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# Polysulfone metal-activated carbon magnetic nanocomposites with enhanced CO<sub>2</sub> capture

Muhammad Nisar, <sup>a</sup> Pascal S. Thue,<sup>b</sup> Myriam B. Maghous,<sup>a</sup> Julian Geshev,<sup>c</sup> Eder C. Lima <sup>b</sup> and Sandra Einloft <sup>a</sup>

In the present study, polysulfone (PSF)-activated carbon nanocomposites were synthesized by a melt mixing technique. Here, 2 wt% activated carbon (CA, CA–Ni, and CA–Co) was used as filler, and effects on thermal, mechanical, magnetic, morphological, and carbon dioxide capture properties were studied. The pyrolysis of wood sawdust produced carbon materials activated by Co and/or Ni salt. The thermal degradation and the amount of metal in the carbon materials were investigated by thermogravimetric analysis. The maximum degradation temperature showed an improvement of up to 3 °C, while the initial degradation temperature decreased up to 4 °C with the addition of metal-activated carbons. The values of  $T_g$  estimated by differential scanning calorimetry appear to be practically identical for pure PSF and its nanocomposites. The elasticity modulus of the nanocomposite shows an enhancement of 17% concerning the neat PSF. The water contact angle showed a decrease with the incorporation of the fillers, indicating the hydrophilic nature of the composite. The carbon dioxide sorption capacity of the nanocomposite showed an enhancement of almost 10% in contrast to neat PSF. Ferromagnetic behavior of the thermoplastic nanocomposite was observed with the introduction of 2.0 wt% metal-carbonized filler. The exceptional magnetic properties, for a thermoplastic material such as polysulfone, make it promising for various industrial applications.

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## 1. Introduction

In recent times, large-scale emission of CO<sub>2</sub> into the atmosphere triggered by fossil-fuel utilization is considered a critical source for climatic changes and global warming.<sup>1</sup> As a record, since 1958, the atmospheric CO<sub>2</sub> concentration dominantly increased every year with the latest highest recorded value of 414 ppm (<https://www.esrl.noaa.gov/gmd/ccgg/trends/>). The rise in CO<sub>2</sub> level in the atmosphere is predicted to reach a value of 450 ppm in 2100, with an increase of more than 2 °C of the global temperature, due to continuing industrial revolution.<sup>2</sup> To limit damage on earth's climate, the effective reduction of CO<sub>2</sub> emission to the atmosphere is vital for the economic development and ecological food production.<sup>3</sup> Not only is the CO<sub>2</sub> capture significant from the environmental point of view, but also the capture of CO<sub>2</sub> from the gas stream is obligatory for other essential application areas, including air refining in a confined gas space and treatment of natural gases.<sup>4</sup> Synthesis of new materials including inorganic, organic, and composite

membranes for gas separation to address the CO<sub>2</sub> issue is gaining interest in last few decades. Despite the excellent separation efficiency of inorganic membranes such as zeolite and alumina, compared to polymeric membranes, the high cost, fragility, complicated processing, and low mechanical properties make them less desirable. However, improved permeability, low cost, relaxed processing, and reasonable gas separation of organic membranes make them the material of choice.<sup>5</sup> The use of polymeric nanocomposites in the carbon capture technology has well-established advantages such as simplicity, energy efficiency, engineering scalability, and economic cost potentiality, over the conventional liquid and solid sorbents.<sup>6,7</sup> Polymeric nanocomposites are multiphase materials in which the matrices are filled with nanosized particles (in the range of 1–100 nm) and can be formed by the introduction of nanofillers into the polymers.<sup>8</sup> The formulation of the nanocomposite membranes commonly depends on the choice of materials that competently adsorb CO<sub>2</sub>, for example, activated carbons, modified silica, zeolites and metal organic frameworks (MOFs).<sup>5</sup> Besides, the design of polymer composites can be advantageous in applications such as gas separation membranes to space transportation.

The membrane technology is gaining interest in various fields such as medicine, biochemistry, food packaging, water treatment, and separation processes.<sup>9,10</sup> For gas and liquid separation, polymers are more favorable to make selective

<sup>a</sup>Programa de Pós-Graduação em Engenharia e Tecnologia de Materiais (PGETEMA), Pontifical Catholic University of Rio Grande do Sul (PUCRS), Porto Alegre, Brazil. E-mail: Nisarchem1984@gmail.com; Einloft@pucrs.br

<sup>b</sup>Institute of Chemistry – Federal University of Rio Grande do Sul (UFRGS), Av. Bento Gonçalves 9500, Porto Alegre, RS, Brazil

<sup>c</sup>Institute of Physics, Federal University of Rio Grande do Sul (UFRGS), Av. Bento Gonçalves 9500, Porto Alegre, RS, Brazil



membranes than inorganic materials, forming a thin membrane that selects what permeates through it.<sup>10,11</sup> The preparation method depends on the morphology and material of the membrane, and the principal methods used to produce polymer membranes are phase inversion, stretching, sintering, track etching, electrospinning, coating, layer-by-layer assembly (LBL), and graft polymerization.<sup>12</sup> The type of filler and the concentration produce different effects on the properties. Thermoplastic polysulfone is commonly used to produce films. It is widely used in engineering, presenting great thermic, mechanic, and biochemical stabilities,<sup>13</sup> like oxidation and hydrolysis resistance, excessive functionality at different pH values, and high rigidity.<sup>14</sup> An example of the advantages obtained by the addition of nanoparticles is the notable reduction of the bacterial attack on filled polysulfone membranes. Because of their advanced properties, polysulfone nanocomposites are a growing focus of the membrane researchers.<sup>14</sup>

In recent years, special attention has been paid to nanoparticles possessing magnetic properties (MNPs) due to their promising use in medicine, biotechnology, water treatment, tissue engineering, data storage, and catalysis.<sup>15–18</sup> The choice of magnetic particles depends on the application's purpose.<sup>19–22</sup> Furthermore, metals are exposed to high toxicity, and oxidation needs proper surface treatment of the magnetic fillers to assure their chemical stability and safety.<sup>23</sup> Many research studies have been reported to fix these complications involving the coating method, including the encapsulation process, by non-magnetic surfaces such as silica, carbons, and polymers, effectively preventing the agglomeration and oxidation.<sup>24,25</sup> Iron-based magnetic fillers are commonly used to provide magnetism, together with cobalt and nickel.<sup>26,27</sup>

