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## 3D multiphoton lithography using biocompatible polymers with specific mechanical properties†

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The fabrication of two- and three-dimensional scaffolds mimicking the extracellular matrix and providing cell stimulation is of high importance in biology and material science. We show two new, biocompatible polymers, which can be 3D structured *via* multiphoton lithography, and determine their mechanical properties. Atomic force microscopy analysis of structures with sub-micron feature sizes reveals Young's modulus values in the 100 MPa range. Assessment of biocompatibility of the new resins was done by cultivating human umbilical vein endothelial cells on two-dimensionally structured substrates for four days. The cell density and presence of apoptotic cells has been quantified.

### Introduction

Mimicking the mechanical properties of an extracellular matrix is of paramount importance in tissue engineering. The bone formation process or neural tissue reconstruction is especially sensitive to the mechanical, topographical and chemical properties of the substrates.<sup>1,2</sup> The matrix closely interacts with the embedded cells and has a direct impact on cell fate.<sup>3,4</sup> For the best possible mimicking of a tissue scaffold with controllable topography,<sup>3</sup> tuning of the mechanical and chemical properties is required.<sup>4,5</sup> All these properties help to guide cell growth and tissue formation, improving cell adhesion and enhancing cell survival.<sup>3–8</sup> Consequently, great efforts have been made to study the impact of cell-matrix interactions at a cellular level.<sup>5</sup> For a better understanding of these interactions, however, there is still a lack of biocompatible materials with determined mechanical properties, which can be structured in 3D with feature sizes ranging from micro to nanoscale. Multiphoton lithography (MPL) and related methods<sup>9</sup> are the only techniques capable of 3D structuring with a resolution in the sub-micrometer

regime. MPL outperforms technologies like stereolithography and electrospinning typically used for tissue engineering in regard to the 3D resolution.<sup>5,6,10,11</sup> 3D structuring of biocompatible polymers helps to better control the scaffolds elastic properties and to adapt the structure for the tissue environment.

In the past, MPL fabricated 3D nanostructures were used for tissue engineering *in vitro*<sup>1,2</sup> and *in vivo*,<sup>12</sup> production of metamaterials with flexible mechanical properties,<sup>13</sup> fabrication of responsive and programmable materials,<sup>14</sup> quantification of forces applied by living cells onto the environment,<sup>11,15</sup> or for structuring soft gelatine-based scaffolds and biocompatible 3D hydrogel woodpiles.<sup>16–20</sup> Most of these applications require a precise knowledge about the mechanical properties of the material. Mechanical properties (such as Young's modulus ( $E$ ), stiffness, *etc.*) of the specific polymers can be investigated *via* atomic force microscopy (AFM). For Young's modulus analysis, the cantilever tip is used as a nanoindenter, and the deformation of the specimen at a given force is recorded.<sup>21,22</sup>

In this contribution, we present two biocompatible resins, which can be structured *via* 3D MPL, and characterize their mechanical properties. The overall performance of these new resins was compared to two resins, which are commonly used in MPL. We show that the new photoresists enable 3D structuring with high aspect ratios and feature sizes in the sub-micrometer regime. For biocompatibility testing, endothelial cells were cultured on polymeric structures for several days. On both resins, closely connected human umbilical vein endothelial cells (HUVECs) with typical endothelial morphology formed a confluent monolayer that covered the glass surface and polymer structures. The increased cell

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density and low amount of apoptotic cells indicate high biocompatibility of new photoresists.

## Materials and methods

### Lithography setup

A scheme of the Workshop of Photonics (WOP, Lithuania) MPL setup is given in Fig. 1a. The two-photon photoinitiators were excited with 515 nm ultra-short laser pulses (CARBIDE, 1 MHz repetition rate, 290 fs pulse duration, Light Conversion, Lithuania). All stated intensities are peak intensities calculated from power measured in front of the objective lens (Zeiss, 63× magnification, NA 1.25), transmission of the objective, and diffraction-limited spot area. The writing was performed in a dip-in configuration.<sup>23</sup> A 3-axis stage (AEROTECH Nanopositioner, USA) was used for sample motion. Optionally, faster lateral writing is performed by a galvanometric mirror scanner (AEROTECH, USA).

