply of reactant to the cathodic reaction sites.

#### Cathode electrode design and architecture

The cathode catalyst layer was deposited by airbrushing an ink containing a mixture of Nafion and cubic  $Cu<sub>2</sub>O$  nanoparticles on a carbon-based Freudenberg H23C2 gas diffusion layer serving as substrate. As anode, a commercially available dimensionally stable electrode composed of a Ti sheet covered by an Ir-MMO was routinely used. Throughout this study, we will refer to the uncoated Freudenberg H23C2 as the gas diffusion layer, ''GDL'', and to the particle-coated Freudenberg H23C2 as gas diffusion electrode, ''GDE''. Fig. 1b shows the schematic structure of a GDE prepared by spraycoating. In this system, the different elements of the GDE are spatially separated and can be assigned to different layers. The lowest layer consists of carbon fibers and acts as mechanical and conductive backbone of the entire structure. Next, the microporous layer (MPL) functions as conductive and hydrophobic substrate, which allows the electronic and  $CO<sub>2</sub>$  transport towards the adjoining catalytic layer. The hydrophobicity, gas permeability and electrical



Fig. 1 Schematic representation of a 3-compartment flow-cell electrolyzer with indications of the transport directions for reactants, products and electrolyte (a). Schematic representation of carbon-based gas diffusion electrode with cross-section (50 µm scalebar) and top view SEM images (400 nm scalebar) of a GDE prepared by spray-coating a dispersion of a cubic Cu<sub>2</sub>O catalyst with Nafion binder onto a carbon gas diffusion layer (b).

conductivity of the GDL are important parameters that influence the  $CO<sub>2</sub>RR$  performance and stability of the GDE. Especially, the hydrophobicity has proven decisive to maintain a sufficient gas  $(CO<sub>2</sub>)$  transport towards the catalytically active sites by preventing a ''flooding'' that is an extensive wetting of the porous GDE structure. For carbon-based GDLs an instability of the wetting characteristics has been observed under application of cathodic potentials and correlated to the catalytic activity towards HER of the carbon structure.<sup>36</sup> To circumvent this effect, PTFE membranes have been investigated as GDL materials, but can suffer from issues of electrical conductivity and mechanical instability.<sup>29</sup> In this study, we use a ''flow-through'' approach, depicted in Fig. 1(b), to minimize flooding issues connected to the use of a carbon-based substrate and focus exclusively on properties of the catalytic layer. The catalytic layer represents the uppermost element of the GDE and is the interface between gaseous transports of  $CO<sub>2</sub>$  and liquid transport of electrolyte. Within the catalytic layer, the electronic, ionic and reactant transport intersect and define the reaction environment of the electrocatalytic  $CO<sub>2</sub>RR$  and the reactivity of the system. The morphology of the catalytic layer obtained by spraycoating is not trivial and showed a porous, 3-dimensional appearance with a rough surface, visible in cross-section and top-view SEM images of Fig. 1b.

In this paper, we use a previously reported nanocubic  $Cu<sub>2</sub>O$ catalyst (see Fig. S1, ESI†) with an edge length of 35 nm to systematically alter the structure of the catalytic layer of a gas diffusion electrode (GDE) for tests in a flow-electrolyzer.<sup>37</sup> By changing macroscopic parameters, as the particle catalyst loading and the ionomer to particle catalyst ratio (Nafion content),

we influence the accessibility of catalytically active sites and the through-plane mass transport in the porous structure of the catalytic layer. In this, we correlate the electrode structure with restriction in mass transport, manifesting in local concentration gradients and alkalization, which in turn influences the selectivity of  $CO<sub>2</sub>RR$  during a high current density operation in a bulk neutral bicarbonate electrolyte. We chose our previously reported and well-characterized cubic  $Cu<sub>2</sub>O$  catalyst as a model catalyst system to investigate the influence of concentration gradients within a flow-cell electrolyzer by variation of three macroscopic parameters:

 Particle catalyst loading: first, we varied the amount of deposited catalyst particles to obtain GDEs with various catalyst loadings that show differences in layer thickness, roughness and ECSA. In doing so, we affect the mean path of transportation from the bulk sources of  $CO<sub>2</sub>$  and KHCO<sub>3</sub> towards the catalytic sites.

