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Designing coexisting multi-phases in PZT multilayer thin films: an effective way to induce large electrocaloric effect

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Coexisting multi-phases in $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ multilayer thin films were successfully fabricated using the sol-gel method. The microstructure and electrical of the multilayer films with different growth sequences, including the up multilayer films and down multilayer films, have been systematically investigated. The results indicate that a large electrocaloric effect (ECE) is obtained at the temperatures much below the Curie temperature. At room temperature (25 °C), the change in temperature (ΔT) values of the up multilayer and down multilayer thin films are 20.2 K with the applied electric field $E = 826 \text{ kV cm}^{-1}$ and 46.3 K with the $E = 992 \text{ kV cm}^{-1}$, respectively. In addition, both the films exhibit outstanding ECE of around 145 °C, and ΔT values of 28.9 K and 14.8 K have been obtained for the up multilayer and down multilayer thin films. The results indicate that the antiferroelectric/ferroelectric (AFE/FE), ferroelectric/ferroelectric (FE/FE) phase transition and the synergistic effect of the AFE/FE and FE/FE phase transition are as effective as the FE/PE phase transition. In particular, the multilayer thin films are endowed with refrigeration ability at multi-temperature zones due to the coexistence of multi-phases.

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Introduction

Caloric materials, including electrocaloric, magnetocaloric, piezocaloric and elastocaloric materials, have attracted considerable attention in recent years due to their applications in various technological fields.^{1–5} Electrocaloric effect (ECE) is considered to be one of the most important thermodynamic effects employed in refrigeration technologies.^{6,7} Electrocaloric materials, such as inorganic ferroelectrics,^{8–10} relaxor ferroelectrics,^{11,12} and organic polymer films,^{13,14} have been widely studied. The electrocaloric effect is a change in the temperature (ΔT) of a ferroelectric (FE) material by the change in entropy (ΔS) upon the application or withdrawal of an electric field under adiabatic conditions. The maximum ΔT values are mostly obtained near the point of first order phase transition and confined to Curie temperature (T_c), which is much higher than the room temperature. For example, Mischenko *et al.* reported that $\Delta T = 12 \text{ K}$ and $\Delta S = 8 \text{ J K}^{-1} \text{ kg}^{-1}$ at 222 °C for $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ thin films were obtained due to ferroelectric/

paraelectric (FE/PE) phase transition.⁶ For the $\text{Pb}_{0.97}\text{La}_{0.02}(\text{Zr}_{0.65}\text{Sn}_{0.3}\text{Ti}_{0.05})\text{O}_3$ thin film, $\Delta T = 20.1 \text{ K}$ was obtained at a temperature corresponding to the antiferroelectric (AFE) phase to paraelectric phase transition.¹⁵ Although a high working temperature may permit cooling applications in many fields, such as automotive, aerospace, or food industries, a lower working temperature is also important and can be used in on-chip refrigeration or other fields. In particular, lower working temperatures are also beneficial to reduce the films fatigue, entitling them with higher breakdown strength.

In the consideration of viewpoints mentioned above, exploring an effective way to reduce the working temperature of electrocaloric materials is very significant for the further expansion of their applications. It was reported that with regards to the ECE of the doped $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ (PZT) thin films, including PNZST¹⁶ and PLZST,¹⁷ which originated from the phase transition between AFE and FE, the ΔT values are 5.5 K and 3.8 K near the room temperature, respectively. A large ΔT (45.3 K) in $\text{Pb}_{0.8}\text{Ba}_{0.2}\text{ZrO}_3$ AFE thin films was observed at room temperature due to the coexistence of the AFE and FE phases at the nanoscale.¹⁸ Besides, the $0.7\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-}0.3\text{PbTiO}_3$ and $\text{PbZr}_{0.52}\text{Ti}_{0.48}\text{O}_3$ thin films were prepared and at morphotropic phase boundary (MPB), the compositions were investigated, which demonstrated that low temperature refrigeration can be realized by utilizing the phase transition at MPB.¹⁹ Hence, it can be concluded that not only the phase transition between FE/PE phases, but also one of the AFE/FE phases or FE/FE phases act as the potential sources for excellent ECE.

