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## Low-temperature carbon-based electrodes in perovskite solar cells

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Carbon-based electrodes have been widely applied in perovskite solar cells (PSCs) because of their chemical inertness and compatibility with up-scalable techniques, signifying their solid potential for mass-production. The material scarcity and complexity of metal ore extraction further highlights that conventionally used noble metal electrodes cannot represent a sustainable option for back-contact in PSCs, while cells with carbon-based electrodes represent an excellent solution to these problems. However, their power conversion efficiencies (PCEs) still lag behind the traditionally processed cells with metal electrodes, resulting in a considerable efficiency gap. To overcome this issue, we propose the use of low-temperature carbon-based (LTCB) electrodes, which offer several key advantages in comparison to mesoscopic high-temperature treated ones: (1) larger choice of selective layers, (2) applicability to all perovskite crystallization methods, (3) compatibility with flexible substrates and (4) faster deposition process. In this review, we analyze numerous techniques to formulate the LTCB-paste and ways to deposit it on the cell stack which have been developed in order to improve the interfacial contact and electrode conductivity. Besides describing the current state-of-the-art perovskite solar cells with LTCB-electrodes, the most promising strategies to enhance the PCE of such photovoltaic (PV) devices are discussed. Overall, we emphasize that PSCs with a LTCB-electrode combine high device stability, low manufacturing costs and low environmental impact, while having options for pushing the efficiency of carbon-based PSCs closer to the record-breaking cells, all of which are vital in order to fulfill the true potential of perovskite PV.

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### Broader context

In order to meet the growing energy demand of the global population and prevent large amounts of green-house emissions, renewable energy sources need to be utilized to a maximum extent. Photovoltaics (PV) is one of the fastest developing renewable energy fields, yet the world electricity share of PV is still below 3%. Halide perovskite photovoltaics is an emerging technology that will decrease the levelized cost of electricity and has a strong potential to become a commercially attractive alternative to conventional silicon-based solar modules, increasing the share of PV power generation in the global energy mix. Although, perovskite photovoltaics have experienced unprecedented development in the last few years, there are stability and cost issues related to the organic hole-conductors and noble metals, used as back-electrodes. Minimization of the CO<sub>2</sub>-footprint of perovskite solar devices requires replacement of the metals with low-cost and sustainable materials, such as carbon-based layers. Most importantly, carbon-based layers provide an excellent chemical and operational stability. Two types of carbon-based electrodes have been successfully developed recently, which are processed at high- and low-temperatures. In this review, we outline the advantage of low-temperature carbon-based contacts, which are most promising to reach the highest power conversion efficiencies in long-term stable perovskite PV devices.

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## 1. Introduction

Ever since the potential of perovskite materials in solar cell applications was discovered in 2009,<sup>1</sup> the photovoltaic (PV) community is still nowadays being impressed by their exceptional light-absorbing and opto-electronic properties. One of the appealing points of this type of photovoltaic device is the versatility of the semiconductor crystal structure.<sup>2–4</sup> This phenomenal tunability of various fundamental properties fuels the intensive research activities across the globe and makes them attractive to researchers not only in the field of PV, but also in the disciplines of light-emitting-diodes (LEDs),<sup>5–8</sup> photodetectors,<sup>9–12</sup> sensors<sup>13–16</sup> and electrochemical cells.<sup>17–19</sup> In PV applications, once the device efficiencies became comparable to those of the well-established technologies such as mono- or poly-crystalline silicon, the aspect of performance

stability became the center of attention for scientists working on perovskite PV.<sup>20–24</sup>

Considering the nature of metal-halide perovskite, it has been noticed that one of its most-appealing points – low energetic barrier for crystal formation – is also one of its biggest drawbacks.<sup>25</sup> This peculiar material characteristic allows for quick liquid processing during cell production, while simultaneously possessing “soft ionic crystal” properties prone to multiple defects and degradation mechanisms due to weak metal-halide bonds.<sup>25–28</sup> Over the years, researchers have developed countless techniques to solve the instability problem of perovskite solar cells (PSCs). However, it is still a challenge to combine highly efficient light absorption and charge extraction with stable performance in one perovskite device.