 Ionomer to particle catalyst ratio: to introduce an impediment for the mass transport, we varied the Nafion content of the ink formulation to obtain GDEs that show different ionomer to catalyst ratios for a constant absolute catalyst loading. Nafion acts as a strong adhesive to introduce a mechanical stability to the catalytic layer, however, the ionomer distribution is a known issue in fuel cell research due to its influence on local reactant transportation and associated mass (oxygen) transport resistances.<sup>38,39</sup> Likewise, the transport of reactants in  $CO<sub>2</sub>RR$  towards the active sites should also be sensitive to the local distribution of the ionomer, acting as a barrier for the  $CO<sub>2</sub>$ and  $HCO<sub>3</sub><sup>-</sup>$  transport.

 Buffer capacity: to induce various buffer capacities, we varied the concentration of the  $KHCO<sub>3</sub>$  electrolyte to alter the buffer capacity within our system. A higher concentration of HCO<sub>3</sub><sup>-</sup> offers more buffer capacity, in turn resulting in decreased pH gradients at the interface and counteracting the effect of alkalization.

The present work is not about setting new number records in product selectivity, but to pinpoint controlling factors for the product selectivity in a technological GDE under more realistic reaction conditions. To characterize the mass transport properties of CO<sub>2</sub>RR GDEs, we employ oxygen reduction limiting current measurements typically used in the hydrogen fuel cell community as diagnostic tool in the field of  $CO<sub>2</sub>$  reduction, the results of which reveal how closely GDE structure and the resulting catalytic selectivity are connected. The conclusions of this work are consistent with previous reports on the importance of near electrode surface  $pH$  and  $CO<sub>2</sub>$  concentration, but expand our understanding of the relationships between catalyst layer structure of a GDE and reaction selectivity during  $CO_2RR$ <sup>12,29,31,33,40,41</sup> The systematic investigation of the effects within our work prompt us to propose the notion of layered ''selectivity zones'', which has not been, to the best of our knowledge, previously described for a Cu-based GDE in a flow-electrolyzer. We believe that our selectivity zone model will aid the future design of efficient Cu-based GDEs for  $CO<sub>2</sub>$  electrolyzers in buffered electrolytes of near-neutral pH.

### Results

#### Effect of particle catalyst loading on  $CO<sub>2</sub>$  electrolysis

In Fig. 2, we present the distributions of four important products observed during  $CO_2RR$  on Cu:  $C_2H_4$ ,  $CH_4$ ,  $H_2$  and HCOO<sup>-</sup>, obtained at fixed applied current densities on electrodes containing varying catalyst loadings. The influence of catalyst loading on the product distribution has been tested at fixed concentration of 1.0 M KHCO<sub>3</sub> and at fixed binder content (10 wt% Nafion). Here, the FE of  $\rm{C_2H_4}$ ,  $\rm{CH_4}$ ,  $\rm{H_2}$  and  $\rm{HCOO}^-$  is displayed as a function of the applied current density for catalyst mass loadings ranging from 0.3 mg cm $^{-2}$  to 2.0 mg cm $^{-2}$ . We specifically focus on this set of products, as they have distinctly different rate-limiting reaction steps, which show either a strong pH-dependence (CH<sub>4</sub>, HCOO<sup>-</sup> and H<sub>2</sub>) or primarily independence  $(C<sub>2</sub>H<sub>4</sub>)$  and can therefore provide insight in the local reaction environment.<sup>42,43</sup> A first key observation is the clear suppression of all pH-dependent products  $(CH_4, HCOO^-$  and  $H_2$ ) at high mass loadings of the catalyst, which was invariably linked to a favored production of ethylene. Note how the FE of  $CH<sub>4</sub>$ , which is a preferred product during  $CO<sub>2</sub>RR$  at high proton concentration, plummeted to below 1%, as soon as catalyst loading was increased to 1.3 mg  $\text{cm}^{-2}$  and higher. In contrast, in experiments using very low catalysts loadings of below 0.4  $\mathrm{mg}\,\mathrm{cm}^{-2}$  the FE for CH<sub>4</sub> raised