Among the other methods used for the synthesis of polymer nanocomposites, melt mixing is the most widely adopted technique due to its industrial applicability, easy operation procedure, high yields, fast production rate, and solventless process to avoid any health risk.<sup>28</sup> More recently, we have studied how different synthetic talcs affect the polyurethane nanocomposites' properties.<sup>29–31</sup> The focus of the present work is to compare the use of different metal-activated carbons obtained from the biomass<sup>32</sup> (low-cost source) as fillers to synthesize polysulfone (PSF) nanocomposites with enhanced CO<sub>2</sub> capture capacity, good thermal, mechanical and magnetic properties by a melt-mixing technique.

## 2. Experimental

### 2.1 Materials

As a polymer matrix, commercial polysulfone (average Mw ~35 000 by LS, average Mn ~16 000 by MO, pellets, Sigma-Aldrich), as well as antioxidant agent Irganox 1010, was used for composite preparation.

Metal-carbonized materials containing nickel (CA-Ni) and cobalt (CA-Co) were obtained following the procedure reported in ref. 32.

As activating agents, CoCl<sub>2</sub> and NiCl<sub>2</sub> metal salts purchased from Neon (São Paulo, Brazil) were utilized without further

treatment; CoCl<sub>2</sub> and NiCl<sub>2</sub> show an oxidation state of +2 in aqueous solutions (pH close to 6).

### 2.2 Preparation of activated carbon-based cobalt and nickel from biomass

Ayous biomass is a waste from wood processing. Some studies carried out in sawmills in the Adamaoua Region, Cameroon, revealed very high use of Ayous trees. They have low durability, and hence, they are widely used for light carpentry. The transformation of this species generates tons of wastes per year. Therefore, any attempt to reuse this waste would be useful for the country. The Ayous residues were kindly provided by Cameroon's sawmill industries and used without any pre-treatment. The residue contains about 98% cellulose, hemicellulose, and lignin, with the remaining 2% made up of extractables (pectins, tannins, and polymers with a low degree of polymerization) and inorganics such as Ca<sup>2+</sup>, Na<sup>+</sup>, Cl<sup>−</sup> and SO<sup>2−</sup>. The Ayous residue was used as a carbon source without any pre-treatment for the preparation of activated carbons with two inorganics, namely, chlorides cobalt(II) and nickel(II). The biomass residue was first ground into sawdust (diameter < 300 μm) before use in the preparation of the activated carbon.<sup>33</sup>

The process preparation is as follows: an appropriate amount of chloride salt of cobalt(II) or nickel(II) was completely dissolved in 60.0 mL of treated water, which was followed by the addition of 60.0 g of dried sawdust. The solution was then mixed continuously at approximately 80 °C for 2 hours, and the sample was dried overnight before the carbonization step. The mass impregnation ratio of the inorganic salt to the Ayous sawdust was 1 : 1 (w/w) for both nickel chloride and cobalt chloride.

The carbonization of the dried powder impregnated with cobalt or nickel salts has been described in our previous study;<sup>32</sup> the final carbonization temperature was 700 °C. For comparison with the nanocomposites, the activated carbon material (C-neat) was prepared under the same conditions but without the addition of cobalt(II) chloride or nickel(II) chloride.

### 2.3 Synthesis of polysulfone nanocomposites

The preparation of nanocomposites was carried out using a Thermo Haake Rheomix-600 (Thermo Electron Corp, Karlsruhe, Germany), operating at 60 rpm and 340 °C. A defined amount of polymer matrix, carbonized metal, and 0.005 g of Irganox1010 were introduced per mixing, which contributes to a total quantity of approximately 60 g. The variation of the filler in the matrix was set from 0 to 2 wt%. In the first step, PSF (~30 g) and the antioxidant were mixed. After 2 min, different quantities of the filler (0–2 wt%) was gradually added to the melted polymer for 3 min. In the last step, the remaining polymer pellets were added by keeping the mixer speed constant at 60 rpm for 5 min. The whole mixing time was approximately 10 min. Finally, the blend was hot-pressed to form sheets at 325 °C under a pressure of 200 bars.



### 3. Characterization

An elemental analyzer (Perkin-Elmer M CHNS/O model 2400) was used to analyze the CNH/O of the Ayous residue and the activated carbon filler. Briefly, 0.05 g of the oven-dried sample was used to determine the total carbon content (C), nitrogen content (N), and hydrogen content (H). The oxygen-containing (O) mass percentage was found as the ash-containing C, N, and H mass percentages were subtracted from the total mass.

The thermal stabilities of the Ayous residue and the activated carbon were checked by thermogravimetric analysis (TGA), exploiting a thermogravimetric analyzer (TA model SDT Q600). The sample was heated up from 20 °C to 800 °C in an inert N<sub>2</sub> atmosphere (10 °C min<sup>-1</sup>) and from 800 °C to 1000 °C in an atmosphere containing oxidants. The oxidant atmosphere allows finding the ash content fraction of the sample.

A transmission electron microscope (TEM, Tecnia G2T20 FEI) was used to perform the morphological analysis to investigate the degree of dispersion on the nanocomposites. Polymeric nanocomposite samples were prepared from ~50 nm thick ultrathin films cut under cryogenic conditions using a Leica ultra cut UCT microtome placed on a grid. The sample morphology was examined by field-emission scanning electron microscopy (FESEM) using an Inspect F50 equipment (FEI Instruments) in secondary electron mode. The samples were placed on an aluminum stub and coated with gold to make them conducting.

Room-temperature magnetic characterization was performed using an EZ9 MicroSense magnetometer, which is the magnetic field, *H*, ranging from -18 kOe to +18 kOe.