Generally, most of the cells are fabricated on a transparent substrate, coated with conductive oxide (e.g. FTO, ITO) which



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functions as a front electrode. The charge selectivity in perovskite cells is obtained by placing a photoabsorber between hole and electron-selective contacts. The cell configuration, where on the transparent front contact an electron selective layer (ESL), perovskite and a hole-selective layer (HSL) are sequentially deposited, is commonly referred to as an n-i-p structure. The cell stack is completed by a counter- or back-electrode. Both electrodes allow an effective lateral charge conduction, while the charge selective layers extract photogenerated electrons and holes from the perovskite and further conduct them to the electrode. The cell structure can also be inverted, resulting in the p-i-n configuration. Some p- and n-layers can only be interchangeably employed, and the question of which device structure offers best power conversion efficiencies (PCEs) and performance stability is still under debate.

Carbon-based perovskite solar cells (C-PSCs) are a cell concept that has been introduced to sort the issues of instability, manufacturing complexity and high costs faced by record-breaking metal/HSL-based PSCs.<sup>29</sup> The hydrophobic nature of carbon promotes lower in-take of moisture into the cell, making it possible to improve the cell lifetime.<sup>30,31</sup> Additionally, carbon electrodes have proved their ability to extract photo-generated holes by themselves allowing researchers to manufacture PSCs without the need of using expensive and unstable HSLs, promoting the concept of HSL-free monolithic perovskite solar cells.<sup>32</sup> Conventional carbon-based PSCs use carbon black and graphite as counter electrodes, that require high processing temperatures to burn out the organic binder.<sup>33,34</sup> This review aims to explore the recent promising progress of low temperature carbon-based PSCs, along with their unique potential to meet the optimal point for game-changing and disruptive PV: low cost, high stability, high efficiency and sustainability (Fig. 1).

Here, we briefly highlight the main challenges of traditional perovskite PV, namely the device stability, high manufacturing

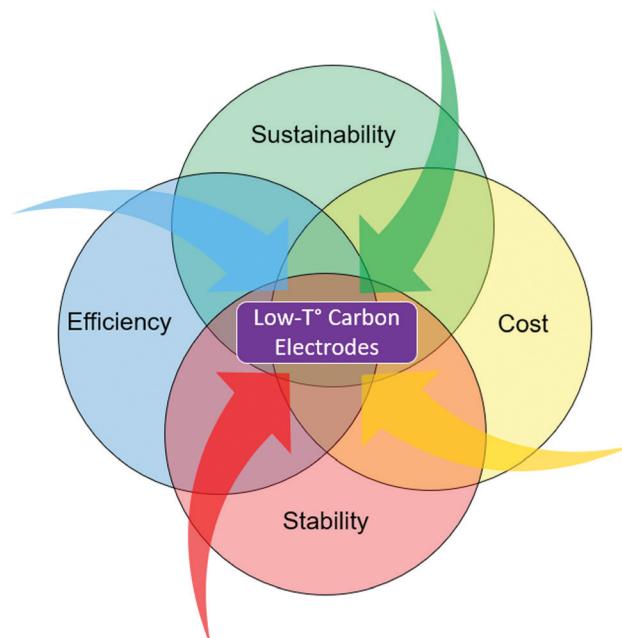


Fig. 1 Illustration of the main characteristics that are required for perovskite to become the next generation PV technology, where we identify low- $T^\circ$  carbon as the key element to reach that goal.

costs, up-scaling and environmental impact, followed by a discussion of how carbon-based cells can overcome these drawbacks. Different concepts of C-PSCs are described as well as the key advantages of low-temperature processed C-PSCs over the high-temperature processed ones. Later, we discuss the recent developments in low-temperature carbon-paste formulations and methods of depositing such a layer on a cell. Finally, we propose a number of strategies to close the efficiency gap between the traditional PSCs and low-temperature carbon-based ones.