### Resin formulation

The pentaerythritol triacrylate (PETA) and the hybrid OrmoComp monomers (OrmoComp® without photoinitiator) were purchased from Sigma-Aldrich (Germany) and micro resist technology (Germany), respectively. The photoresist BisSR consists of 29% of Bis-GMA (Esschem Europe, England) and 71% ethoxylated bisphenol A dimethacrylate (SR348C) (SAR-TOMER, France), both used as received and stirred with

a magnetic stirrer until homogeneously mixed. The resin M10 consists of 18.7% pentaerythritol tetra(3-mercaptopropionate) (PETMP), 6.4% di(but-1-yne-4-yl)carbonate (DBC) and 74.7% 1,6-bis-[2-methacryloyloxyethoxycarbonylamino]-2,4,4-trimethylhexane (UDMA) and 2% of propylgallat as stabilizer. DBC was synthesized as described elsewhere.<sup>24</sup> The schemes of the chemical structures are shown in Fig. 1b. Bis(2,4-trimethylbenzoyl)-phenylphosphineoxide (IC819) (Sigma-Aldrich, Germany) was used as photoinitiator. 2 wt% of IC819 were used for M10 and 1 wt% for BisSR, OrmoComp®, and PETA, respectively. The photo-initiator was gently mixed into the resin for 10 hours using a magnetic stirrer. All resin formulations were stored at 4 °C.

### 3D structuring

For stability testing, 3D grids with a height of 90 μm and a side length of 30 μm were manufactured. Thereby the thickness of the horizontal bars was set to 1.5 μm (by multiple scans with overlap) with a horizontal periodicity of 8 μm. To reduce optical aberrations, the structures were written in the dip-in configuration.<sup>23</sup> The intensity was set to maximize writing speed, but still lower than the damage threshold of the resins. For the structuring of PETA, OrmoComp®, and M10, an intensity (peak intensity at the focal plane) of 0.43 TW cm<sup>-2</sup> was used, while for BisSR an intensity of 0.48 TW cm<sup>-2</sup> was applied. In the case of M10, each voxel is exposed three times (triple voxel exposure). All structures were written with a speed of 15 mm s<sup>-1</sup>. For development, OrmoComp® and M10 structures were rinsed with acetone. PETA and BisSR structures were rinsed with ethanol.

The samples for AFM nanoindentation experiments were prepared as follows: OrmoComp® support-bars of 3 μm height were written in advance for all four tested resin formulations in the dip-in configuration. The spacing between the support bars is 75 μm. Thereafter, 35 OrmoComp® lines with a distance of 2 μm to the glass surface and 5 μm to each other were written in between two support-bars. The starting intensity for the first line was 0.074 TW cm<sup>-2</sup> and the incremental intensity step for each following line was 0.074 TW cm<sup>-2</sup> (writing speed 5 mm s<sup>-1</sup>). For the PETA, BisSR, and M10, the same procedure and parameters were applied. A lower writing speed of 1 mm s<sup>-1</sup> was used for M10, to achieve similar feature sizes. The PETA and BisSR resin was developed with ethanol and the OrmoComp® and M10 with acetone.

### Young's modulus characterization

The elasticity measurements were performed with an atomic force microscope (JPK Nano Wizard, Germany) using the QI™ mode. The AFM is mounted on top of an Olympus IX71 inverted optical microscope. The preparation of the sample is shown in detail in Fig. 2. Cantilever and sample were immersed in deionized water and thermally equilibrated for 1 h. The Young's modulus was measured with a qp-BioAC-CI cantilever (Nano-AndMore, Germany; tip radius = 30 nm; spring constant glass = 0.3 N m<sup>-1</sup>). Before each measurement, the exact cantilever spring constant and the sensitivity were determined on the

