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## 1. Introduction

Manganese is a strategic material applied in the metallurgical industry and for some nonferrous applications.<sup>1</sup> Traditional manganese metallurgy is a typical hydrometallurgical technology that generally involves ore milling, acid leaching, purification, and final electrowinning as the four main steps.<sup>1,2</sup> Given the sustained consumption of high-grade manganese ores, low-grade ore is increasingly being utilized. This condition causes the traditional hydrometallurgical process to be increasingly uncompetitive and uneconomical due to the increasing energy waste and serious environmental issue.

A new manganese-leaching method originally proposed for flue-gas desulfurization and for studying NO removal application has been developed, and thus provides a promising prospect for the manganese industry.<sup>3–8</sup> For flue-gas desulfurization, the commonly accepted reaction processes are expressed in eqn (1)–(6).<sup>7,9,10</sup> In these reactions, ores containing manganese oxide compounds ( $\text{MnO}_2$ ,  $\text{Mn}_2\text{O}_3$ ,  $\text{Mn}_3\text{O}_4$ ) work as the active material to react with  $\text{SO}_2$ .

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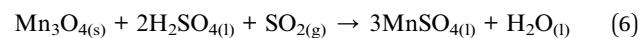
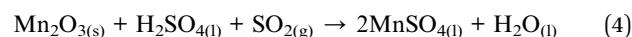
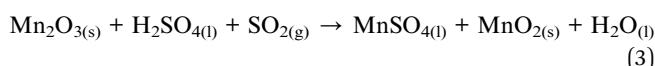
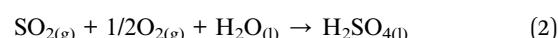
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† Electronic supplementary information (ESI) available: Fig. S1: The XRD patterns of the  $\alpha$ ,  $\beta$ ,  $\gamma$  and  $\delta$ -four different  $\text{MnO}_2$ ; Fig. S2: The Mn 2p spectrum of  $\alpha$ ,  $\beta$ ,  $\gamma$  and  $\delta$ -four different  $\text{MnO}_2$ ; Fig. S3: The XRD pattern of the used natural  $\text{MnO}_2$  ore; Table S1: The calculation of MD decomposition with different initial concentration, and the calculation method of MD concentration. See DOI: 10.1039/c9ra09810k

# Removal of manganous dithionate ( $\text{MnS}_2\text{O}_6$ ) with $\text{MnO}_2$ from the desulfurization manganese slurry†

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Manganese desulfurization has been increasingly explored, but the generated manganous dithionate (MD) by-product affects the valuable use of the desulfurized slurry. In this study,  $\alpha$ - $\text{MnO}_2$ ,  $\beta$ - $\text{MnO}_2$ ,  $\gamma$ - $\text{MnO}_2$ , and  $\delta$ - $\text{MnO}_2$  were prepared for MD removal in desulfurization manganese slurry. Results showed that  $\delta$ - $\text{MnO}_2$  had the best activity among the four because of its porosity and favorable surface properties. The operation conditions showed that 12.00 g  $\text{L}^{-1}$  MD can be removed by more than 80.00% under the conditions of 1.4 mol  $\text{L}^{-1}$  sulfuric acid, 100 g  $\text{L}^{-1}$   $\delta$ - $\text{MnO}_2$  dosage, and reaction at 90 °C for 3 h. The MD removal with  $\text{MnO}_2$  followed the decomposition–oxidation pass and direct oxidation–reduction reaction and consequently induced structure destruction and crystalline transfer. MD removal with natural  $\text{MnO}_2$  ore was also examined, and natural  $\text{MnO}_2$  ore in the  $\delta$  type was found to have prominent activity. Thus, this type of natural  $\text{MnO}_2$  may serve as a good alternative to pure  $\text{MnO}_2$  for decreasing the cost of MD removal from desulfurization manganese slurry.



During continuous  $\text{SO}_2$  removal, ore manganese is leached to generate lixivium-containing  $\text{MnSO}_4$ , which is used for electrolytic manganese production (EMP). Compared with traditional acid leaching, desulfurization-based leaching omits sulfuric acid preparation and is energy saving because no calcination is required. Consequently, the technique renovation of manganese metallurgy industry may be greatly developed if traditional acid manganese leaching is replaced by manganese ore-based flue-gas desulfurization.

However, redox reaction between manganese oxide and  $\text{SO}_2$ , especially  $\text{MnO}_2$ , has the inevitable by-product manganous dithionate (MD), which is formed following 7 or 8 dues to incomplete oxidation.<sup>10,11</sup> MD significantly restrains electrowinning during EMP.<sup>10,12</sup> This process may be result in low product purity and some secondary pollution if the final product is  $\text{MnSO}_4$ . Therefore, the MD of manganese ore-based desulfurization must be managed to determine the economic value of this technology and further broaden its application.

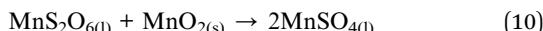
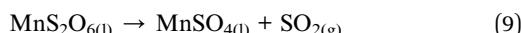


or



A low MD concentration ( $<6 \text{ g L}^{-1}$ ) of desulfurized manganese slurry obtained may be due to the following two different aspects: (1) the formation suppression during desulfurization and (2) desulfurized slurry MD removal. Regulating the acidity of manganese slurry, inlet  $\text{SO}_2$  concentration, and manganese composition can reduce MD formation.<sup>13–15</sup> However, we found that controlled MD formation is usually achieved at the expense of desulfurization performance and/or manganese leaching.<sup>16</sup> Consequently, a highly efficient MD removal method must be further explored.

Theoretically, MD can be decomposed into  $\text{MnSO}_4$  and  $\text{SO}_2$  at a relatively high temperature ( $>140 \text{ }^\circ\text{C}$ ) or strong acid condition (eqn (9)).<sup>4</sup> Qu *et al.* studied manganese leaching with  $\text{MnS}_2\text{O}_6$  and they found that  $\text{S}_2\text{O}_6^{2-}$  can be somehow oxidized by  $\text{MnO}_2$  (eqn (10)).<sup>17</sup> However, studies on the MD elimination using  $\text{MnO}_2$  is still superficial, primarily focusing on the exploration of technical conditions. The reaction mechanism and kinetics remain unclear. Moreover, laboratory studies commonly use pure  $\text{MnO}_2$ . Thus, the significance of research results for industrial application remains to be verified.



In this study, four types of  $\text{MnO}_2$  with different crystalline structures were prepared by coprecipitation and hydrothermal methods to eliminate MD from desulfurized manganese slurry. The susceptibility and influences of  $\text{MnO}_2$  crystalline, dosage, slurry acidity, and reaction temperature on MD removal were tested and discussed. The reaction mechanism of MD removal with  $\text{MnO}_2$  was proposed on the basis of the experimental phenomenon and characterization before and after the reaction. Finally, the applicability of natural  $\text{MnO}_2$  for MD removal was verified. The results showed good confirmation of the entire study.