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## 2. Motivation behind perovskite solar cells with carbon-based electrodes

### 2.1. Stability issue in perovskite solar cells

It is well-known that perovskite solar cells are more susceptible to degradation than mature PV technologies such as amorphous/crystalline Si and thin film technologies (e.g. CdTe, CIGS).<sup>35,36</sup> Many systematic investigations and review publications have shown that the degradation of perovskite is an extremely complex problem including issues related to moisture, oxygen, UV light, heat and electrical bias.<sup>37–41</sup> Moreover, this also makes the assessment of PSC stability complicated as it highly depends on the measurement conditions. To resolve this ambiguity, scientists in the perovskite community have recently proposed a number of standardized procedures for studying the stability of perovskite PV devices based on ISOS protocols.<sup>42</sup> In this review we would like to focus the reader's attention on the intrinsic stability of back contacts and organic hole-selective layers that are implemented in PSCs (Fig. 2). Therefore, the main

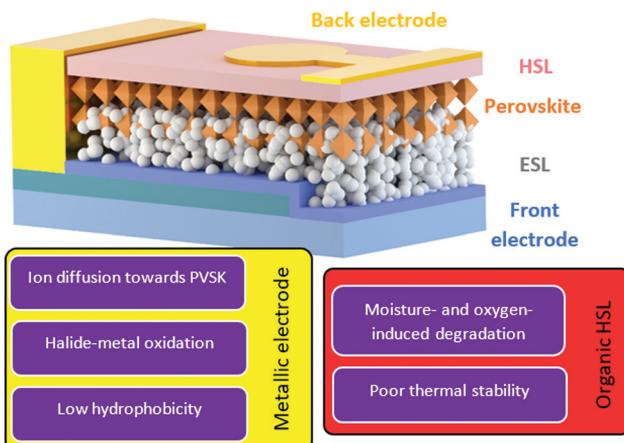


Fig. 2 Basic mesoporous n-i-p perovskite cell configuration and the main drawbacks of metallic electrodes and organic HSLs, affecting the performance stability of such cells. HSL and ESL denote hole- and electron-selective layers, respectively.

degradation mechanisms related to the ambient environment, containing oxygen and moisture, are accentuated in this chapter.

**2.1.1. Moisture-induced degradation of perovskite.** It has been found in numerous studies that perovskites with  $\text{CH}_3\text{NH}_3\text{I}$  readily decompose under humid conditions into  $\text{CH}_3\text{NH}_2$  and  $\text{HI}$  gases, resulting in the formation of  $\text{PbI}_2$  in unsealed cells.<sup>25,43–46</sup> Highly polar water molecules can directly affect the hydrogen bonds between the organic A-cation and inorganic X-anions in the  $\text{ABX}_3$  perovskite structure,<sup>47</sup> resulting in the loss of  $\text{CH}_3\text{NH}_3\text{I}$  via sublimation.<sup>43</sup> However, it has also been demonstrated that perovskite is more likely to firstly form monohydrate  $\text{CH}_3\text{NH}_3\text{PbI}_3 \cdot \text{H}_2\text{O}$  and dihydrate  $(\text{CH}_3\text{NH}_3)_4\text{PbI}_6 \cdot 2\text{H}_2\text{O}$  complexes in the presence of water, which also leads to the formation of  $\text{PbI}_2$ .<sup>25,48–50</sup> Replacing the  $\text{CH}_3\text{NH}_3$  cation with a commonly used formamidinium –  $\text{HC}(\text{NH}_2)_2$  cation does not yield an improvement in moisture stability, as the latter can also decompose into ammonia and sym-tryazine in the presence of water.<sup>51,52</sup> The *ab initio* molecular dynamics simulations show that  $\text{CsPbI}_3$  has a higher interaction with water molecules and thanks to the low lattice distortion, the moisture-induced degradation is suppressed in such a material, in comparison to that of the  $\text{CH}_3\text{NH}_3\text{PbI}_3$ .<sup>53</sup> Partial substitution of the cation with Cs was found to improve the moisture-tolerance of perovskites,<sup>30,52</sup> however at the cost of less optimal bandgap and light-absorption properties.<sup>45,54</sup> While, on the other hand, barriers at the interface with perovskite can efficiently improve the quality of the perovskite film, reduce the interface recombination, enhance the surface hydrophobicity and therefore protect the perovskite from moisture.<sup>55–61</sup> For example, additional two-dimensional (2D)  $\text{A}_2\text{PbI}_4$  perovskite layers using pentafluorophenylethylammonium (FEA) have been introduced on top of the 3D bulk perovskite film, enabling a power conversion efficiency of over 22% and superb stability of retaining 90% of the initial PCE during operation conditions for 1000 hours in humid air under one sun illumination without encapsulation.<sup>55</sup> An additional thin layer of lead oxysalt with wide-bandgap has been proved to be an excellent interlayer to passivate the