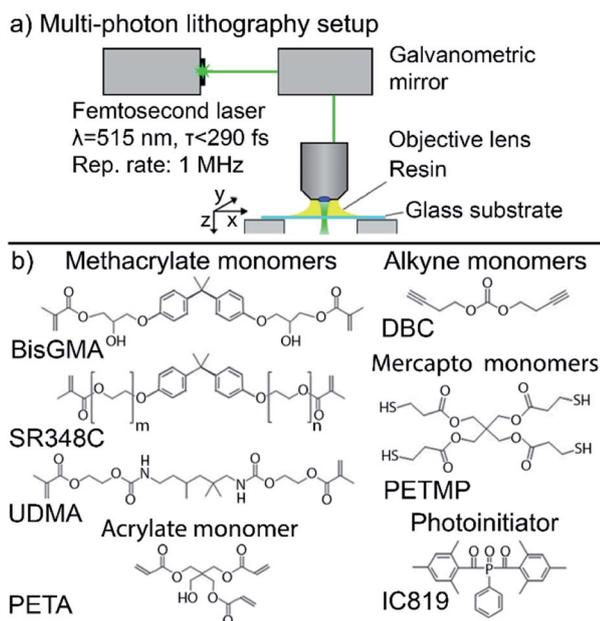
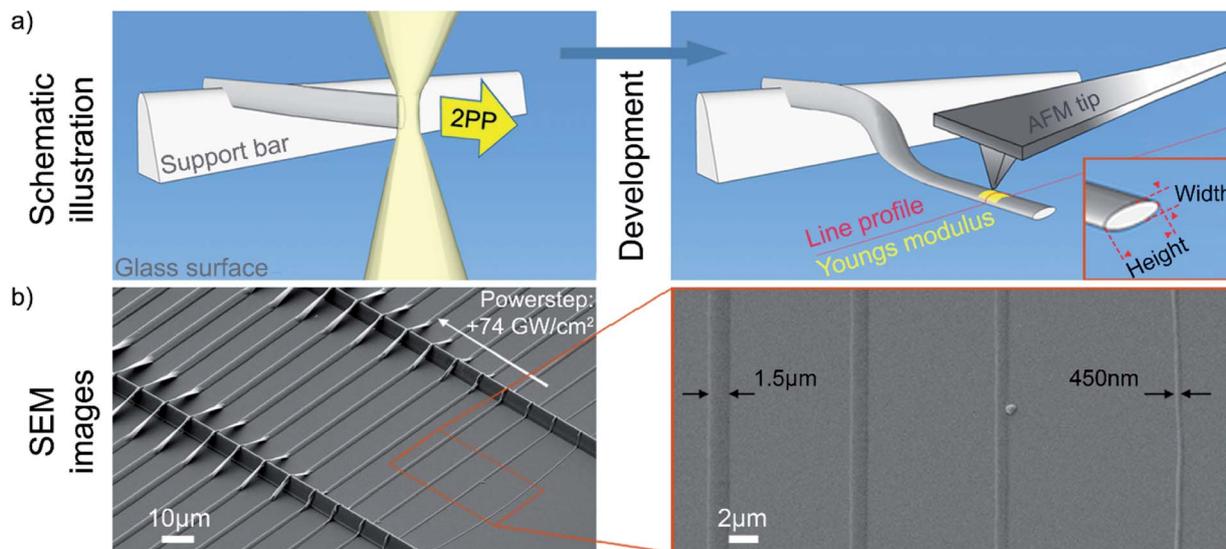


Fig. 1 (a) Schematic illustration of the MPL setup. A fs-pulsed laser beam is focused through a microscope objective lens (NA 1.25). The setup is operating in dip-in configuration. Movement of the focal spot within the photoresist is initiated by a combined galvo-mirror and a 3-axis stage. (b) Chemical structures of the monomers and the photoinitiator: methacrylate monomers SR348C, BisGMA, UDMA; acrylate monomer: PETA; mercapto monomer: PETMP; alkyne monomer: DBC; and the photoinitiator IC819.





**Fig. 2** (a) Schematic illustration of the line fabrication process. Resin is dropcasted onto a glass surface. First, support bars were written with OrmoComp® in all cases. Second, the resin was changed and hanging polymer lines were structured orthogonally to the supporting bars (yellow laser focus). Neighboring lines were written with increasing intensity in steps of  $0.074 \text{ TW cm}^{-2}$ . (a) (right) Shows a schematic drawing, which depicts a developed hanging polymer line, which is tilted by  $90^\circ$  after development. The line profile and Young's modulus are measured using AFM. (b) Scanning electron microscopy (SEM) image (sample tilt of  $45^\circ$ ), of exemplary polymer lines (OrmoComp). Here, two supporting bars (height =  $3 \mu\text{m}$ , line-to-line distance =  $75 \mu\text{m}$ ) with sample lines are shown. The right-hand side image in (b) shows four smallest lines. The smallest developed line is  $450 \text{ nm}$  high; the largest  $1.5 \mu\text{m}$ .

substrate adjacent to the polymer lines using the contact based calibration method (JPK, Germany). Force mapping was done using the JPK QI™ mode (400 points per polymer line profile, performed in the central region of the polymer line). The outline of the polymer line is excluded for a constant tip-sample contact area (see ESI, Fig. S1†). The indentation force was constant at a value of  $2 \text{ nN}$  to ensure nonlinear deformation of the polymer sample. The interaction between a rigid sphere (as an approximation for AFM tip) and an elastic surface (polymer lines) is described best by the Hertz model, thus to determine Young's modulus from the force distance curves.<sup>25</sup>  $E$  was determined by averaging over 400 data points in three technical replicas.

### Cell culture

Primary HUVEC cells were a kind gift from Prof. J. Breuss (Medical University of Vienna, Austria). The cells were cultured in M199 (Carl Roth, Karlsruhe, Germany) supplemented with 10% BCS (Sigma-Aldrich, Austria), LVES (Life Technologies, USA), GlutaMAX (100x, Life Technologies, USA) and penicillin-streptomycin ( $100 \text{ IU ml}^{-1}$  penicillin  $100 \mu\text{g ml}^{-1}$  streptomycin) at  $37^\circ\text{C}$  and 5%  $\text{CO}_2$ .