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Furthermore, a theoretical analysis for developing ferroelectric materials with high ECE near an invariant critical point (ICP) was proposed; the enhanced ECE can be attributed to the increase in the entropy induced by the coexisting multi-phases.²⁰

In order to build coexisting multi-phases in electrocaloric materials, in this study, the $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ multilayer thin films were fabricated on a $\text{Pt}(111)/\text{Ti}/\text{SiO}_2/\text{Si}$ substrate. As shown in Fig. 1(a) and (b), the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$, $\text{PbZr}_{0.8}\text{Ti}_{0.2}\text{O}_3$ and $\text{PbZr}_{0.52}\text{Ti}_{0.48}\text{O}_3$ individual layers can provide an antiferroelectric orthorhombic phase, rhombohedral phase and morphotropic phase, respectively.²¹ The results indicate that the ECE can be enhanced by making use of the phase transition in the individual layer, and the synergistic effect of AFE/FE and FE/FE phase transitions is as effective as the effect of FE/PE phase transition. In particular, the multilayer thin films are endowed with refrigeration ability at the multi-temperature zones due to the coexisting multi-phases. The results further confirmed that the construction of bilayer or five-layer films is an effective way to enhance the ECE of PZT-based films, similar to our previous studies.^{22,23} In order to further confirm the validity of enhancing ECE by constructing coexisting multi-phases, in this study, the ECE effect of three-layered PZT films have been systematically investigated.

Experimental section

Fabrication of multilayer films

First, the precursor solution was prepared. $\text{Pb}(\text{CH}_3\text{COO})_2 \cdot 3\text{H}_2\text{O}$ (Sinopharm Chemical Reagent Co. Ltd, $\geq 99.5\%$) was dissolved in 2-methoxyethanol (Sinopharm Chemical Reagent Co. Ltd, $\geq 99\%$) and refluxed at 120°C for half an hour. After the solution was cooled down to room temperature, titanium

isopropoxide (Alfa, 99%) and zirconium *n*-propoxide (Alfa, 70% w/w in *n*-propanol) were added, in sequence. After refluxing for an hour, the concentration of the solution was adjusted to 0.4 mol L^{-1} by adjusting the volume of 2-methoxyethanol. Moreover, 10 mol% excess of $\text{Pb}(\text{CH}_3\text{COO})_2 \cdot 3\text{H}_2\text{O}$ was used to compensate the lead volatility during the processing. After aging the precursor solution for 24 hours, $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ multilayer thin films were deposited on $\text{Pt}(111)/\text{Ti}/\text{SiO}_2/\text{Si}$ substrates through a spin coating process at 4000 rpm for 15 s. The deposition of each layer was followed by pyrolysis at 375°C for 3 min, and each composition was spin coated for two layers. The total thickness of the films was determined by regulating the number of spin coatings. At last, the multilayer thin films were annealed *via* rapid temperature annealing (RTA) at 700°C for 5 min.

Microstructure characteristics

The crystalline structures of the thin films were analyzed using a Philips X'pert X-ray diffractometer (XRD) with $\text{Cu K}\alpha$ radiation generated at 40 kV and 40 mA. The surface morphology of the thin films was observed by atomic force microscopy (AFM) using a commercial setup of a scanning probe microscope system (CSPM5600 of Benyuan), and the cross-section micrograph of the thin film was obtained by SEM (Helios Nanolab600i) with an accelerating voltage of 20 kV.

Electrical measurements

Platinum top electrodes with a diameter of $200\text{ }\mu\text{m}$ were deposited by DC magnetron sputtering. Ferroelectric properties were measured using a Radiant Precision Workstation Ferroelectric Measurement System; three unique electrodes were tested for each sample. With the help of the Agilent 4294A precision impedance analyzer, the temperature dependence of the dielectric properties of the samples was measured at the frequency of 10 kHz with a 500 mV AC amplitude. The capacitance of the samples with the applied electric field was measured at 1 MHz with a 50 mV ac amplitude. The temperature was increased from room temperature (25°C) to 180°C using a Sigma heating system with the heating rate of 3°C min^{-1} .

Results and discussion

Microstructure

The XRD diffraction patterns shown in Fig. 1 indicate that both the up multilayer films and down multilayer films have a pure perovskite structure without any trace of secondary phases. The multi-phases, namely the orthorhombic AFE (O_{AFE}) phase originating from the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ layer, the rhombohedral FE (R_{FE}) phase originating from the $\text{PbZr}_{0.8}\text{Ti}_{0.2}\text{O}_3$ layer and the tetragonal FE (T_{FE}) phase originating from the $\text{PbZr}_{0.52}\text{Ti}_{0.48}\text{O}_3$ layer, are observed and coexist in the multilayer films. Since the $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ layer, which is closer to the $\text{Pt}(111)/\text{Ti}/\text{SiO}_2/\text{Si}$ substrate, possesses a different crystal lattice constant, the mismatch stress between the bottom $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ layer and Pt leads to the mixed orientation of (100) and (111) in the up