to above 20%, see Fig. 2b. While this trend was qualitatively in line with the production of  $H_2$  and  $HCOO^-$  (Fig. 2c and d) the change in FE for  $C_2H_4$  showed the opposite behavior, see Fig. 2a. Here, the decrease of catalyst loading below 0.4 mg  $cm^{-2}$  resulted in a FE for  $C_2H_4$  of below 20%, whereas higher loadings allowed for a more selective  $C_2H_4$  production and increased FE to around 30%. Due to the well-known sensitivity of  $CO<sub>2</sub>RR$  selectivity to the electrode potential, we plotted the product FE against IR-free RHE potentials in Fig. S2 (ESI†). Note that as the shift in selectivity is also visible on an IR-free potential scale, we thereby succeed in excluding variations in electrode potential as the sole origin of the observed effect. Additional information of FE for the remaining  $CO<sub>2</sub>RR$ products (EtOH, PrOH and CO) are given in Fig. S3 (ESI†) and agree with the observed favorable production  $C_{2+}$  compounds at high catalyst loadings. We also plotted the FE of gas products as a function of time, see Fig. S4 (ESI†), which confirmed the applied current density as cause for the observed change in selectivity over the investigated testing time of 18 hours. Only for the low loading samples of 0.3 mg cm<sup>-2</sup> and 0.4 mg cm<sup>-2</sup> a decline in  $CO_2RR$ selectivity could be observed at constant current, which suggests a decreasing stability with decreasing particle catalyst loading. Morphological investigation of the GDEs prepared by deposition of various catalyst loadings showed a clear dependence on the absolute catalyst loading. Here, top-view SEM images after  $CO<sub>2</sub>$ Purer<br>
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Fig. 2 Faradaic efficiency as a function of applied current density at varying catalyst mass loadings for  $C_2H_4$  (a), CH<sub>4</sub> (b), H<sub>2</sub> (c) and HCOO<sup>-</sup> (d). Reactions were conducted under following conditions: 3 cm<sup>2</sup> of geometric surface area of cathode, 1 M KHCO<sub>3</sub> and 10 wt% of Nafion used as binder in catalyst ink. Additional products (CO, EtOH, and PrOH) are given in Fig. S3 of the ESI.† Dashed lines are shown to guide the eye.

electrolysis are given in Fig. S5a and b (ESI†). We observed a progressive roughening and introduction of pores to the surface upon increase of particle loading. Such structural changes suggest an increase in electrochemically accessible surface area (ECSA), which we have investigated by quantification of the electrochemical charging of the double layer (see Fig. S6, ESI†). As a measure of the ECSA, we calculated the double-layer capacitance, shown in Fig. S5c (ESI†), which showed an increase with particle loading and agrees with our observation of a progressive surface roughening in SEM images. In accordance with an increased ECSA, we noticed a higher catalytic activity during  $CO<sub>2</sub>RR$  for the high particle loadings visible in the polarization curves of Fig. S5d (ESI†). Our observations suggest that the catalytic selectivity during high-rate  $CO<sub>2</sub>RR$  is sensitive to the structure of the catalytic layer, which can be affected by variation of the catalyst loading. We suspect that the correlation between catalytic selectivity and catalyst loading originates in changes of the mass transport (e.g. transport of  $CO_2$  and  $HCO_3$ <sup>-</sup>), which in turn affect the local pH and reactant concentration near the electrode.

#### Effect of particle catalyst to ionomer ratio (Nafion content) on CO<sub>2</sub> electrolysis

In order to further investigate the mass transport as potential origin of shifts in catalytic selectivity, we varied the binder

content within the catalytic layer. Inspired by fuel cell research, we suspect that increasing amounts of ionomer within the catalytic layer represents a barrier for the mass transport of reactive species as dissolved  $CO_2$  and  $HCO_3^-$  towards reaction sites. Fig. 3 shows the effect of an increase in Nafion content within the catalytic layer of a GDE on the selectivity during  $CO<sub>2</sub>RR$ . A suppression of CH<sub>4</sub> and HCOO $^-$  is evident in samples with high Nafion content, see Fig. 3b and d, similar to what we have observed at high catalyst mass loadings. Interestingly, samples with high Nafion content (30 and 50 wt%) show a suppression of HER and increased  $C_2H_4$  FE only at a relatively low current density of smaller than 300 mA  $cm^{-2}$  (Fig. 3a and c). A further increase of current density, results in a strong rise of FE for HER at the cost of total  $CO<sub>2</sub>RR$  FE. We suspect that this change in selectivity at high currents is caused by an excessive content of Nafion, which reduces the mass transport to a point, where the reactant  $(CO<sub>2</sub>)$  transport becomes limiting for  $CO<sub>2</sub>RR$  and causes the HER to dominate in the process. While such a correlation between the Nafion content and the limited reactant transport is restricting for  $CO<sub>2</sub>RR$  selectivity for a current density larger than 300 mA  $cm^{-2}$ , it shows an increase at lower rates. Excessive amounts of ionomer influence potentially the electrical accessibility of the catalyst particles, which is why we investigated the change in electrochemical double layer Experience of Froit Commons and Center of Posts Article is a control of the state of the state of the state of the common o