The values of *T<sub>g</sub>* of pure polysulfone and metal nanocomposites were obtained using a Perkin-Elmer differential calorimeter (TA Instruments model Q20). The heating rate was 10 °C min<sup>-1</sup> from -25 to 200 °C in a nitrogen atmosphere. Thermal decomposition of pure PSF and its nanocomposites was performed by thermogravimetric analysis (TGA) using an SDT Q600 thermal analyzer (TA Instruments) at a scanning rate of 20 °C min<sup>-1</sup> from 25 °C to 800 °C at a constant nitrogen flow of 100 mL min<sup>-1</sup> for polymeric nanocomposites and air for carbon materials.

The pressure-decay technique determined the CO<sub>2</sub> sorption capacity. The dual-chamber gas sorption cell was similar to that reported in Koros *et al.*<sup>34</sup> Before measurements, 0.7 g of the sample was weighed and dried at 70 °C (343.15 K) for 1 h. CO<sub>2</sub> sorption experiments were carried out at 45 °C (318.15 K) and 4

bars. The CO<sub>2</sub> sorption capacity was calculated using eqn (1) and (2):

$$n_{\text{CO}_2} = \frac{p_i V_{\text{gc}}}{Z(p_i, T_i) R T_i} - \frac{p_{\text{eq}} (V_t - V_p)}{Z(p_{\text{eq}}, T_{\text{eq}}) R T_{\text{eq}}} \quad (1)$$

$$w_{\text{CO}_2/\text{g}} = \frac{n_{\text{CO}_2} M}{W_s} \quad (2)$$

where *w<sub>CO<sub>2</sub>/g</sub>*

 is the weight of gas adsorbed by the sample; *p<sub>i</sub>* and *T<sub>i</sub>* the pressure and temperature in the gas chamber, respectively; *p<sub>eq</sub>* and *T<sub>eq</sub>* the parameters at equilibrium; *V<sub>gc</sub>* the gas chamber's volume; *V<sub>p</sub>* the volume of the sample; *V<sub>t</sub>* the total volume of the sorption cell. The coefficient of compressibility “*Z*” for CO<sub>2</sub> is obtained using Span–Wagner equations of state.<sup>35</sup>

The mechanical properties were analyzed using an HP model D-500 dynamometer according to ASTM D 638-10 at ~25 °C. For each weight percentage of the nanocomposite, the average of results of five measurements (typical deviation ~5%) is presented. The bone-shaped samples of overall length 30 mm, width 4.0 mm, and thickness 0.5 mm were tested at a crosshead rate of 50 mm min<sup>-1</sup>.

A goniometer (Phoenix 300, SEO) was used to measure the static water contact angle by the sessile drop method. Images were obtained using a “Drop Shape Analysis system.” The mean contact angle was calculated by adding five drops of deionized water onto each sample, considering an experimental error of 2 degrees among the measurements.

## 4. Results and discussion

### 4.1 Elemental analysis of the Ayous biomass and metal-activated carbons

The elemental composition of the activated carbon material containing nickel and cobalt metals is given in Table 1. When compared with the precursor material, the prepared activated carbons showed a very high content of carbon and a low content of oxygen. The Ayous residue biomass contained initially 46.05% of carbon, 6.26% of hydrogen, and 45.78% of oxygen. Notwithstanding, after pyrolysis and the washing process, the carbon contents in the CA–Ni and CA–Co materials increased to 58.05% and 53.57%, respectively. Indeed, the aromatic structure of the materials was formed during the carbonization process in the presence of nickel or cobalt metals, as indicated by the enhanced carbon content.<sup>33</sup>

**Table 1** CNH/O elemental composition and texture properties of Ayous biomass and activated nickel- and cobalt-containing carbons

Samples	% C	% H	% N	% O <sup>a</sup>	% Ash <sup>b</sup>	M-content (%)	<i>S</i> <sub>BET</sub> <sup>c</sup> (m <sup>2</sup> g <sup>-1</sup> )	<i>V</i> <sub>tot</sub> <sup>c</sup> (cm <sup>3</sup> g <sup>-1</sup> )	<i>D<sub>p</sub></i> <sup>c</sup> (nm)
Biomass	46.05	6.26	0.33	45.78	1.56	0.00	—	—	—
CA–Ni	58.05	2.31	0.15	11.29	28.20	26.64	381	0.321	3.3
CA–Co	53.57	2.49	0.38	19.97	23.60	22.04	619	0.340	2.2

<sup>a</sup> Yield by difference (% O = 100% – % C – % H – % N – % Ash). <sup>b</sup> Obtained by TGA. <sup>c</sup> *S*<sub>BET</sub> = BET surface area; *V*<sub>tot</sub> = total pore volume; *D<sub>p</sub>* = average pore diameter.



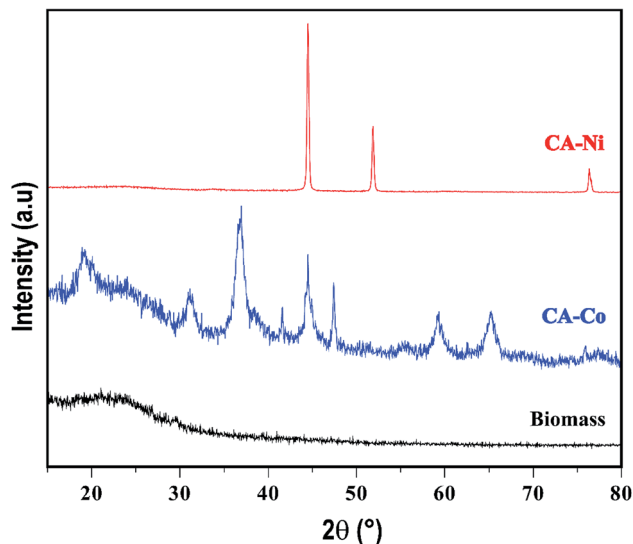


Fig. 1 XRD analysis of the biomass and metal-activated carbons.

The ash content was determined by TGA analysis. The residue remained in the TGA analysis performed in a synthetic air atmosphere is commonly attributed to the ash content. The ash content was used to determine the amount of nickel or cobalt present in the metal-carbon materials after the

preparation. One can obtain the carbon-composite (CA-M) metal content knowing the ash content of the Ayous biomass residue and metal-carbon materials. As one can see in Table 1, the CA-Ni composite showed more metal embedded in the structure of the carbon sample; moreover, it also shows the textural parameters of the synthesized activated carbon. The sample CA-Co shows the highest surface area, total pore volume, and the smallest pore diameter.