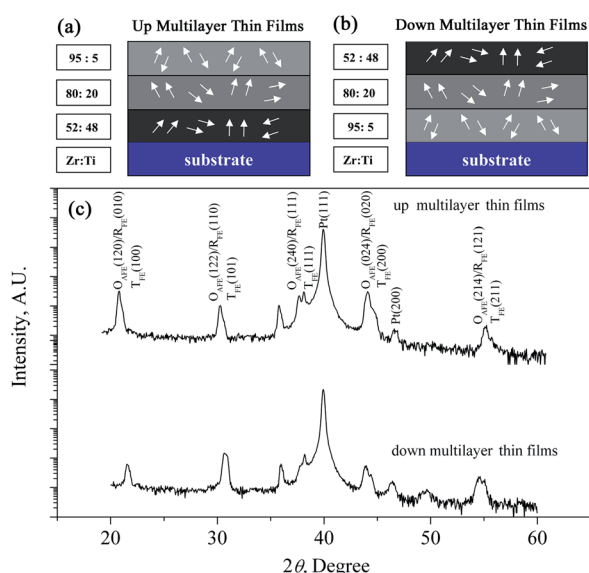


Fig. 1 Schematics of $\text{PbZr}_x\text{Ti}_{1-x}\text{O}_3$ multilayer thin films: (a) up multilayer thin films; (b) down multilayer thin films. (c) XRD patterns of the multilayer thin films.



multilayer films and (110) orientation in the down multilayer films; these results are in accordance with those obtained in our previous study.²²

AFM and SEM were carried out to characterize the surface morphology and cross-sectional morphology of the multilayer thin films, as shown in Fig. 2. The up multilayer films exhibited fine grains (size = ~ 90 nm) and dense surface structure. The down multilayer thin films, showed larger grain size (size = ~ 2 μm) and clear grain boundaries, while some fine grains (size = ~ 100 nm) can be seen on the surface of larger grains. The surface morphologies observed *via* SEM, as shown in Fig. 2(c) and (d), are consistent with that of the AFM images. It was reported that the activation energy for nucleation decreased with the increase in the Ti content in the PZT films.^{24,25}

In this study, the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ layer acts as the top layer for the up multilayer films, where the Zr-rich layer leads to the smaller grain size. For the down multilayer films, the Ti-rich layer of $\text{PbZr}_{0.52}\text{Ti}_{0.48}\text{O}_3$ possesses lower nucleation energy and results in the larger grain size.^{24,25} The cross-sectional images of the multilayer films are given in Fig. 2(e) and (f); the results indicate that the thickness of the multilayer films is approximately 300 nm. The differences in the microstructure of the up and down multilayer films are mainly induced by the different growth sequences. It was also reported that the grain size, thickness effects, substrates and associated processing conditions had deep influences on the electrical responses of PZT-based films.^{26–28}

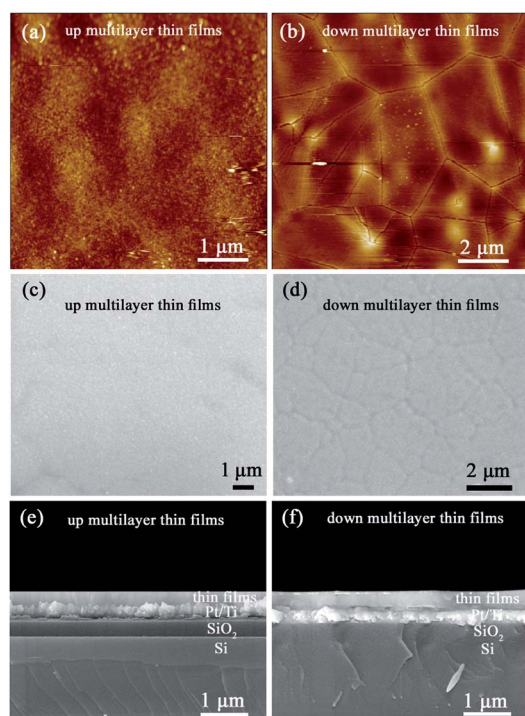


Fig. 2 AFM images of (a) up multilayer thin films and (b) down multilayer thin films. SEM images of the surface of (c) up multilayer thin films and (d) down multilayer thin films. SEM cross-sectional images of (e) up multilayer thin films and (f) down multilayer thin films.