### Biocompatibility testing

The endothelial cells (primary HUVEC, passage 6) were seeded onto glass slides with 2D polymer structures (2 grids with a size of  $100 \times 100 \times 15 \mu\text{m}$ , grid constants  $25 \mu\text{m}$  and 2 grids with a size of  $90 \times 90 \times 15 \mu\text{m}$ , grid constants  $30 \mu\text{m}$ ), coated with 0.2% gelatine in phosphate-buffered saline (Carl Roth, Austria) at a density of  $10^5$  cells per  $\text{cm}^2$ . Medium exchange was performed on a daily basis. Four days post seeding, the cells were

washed with pre-warmed PBS and fixed with 4% paraformaldehyde (PFA, Sigma-Aldrich) for 15 minutes at room temperature. Subsequently, cell nuclei were stained with 4',6-diamidino-2-phenylindole (DAPI) for 30 minutes at room-temperature. Microscopic images were taken using a Zeiss Axiovert 200 (ZEN 2 blue edition) using a 10x A-PLAN (NA 0.25) and 20x LD PLAN-Neofluar (NA 0.4) objective lens. A bare glass surface in the surrounding of the grids was used as negative control. This allows taking the local cell density for each sample into account. For quantification, a cell density ratio was used, which is defined as ratio of cell density on the polymer grid ( $N = 4$ ) to cell density on a negative control. Additionally, a Caspase-Glo® 3/7 assay (Promega, WI, USA) is used for the detection of apoptosis or secondary necrosis.<sup>26</sup> By adding the kit reagent (containing DEVD substrate and luciferase) to the supernatant, the DEVD substrate is cleaved by caspases releasing the substrate aminoluciferin. Upon cleavage by luciferase phosphorescence light is detected by a photometer.

## Results

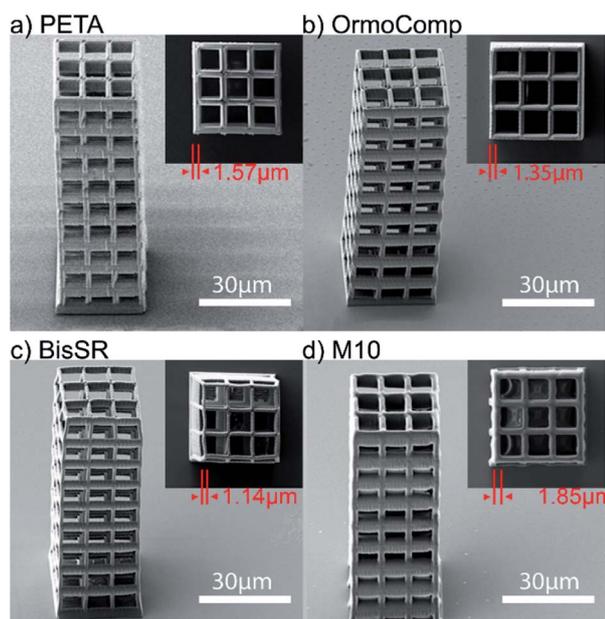
Multiphoton structuring was performed using a  $515 \text{ nm}$  femtosecond laser (see details of setup in the Material and methods section). The first resin, BisSR, consists of bisphenol-A-glycidyl dimethacrylate (Bis-GMA) and ethoxylated bisphenol A dimethacrylate (SR348C). The second resin, named M10, is a mixture of monomers carrying methacrylate-, mercapto- and alkyne reactive groups. Thereby, the added mercapto- and alkyne monomers lead to delayed gelation inducing both a higher monomer conversion and a lower shrinkage stress.<sup>27</sup>



The chemical structures of the monomers are shown in Fig. 1b. In order to be able to create large scale structures that can withstand strong mechanical forces (e.g. re-immersion into water), a high (about 1 wt%), but tolerable photoinitiator concentration was chosen.<sup>28</sup> These novel resins were compared to two established resin formulations, namely OrmoComp® and pentaerythritol triacrylate (PETA), both containing 1 wt% IC819. To compare the mechanical stability of the polymers, freestanding scaffolds with a height of 90  $\mu\text{m}$  and a side length of 30  $\mu\text{m}$  were fabricated (Fig. 3a–d).