#### 4.2 XRD analysis of the nanofiller

Fig. 1 presents the XRD patterns of the biomass (CA) and different metal particles embedded in the amorphous carbon. The CA has an amorphous structure,<sup>36</sup> where the XRD of Ni-C showed typical sharp peaks at  $2\theta = 44.5$ ,  $51.8$ , and  $76.3^\circ$  corresponding to planes (111), (200), and (222), respectively, representing the face-centered cubic (fcc) structure of Ni.<sup>37</sup> The mean crystallite size of Ni was estimated employing the Scherrer<sup>38</sup> equation through the broadening of the maximum intense peak (111), and it was 46 nm. Finally, in the XRD of Co-C particles, it can be seen that the pattern of a simple cubic crystalline structure was represented by diffraction peaks at  $2\theta$ :  $20.1$ ,  $31.0$ ,  $36.7$ ,  $44.4$ ,  $47.4$ ,  $59.2$  and  $65.2^\circ$  corresponding to the (111), (220), (311), (222), (422), (511) and (440) planes.<sup>39</sup> The peak at  $36.7$  (311) was used to calculate the crystal size, and it was 11 nm. In the resume, the XRD of the M-C particles shows that all the metals have crystalline nanometric structures.

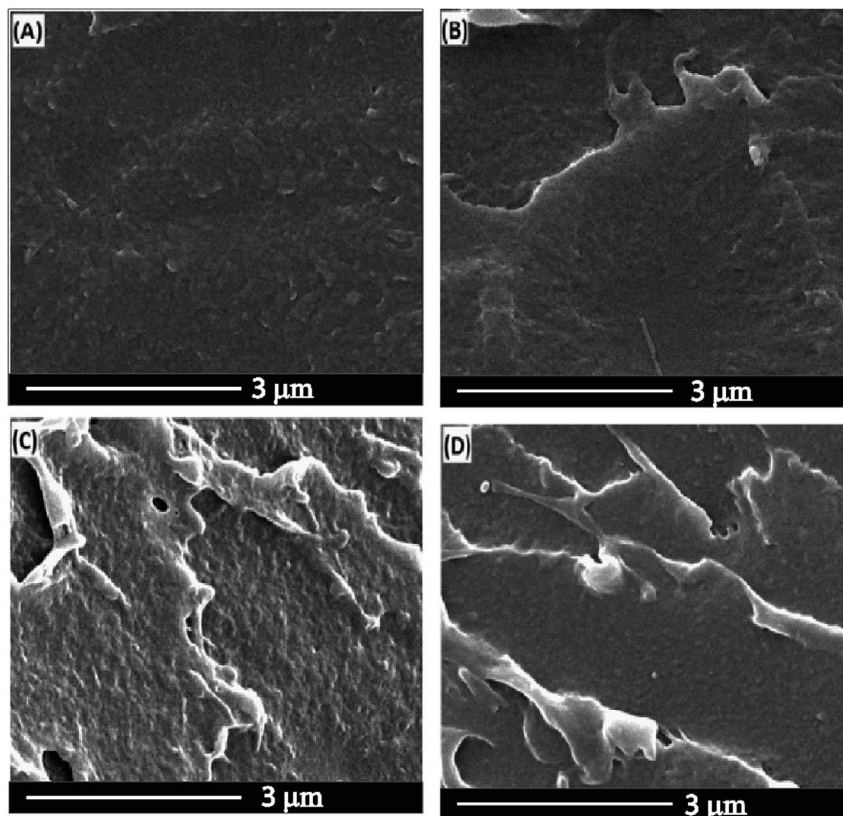


Fig. 2 SEM micrographs of (A) cross-section of PSF-neat, (B) PSF-CA, (C) CA-Ni, and (D) PSF-CA-Co.





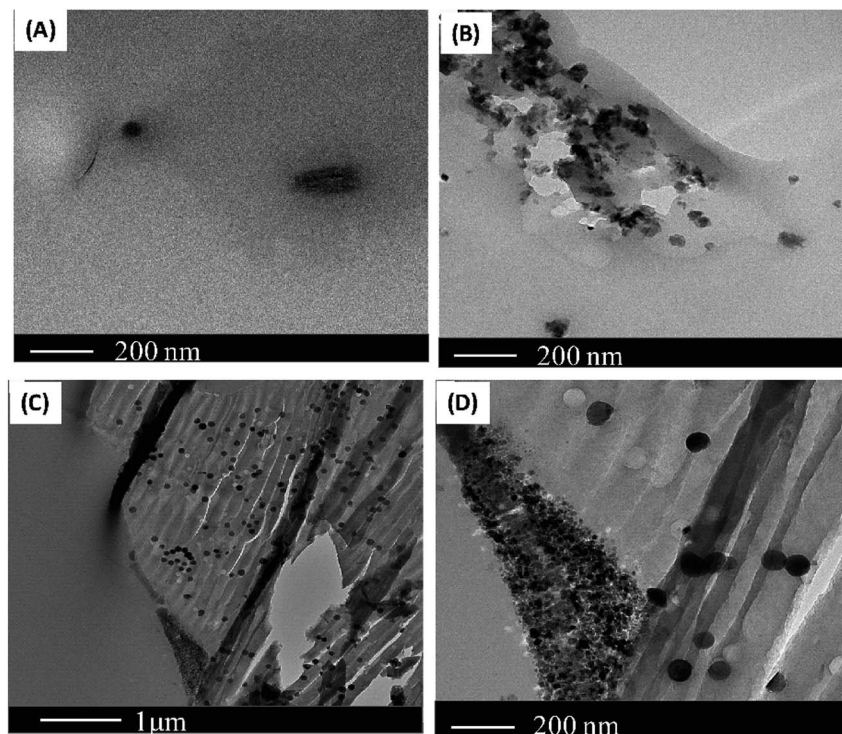


Fig. 3 TEM images of PSF-CA-neat (A), PSF-CA-Co (B), PSF-CA-Ni (C), and (D).