Dielectric properties

The dielectric spectra, namely those of the temperature dependence of the dielectric properties and the characteristics of capacitance with applied electric field, are always used to investigate the phase structure and the phase transition behaviour of the materials. In this study, the dielectric constant (ϵ_r) and loss were measured using an Agilent 42941A impedance analyzer at 10 kHz and 500 mV ac amplitude; the temperature was increased from room temperature (25 °C) to 180 °C by the Sigma heating system with the heating rate of 3 °C min^{-1} . The capacitance of the samples with the applied electric field was measured at 1 MHz.

In Fig. 3, it can be seen that the spectrum of the up multilayer thin films shows an unclear peak at 120 °C, which is associated with the $\text{O}_{\text{AFE}}/\text{R}_{\text{FE}}$ phase transition of the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ layer, according to the PZT phase diagram.²¹ It needs to be stressed that no peak corresponding to the AFE/FE transition was observed in the curve of the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ single layer thin film.⁶ The dielectric constant of the down multilayer thin films has a broad peak corresponding to the $\text{R}_{(\text{FE}, \text{LT})}/\text{R}_{(\text{FE}, \text{HT})}$ phase transition of the $\text{PbZr}_{0.8}\text{Ti}_{0.2}\text{O}_3$ layer at around 150 °C.²¹ The broadening of the peak is typical in the curves of thin films, and may be induced by the interfacial strain and concentration gradients. In addition, the temperature dependence of the dielectric constant and dielectric loss around the room temperature indicates the phase transition of $\text{R}_{\text{FE}}/\text{T}_{\text{FE}}$ in the $\text{PbZr}_{0.52}\text{Ti}_{0.48}\text{O}_3$ MPB composite, but the $\text{O}_{\text{AFE}}/\text{R}_{\text{FE}}$ phase transition in the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ antiferroelectric layer cannot be observed at room temperature. The up and down multilayer films exhibit different variation trends of the dielectric spectrum, which implies that the thin film growth sequence has a deep influence on the phase transition of AFE/FE and FE/FE, which may be caused by the different misfit strain in the multilayer thin films.

The applied electric field dependence of capacitance of the up and down multilayer films is shown in Fig. 3(c) and (d),

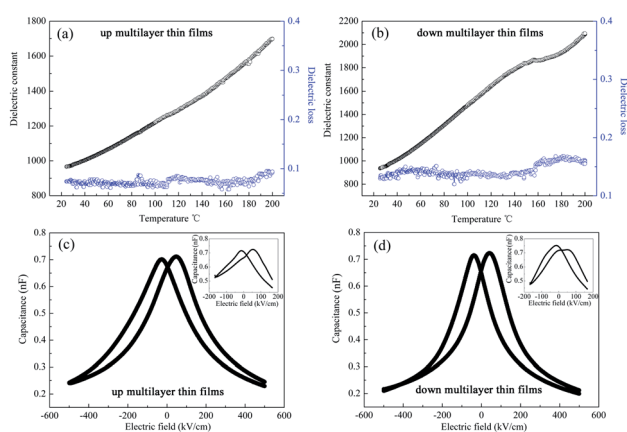


Fig. 3 Temperature dependence of the dielectric properties measured at 10 kHz for (a) up multilayer films and (b) down multilayer films. The capacitance with the applied electric field measured at 1 MHz for (c) up multilayer films and (d) down multilayer thin films.

respectively. It was reported that the capacitance vs. applied electric field of the AFE or FE thin films displays a double butterfly shape²³ and a single butterfly shape, respectively.²⁹ When a lower electric field of 175 kV cm⁻¹ is applied, as shown in the insets of Fig. 3, the non-symmetric curves of capacitance with the applied electric field can be observed, which demonstrates the coexistence of AFE phase and FE phase in the multilayer films. In particular, the AFE characteristic in the down multilayer thin films were more distinct than that in the up multilayer thin films. When the applied electric field reaches 500 kV cm⁻¹, the curves exhibit single butterfly characteristics, which indicates that only the FE phase existed in the multilayer films due to the electric field-induced AFE/FE phase transition.