**Fig. 3** Faradaic efficiency as a function of applied current density with varying Nafion contents for  $C_2H_4$  (a),  $CH_4$  (b),  $H_2$  (c) and HCOO<sup>-</sup> (d). Conditions were as follows: 3 cm<sup>2</sup> of geometric surface area, 0.7 mg cm<sup>-2</sup> catalyst mass loading and 1 M KHCO<sub>3</sub>. Additional products (CO, EtOH, and PrOH) are given in Fig. S11 of the ESI.† Dashed lines are shown to guide the eye.

capacitance and catalytic activity. Here, we only observed minor changes in double layer capacitance with varied Nafion loading, but a lower catalytic activity of the 50 wt% Nafion sample was apparent (see Fig. S7, ESI†). Again, to exclude differences in electrode overpotential as cause of the observed trend, we plotted IR-free RHE electrode potentials against the product FE in Fig. S8 (ESI†), which still clearly shows the ionomer induced shift in selectivity. In agreement with our previous observation, the FE for gas products as a function of time showed only small changes at constant current for the electrodes prepared with different Nafion loadings, see Fig. S9 (ESI†), suggesting a stability of the system over the investigated testing time. Furthermore, we have also investigated the change in surface structure at different Nafion contents by SEM, shown in Fig. S10 (ESI†). Here, an intermediate content of Nafion (10 and 30 wt%) resulted in a rough surface of the catalytic layer, whereas the extreme cases of 0 wt% and 50 wt% showed a relatively smooth surface. Noteworthy is the pronounced coverage of the  $Cu<sub>2</sub>O$  cubes supposedly by the ionomer in the 50 wt% Nafion sample, visible in images of higher magnification, consistent with the idea of representing a distinct barrier for the mass transport. Additional  $CO<sub>2</sub>RR$ products (CO, EtOH and PrOH) are given in Fig. S11 (ESI†), which showed a higher selectivity for EtOH with increased Nafion content at moderate currents. Our observations on the effects of increased Nafion content are qualitatively in line with the effect of particle catalyst loading. In both cases, we generally observed a higher selectivity for  $C_{2+}$  products when either binder content or particle loading was increased. It seems feasible that a similar origin causes the observed selectivity shifts, given their high qualitative agreement. **Example 2021**<br> **Context** Article consider the consideration of the considered on the consideration of the consideration of the considera

#### Effect of buffer capacity (KHCO<sub>3</sub> concentration) on  $CO<sub>2</sub>$ electrolysis

Fig. 4a-f shows the influence of the bulk  $KHCO<sub>3</sub>$  concentration on the  $C_{2+}$  ( $C_2H_4$ , EtOH and PrOH) and  $C_1$  (CH<sub>4</sub>, HCOO<sup>-</sup>) selectivity during  $CO<sub>2</sub>$  electrolysis in the flow-cell. Here, we used different Nafion contents of 10 wt% to 50 wt% and a constant catalyst loading of about 0.7 mg  $\rm cm^{-2}.$  For the 50 wt% Nafion sample we observed no significant change in catalytic selectivity, when increasing electrolyte concentration from  $0.1$  M to  $1.0$  M KHCO<sub>3</sub>, see Fig. 4a and d. Both concentrations showed the highest  $C_{2+}$  selectivity of roughly 40% FE at 200 mA  $cm^{-2}$ , whereas a larger current density resulted in the increase of the competing HER (Fig. S12a, ESI†). Further increase of KHCO<sub>3</sub> electrolyte to 3 M lowered the  $C_{2+}$  FE and favored HER over the whole investigated current range. In contrast, the FE for  $C_1$  products seemed largely unaffected by the change in  $KHCO<sub>3</sub>$  concentration. Next, the 30 wt% Nafion sample showed a clear dependence of  $C_{2+}$  and  $C_1$  FE on the KHCO<sub>3</sub> concentration during  $CO<sub>2</sub>RR$ , see Fig. 4b and e. While we were able to achieve a combined  $C_{2+}$  FE of almost 70% at 600 mA  $\text{cm}^{-2}$ , the use of higher KHCO<sub>3</sub> concentrations of 1 and 3 M led to a decreased  $C_{2+}$  FE to around 50% and 30%, respectively. For the FE of  $C_1$  products we observed an inverse behavior, here 3 M KHCO<sub>3</sub> showed the highest combined  $C_1$  FE of roughly 20%, while the use of 1 M and 0.1 M KHCO<sub>3</sub> led to a subsequent decrease. Our observations during  $CO<sub>2</sub>RR$ , using a 10 wt% Nafion sample were quite similar to the case of a 30 wt% Nafion sample, see Fig. 4c and f. Again, we achieved the highest  $C_{2+}$  selectivity at the lowest KHCO<sub>3</sub> concentration of 0.1 M,