### 4.3 Morphological analysis

The dispersion of the filler in the PSF matrix is ascertained by SEM analysis. It is clear from Fig. 2 that, by incorporating the filler in the polymer, the cross-section morphology changed. A better-defined layered morphology appeared with the addition of the fillers, which shows that the polymer is coated around the filler. Furthermore, the nanofiller particles were invisible, indicating a uniform dispersion of the nanofillers in the PSF matrix. Moreover, the presence of metal-activated carbons turns the PSF membrane surface rougher due to the presence of more hydrophilic carbon-based fillers.

Fig. 3 shows the TEM images of the PSF nanocomposites with 2 wt% nanofillers. The filler is very well distributed in the PSF matrix, with no apparent evidence of agglomerates. It can be seen that, in the polymer matrix, the metal particles, cobalt, and nickel, see Fig. 3 (B), (C) and (D) respectively, are surrounded by amorphous carbons. It can be noted that the existence of the black spots in Fig. 3(B), (C) and (D) is due to the presence of the nanoscale metal particles in the PSF matrix. The presence of these black spots is noticeable in the sample containing the nickel particles in the PSF matrix. The existence of the metal as a block spot in the polymer and a similar morphology have been reported in other studies.<sup>40–42</sup> The micrographs do not present filler aggregation.

The XRD peaks of PSF and its nanocomposites containing the metal particles are shown in Fig. 4. Diffractogram of PSF and nanocomposites analyzed in the  $2\theta$  range from 0 to 80 degrees showed only a peak of  $2\theta$  at  $17.5^\circ$  without any change in the peak for its nanocomposites. This is because the small

amount of metal particles might be uniformly dispersed into the polymer matrix, resulting in no significant changes in the peaks.

### 4.4 Thermal stability analysis

The thermal degradation properties of all samples shown by TGA analysis are resumed in Table 2 and Fig. 5. The results indicated a slight enhancement in the maximum degradation temperature ( $T_{\max}$ ) around  $3^\circ\text{C}$  for the sample with the addition

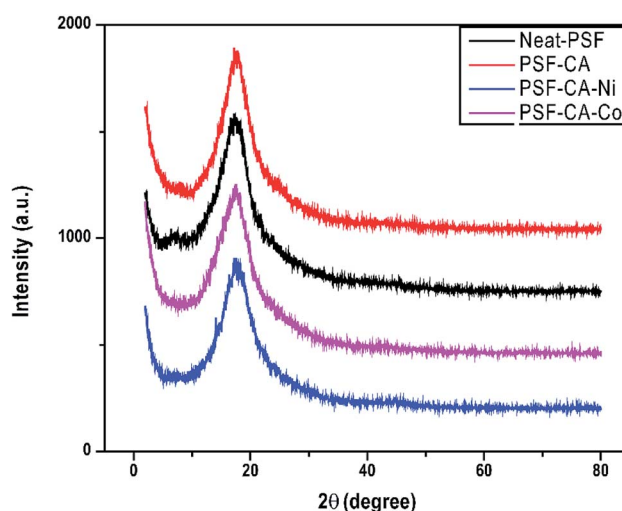


Fig. 4 XRD patterns of neat PSF and nanocomposites with different fillers.

Table 2 Thermal properties of neat PSF and PSF-C-M nanocomposites

Samples	Filler (%)	Metal <sup>a</sup> (%)	Filler <sup>b</sup> (%)	$T_{\text{onset}}$ (°C)	$T_{\text{max}}$ (°C)	$T_g^c$
PSF-neat	0	0	32.5	523	543	190
PSF-CA	2.0	0	32.8	525	544	190
PSF-CA-Ni	2.0	0.5	32.3	521	543	191
PSF-CA-Co	2.0	0.4	34.0	519	546	191

<sup>a</sup> Calculated from the TGA residue. <sup>b</sup> Calculated from the TGA residue. <sup>c</sup> Calculated from the DSC.

of filler CA-Co, whereas the rest of the samples (PSF-CA and PSF-CA-Ni) showed a similar maximum degradation temperature to that of neat PSF. The thermal stability enhancement in the nanocomposites could be attributed to the fillers serving as a barrier, hindering the oxygen-molecules' transmission into the nanocomposites as well as to the labyrinth effect, which deferred the volatilization.<sup>43</sup> The small amount of the filler around 2 wt% was not sufficient to impart a reasonable barrier and labyrinth effect on the thermal enhancement stability of the nanocomposites. Furthermore, the initial degradation temperature ( $T_{\text{onset}}$ ) of the nanocomposites containing metals (Ni or Co) in the filler was slightly lower around 4 °C than that of neat PSF. Previous studies showed the influence of metals (Ni, Al, Fe, Cu, and Co) on the thermal behavior of plastics, for instance, polypropylene,<sup>44</sup> linear low-density polyethylene,<sup>45</sup> chitosan,<sup>46</sup> or high-density polyethylene.<sup>47</sup>

These results indicated that the surface contact of the metals with polymer could stimulate the degradation of the organic part at different rates. Pd nanoparticles accelerated the thermal degradation of PET and PA6.<sup>48</sup> Our results support the works as mentioned earlier; Table 2 shows that upon incorporation of CA (activated carbons without metals) into the sample PSF-CA, the  $T_{\text{onset}}$  showed an improvement of 2 °C, whereas the addition of the same filler with metals decreased the initial thermal stability. It is thus concluded that the filler containing metals behaves as a catalyst resulting in polymer's degradation, the

latter beginning at relatively low temperatures.<sup>49</sup> Due to the aromatic structure of the PSF backbone, the residual mass of the sample remains around 32 wt% at 800 °C, which, in turn, forms more thermally stable carbonaceous materials.<sup>50</sup>