Electrocaloric effect

An in-direct method was employed to evaluate the ECE of the multilayer thin films. The dependence of hysteresis loops (abbreviated as $P(E)$) on temperature was measured at a frequency of 100 Hz at a 5 K interval from 25 °C to 160 °C. A lower electric field of 826 kV cm⁻¹ was applied for the up multilayer thin films and a higher electric field of 992 kV cm⁻¹ was applied for the down multilayer thin films. The representative hysteresis loops given in Fig. 4(a) and (b) correspond to the up multilayer and down multilayer thin films. The shape of $P(E)$ loops exhibits some differences between the up and down multilayer films, which may be caused by the microstructure differences, such as mismatch stress and grain size, induced by the different growth sequence.

We assumed the reversible adiabatic changes following the Maxwell relationship, as shown in eqn (1), and the temperature change ΔT and entropy change ΔS for a material of density ρ with specific heat capacity C are expressed in eqn (2) and (3):^{6,7}

$$\left(\frac{\partial P}{\partial T}\right)_E = \left(\frac{\partial S}{\partial E}\right)_T \quad (1)$$

$$\Delta S = -\frac{1}{\rho} \int_{E_1}^{E_2} \left(\frac{\partial P}{\partial T}\right)_E dE \quad (2)$$

$$\Delta T = -\frac{1}{\rho C} \int_{E_1}^{E_2} T \left(\frac{\partial P}{\partial T}\right)_E dE \quad (3)$$

The values of $(\partial P/\partial T)$ were obtained from the fourth-order polynomial fits to the $P(T)$ data extracted from the upper branches of $P(E)$ loops in $E > 0$ (see the inset of Fig. 4(a) and (b)). According to the composition of each layer in the multilayer films, both the up multilayer and down multilayer thin films can be considered as Zr-rich lead-based thin films. The heat capacity $C = 330 \text{ J K}^{-1} \text{ kg}^{-1}$ and density $\rho = 8.3 \text{ kg cm}^{-3}$ can be selected for the Zr-rich lead-based thin films.^{6,17} As shown in Fig. 4(c) and (d), as expected, $\Delta T = 20.2 \text{ K}$ for the up multilayer thin films and $\Delta T = 46.3 \text{ K}$ for the down multilayer thin films are achieved at room temperature, which are mainly induced by the phase transition of $R_{\text{FE}}/T_{\text{FE}}$ at MPB in the $\text{PbZr}_{0.52}\text{Ti}_{0.48}\text{O}_3$ layer and $O_{\text{AFE}}/R_{\text{FE}}$ in the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ layer. It was reported that the presence of the monoclinic (M_A , M_B) phases between the R_{FE} and T_{FE} phase transition makes the lattice more frustrated and causes huge ΔS and ΔT values,¹⁹ particularly accompanying AFE/FE phase transition under electric field.¹⁸ It is also worth mentioning that both the films exhibit outstanding ECE at around 145 °C, much below the T_c . The peak of $\Delta T = 28.9 \text{ K}$ and 14.8 K for the up multilayer thin films and down multilayer thin films is observed, which is mainly attributed to the AFE/FE phase transition of the $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ layer and the FE/FE phase transition of the $\text{PbZr}_{0.8}\text{Ti}_{0.2}\text{O}_3$ layer and $\text{PbZr}_{0.52}\text{Ti}_{0.48}\text{O}_3$ layer according to the relationship between the dielectric constant and temperature. Insets of Fig. 4(c) and (d) give the entropy change ΔS with the increase in temperature. The maximum ΔS is $22.8 \text{ J K}^{-1} \text{ kg}^{-1}$ and $51.2 \text{ J K}^{-1} \text{ kg}^{-1}$ for the up and down multilayer thin films, respectively. The ECE improved significantly in comparison with our previous study, which may be attributed to the negative effect of the PbZrO_3 antiferroelectric layer.²² Honestly, besides the synergistic effect of multi-phases transition, which is one of the key factors to enhance the ECE, the effect of the domain architecture,³⁰ polarization,³¹ electrostatic interactions³² and misfit strain³³ in the multilayer films should be deeply investigated in further studies, as they may also play an important role in the enhancement of ECE in the multilayer thin films compared with the single-layer thin films. For comparison, Table 1 lists the electrocaloric effect of the representative lead-containing materials, where it can be found that the PZT multilayer films possess excellent ECE both at room temperature and around 145 °C.