## 2. Experimental

### 2.1 Materials and methods

MD-containing slurry was self-made using the pilot-scale system of manganese ore slurry-flue-gas desulfurization. The raw slurry had a pH of 1.6 and contained  $15.35 \text{ g L}^{-1}$   $\text{Mn}^{2+}$  ion and  $12.00 \text{ g L}^{-1}$   $\text{MnS}_2\text{O}_6$ . The  $\text{KMnO}_4$  (AR),  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$  (AR),  $(\text{NH}_4)_2\text{S}_2\text{O}_8$  (AR), and  $\text{H}_2\text{SO}_4$  (98%) were bought from Chron Chemicals (Chengdu, China) without further treatment.

Table 1 Analysis of the natural manganese ore used (wt%)

Components	Mn	Ca	Mg	Co
Content	40.35	0.72	3.41	0.025
Components	Ni	Zn	Fe	Cu
Content	0.025	0.001	0.010	0.0032

Natural  $\text{MnO}_2$  ore was shipped from the Gabonese Republic. Its main components based on the ICP-OES analysis after digestion are listed in Table 1.

### 2.2 Preparation of different $\text{MnO}_2$

$\alpha\text{-MnO}_2$ ,  $\gamma\text{-MnO}_2$ , and  $\delta\text{-MnO}_2$  were prepared *via* coprecipitation. Specifically, 2.18 g of  $\text{KMnO}_4$  (AR, Chron Chemicals, Chengdu, China) and 3.50 g of  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$  (AR, Chron Chemicals) were dissolved in 50 mL of deionized (DI) water (the mole ratio of  $\text{KMnO}_4/\text{MnSO}_4 \cdot \text{H}_2\text{O}$  was 2/3). A new beaker was then preloaded with 100 mL of DI water and placed in an  $80 \text{ }^\circ\text{C}$  water bath. The prepared  $\text{MnSO}_4$  and  $\text{KMnO}_4$  solutions were poured into the beaker at the same time, and the mixture was continuously mixed with a magnetic stirrer for 2 h. When the reaction process was completed, the obtained liquid–solid mixture was naturally cooled to room temperature and followed with repeated DI water washing until the pH of filtrate was almost 7. Finally, the mixture was dried at  $80 \text{ }^\circ\text{C}$  for 12 h, and the obtained subparticle was the  $\alpha\text{-MnO}_2$ . Compared with  $\alpha\text{-MnO}_2$  preparation,  $\gamma\text{-MnO}_2$  synthesis involved a relatively lower thermostatic reaction temperature of  $40 \text{ }^\circ\text{C}$ . For the preparation of  $\delta\text{-MnO}_2$ , a different  $\text{KMnO}_4/\text{MnSO}_4 \cdot \text{H}_2\text{O}$  ratio of 4/3 was used. This solution was prepared with 2.18 g of  $\text{KMnO}_4$  and 1.75 g of  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$  dissolved in 50 mL of DI water and was used as reactants for the following synthesis process.

The hydrothermal method was used to prepare  $\beta\text{-MnO}_2$  by using the precursors  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$  and  $(\text{NH}_4)_2\text{S}_2\text{O}_8$  (AR, Chron Chemicals). First, 8.45 g of  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$  and 11.41 g of  $(\text{NH}_4)_2\text{S}_2\text{O}_8$  were separately dissolved in 80 mL of DI water as substitute solution. For  $\beta\text{-MnO}_2$  preparation,  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$  solution was slowly instilled into  $(\text{NH}_4)_2\text{S}_2\text{O}_8$  and allowed to react for 20 min with continuous magnetic stirring. Subsequently, the mixture was transferred to PTFE jars and subjected to a 12 h hydrothermal reaction at  $140 \text{ }^\circ\text{C}$ . Subsequently, the mixture was naturally cooled to room temperature, and the following treatments, including filtration, washing, and drying, were performed similar to the coprecipitation method.

### 2.3 Removal of MD

Approximately 50 mL of desulfurized solution was placed into a 100 mL conical flask and then added with the calculated volume of sulfuric acid and  $\text{MnO}_2$  or manganese ore. The flask was sealed with parafilm and placed in a thermostatic water bath for MD removal with continuous magnetic stirring. When the reaction was completed, the reaction mixture was rapidly filtered, and the MD concentration of the filtrate was measured to calculate the removal efficiency of MD (eqn (11)), where  $\eta$  (%) is the of MD removal efficiency, and  $C_0$  and  $C_1$  ( $\text{g L}^{-1}$ ) are the initial and final MD concentrations, respectively.

MD concentration before and after the removal reaction was determined by the distillation-iodometric method with some improvements.<sup>18</sup> Specifically, 1.0 mL of the filtrate was placed into a triangular flask and then added with 10.0 mL of 1+1  $\text{H}_2\text{SO}_4$ . The flask was heated for distillation until acid mist formed and then cooled down naturally. The two-stage standard



iodine solution ( $0.0100 \pm 0.0005 \text{ mol L}^{-1}$ ) was used for  $\text{SO}_2$  adsorption, and highly pure nitrogen gas was used as carrier gas during the entire distillation. After the entire reaction, residual iodine was titrated using standard sodium thiosulfate ( $0.0100 \pm 0.0005 \text{ mol L}^{-1}$ ). To calculate MD concentration, a blank test was needed, which involved the use of the same volume of DI water in place of the sample. The blank was subjected to the same treatment and titration. For the blank test, the titration volume of sodium thiosulfate was  $V_0$  (mL), and the volume of sodium thiosulfate used for the sample titration was  $V_1$  (mL). The concentration of MD was calculated as in eqn (12), where  $C_{\text{MD}}$  is the concentration of MD ( $\text{g L}^{-1}$ ),  $V$  is the sample volume used for test (mL),  $c$  is the concentration of sodium thiosulfate ( $\text{mol L}^{-1}$ ), and  $m$  is the molar mass of MD (215.07).

$$\eta = \frac{C_0 - C_i}{C_0} \times 100\% \quad (11)$$

$$C_{\text{MD}} = \frac{(V_0 - V_1) \text{ cm}}{2V} \quad (12)$$

## 2.4 Characterization

The crystallographic form of the prepared  $\text{MnO}_2$  and natural manganese ore was analysed using an X-Pert PRO MPD diffractometer (Panalytical, NL) employing  $\text{Cu K}\alpha$  radiation at 30 kV and 20 mA. The step-scanning run over  $2\theta$  ranged at  $10\text{--}80^\circ$ , and crystalline phases were identified by the reference data from the International Center for Diffraction Data (JCPDs). Scanning electron microscopy (JEOL 7100F, Japan) with an acceleration voltage of 15.0 kV was used for the morphology characterization of the prepared  $\text{MnO}_2$ . SEM images with different magnifications were captured to obtain as much information as possible. X-ray photoelectron spectroscopy (XSAM-800, Kratos Co., UK) with Al (1486.6 eV) under ultra-high vacuum at 12.0 kV and 15.0 mA was applied to determine  $\text{MnO}_2$  surface chemistry before and after MD removal. Energy calibration was performed by recording the core level spectra of Au 4f<sub>7/2</sub> (84.0 eV) and Ag 3d<sub>5/2</sub> (368.30 eV).