Fig. 4 Effect of variations in KHCO<sub>3</sub> concentration on the CO<sub>2</sub>RR selectivity towards C<sub>2+</sub> products using 50 wt% (a), 30 wt% (b), and 10 wt% (c) of Nafion. Effect of variations in KHCO<sub>3</sub> concentration on the CO<sub>2</sub>RR selectivity towards C<sub>1</sub> products using 50 wt% (d), 30 wt% (e), and 10 wt% (f) of Nafion. In all cases Cu<sub>2</sub>O loading was const. at 0.7 mg cm<sup>-2</sup>. Additional information on FE of H<sub>2</sub> and CO are given in Fig. S12 (ESI†).

which enabled a combined FE of almost 60% over a broad range of cathodic currents. The use of an increased  $KHCO<sub>3</sub>$  concentration of 1 and 3 M resulted in a dramatically decreased  $C_{2+}$  FE of 40% and 5%, respectively. At the same time, the highest  $C_1$  FE observed on the 10 wt% Nafion sample increased from a maximum of 13%, towards 17% and roughly 23% for respective  $KHCO<sub>3</sub>$  concentrations of 0.1 M, 1.0 M and 3.0 M. In parallel to the  $CO<sub>2</sub>RR$ , the HER also proved sensitive to  $KHCO<sub>3</sub>$  concentration and showed an overall increase with  $KHCO<sub>3</sub>$  concentration, whereas the 50 wt% sample seemed to be generally less sensitive to the buffer concentration (Fig. S12a–c, ESI†). At all Nafion contents we observed a higher selectivity for  $C_{2+}$  products and generally lower HER and  $C_1$ FE, when we employed  $KHCO<sub>3</sub>$  electrolytes of a lower concentration during electrolysis, however, this effect seemed to be dependent on Nafion content and was most pronounced for the lowest Nafion content of 10 wt%.

#### Implementation of the ORR as a diagnostic tool for benchmarking the mass transport limitations within a complex porous electrode system

As the effects of the local pH, the mass transport and the catalyst kinetics are superimposed and, therefore, often difficult to be

unambiguously deconvoluted, especially due to parallel reaction pathways of  $CO<sub>2</sub>RR$  on Cu and the competing HER, we resorted to the oxygen reduction reaction (ORR) for further discussion of the correlation between binder content and mass transport. In doing so, we were able to exploit the more positive standard reduction potential of the ORR, with respect to the  $CO<sub>2</sub>RR$ , to fully avoid the HER. Hence, we obtained data that we can interpret with overall less complexity, schematically depicted in Fig. 5a. We take the view that such an approach allows for a more direct investigation of the mass transport limitations within our system. To probe the mass transport towards the catalytically active centers of the  $Cu<sub>2</sub>O$  particles, we varied the partial pressure of  $O_2$  in an  $N_2$  feed at a constant electrode potential of  $-0.45$   $V_{\text{RHE}}$ . We chose this potential to achieve the highest possible rate of ORR, while avoiding a region of considerable HER activity, indicated in Fig. 5b. By tracing the change in ORR current as a function of  $O_2$  partial pressure at a fixed electrode potential, we can directly access changes in mass transport caused by variations in binder content. In Fig. 5c, we can see a rise in ORR current with increase in partial pressure of  $O<sub>2</sub>$  until around 0.3 bar, where the ORR current of the 10 wt% Nafion sample approaches a Experimental Science<br>
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Fig. 5 Schematic representation of CO<sub>2</sub>RR and ORR on the Cu surface of a GDE (a). Cyclic voltammetry under different ratios of O<sub>2</sub>/N<sub>2</sub> saturated gas atmosphere in 2 M KHCO<sub>3</sub> for a 10 wt% of Nafion GDE. Different colors are indicating a potential regime of pure ORR or mixed regime of HER and ORR (b). ORR current as a function of partial O<sub>2</sub> pressure from O<sub>2</sub>/N<sub>2</sub> mixtures in 2 M KHCO<sub>3</sub> for different Nafion contents in the catalytic layer at a constant electrode potential of  $-0.45$  V<sub>RHE</sub> with dashed lines to guide the eye. Different levels of shading indicate the primary limitation, either mass transport or reaction kinetics (c).