The thickness of the horizontal bars was set to 1.5  $\mu\text{m}$  and the distance between each bar was set to 8  $\mu\text{m}$ . For the PETA and OrmoComp® structuring, an intensity of  $I_{\text{ex}} = 0.43 \text{ TW cm}^{-2}$  was used, resulting in a lateral feature size of  $l_f = 1.57 \mu\text{m}$  and  $l_f = 1.35 \mu\text{m}$ , respectively. For the BisSR structure,  $I_{\text{ex}} = 0.48 \text{ TW cm}^{-2}$  results in  $l_f = 1.14 \mu\text{m}$  and for the M10 structure  $I_{\text{ex}} = 0.43 \text{ TW cm}^{-2}$  yields  $l_f = 1.85 \mu\text{m}$ . For the structuring of M10, each voxel was triple exposed to enhance the mechanical stability, which most probably caused the deviation of the bar thickness (higher value) compared to the designed one. On the other hand, the difference in the feature size observed for BisSR (lower value) relative to the set value is most likely introduced by shrinkage during the polymer development processes. The results show that these formulations allow creating large-scale 3D structures similar to those written with the established OrmoComp® and PETA formulations.

Kunik *et al.* have shown that the writing parameters strongly depend on the surface proximity.<sup>29</sup> In particular, the polymerization



**Fig. 3** (a–d) SEM images of 3D structures fabricated using MPL. The SEM images (sample tilt of 45°), show test scaffolds with 90  $\mu\text{m}$  height and 30  $\mu\text{m}$  side length. For fabrication, an intensity of  $0.43 \text{ TW cm}^{-2}$  (speed  $15 \text{ mm s}^{-1}$ ) was used for structuring of the (a) PETA photoresist and (b) OrmoComp® photoresist, resulting in lateral feature sizes  $l_f = 1.57 \mu\text{m}$  and  $l_f = 1.35 \mu\text{m}$ , respectively. For structuring the (c) BisSR – photoresist and (d) M10 – photoresist,  $0.48 \text{ TW cm}^{-2}$  and  $0.43 \text{ kW cm}^{-2}$  were used, resulting in  $l_f = 1.14 \mu\text{m}$  and  $1.85 \mu\text{m}$ , respectively.

at a surface starts by forming polymer islands directly at the interface. Such a heterogeneous 2D polymer growth has an impact on the mechanical properties of structures. In order to exclude such impact, 3D structured hanging lines with various feature sizes were produced (Fig. 2a). In order to characterize the mechanical properties of structured polymer lines at a nanoscopic scale, an atomic force microscopy was used. However, determining the Young's modulus of the 3D hanging nanostructures is a challenging task, which would require a complicated force measurement protocol to exclude the effects of bending and deforming of hanging nanostructures under the pressure of the AFM cantilever. Therefore, we produced micro- and nano-sized lines with length of 75  $\mu\text{m}$  at 2  $\mu\text{m}$  above the glass surface (hanging 3D structure). Due to the large length and small distance to a glass substrate, the written lines were attaching to the glass surface upon development. In addition to that, lines were tipped (rotated) by 90 degrees (see Fig. 2a). Consequently, the side surface of the polymer line was lying flat on the glass surface (Fig. 2a and b). Being supported by a substrate, the standard nanoindentation protocols could be applied for the Young's modulus measurements. Overall, such production method ensures the homogeneity of written nanostructures, and simplifies the determination of their mechanical properties. The line dimensions were tuned by adjusting the writing intensity, in increments of  $0.074 \text{ TW cm}^{-2}$  from line to line. In detail, 35 polymer lines, 2  $\mu\text{m}$  above the surface and spaced 5  $\mu\text{m}$  apart of each other were written. Fig. 2b shows scanning electron microscopy (SEM) images of such lines.

For probing the Young's moduli and line profiles, qp-BioAC-CI cantilevers were used. The exact cantilever spring constant was determined according to the Material and methods section. The Hertz model was used to retrieve the Young's modulus from the measured force distance curves, obtained from three technical replicas (see Fig. 4).