## 3. Results and discussion

### 3.1 $\text{MnO}_2$ preparation and characterization

Fig. 1 presents the SEM images of the prepared four different  $\text{MnO}_2$ .  $\alpha\text{-MnO}_2$  showed a homogeneous nanorod structure with a length of approximately 200–400 nm.  $\beta\text{-MnO}_2$  represented a similar structure to that of  $\alpha\text{-MnO}_2$ , but its diameter was relative larger and the length extended to range of 600–800 nm. In contrast with the above two compounds,  $\gamma\text{-MnO}_2$  and  $\delta\text{-MnO}_2$  resembled a nanosphere structure.  $\gamma\text{-MnO}_2$  nanosphere ranged from 200 nm to 500 nm in diameter and seemed to be assembled by organized short cylindrical nanorods radiating outward. The  $\delta\text{-MnO}_2$  sphere was likely to be constructed by a multi-layer nanowire, and the sphere diameter was relatively large ranging at approximately 500–800 nm. The morphology characterization of the prepared  $\text{MnO}_2$  was consistent with that in previous studies,<sup>19,20</sup> confirming the preparation method used in this study. The XRD patterns in the Fig. S1† confirmed the classification, and the patterns of  $\alpha\text{-MnO}_2$ ,  $\beta\text{-MnO}_2$ ,  $\gamma\text{-MnO}_2$ , and  $\delta\text{-MnO}_2$  were highly concordant with their reference data JCPDS 44-0141 ( $\alpha\text{-MnO}_2$ ), JCPDS 24-0735 ( $\beta\text{-MnO}_2$ ), JCPDS 14-0644 ( $\gamma\text{-MnO}_2$ ), and JCPDS 80-1098 ( $\delta\text{-MnO}_2$ ).<sup>21–23</sup>

To identify the composition and surface chemistry, we carried out X-ray photoelectron spectroscopy (XPS) characterization of all four types of  $\text{MnO}_2$ . Fig. S2† shows the high-resolution Mn 2p spectrum, and the Mn 2p<sub>3/2</sub> characteristic peaks located close to 642.0 eV. This result identified that the manganese is typically  $\text{Mn}(\text{IV})\text{O}_2$ , even though some differences occurred causing energy peak shift.<sup>23</sup> Fig. 2 illustrates the high-resolution O 1s spectrum. The characteristic peaks with a binding energy range of 529–530 eV corresponded with the lattice oxygen ( $\text{O}_L$ ). Peaks with 531–532 eV binding energies were assigned to the defect oxide or surface oxygen ions ( $\text{O}_A$ ), and those higher than 533 eV were due to the adsorbed water ( $\text{O}_H$ ).<sup>23–25</sup> Compared with that of the three other samples, the O 1s spectrum of  $\beta\text{-MnO}_2$  showed a shift to the relatively lower binding energy region, which may be attributed to hydrothermal reaction and is commonly observed in previous

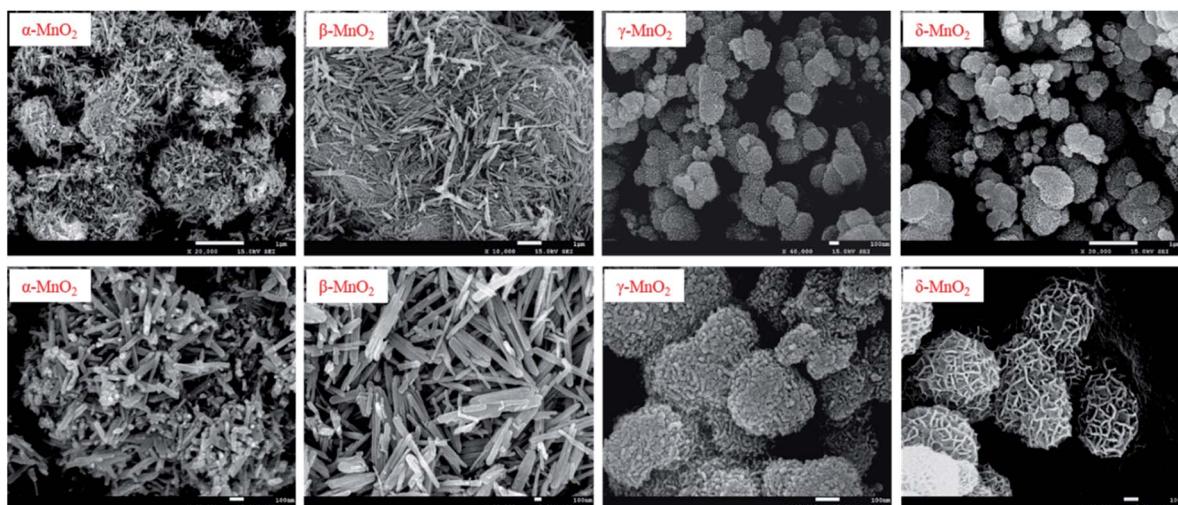


Fig. 1 SEM images of the  $\text{MnO}_2$  prepared with different crystalline.