perovskite surface with reduced defect density. More importantly, this barrier layer effectively protects the underneath perovskite layer with enhanced water resistance, therefore leading to an excellent stability of the device of 96.8% from the initial PCE after operation at maximum power point under illumination for 1200 hours at 65 °C.<sup>62</sup> The introduction of an inorganic  $\text{WO}_3$  interlayer between the perovskite and HSL has been demonstrated, which helped to increase the PSC moisture stability, maintaining 60% of the initial PCE for over 160 h under humidity over 80%.<sup>61</sup>

**2.1.2. Intrinsic and moisture stability of organic HSLs.** The PSC structure which is commonly shown in the literature includes a metal-based electrode and an organic HSL such as 2,2',7,7'-tetrakis(*N,N*-di-methoxy-phenylamine)-9,9'-spirobifluorene (spiro-OMeTAD), poly(3,4-ethylene dioxythiophene):poly(4-styrenesulfonate) (PEDOT:PSS) or polytriarylamine derivatives (PTAA).<sup>47,63,64</sup> Most of them are very sensitive to the presence of water in an ambient atmosphere. In order to facilitate an efficient charge transport, spiro-OMeTAD (which has low intrinsic hole mobility) requires it to be doped with an additive such as bis(trifluoromethane)sulfonimide lithium salt (LiTFSI), which is hydrophilic and therefore serves as a source of rapid degradation in the presence of moisture.<sup>47,65,66</sup> In addition to LiTFSI, spiro-OMeTAD can be doped with *tert*-butyl pyridine (*t*BP) to increase the photovoltaic performance, but it can also degrade perovskite, as pyridine molecules can diffuse to the perovskite layer and form a  $\text{PbI}_2$ -pyridine complex.<sup>67,68</sup> Qi *et al.* have found how the often occurring pinholes (Fig. 3a) in a spiro-OMeTAD layer can facilitate the rapid ingress of moisture into the perovskite layer (Fig. 3b).<sup>69,70</sup> However, by replacing the commonly used dopant LiTFSI with  $\text{Zn}(\text{TFSI})_2$  (which was additionally doped with *t*BP) a significant improvement in both photovoltaic performance and long-term stability has been reported,<sup>71</sup> owing to one order of magnitude enhancement in the hole mobility and a facilitated oxidation process of spiro-OMeTAD by complexation between the zinc cation and *t*BP even in the absence of oxygen and light, which is completely different from the conventional mechanism of LiTFSI.<sup>72</sup> Nevertheless, the use of dopants is normally problematic due to undesired ion migration and oxidation procedure, inducing stability issues.<sup>73</sup> Therefore, dopant-free HSL becomes a more promising material for stabilizing PSCs.<sup>74–77</sup> Fabrication