plateau. This transition supposedly originates in a change from a primarily mass transport dominated regime, towards one, were activation resistances are denying higher reduction rates. The regimes of mass transport and catalytic kinetics are indicated by different levels of shading in Fig. 5c, but should be rather understood as a visual orientation and not as a strict border between the two. A comparison of three samples with Nafion loadings ranging from 10 to 50 wt% shows an increased ORR current in the mass transport domain of below 0.3 bar of  $O<sub>2</sub>$  partial pressure for lower loadings of the ionomer, however, this difference seemed to decrease progressively with a higher partial  $O_2$  pressure (Fig. S13, ESI†). The observed behavior suggests that the mass transport remains limiting even at higher O<sub>2</sub> partial pressure for samples of high Nafion content, whereas samples of reduced binder content showed primarily kinetic limitations at a similar partial pressure of  $O<sub>2</sub>$  and constant electrode potential. Our results suggest that the binder content of the catalytic layer of a GDE interferes with the reactant transport. Here, a high binder content induces larger resistances for the reactant transport and can lead to significant mass transport limitations. Puper<br>
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## **Discussion**

#### Electrode structure determines concentration gradients during CO<sub>2</sub> electrolysis

Combining our observations, we can schematically depict the proposed influence of the catalytic layer structure on the selectivity during high-rate  $CO<sub>2</sub>RR$  electrolysis in a pH-neutral buffering media. Fig. 6a, shows a schematic GDE and illustrates the relevant reactions, as well as the through-plane transport of reactants and products in the catalytic layer during  $CO<sub>2</sub>RR$ . While  $CO<sub>2</sub>$  is fed in a gaseous state to the GDE, we take the view that  $CO<sub>2</sub>$  is highly likely to physically dissolve in the electrolyte prior to its reduction on the catalyst surface due to the presumable presence of a native solvent layer caused by the hydrophilicity of charged electrodes. Accordingly, the transport of reactive species (CO<sub>2</sub> and HCO<sub>3</sub><sup> $-$ </sup>) and products has to occur through a diffusion layer of finite thickness to reach or leave the electrode surface. On the catalyst, OH<sup>-</sup> is being produced during the reductive reaction of  $CO<sub>2</sub>$  and  $H<sub>2</sub>O$ . The OH<sup>-</sup> can readily react with the present buffering  $\mathrm{HCO_3}^-$  anions that are diffusively transported from the bulk electrolyte, which reduces



Fig. 6 Scheme qualitatively visualizing the flux of reactive species and products with indications of their respective transport directions throughout the structure of a Cu-GDE during  $CO_2$ RR in KHCO<sub>3</sub> (a). Schematic representation of the proposed influence of variations in the particle catalyst loading (b and c) and the ionomer to catalyst ratio (b and d) on the concentration gradients of HCO<sub>3</sub><sup>-</sup> (grey), CO<sub>2</sub> (red) and OH<sup>-</sup> (blue) throughout the catalytic layer.

the local pH increase near the surface and creates  $\overline{{\rm CO_3}^{\rm 2-}}$  in the process. The change of the local pH is a function of the current density that is a measure of the OH<sup>-</sup> production rate and the molar flux of  $HCO_3^-$  anions transported towards the electrode surface in a diffusive manner. The generated  $CO_3^2$  is being transported towards the bulk of the electrolyte, where it can equilibrate with excess  $CO<sub>2</sub>$  to regenerate the buffer by formation of  $HCO_3^-$ , therefore, preventing larger changes in bulk pH. It is important to note that in GDEs the source of  $CO<sub>2</sub>$  and buffering  $HCO_3^-$  anions are on opposing sides as indicated by opposed directions of arrows in Fig. 6a. This phase asymmetric feed implies a largely decoupled transport of dissolved  $CO<sub>2</sub>$ and  $HCO_3$ <sup>-</sup> towards the electrode surface of GDEs in flowelectrolyzers, which is in contrast to conventional electrodes that are fully submerged in liquid electrolytes during  $CO<sub>2</sub>RR$  in H-cell setups.