Fig. 4 shows the results of the Young's modulus analysis of the 3D written structures, each consisting of one of the four polymers. The PETA resin formed the stiffest lines with an average  $E$ -modulus of  $221 \pm 40 \text{ MPa}$  and the developed lines did not significantly depend on the writing intensity. The heterogeneities of the measured  $E$ -values could be induced by a heterogeneous softer gel phase around the core of the polymer,<sup>27</sup> introduced during the development process. The smallest developed PETA-line measured  $w = 86 \text{ nm}$  in width and  $h = 684 \text{ nm}$  in height. In contrast, OrmoComp® structures are softer and show an  $E$ -modulus increase in the range of  $47 \pm 5 \text{ MPa}$  to  $102 \pm 29 \text{ MPa}$  with increase of feature size (Fig. 4b). For the smallest lines  $w = 110 \text{ nm}$  and  $h = 846 \text{ nm}$  is measured. The tendency to higher  $E$ -modulus with increasing structure size is broken by the smallest line (first point in Fig. 4b), which shows an  $E$ -modulus 15 MPa higher than the following two (larger) lines. This is probably an artefact, introduced by too high indentation depth compared to the width of the line. In such case the measured  $E$ -modulus is shifting<sup>30</sup> towards the  $E$ -modulus of the substrate ( $E_{\text{glass}} = 50 \text{ GPa}$ ).<sup>22</sup> Similar to PETA, the BisSR resin does not show a writing intensity dependent increase of the  $E$ -modulus (Fig. 4c, average  $E$ -modulus of  $103 \pm 14 \text{ MPa}$ ). The smallest lines (Fig. 4c), have  $w = 126 \text{ nm}$  and  $h = 272 \text{ nm}$  and  $E = 88 \pm 9 \text{ MPa}$ . The Young's modulus of M10