The impacts of the filler on  $T_g$  of neat PSF and its nanocomposites are presented in Table 2 and Fig. 6.  $T_g$  is typically used to understand the structure of the membrane when an amorphous polymer like polysulfone is employed.  $T_g$  of the nanocomposites shows an improvement of around 1 °C, although this effect is not very significant and lies in the error limits of the equipment. Meanwhile, there is a tendency of enhancement of  $T_g$ , which can be achieved by the incorporation of higher amounts of the filler. From the above-mentioned results, one can infer the existence of interactions between the polymeric chain and the nanofiller particles. This implies an increase in the rigidity of the polymer chain and, hence, an increase in the amount of energy needed for the polymer chain movement or breakage.<sup>51</sup>

#### 4.5 Carbon dioxide capture capacity

The CO<sub>2</sub> sorption capacity of PSF and its nanocomposites was studied at 4 bars and 318.15 °C, as shown in Fig. 7. The interaction between the polar groups and the CO<sub>2</sub> molecule<sup>52,53</sup> leads, probably, to the adsorptive properties (49.3 mg CO<sub>2</sub>/g ± 0.31) of PSF. Fig. 7 shows that the CO<sub>2</sub> capture capacity of the

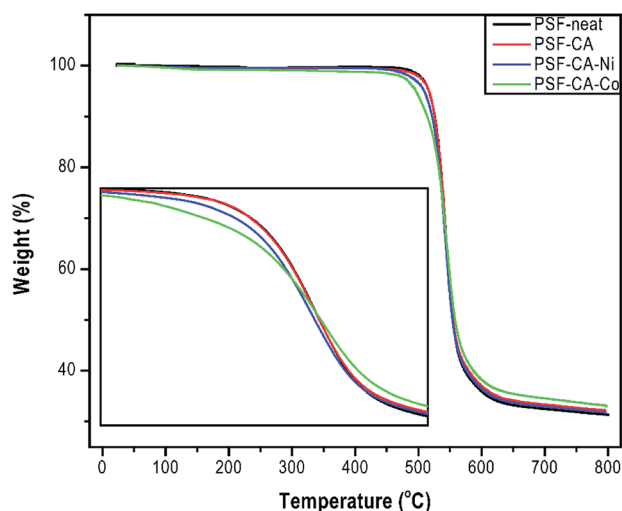


Fig. 5 TGA thermogram of PSF-neat and its nanocomposites.

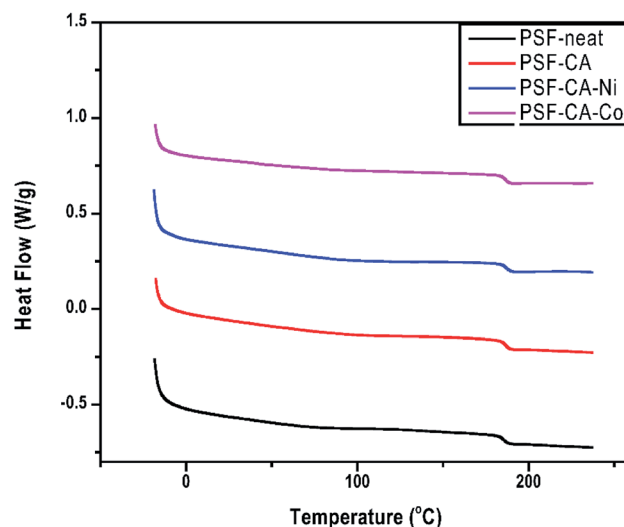


Fig. 6 DSC thermograms of PSF-neat and its nanocomposites.



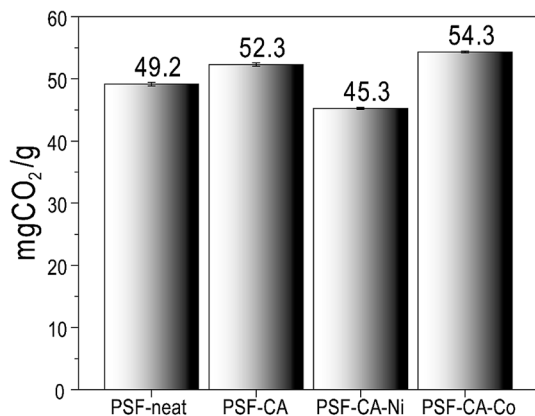


Fig. 7 CO<sub>2</sub> capture capacity of PSF-neat and its nanocomposites at 45 °C.

nanocomposites was slightly improved with the filler's addition. The nanocomposite with 2 wt% of C-neat (activated carbons without metals) and C-Co (activated carbons with cobalt) shows a sorption capacity of 52.32 mg CO<sub>2</sub>/g ± 0.26 and 54.32 mg CO<sub>2</sub>/g ± 0.16, respectively, which is almost 10% higher than that of pure PSF. The high uptake of CO<sub>2</sub> by the nanocomposites is associated with the existence of activated carbons in the polymer structure with the presence of a large number of ultra-micropores, which helps in the trapping of the CO<sub>2</sub> molecules.<sup>54</sup> Furthermore, the nanocomposite with the addition of C-Ni (activated carbons with nickel) shows a slight decrease in the capture capacity of CO<sub>2</sub>. Most probably, this minor decreasing effect of the nanocomposite comes from some agglomeration of filler's in the matrix of PSF. Ko *et al.*<sup>55</sup> immobilized primary, secondary and tertiary amines on mesoporous silica and used it as an absorbent for CO<sub>2</sub> capture. The maximum capacity of primary, secondary, and tertiary amine-supported silica was 0.95, 0.75, and 0.17 mmol CO<sub>2</sub>/g, where our sample shows a high sorption capacity of 54.3 mg CO<sub>2</sub>/g (~1.2 mmol CO<sub>2</sub>/g). Similarly, Huang *et al.*<sup>56</sup> used a polyurea and alkylated graphene oxide IL capsule for CO<sub>2</sub> capture, reporting an absorption of only 3.0 mg CO<sub>2</sub>/g at a pressure of 1.3 bars. More recently, Khadry *et al.*<sup>5</sup> have reported the synthesis of polyvinylidene-fluoride-hexafluoropropylene (PVDF-HFP) amino-silica composites by a phase separation technique and prepared membranes for CO<sub>2</sub> capture. Their results indicated CO<sub>2</sub> uptake of 33.75 mg CO<sub>2</sub>/g with the highest loading of 40 wt% of SiO<sub>2</sub> in the composite material. Herein, we demonstrate CO<sub>2</sub> uptake to be higher than their results with the incorporation of a tiny amount of 2.0 wt% of activated carbon into the polymer matrix. The reason for the highest CO<sub>2</sub> capture by the sample PSF-CA-Co could be the higher BET surface area and micropore volume of the activated carbon, as clear from Table 1. The activation of the biomass with the cobalt leads to a high surface area and pore volume, which, in turn, provides the maximum adsorption sites for the petite size CO<sub>2</sub> molecule to be captured by the micropores.<sup>57</sup> Huang *et al.*<sup>58</sup> reported the preparation of activated carbons from coconut shells and investigated the effect of experimental conditions on the