The proposed effect for variation of ionomer to catalyst ratio (Nafion content) and particle catalyst loading is depicted in Fig. 6b–d and is largely associated to the through-plane concentration gradients of  $CO_2$  and  $HCO_3^-$  within the catalytic layer. Here, the effect of increasing the particle catalyst loading can be rationalized by a larger mean path of transportation for  $CO<sub>2</sub>$ and  $HCO_3^-$  through the thicker catalytic layer. This longer distance of transportation results in a further decrease along the concentration gradients for both species, see Fig. 6b and c. This would in turn cause regions of high alkalinity and depletion of  $CO<sub>2</sub>$ , respectively. We suspect that the increase in Nafion content causes a quite similar drop in reactant concentration throughout the layer. Here, as we have shown from our ORR measurements, an extensive content of Nafion in the catalytic layer presents a barrier for the mass transport of reactants, e.g.  $O_2$  or  $CO_2$ , towards the Cu sites. Such impediment of the mass transport can be rationalized by a slower through-plane transport of reactants  $(CO_2$  and  $HCO_3^-$ ) and steeper associated concentration gradients perpendicular to the catalytic layer, see Fig. 6b and d. Essentially, the outcome is similar to the increased particle loading and results in regions of high alkalinity and depletion of  $CO<sub>2</sub>$  at high ionomer content. Additionally, both, the Nafion content and particle catalyst loading influenced the apparent morphology of the catalyst layer (see Fig. S5 and S10, ESI†), which has often been reported in literature to change the catalytic selectivity. However, given the comparatively small change in double layer capacitance (see Fig. S6 and S7, ESI†), we take view that such morphological changes did not critically influence the overall performance. A more detailed discussion on the change in morphology can be found in the ESI† of this work. Chere of the content of state on the surface of the content of the commons are also the content of the commons are co

Finally, the effect of an increased  $KHCO<sub>3</sub>$  bulk concentration can also be rationalized by a discussion of the  $\mathrm{HCO_3}^-$  concentration gradient. Here, the generally higher  $\mathrm{HCO_3}^-$  concentration offers a higher buffer capacity and can in turn reduce the pH gradient throughout the catalytic layer. An additional effect could be caused by the sensitivity of the physical solubility of  $CO<sub>2</sub>$  for the ionic strength, which could lead to a depletion of  $CO<sub>2</sub>$  reactant at high KHCO<sub>3</sub> concentrations.

In line with the proposed emergence of concentration gradients, as suggested within the present work and visualised in Fig. 6, previous studies reported on considerable local deviations from bulk reactant concentrations during  $CO<sub>2</sub>RR$ based on calculations from transport models. Here, most studies focused on the electrode to catholyte interface and described a depletion in  $CO<sub>2</sub>$  concentration and an increase in OH<sup>-</sup> and  $CO_3^2$ <sup>-</sup> concentration in this near-electrode surface region. The magnitude of the emerging concentration gradients was suggested to be heavily dependent on the diffusion layer thickness, which is highly sensitive to convective interferences through effects such as buoyancy.<sup>12,14,31,44</sup> Studies that additionally included the thickness of an extended catalyst layer in their transport models reported on an inhomogeneous reactant concentration throughout the catalyst layer during high-rate electrolysis, which is qualitatively in agreement with our proposition depicted in Fig.  $6.26,32,45$ 

#### Concentration gradients establish ''selectivity zones''

As a consequence of the through-plane concentration gradients for  $CO<sub>2</sub>$  and pH within the catalytic layer, we propose zones of distinctly different  $CO<sub>2</sub>RR$  selectivity as a function of distance from the MPL substrate in direction of the catholyte, shown in Fig. 7. Here, a schematic cross section of a GDE with indications for the suggested change in local reaction environment and catalytic selectivity dependent on the spatial location within the catalytic layer is depicted. The zone closest to the MPL shows the highest proximity to the gaseous  $CO<sub>2</sub>$  feed and furthest distance from the bulk  $KHCO<sub>3</sub>$  electrolyte, which results in a region of high pH and  $CO<sub>2</sub>$  concentration. With increasing distance from the MPL, those conditions reverse and can result in a  $CO<sub>2</sub>$ -deficient zone with lower pH value. Our observed experimental catalytic  $CO<sub>2</sub>$  selectivities directly correlate and support the zone model. Here, the region of high  $pH$  and  $CO<sub>2</sub>$  concentration directly adjacent to the MPL gives optimal conditions for selective production of pH independent  $CO<sub>2</sub>RR (C<sub>2+</sub>)$  products, as ethylene. With further distance from the MPL, the pH value decreases and the catalytic selectivity can shift towards  $CO<sub>2</sub>RR$  products, which are preferred at higher proton concentration  $(C_1)$ , e.g. CH<sub>4</sub>. Finally, in the outermost region of the catalytic layer  $CO<sub>2</sub>$  concentration might become deficient, which shifts the catalytic selectivity towards an increased competition by HER. The proposed ''selectivity zone'' model is qualitatively in line with recent computational studies that report on pronounced differences in spatial production rates for individual  $CO<sub>2</sub>RR$  products throughout the extended structure of the catalyst layer. Based on micro kinetic calculations, the studies revealed pronounced differences in local reaction rates that arise from a non-uniform reactant distribution. The reactant concentration gradients have been described to establish in-plane as well as through-plane of the catalyst layer, causing a complex spatial distribution in  $CO_2RR$  and HER activity.<sup>26,32,45,46</sup>