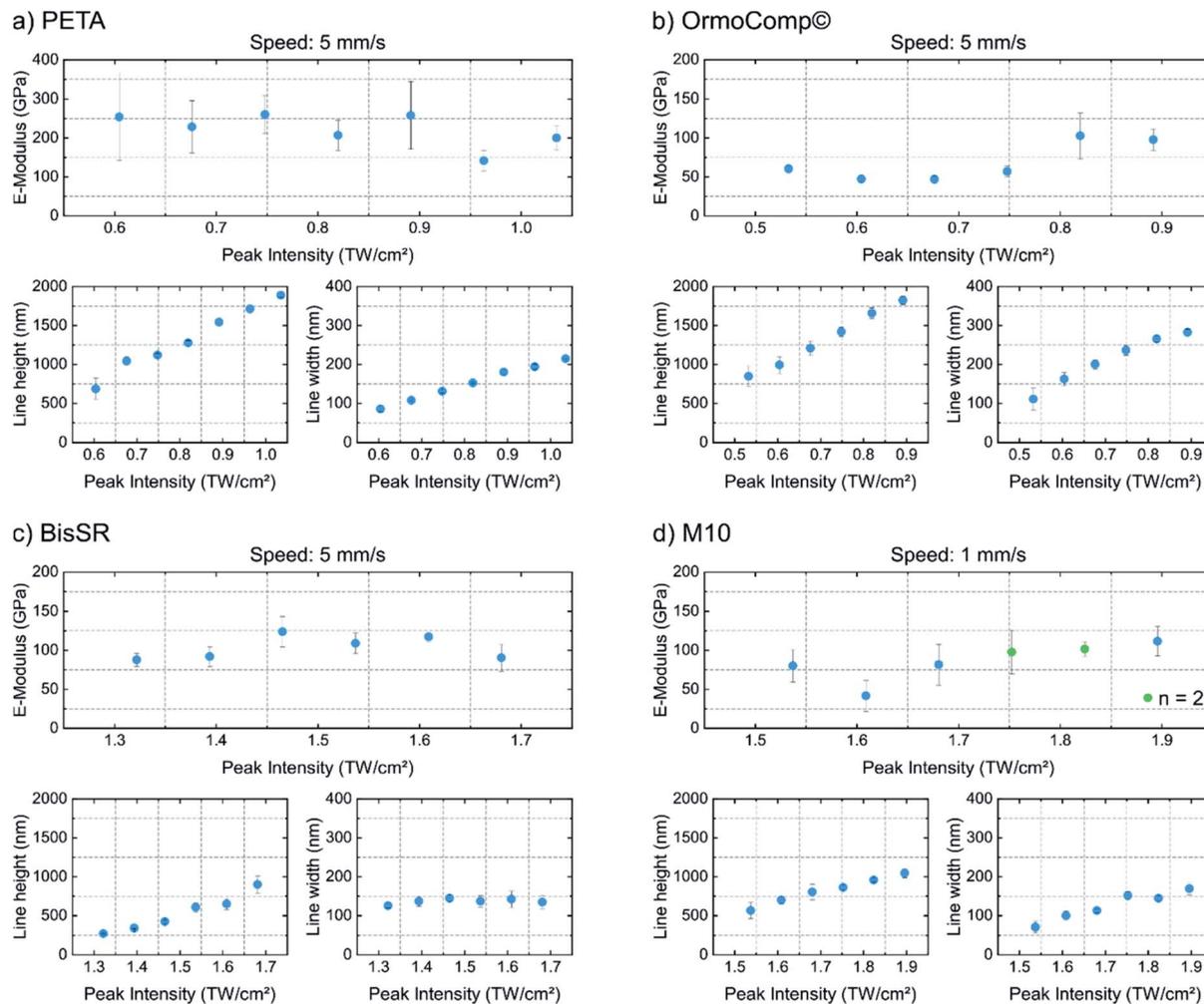


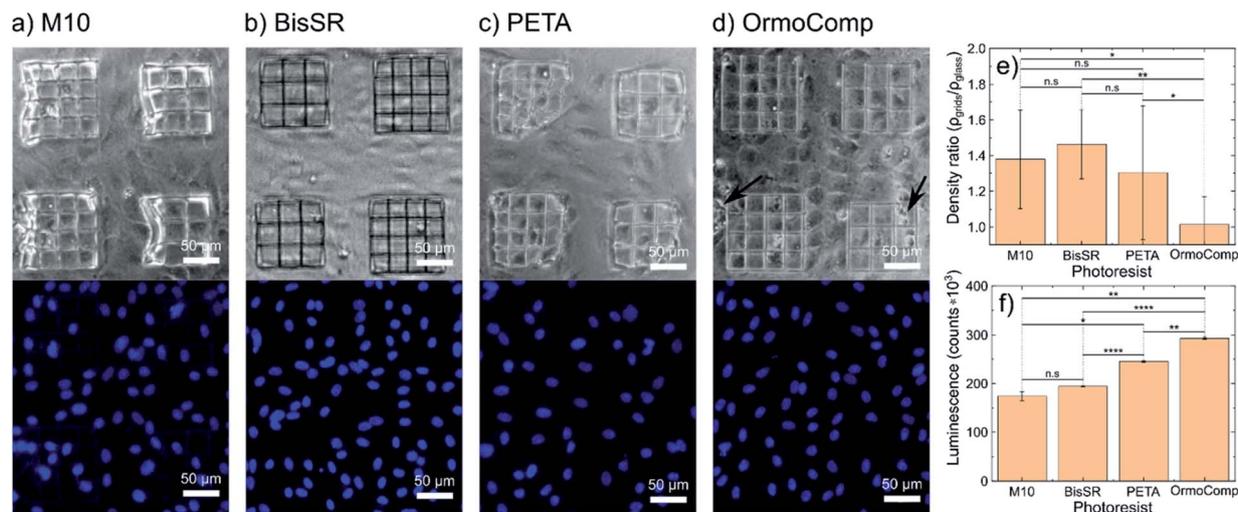
Fig. 4 Young's modulus ( $E$ -modulus) and the feature sizes. In each image: the upper diagram shows  $E$  with respect to the applied writing intensity. In the lower diagram (left), the determined polymer line height ( $h$ ) and (right) the polymer line width ( $w$ ) are shown. Materials: (a) PETA, (b) OrmoComp®, (c) BisSR, and (d) M10. Lines were written with a writing speed of  $5 \text{ mm s}^{-1}$  in case of (a–c) and with  $1 \text{ mm s}^{-1}$  in (d).

shows an intensity dependent increase from  $41 \pm 21 \text{ MPa}$  to  $120 \pm 20 \text{ MPa}$ . As already observed in OrmoComp®, the Young's modulus of the smallest polymer line is influenced by the stiffness of the glass (Fig. 4d). Here it is worth to mention, that the observed feature sizes yield a high aspect ratio, which cannot be attributed to the typical point spread function of a laser beam. Aspect ratios are found to be 8.7 (on average) for PETA lines, 6.4 for OrmoComp lines, 6.2 for M10 lines, and from 2 to 6.6 for BisSR lines. Similar results were also shown by other studies<sup>31,32</sup> and were attributed to self-focusing, self-trapping, or dispersion effects, leading to polymerization beyond the resolution limit.<sup>33</sup>

To assess the biocompatibility of the photoresists, human umbilical vein endothelial cells ( $10^5$  HUVEC per  $\text{cm}^2$ ) were seeded on 2D polymer gratings. After four days of cultivation, phase-contrast images were taken for cell morphology comparison and cells were fixed and stained with 4',6-diamidino-2-phenylindole (DAPI) and CD31-FITC for visualization of the cell nuclei distribution (Fig. 5) and junctions (Fig. S3†) of the cells on the grids, respectively. Fig. 5 shows phase-contrast and