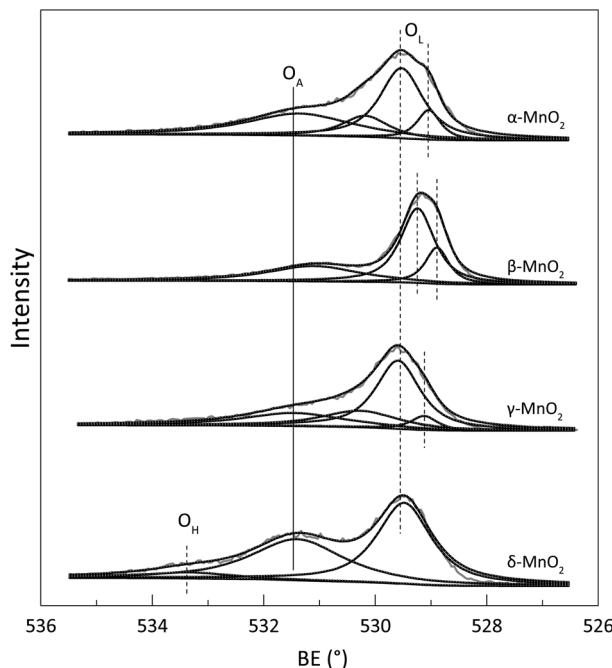


Fig. 2 The O 1s spectrum of the prepared  $\alpha$ -,  $\beta$ -,  $\gamma$ - and  $\delta$ - $\text{MnO}_2$ .

works.<sup>23,26</sup> Table 2 lists the  $O_A$  contents of the  $\alpha$ -,  $\beta$ -,  $\gamma$ -, and  $\delta$ - $\text{MnO}_2$ , which were 46.96%, 29.74%, 42.67%, and 43.32%, respectively. Theoretically, a high content of surface  $O_A$  indicates that the sample has strong oxidizability because of its high mobility for the potential oxidation reaction.<sup>27</sup> Thus, the oxidation susceptibility of the four types of  $\text{MnO}_2$  followed the order  $\alpha\text{-MnO}_2 > \gamma\text{-MnO}_2 > \delta\text{-MnO}_2 > \beta\text{-MnO}_2$ . Notably, the liquid–solid reaction was a multi-factorial process. Thus, effective contact surface area and interfacial mass transfer and must be analysed to make a comprehensive conclusion.

### 3.2 MD removal with different $\text{MnO}_2$

Fig. 3 demonstrates the activity of four different  $\text{MnO}_2$  for the MD removal from the true desulfurized manganese slurry. The activity of four different  $\text{MnO}_2$  used for the MD removal followed the sequence  $\delta\text{-MnO}_2 > \alpha\text{-MnO}_2 > \beta\text{-MnO}_2 > \gamma\text{-MnO}_2$ .  $\delta\text{-MnO}_2$  showed the best activity the MD oxidation under  $1.4 \text{ mol L}^{-1}$  sulfuric acid at  $60^\circ\text{C}$ , with an MD removal efficiency of 25.63%.

Table 2 The surface oxygen chemistry based on the O 1s manipulation<sup>a</sup>

Samples	$O_L$		$O_A$		$O_H$	
	BE	%	BE	%	BE	%
$\alpha\text{-MnO}_2$	529.04–529.53	53.05	530.18–531.36	46.96	NA	NA
$\beta\text{-MnO}_2$	528.89–529.24	70.26	531.10	29.74	NA	NA
$\gamma\text{-MnO}_2$	529.12–529.59	57.33	530.27–531.45	42.67	NA	NA
$\delta\text{-MnO}_2$	529.48	50.80	531.40	43.32	533.34	5.88

<sup>a</sup> NA: not detected.

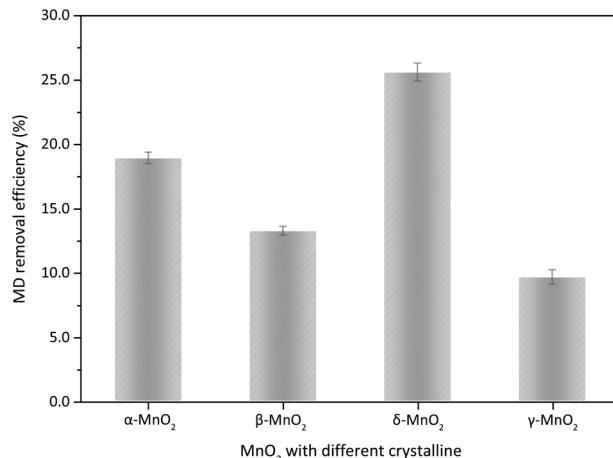


Fig. 3 The MD removal with different type of  $\text{MnO}_2$  (reaction conditions:  $8.00 \text{ g L}^{-1}$  MD,  $1.4 \text{ mol L}^{-1}$  sulfuric acid,  $100 \text{ g L}^{-1}$  of  $\text{MnO}_2$  addition, reacted at  $60^\circ\text{C}$  for 3 h).

The valence of sulphur in MD is a transient state  $\text{V}$ ,  $\text{S}_2\text{O}_6^{2-}$  removal with  $\text{MnO}_2$  is an oxidation process, and the activity of surface oxygen directly relate to the removal performance. As shown in Table 2, the  $O_A$  content of four different  $\text{MnO}_2$  followed the order  $\beta\text{-MnO}_2 < \gamma\text{-MnO}_2 < \delta\text{-MnO}_2 < \alpha\text{-MnO}_2$ . If the surface  $O_A$  of  $\text{MnO}_2$  is key factor to MD removal,  $\alpha\text{-MnO}_2$  should show the relatively best and  $\beta\text{-MnO}_2$  exhibit the relatively worst MD removal performance. As shown in Fig. 3, the  $\delta\text{-MnO}_2$  demonstrated relative lower surface  $O_A$  compared with  $\alpha\text{-MnO}_2$ , while it showed the highest MD removal efficiency. This finding indicates that surface  $O_A$  content was not the limiting factor for MD removal of four different  $\text{MnO}_2$ , it should be the effective surface area and/or interfacial mass transfer, which greatly affected the activity of MD removal.

$\text{MnO}_2$  with different crystallographic structures show different tunnel structures;  $\alpha\text{-MnO}_2$  and  $\beta\text{-MnO}_2$  have  $[2 \times 2]$  and  $[1 \times 1]$  1D tunnel structures, respectively;  $\gamma\text{-MnO}_2$  has  $[1 \times 1]$  and  $[1 \times 2]$  alternating 1D structure, and  $\alpha\text{-MnO}_2$  has a layered structure.<sup>19,28</sup> For the three types of 1D structure  $\text{MnO}_2$ , their average chemical binding of Mn–O were  $1.98 \text{ \AA}$  ( $\alpha\text{-MnO}_2$ ),  $1.88 \text{ \AA}$  ( $\beta\text{-MnO}_2$ ) and  $1.91 \text{ \AA}$  ( $\gamma\text{-MnO}_2$ ).<sup>23</sup> This finding indicates that  $\alpha\text{-MnO}_2$  has the best surface oxygen mobility among the structures.<sup>29</sup> Moreover, the  $[2 \times 2]$  tunnel structure has stronger oxidation susceptibility than the  $[1 \times 1]$  1D tunnel structure.<sup>23,30</sup> These findings, including the experimental results in this study, may be used to explain why  $\delta\text{-MnO}_2$  had relatively better activity for MD removal than  $\gamma\text{-MnO}_2$ ,  $\beta\text{-MnO}_2$  and  $\gamma\text{-MnO}_2$ . In contrast with  $\alpha$ -,  $\beta$ -, and  $\gamma$ - $\text{MnO}_2$ ,  $\delta\text{-MnO}_2$  had a layered structure and showed a reticular, hollow nanosphere morphology (Fig. 1). Zhang *et al.* characterized  $\delta\text{-MnO}_2$ , showing the relative largest BET surface area among the four types of  $\text{MnO}_2$ .<sup>20,23</sup> This result indicates that  $\delta\text{-MnO}_2$  may provide more contacted reaction surface area and much more active sites could be exposed for interfacial reaction compared with the other forms. Moreover, the detected surface  $O_H$  forecasted that  $\delta\text{-MnO}_2$  had better hydrophilicity, which results in better molecular diffusion and mass transfer in aqueous reaction system. Therefore, we can