Leakage current $I(t)$ measurements with their maximum field were investigated at 160 °C, as shown in Fig. 5. It can be seen that the steady-state leakage current for the up multilayer thin films and down multilayer thin films are 6 nA and 1.1 nA, respectively. The lower leakage current also indicates that the higher electric field can be applied for the down multilayer thin films. In addition, the less joule heat would be induced by the

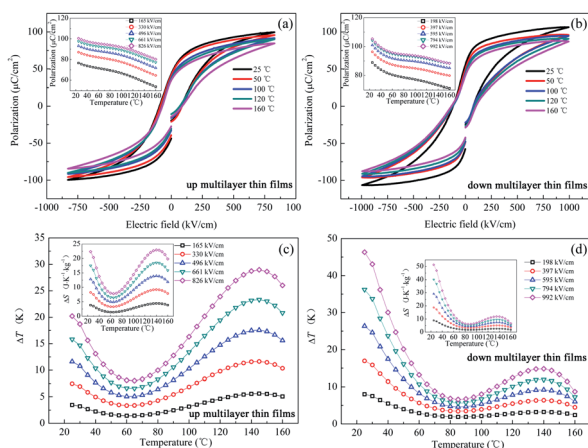


Fig. 4 $P(E)$ loops at selected temperatures for (a) up multilayer thin films and (b) down multilayer thin films. ΔT at selected electric fields for (c) up multilayer thin films and (d) down multilayer thin films.



Table 1 Electrocaloric characteristics of lead-containing thin films

Materials	ΔT (K)	ΔS (J K ⁻¹ kg ⁻¹)	Phase transition	T (°C)	Ref.
PZT up multilayer films	20.2	22.3	AFE/FE	25	This work
	28.9	22.8	FE/FE	145	
PZT down multilayer films	46.3	51.2	AFE/FE	25	This work
	14.8	11.8	FE/FE	140	
PbZr _{0.95} Ti _{0.05} O ₃	12	8	AFE/PE	226	6
Si doped PbZr _{0.95} Ti _{0.05} O ₃	8.5	5.89	AFE/PE	203	37
PbZrO ₃	11.4	—	AFE/PE	235	34
Pb _{0.97} La _{0.02} Zr _{0.75} Sn _{0.18} Ti _{0.07} O ₃	53.8	63.9	AFE/FE	5	16
Pb _{0.8} Ba _{0.2} ZrO ₃	45.3	46.9	AFE/FE	17	18
PbZr _{0.52} Ti _{0.48} O ₃	11.1	—	FE/FE	387	19
PMN-PT 67/33	14.5	—	FE/PE	150	35
PbZr _{0.95} Ti _{0.05} O ₃ /PbZr _{0.52} Ti _{0.48} O ₃ bilayer films	24.8	20.5	AFE/FE	125	23
	10.7	11.9	FE/FE	25	
PZT multilayer films	9.1	10	AFE/FE	25	22
	17.9	13.1	FE/FE	180	
PZT/BaTiO ₃ multilayer films	1.85	—	FE/PE	135	38
PbZr _{0.53} Ti _{0.47} O ₃ /CoFe ₂ O ₄ multilayer films	−52.2	94.23	—	−223	36

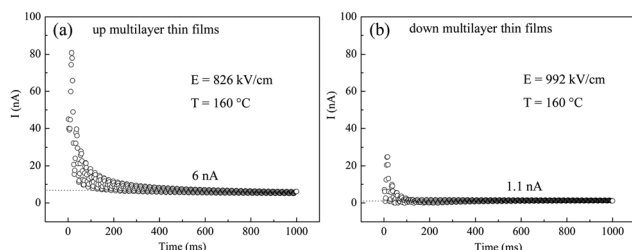


Fig. 5 Leakage current measurements of multilayer films at 160 °C (a) up multilayer thin films and (b) down multilayer thin films.

lower leakage current, which is beneficial for the refrigeration to work steadily.

Conclusions

In summary, we experimentally showed that the ECE in PbZr_xTi_{1-x}O₃ multilayer thin films can be significantly enhanced by the coupling effect of the AFE/FE phase transition and FE/FE phase transition. Our study highlights the importance of the multi-phases coexisting in the PbZr_xTi_{1-x}O₃ multilayer thin films. The results presented for the up multilayer and down multilayer thin films demonstrate the potential to achieve a large ECE. $\Delta T = 20.2$ K for the up multilayer thin films and $\Delta T = 46.3$ K for the down multilayer thin films have been achieved at room temperature, and $\Delta T = 28.9$ K and 14.8 K have also been observed in the up multilayer and down multilayer thin films, respectively. These results indicate that the AFE/FE or FE/FE phase transitions are as effective as the FE/PE phase transition, and large electrocaloric responses can be obtained at temperatures much below the Curie temperature.

Conflicts of interest

There are no conflicts to declare.

Acknowledgements

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