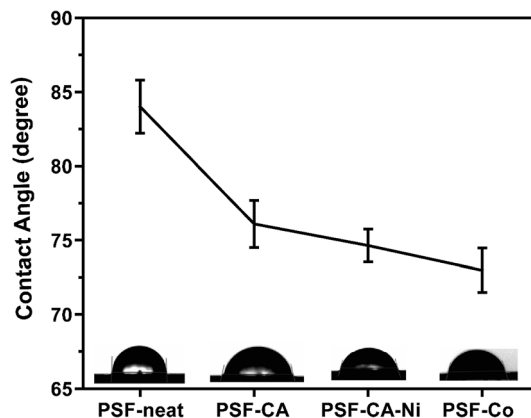


Fig. 8 Water contact angle measurement of all samples at 25 °C.

textural properties of the final product. Their results indicated the highest CO<sub>2</sub> capture by the sample having the highest BET specific surface area and total pore volume; our results are in close agreement with their findings, thus supporting the results of Hung *et al.* These results indicated that the presence of an appropriate amount of filler has a positive influence on CO<sub>2</sub> capture capacity, as can be seen from Fig. 7.

#### 4.6 Contact angle measurement

The water contact angle of neat PSF and its nanocomposites was estimated by the sessile drop method to evaluate the wettability of a membrane; the contact of a smooth surface with a water drop is considered the most convenient method. Thus, the hydrophilicity of the materials can be qualitatively obtained using this measurement.<sup>59,60</sup> A significant trend of decline in the contact angle with the incorporation of the activated carbon with or without metals is observed in Fig. 8. Dropping of the contact angle leads to the indication that the introduction of hydrophilic activated carbons can be advantageous to increase the membrane hydrophilicity.<sup>61</sup> It has already been shown<sup>59,61–63</sup> that adding different fillers (*i.e.*, carbon nanotubes, graphene oxide, clay) may result in an upturn in the hydrophilic nature of the PSF-composites.

#### 4.7 Mechanical behavior of nanocomposites

Stress-strain curves and elongation at break of the PSF and its nanocomposites with the addition of carbon-based fillers are presented in Table 3 and Fig. 9. The addition of activated carbons to the polymer matrix significantly affects, see Fig. 9 (A),

Table 3 Tensile modulus and elongation at a breakpoint for pure PSF and nanocomposites

Samples	Filler (%)	Tensile modulus (MPa)	Elongation at break (%)
PSF-neat	0	1250	7.3
PSF-CA	2.0	1464	3.3
PSF-CA-Ni	2.0	1054	2.7
PSF-CA-Co	2.0	1451	3.4



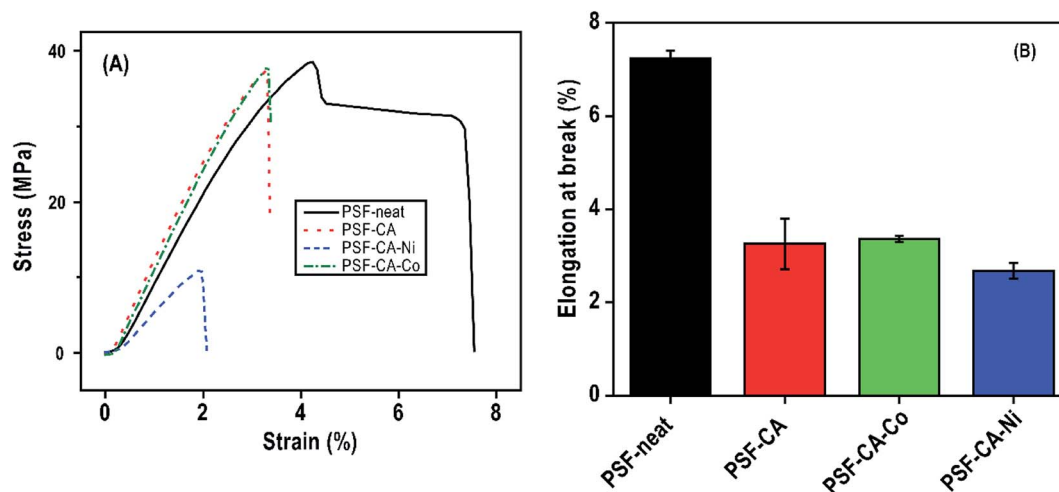


Fig. 9 Characteristic stress–strain curves of PSF and nanocomposites (A). Elongation at break (B).

the elastic modulus (enhanced from 1250 to 1464 MPa) despite the meager amount of the filler around 2 wt%. Among the synthesized composite materials, samples PSF-CA and PSF-CA-Co appear to afford maximum reinforcement, *i.e.*, enhancement of almost 17% in the elastic modulus as contrasted with neat PSF. Such an improvement could be attributed to the addition of the stiff-activated carbon with metals, which may prominently affect the mechanical behavior of the composite and by the uniform dispersion, which favors the formation of strong interface PSF/activated carbon nanocomposites.<sup>64</sup> However, in comparison with the neat PSF, a decrease in the modulus of the sample PSF-CA-Ni was observed. This is most probably caused by some agglomeration of metal-activated carbons in the PSF matrix, which limits the reinforcement influence of the nanofiller substantially since it restricts the development of significant polymer/filler interfacial adhesion bonds.