conclude that the better MD removal performance of  $\delta$ -MnO<sub>2</sub> is attributed to the synergy work of the relative high O<sub>A</sub> content, improved porosity, and hydrophilicity.

### 3.3 Influences of reaction parameters

In this section, the  $\delta$ -MnO<sub>2</sub> that has the best reaction activity was used to discuss the influences of operation parameters on MD removal, including the reaction temperature, duration time, sulfuric acid content, MnO<sub>2</sub> dosage and MD concentration.

**3.3.1 Reaction temperature.** The operation conditions, including initial MD concentration, sulfuric acid content, and  $\delta$ -MnO<sub>2</sub> addition, were kept constant. The influence of reaction temperature on the MD removal was discussed. As shown in Fig. 4, MD removal efficiency gradually increased with increased reaction temperature, indicating that the temperature significantly affected MD removal. At 60 °C, 25.63% of MD decomposed after 3 h of reaction. This value increased to 95.07% with increased temperature to almost 100 °C. Under high reaction temperature, the high molecular kinetic energy of reactants increased the probability of effective collision. Moreover, the MD molecules will become unstable under high reaction temperature and is active to react with  $\delta$ -MnO<sub>2</sub>. Considering economy and practical operation, the optimum reaction temperature should be 90 °C, and more than 85.00% of the MD could be removed.

**3.3.2 Duration time.** The operation conditions, including initial MD concentration, sulfuric acid and  $\delta$ -MnO<sub>2</sub> addition, and reaction temperature, were kept constant. The results confirmed that MD removal changed with duration time. As the reaction continued, MD concentration gradually decreased (Fig. 5). Only 51.68% of the MD could be decomposed within 1 h of reaction, and this value increased to 85.94% at 3 h reaction time. Further prolonged reaction time was not recommended even though the removal efficiency also further increased. The reduced reaction rate may be due to (1) decreased reactant

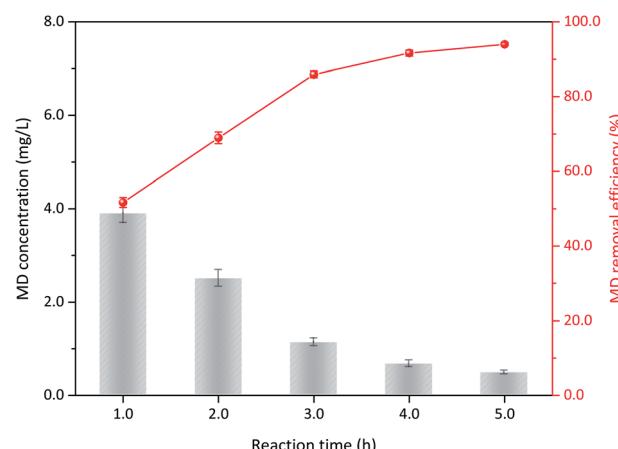


Fig. 5 The influence of reaction time on MD removal (reaction conditions: 8.00 g L<sup>-1</sup> MD, 1.4 mol L<sup>-1</sup> sulfuric acid, 100 g L<sup>-1</sup>  $\delta$ -MnO<sub>2</sub>, reacted at 90 °C).

concentration and (2) the evolution of surface physicochemical properties.<sup>31</sup> With continuous reaction, the concentration of reactants gradually decreased, slowing mass transfer. Moreover, the reaction between the  $\delta$ -MnO<sub>2</sub> and MD may also result in structure destruction and surface chemistry, such as layered structure, crystal structure, and composition of surface oxygen.  $\delta$ -MnO<sub>2</sub> and MD worked synergistically to gradually reduce the reaction rate. Therefore, a too long reaction time only decreases production efficiency for industrial application. The recommended duration time is not more than 3 h.

**3.3.3 Sulfuric acid concentration.** The operation conditions, including initial MD concentration,  $\delta$ -MnO<sub>2</sub> addition, and reaction temperature, was maintained constant to determine the effect of sulfuric acid addition on MD removal. At 1.0 mol L<sup>-1</sup> acid concentration, the removal efficiency of MD was 61.34% after 3 h of reaction and only slightly increased at an acid content of 1.2 mol L<sup>-1</sup> (66.32%, Fig. 6). Subsequently,

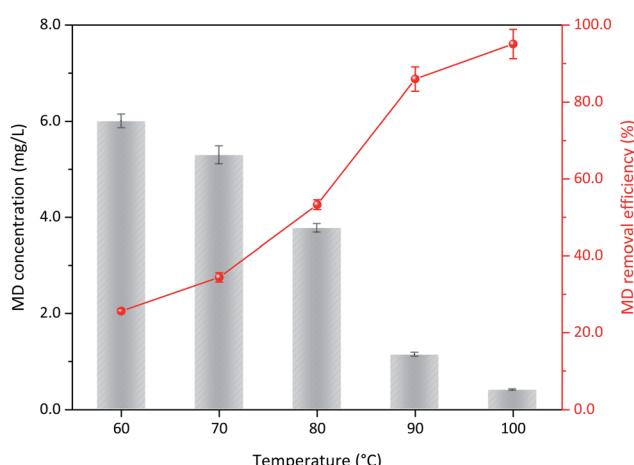


Fig. 4 The influence of reaction temperature on the MD removal with  $\delta$ -MnO<sub>2</sub> (reaction conditions: 8.00 g L<sup>-1</sup> MD, 1.4 mol L<sup>-1</sup> sulfuric acid, 100 g L<sup>-1</sup>  $\delta$ -MnO<sub>2</sub>, reacted 3 h).