Based on the proposed selectivity zones, a selective  $CO<sub>2</sub>RR$ electrolyzer for production of  $C_{2+}$  compounds in buffering electrolytes would require the deliberate introduction of an impediment for the transport of buffering anions. This could



Fig. 7 Schematic cross section of a Gas Diffusion Electrode (GDE) of a CO<sub>2</sub> electrolyzer comprising the Gas Diffusion Layer, GDL (including its Microporous Layer, MPL) and Cu catalyst layer (not drawn to scale). Focus is on the cross section of the enlarged Cu catalyst layer illustrating the concept of spatial "selectivity zones". Zones are denoted by their major reduction products ("C<sub>2+</sub>" blue, "C<sub>1</sub>" aqua, and "H<sub>2</sub>" green). Origin of the zones are the spatial through-plane variations in local pH (proton activity, red arrow) and local CO<sub>2</sub> concentration (CO<sub>2</sub> availability, blue arrow). The red and black spatial distribution curves illustrate schematically the production rate of hydrogen and the production rate ratio of  $C_{2+}/C_1$ .

be realized by controlling the structure of the GDE through an increased thickness and a higher density of the catalytic layer, if the transport of  $CO<sub>2</sub>$  remains sufficient. Next to the discussed parameters within this work, further structural control of the catalytic layer could be achieved by variations in the deployed catalyst particle size or introduction of conductive supporting materials of a defined porosity. Additionally, operation conditions could achieve a similar effect and contribute for further increase in  $C_{2+}$  selectivity. Here, lowering electrolyte flow-rates and avoiding bubble formation at the electrode to electrolyte interface could reduce the interfacial convection and in turn lead to creation of an increased hydrodynamic boundary layer thickness, further limiting the transport of buffering anions. We hypothesize that the notion of spatial ''selectivity zones'' (selectivity zone model) has a broader validity; as a result of this, the structure–selectivity-relationships described here should be also applicable to other (non-Cu)  $CO<sub>2</sub>RR$  systems or even to other reaction processes in GDEs. Similar interrelations of catalyst layer thickness and  $CO<sub>2</sub>RR$  selectivity in buffered electrolytes have been reported for CO evolving systems of Ag and Au catalysts, as well as for systems deploying Sn particles for selective formation of HCOO<sup>-</sup>.<sup>25,47-51</sup> At its core, the selectivity zones model describes a dependency of the HER and  $CO<sub>2</sub>RR$  reaction rates on the spatial reactant concentration due to concentration overpotentials and accordingly should apply to various systems in the field of electrocatalytic  $CO<sub>2</sub>RR$ .

## Conclusion

In this study, we have investigated relations between electrode structure, more specifically, catalyst loading and Nafion content,

and the resulting product selectivity of Cu-based  $CO<sub>2</sub>RR$  electrolysis at high currents in a bulk pH-neutral flow-electrolyzer. We found that with increasing catalyst loading, that is catalyst layer thickness, or Nafion content the production of pH-sensitive products (e.g.  $H_2$ , CH<sub>4</sub> and HCOO<sup>-</sup>) could be suppressed and C<sub>2+</sub> species were produced more selectively. To explain this, we showed that the Nafion content influences the mass transport using an ORR limiting current analysis at varying oxygen partial pressure as a diagnostic tool. We concluded that such changes in mass transport define and control the local reaction environment in form of  $pH$  and  $CO<sub>2</sub>$  concentration, and hence can be used to deliberately tune the reaction selectivity. Here, concentration gradients in through-plane direction of the porous catalytic layer are more pronounced and shift the observed catalytic selectivity during  $CO<sub>2</sub>RR$  electrolysis. Varying the KHCO<sub>3</sub> electrolyte concentration showed that the selectivity of the system is highly sensitive to the concentration of the buffering media and agreed with our proposal that the local pH variations are crucial in determining the  $CO<sub>2</sub>RR$  selectivity. Our study demonstrates how the structure of the catalytic layer is a key parameter to influence local mass transport and provides an effective way to tune the selectivity during pH neutral (bulk)  $CO<sub>2</sub>RR$  electrolysis at high currents.

# Conflicts of interest

There are no conflicts to declare.

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