Elongation at a breakpoint is a measure associated with the material's ductility. Generally, the addition of nanoparticles

turns the nanocomposites more fragile.<sup>64</sup> It is clear from Fig. 9 (B) and Table 3 that the elongation at break is reduced by almost 70% as compared to the pure PSF as the filler is included. The nanoparticles toughly constrain the movement of the polymer chain during the stress.<sup>65</sup> The superior intrinsic mechanical behavior of the filler and an interfacial interaction of the filler/PSF matrix is the crucial motivation for the enhancement of mechanical properties.<sup>66</sup>

#### 4.8 Magnetic characterization

Fig. 10 presents the major magnetization hysteresis loops of PSF-CA-Ni and PSF-CA-Co nanocomposites. The nanocomposite with Co filler saturates in magnetic fields much higher than the others (see the insets in this figure), which should be attributed to the higher magnetic anisotropy energy of Co as compared to that of Ni. The amplitude of  $H$  used here was sufficiently significant to circumvent minor loop effects.<sup>67–69</sup> This difference in anisotropy could also explain the preferably

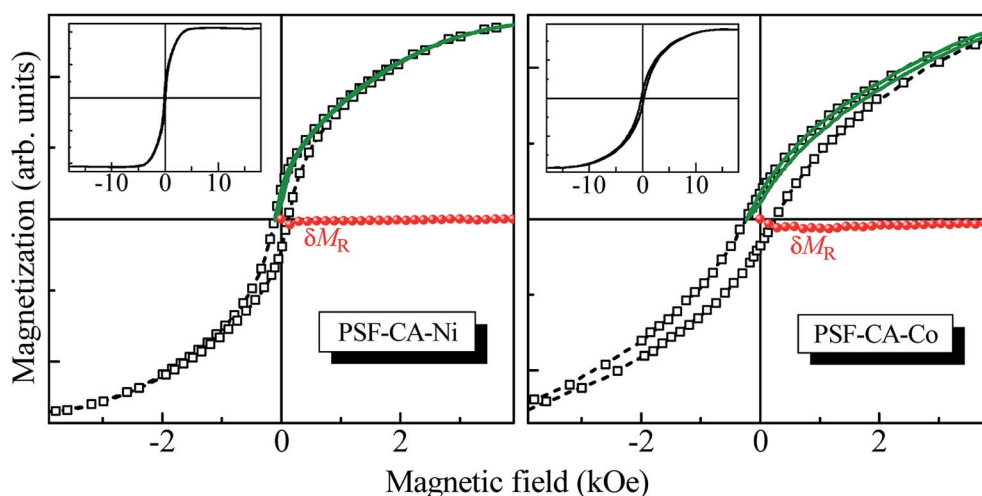


Fig. 10 Major magnetization hysteresis loops (empty squares) and the respective interaction  $\delta M_R$  plots (full circles), constructed from recoil curves (solid lines) with the recoil field equal to  $H_C$  for the PSF-CA-Ni (left panel) and PSF-CA-Co (right panel) nanocomposites. The insets show the major loops in the whole field range.





higher value of the coercive field  $H_C$  ( $\approx 240$  Oe) of the nanocomposite with the Co filler as compared to that with Ni ( $\approx 100$  Oe). However, the value of the normalized remnant magnetization of 0.10 of the Co-filler sample is smaller than that of the Ni-filler nanocomposite equal to 0.14. This result could be attributed to the stronger dipolar interactions present in the Ni-filler nanocomposite.

The effects of magnetic interactions of the nanocomposites with magnetic fillers were estimated herein through the recently introduced recoil-loop  $\delta M_R$  plots.<sup>70,71</sup> Any nonzero deviation of  $\delta M_R(H)$  should be ascribed to the magnetic interactions if the magnetic anisotropy is uniaxial. For the present study, we used recoil loops (also shown in Fig. 10) with a recoil field equal to  $H_C$ . The  $\delta M_R$  plot for the Ni filler sample indicates no noticeable magnetic interactions, given that  $\delta M_R \approx 0$  for all  $H$  values. In contrast, the  $\delta M_R$  plot obtained for the Co-filler nanocomposite is weak though noticeably negative, stabilizing the demagnetized state interactions. The latter leads to a decrease in the remnant magnetization, explaining the experimental observation.

## 5. Conclusions

The use of cost-effective materials as fillers for the synthesis of polymeric nanocomposites is an exciting area of research. We demonstrated the use of a new cost-effective carbon-based magnetic filler for the synthesis of polysulfone magnetic nanocomposites. The activation of the carbon with metals, here either Ni or Co, leads to the encapsulation of these metals by amorphous carbons, protecting them from natural oxidation and improving their dispersion within the polymer matrix. Morphological SEM and TEM analyses show that the filler was uniformly dispersed in the polymer matrix. The maximum degradation temperature of the nanocomposites was enhanced by the addition of the fillers, indicating an improvement of 3 °C. The initial degradation temperature of the nanocomposites shows a decrease of 4 °C as compared to neat PSF, which can be explained by the catalytic action of the metals in the filler. The glass transition temperature did not show any effective change with the filler loading.

Moreover, the contact angle of the nanocomposites was reduced, indicating the hydrophilic nature of the nanocomposites. The elastic modulus of the nanocomposites indicated a significant improvement of around 17% at such low loading of fillers of 2 wt%. A critical usage of a polymeric nanocomposite is as a membrane for CO<sub>2</sub> capture. Our results indicated that, when contrasted with the pure PSF matrix, the absorption capacity of the nanocomposites was enhanced by almost 10%. The nanocomposites showed ferromagnetic behavior with the addition of the Ni- and Co-activated carbon. These results are significant, given that the majority of the studies on such systems reported magnetic properties at low temperatures, whereas we obtained a high coercive field of  $\approx 240$  Oe at ambient temperature. Thus, we synthesized multifunctional PSF nanocomposites using a cost-effective filler, which can be beneficial in various industrial applications. This material has the potential to be used in a variety of applications, where a flexible magnetic material with good

processability is required, for example, electromagnetic device applications such as electromagnetic interference suppression, aircraft industries, and microelectronics.

## Conflicts of interest

The authors declare that there is no conflict of interest.

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