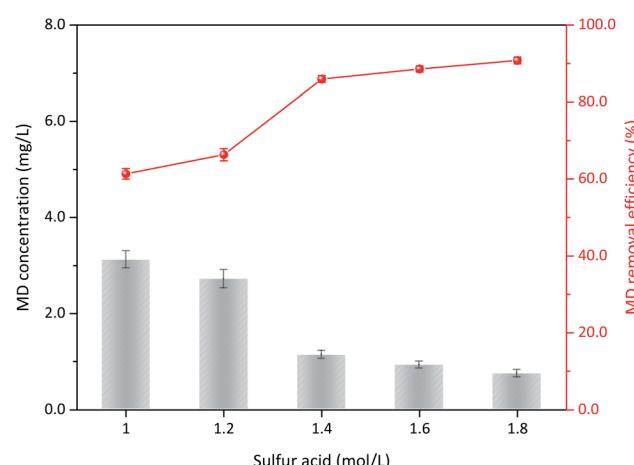


Fig. 6 The influence of sulfuric acid content on the MD removal (reaction conditions: 8.00 g L<sup>-1</sup> MD, 100 g L<sup>-1</sup>  $\delta$ -MnO<sub>2</sub>, reacted at 90 °C for 3 h).



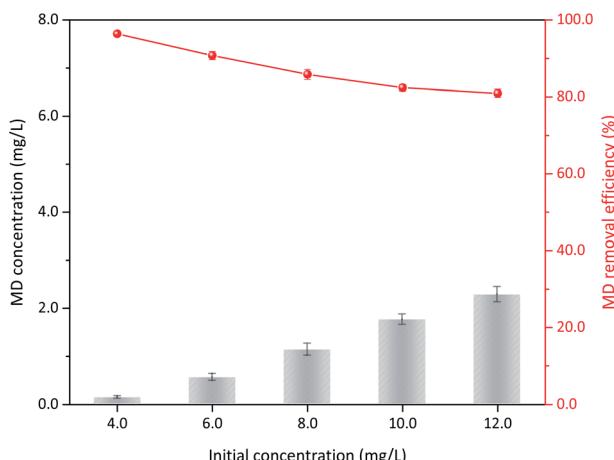


Fig. 7 The influences of initial MD concentration on MD removal (reaction conditions:  $1.4 \text{ mol L}^{-1}$  sulfuric acid,  $100 \text{ g L}^{-1}$   $\delta\text{-MnO}_2$ , reacted at  $90^\circ\text{C}$  for 3 h).

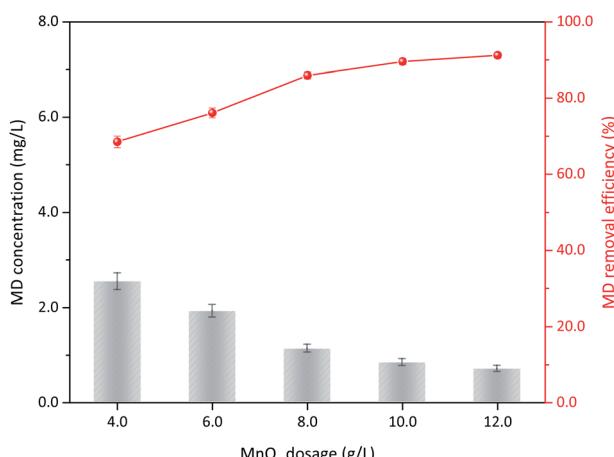


Fig. 8 The influences of  $\delta\text{-MnO}_2$  dosage on the MD removal (reaction conditions:  $8.00 \text{ g L}^{-1}$  MD,  $1.4 \text{ mol L}^{-1}$  sulfuric acid, reacted at  $90^\circ\text{C}$  for 3 h).

MD removal efficiency increased with increased sulfuric acid content from  $1.2 \text{ mol L}^{-1}$  to  $1.4 \text{ mol L}^{-1}$ . The removal efficiency clearly increased from 66.32% to 85.95%. Subsequently, further addition of sulfuric acid addition was unnecessary, and the MD removal efficiency remained relatively stable.  $\text{H}^+$  reportedly plays an important role in the  $\delta\text{-MnO}_2$  redox reaction, and a strong  $\text{H}^+$  atmosphere can accelerate the oxidability of  $\text{MnO}_2$ .<sup>32</sup> For the MD removal using  $\text{MnO}_2$ , the  $\text{MnO}_2$  was reduced to  $\text{Mn}^{2+}$ , and the redox potential between them ( $E_{\text{MnO}_2/\text{Mn}^{2+}}$ ) could be calculated as in eqn (13).<sup>32,33</sup> Therefore, the increased acidity can promote the reduction potential of  $\text{MnO}_2$ , but a concentration higher than  $1.4 \text{ mol L}^{-1}$  is unnecessary.

$$E_{\text{MnO}_2/\text{Mn}^{2+}} = 1.229 - 0.118\text{pH} - 0.0296 \lg C_{\text{Mn}^{2+}} \quad (13)$$

**3.3.4  $\delta\text{-MnO}_2$  dosage.** The operation conditions, including initial MD concentration, sulfuric acid concentration, and reaction temperature, were kept constant. The influence of  $\delta\text{-MnO}_2$  dosage on the MD removal is illustrated in Fig. 7. When  $60 \text{ g L}^{-1}$   $\delta\text{-MnO}_2$  was added, the MD concentration was reduced from  $8.00 \text{ g L}^{-1}$  to  $2.54 \text{ g L}^{-1}$ , showing 68.51% MD removal efficiency. The final concentration number decreased to  $1.13 \text{ g L}^{-1}$  (85.95%) with increased  $\delta\text{-MnO}_2$  to  $100 \text{ g L}^{-1}$ . Subsequently, only limited improvement was observed with further increased  $\delta\text{-MnO}_2$  dosage. With increased  $\delta\text{-MnO}_2$  addition, further active sites can participate to remove the MD, and a high MD removal efficiency is obtained.<sup>34</sup> Notably, the initial concentration of MD, acidity, and temperature were constant, which means MD could take part in the surface reaction had a maximum, excess  $\delta\text{-MnO}_2$  supply cannot improve the reaction efficiently. Consequently,  $100 \text{ g L}^{-1}$   $\delta\text{-MnO}_2$  addition content for MD removal is recommended in this study.