fluorescence microscopy images of HUVECs on 2D lithography structures written with M10, BisSR, PETA, and OrmoComp® on a glass surface (see Fig. 5a–d). A plain glass substrate near to the polymeric grids was used as a negative control. For each photoresist, four scaffolds with grid constants of 25 and  $30 \mu\text{m}$  were structured. Biocompatibility was assessed by judgment of the cell density (indicating cell growth/cell division), presence of apoptotic cells, and uniform distribution of cell nuclei on the polymeric grids compared to the adjacent glass surface. Cell density ratios for all four tested polymers are presented in Fig. 5e. As can be seen, the OrmoComp® grid exhibits almost the same density of cells as a bare glass substrate. Grids made of PETA show on average 30% higher density compared to the negative control. The biocompatible resins M10 and BisSR show 38% and 46% increase of the cell density, respectively. The significance of the cell density ratio was tested by nonparametric Kruskal–Wallis multiple comparisons test. Both M10 and BisSR grids show a significant ( $p < 0.05$ ) increase in the cell density ration compared to the grids made from OrmoComp. Additionally, the biocompatibility of M10 and BisSR was confirmed by an *in vitro*





**Fig. 5** Phase-contrast (upper row) and corresponding fluorescence microscopy images of cell nuclei (stained with DAPI; lower row) of primary endothelial cells (HUVEC) on 2D grids of the polymers (a) M10, (b) BisSR, (c) PETA and (d) OrmoComp®. (e) Averaged (over four 2D grids) HUVEC density (relative to negative control) for all four photoresist used in this work. (f) Extracellular Caspase-Glo® 3/7 activity. The significance of the biocompatibility tested in a 2-way ANOVA, Tukey's multiple comparisons test (horizontal bars, each ending in the center of the two compared luminescence bars).

assay (Caspase-Glo® 3/7, Promega, WI, USA). Extracellular active effector caspases (DEVD-aminofluoromethylcoumarine cleavage activity) are detected by luminescence increase. The luminescence is proportional to the amount of the extracellular caspase-3 and caspase-7, correlating in turn to the amount of apoptotic/secondary necrotic cells. The highest biocompatibility (defined here as low amount of released caspase enzymes) is observed for the polymers M10 and BisSR ( $174\,065 \pm 9062$  and  $194\,494 \pm 1154$  counts) (Fig. 5f). No significant difference between these two samples were observed (2-way ANOVA, Tukey's multiple comparisons test). The cells cultivated on PETA grids show a significant higher amount of extracellular caspases ( $245\,403 \pm 1353$  counts;  $p < 0.0001$  compared to BisSR). Cells grown on OrmoComp exhibit the highest number of extracellular caspases ( $293\,016 \pm 2307$  counts;  $p < 0.01$  compared to PETA). Values are presented as mean  $\pm$  S.D. Results are derived from a single experiment in technical triplicates. In general, the formation of a confluent monolayer of cells on BisSR and M10 photoresists indicates a good biocompatibility. The uniform distribution of cell nuclei on the glass surface and the M10 grids indicates the material's non-toxicity. For BisSR, an enhanced affinity of the cells to the polymer lines was observed (Fig. 5b). Our biocompatibility results are encouraging and should be validated on wider level of cell types and conditions. However, such a task is beyond the scope of this manuscript but hopefully will trigger further research in this direction.

## Conclusion

In this contribution, we introduced two new biocompatible resin formulations BisSR and M10. We characterized their 3D MPL writing capability and mechanical properties. The Young's modulus of single polymeric lines was determined as a function of illumination intensity. The measured Young's modulus of

BisSR lines was around 80 MPa and independent from writing intensity. In contrast, an increase in the writing intensity for M10 lines leads to the rise of Young's modulus from 40 to 120 MPa. The M10 resin was designed to provide reduced shrinkage stress and high monomer conversion.<sup>27</sup> In comparison, 3D structures made of the BisSR experience around 9% of post-polymerization shrinkage. Furthermore, we were able to structure the polymers in a sub-micrometer range. The results indicate that, M10 lines with even sub-100 nm thickness withstand development. Analysis of human endothelial cells on structured polymeric grids indicates a better biocompatibility of the two new photoresists BisSR and M10 compared to common MPL photoresists. The biocompatibility of these materials has been exclusively shown for *in vitro* cell cultures. However, we believe that our new materials would be suitable for tissue engineering *in vivo*<sup>12</sup> and here determined mechanical parameters of new photoresists would help in the implementation of mechanical metamaterials<sup>13</sup> and reversibly deformable microstructures.<sup>14</sup>

## Author contributions

J. J. conceived the project and carried out most of the writing. The cooperation regarding the M10 formulation was initiated by T. G. and T. K. Bo. B. performed the main experimental work and analyzed the data. Y. O., D. S., Bi. B., helped with the experimental work and data analysis P. H., T. K. helped with the experimental design. A. K, S. M. helped with the experimental work. D. H., T. G. provided the M10 polymer. All authors contributed to writing and editing the manuscript.

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## Conflicts of interest

There are no conflicts to declare.

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