**3.3.5 Initial MD concentration.** Sulfuric acid addition,  $\delta\text{-MnO}_2$  dosage, and reaction temperature were kept constant. Varied MD removal with initial concentration was also considered. Approximately 96.40% MD could be removed when the initial concentration was  $4.00 \text{ g L}^{-1}$ , and the apparent removal

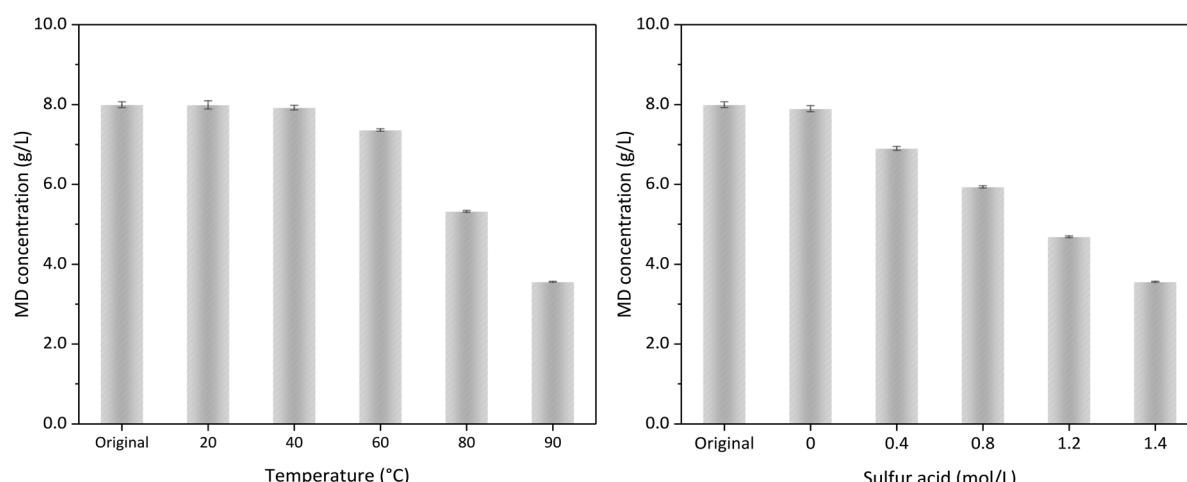


Fig. 9 The MD removal (a) in  $1.4 \text{ mol L}^{-1}$  sulfuric acid at different temperature, and (b) a constant temperature at  $90^\circ\text{C}$  with different sulfuric acid dosage.



efficiency only showed a limited reduction with increased initial MD concentration (Fig. 8). Under the conditions of  $1.4 \text{ mol L}^{-1}$  sulfuric acid,  $100 \text{ g L}^{-1}$   $\delta\text{-MnO}_2$  dosage, and  $90^\circ\text{C}$  reaction temperature, up to  $10.00 \text{ g L}^{-1}$  MD could be reduced to less than  $2.00 \text{ g L}^{-1}$ . The corresponding removal efficiency was only decreased 15.44% to 80.96% when the initial concentration of MD increased three times to  $12.00 \text{ g L}^{-1}$ . This finding indicated that  $\delta\text{-MnO}_2$  had prominent stability and activity for MD removal under the optimized reaction conditions. Furthermore, the MD removed per unit  $\delta\text{-MnO}_2$  could be the best proof, which conspicuously raised from  $38.6 \text{ mg L}^{-1} \text{ g}^{-1}$  to  $97.1 \text{ mg L}^{-1} \text{ g}^{-1}$   $\delta\text{-MnO}_2$  when the MD concentration was changed from  $4.00 \text{ g L}^{-1}$  to  $12.00 \text{ g L}^{-1}$  (Table S1†). The gradually reduced removal efficiency was attributed to the significant increase in initial MD concentration.

### 3.4 Mechanism analysis of MD removal

Fig. 9 shows the influence of temperature and acid concentration on the MD removal without  $\delta\text{-MnO}_2$  addition. Under  $1.4 \text{ mol L}^{-1}$  sulfuric acid and temperature higher than  $60^\circ\text{C}$ , a part of MD could be decomposed without  $\delta\text{-MnO}_2$  addition. Fig. 4 reveals that  $\delta\text{-MnO}_2$  played a critical role for MD removal in the desulfurized manganese slurry. The influence of sulfuric acid content represented in Fig. 9b and 6 showed almost the same conclusion. Without any  $\delta\text{-MnO}_2$  addition, MD removal could be due to the MD self-decomposition under strong acidity condition. We found that the reaction products could discolour the C.1. Acid Violet 7 (18055) using the high-purity nitrogen as carry gas, which illustrated the formation of  $\text{SO}_2$  in the strong acidity and high temperature condition (eqn (10)).

Fig. 10 shows the SEM images of  $\delta\text{-MnO}_2$  before and after MD removal. The uniform nanomesh-structure of  $\delta\text{-MnO}_2$  was clearly destroyed and presented a new analogous fusion surface after MD removal.<sup>35</sup> The destroyed structure followed clear agglomeration because the particle size of the used  $\delta\text{-MnO}_2$

residue was big. Fig. 11 illustrates the XRD patterns of the new  $\delta\text{-MnO}_2$  and reacted residue. The characteristic peaks belonging to  $\delta\text{-MnO}_2$  almost disappeared after MD removal. Alternatively, some characteristic peaks corresponding to  $\alpha\text{-MnO}_2$  were detected. This transformation indicated that MD removal resulted in the destruction of the 2D layered structure of  $\delta\text{-MnO}_2$  and consequently transferred to the  $[2 \times 2]$  1D  $\alpha\text{-MnO}_2$ .<sup>35</sup> The MD removal shown in Fig. 3 indicates that the reaction activity of the four different  $\text{MnO}_2$  structures followed order  $\delta\text{-MnO}_2 > \alpha\text{-MnO}_2 > \gamma\text{-MnO}_2 > \beta\text{-MnO}_2$ . This result indicates that the newly formed  $\alpha\text{-MnO}_2$  could remain effective for MD removal even though its activity is relative worse. This transformation of microcrystalline structure may also explain the influence of duration time shown in Fig. 5. The newly formed  $\alpha\text{-MnO}_2$  partially resulted in the gradually reduced reaction rate.

Based on the characterization, including SEM and XRD before and after the MD removal reaction, and considering previous results, the MD removal with  $\text{MnO}_2$  may occur *via* the two following mechanisms. First is the decomposition-oxidation pathway (DO), in which MD is transferred to dithionic acid ( $\text{H}_2\text{S}_2\text{O}_6$ , eqn (14)) and then decomposed to  $\text{H}_2\text{SO}_4$  and  $\text{SO}_2$  (eqn (15)) the high temperature and strong acidity.<sup>36</sup> The generated  $\text{SO}_2$  further reacts with  $\text{MnO}_2$  to generate  $\text{MnSO}_4$  (eqn (1)). Second is the direct oxidation-reduction (OR) reaction between the MD and  $\text{MnO}_2$ , which could be expressed by two half-reactions; the reduction half-reaction involves  $\text{Mn}(\text{IV})\text{O}_2$  obtaining two electrons to the divalent state ( $\text{Mn}(\text{II})$ ) (eqn (16)),<sup>37</sup> and the oxidation half-reaction involves  $\text{S}_2\text{O}_6^{2-}$  donating electrons to  $\text{SO}_4^{2-}$  (eqn (17)). The two half-reactions could be integrated into eqn (18), and its Gibbs free energy was calculated to be  $-279.70 \text{ kJ mol}^{-1}$ .

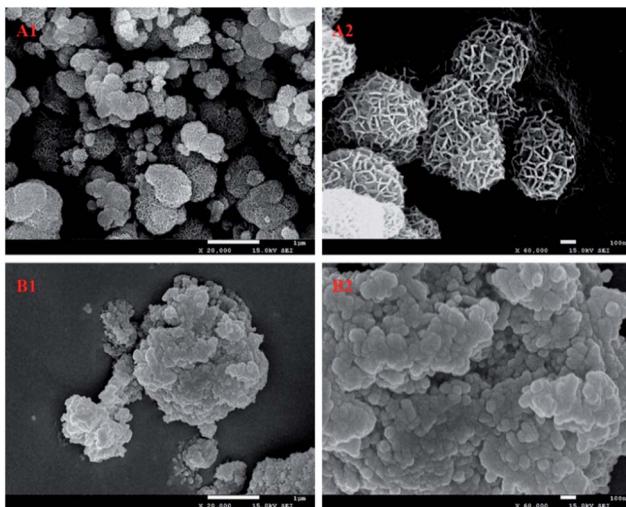
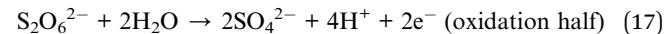
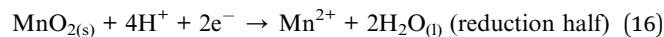
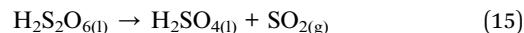


Fig. 10 The SEM image of  $\delta\text{-MnO}_2$  before (A1 and A2) and after (B1 and B2) the MD removal.

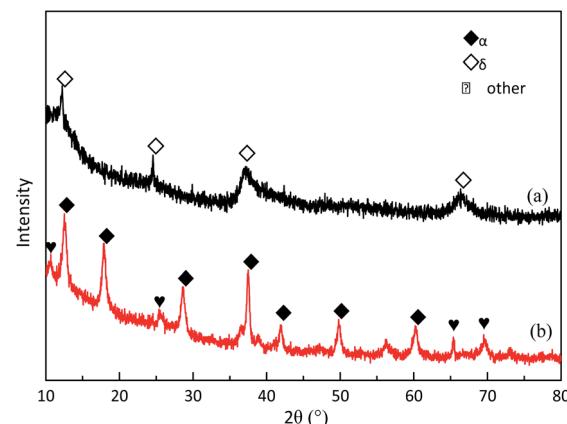


Fig. 11 The XRD patterns of  $\delta\text{-MnO}_2$  before (a) and after (b) the MD removal.



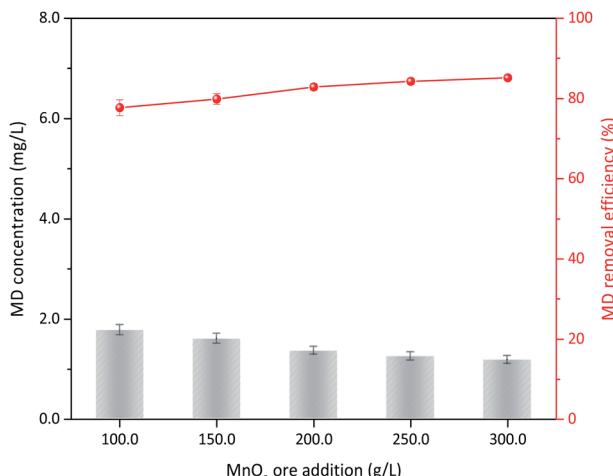
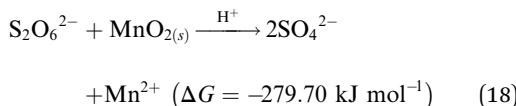


Fig. 12 MD removal with the natural MnO<sub>2</sub> ore (reaction conditions: 8.00 g L<sup>-1</sup> MD, 1.4 mol L<sup>-1</sup> sulfuric acid, reacted at 90 °C for 3 h).



### 3.5 MD removal with natural manganese oxide ore

On the basis of the aforementioned results, MD removal with natural manganese oxide ore was carried out under relative optimum conditions. The XRD analysis indicated that MnO<sub>2</sub> in the ore was primarily the δ type (Fig. S3†), which had the best activity for MD removal among the four types of MnO<sub>2</sub> mentioned in this study. For the feasibility test, the operation conditions of 8.00 g L<sup>-1</sup> MD, 1.4 mol L<sup>-1</sup> sulfuric acid, 90 °C reaction temperature, and 3 h of reaction were used. MD removal at different ore dosages is shown in Fig. 12. MD removal showed a similar tendency with the synthesized δ-MnO<sub>2</sub>. When 100 g L<sup>-1</sup> ore were added, the final MD concentration was only 1.78 g L<sup>-1</sup> (corresponded MD removal efficiency was 77.74%), which was even lower than the same content of pure δ-MnO<sub>2</sub> used. Increasing the dosage of MnO<sub>2</sub> ore slowly increased the removal efficiency. This finding indicated that natural MnO<sub>2</sub> ore is suitable for MD removal from desulfurization manganese slurry. In industrial applications, the desulfurization slurry should be further filtered before MD removal, and the MD removal residue can be returned to the front desulfurization section.

## 4. Conclusions

α-MnO<sub>2</sub>, β-MnO<sub>2</sub>, γ-MnO<sub>2</sub>, and δ-MnO<sub>2</sub> were prepared for MD oxidation removal in desulfurized manganese slurry. Results showed that δ-MnO<sub>2</sub> had the best oxidation activity due to its porosity and favorable surface properties. The optimal conditions were 1.4 mol L<sup>-1</sup> sulfuric acid, 100 g L<sup>-1</sup> δ-MnO<sub>2</sub> dosage, and reaction at 90 °C for 3 h, which can remove more than 80.00% of MD with an initial MD concentration of 12.00 g L<sup>-1</sup>.

The MD removal with MnO<sub>2</sub> followed the DO pass and direct OR reaction, and consequently induced structure destruction and crystalline transfer. MD removal with natural MnO<sub>2</sub> ore was also performed, and the natural MnO<sub>2</sub> ore in the δ type showed prominent activity. Thus, this type of natural MnO<sub>2</sub> ore can be a good alternative to pure MnO<sub>2</sub> for decreasing the cost of MD removal from desulfurization manganese slurry.

## Conflicts of interest

There are no conflicts to declare.

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