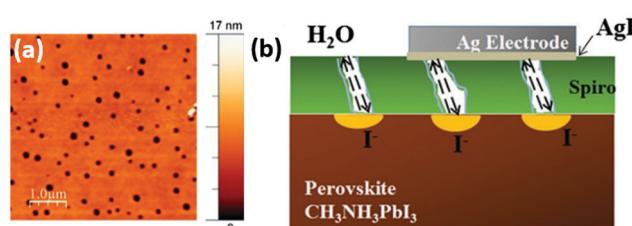


Fig. 3 (a) AFM images of the spiro-OMeTAD layer surface with multiple pinholes of 135 nm average diameter. (b) Schematic drawing of the perovskite degradation and halide diffusion in the presence of pin-holes in spiro-OMeTAD. Adapted and reproduced with permission from ref. 69 and 70.



of di(1-benzothieno)[3,2-*b*:2',3'-*d*]pyrrole (DBTP) derivatives with arylamine wings such as *m*DPA-DBTP has proven to be an effective route to synthesize dopant-free HSLs with exceptional hole-transport properties, arising from the good molecular backbone planarity, enhanced  $\pi$ - $\pi$  stacking and well-aligned valence band maximum.<sup>78</sup> The devices with *m*DPA-DBTP exhibited PCE of 18.09%, and retained 81% of its original PCE after 33 days under air-storage, whereas in comparison, the PSC devices with doped spiro-OMeTAD have completely degraded (PCE < 1%) under the same storage conditions. In addition, two copper phthalocyanine (CuPc) derivatives, CuPc-Bu (containing butyl groups) and CuPc-OBu (containing butoxy groups), have also been developed for dopant-free HSLs in PSCs, which achieved PCE of 14.3% and 17.6%, respectively.<sup>79</sup> PSCs with CuPc-OBu HSL exhibited remarkably improved ambient stability under storage in an environment with 85% relative humidity without encapsulation, owing to the high moisture resistivity of the CuPc-OBu. Moreover, a highly efficient polymeric HTM has also been demonstrated by incorporating the diethylene glycol (DEG) groups, which could be used to fabricate highly-efficient PSCs with a certified PCE of 20.10%. The champion device also presents an impressive long-term stability, by retaining 92.25% of the initial PCE after storage in ambient air for 30 days.<sup>75</sup> A popular choice of HSL in p-i-n cells, PEDOT:PSS, can react with moisture and oxygen in ambient air.<sup>45,63,64,80-82</sup> Despite the advantages offered by these HSLs, it becomes clear that these layers have to be protected by a hydrophobic layer (such as carbon-based electrode), in order to suppress water ingress into the perovskite absorber.

Some studies have attempted to develop efficient HSL-free PSCs to overcome this issue. Etgar *et al.* reported an HSL-free concept for perovskite solar cells with a  $\text{CH}_3\text{NH}_3\text{PbI}_3/\text{TiO}_2$  heterojunction cell yielding a PCE of 5.5%.<sup>83</sup> The idea consisted of having a thick perovskite layer on top of the mesoporous  $\text{TiO}_2$  acting both as a photoabsorber and selective layer.

On the other hand, inorganic HSLs such as  $\text{NiO}_x$  and CuI can offer much better chemical stability and carrier mobility than the organic ones.<sup>30,64,84</sup> You *et al.* have demonstrated how PSCs with PEDOT:PSS completely deteriorate over the course of 5 days in an ambient environment (25 °C with 30–50% humidity), while the ones with  $\text{NiO}_x$  as HSL maintained their initial PCE for almost 60 days.<sup>64</sup> Although in most cases  $\text{NiO}_x$  serves as a p-contact in p-i-n cells, there are also several reports displaying the capability of  $\text{NiO}_x$  to be integrated on top of perovskite. A low-temperature processing of  $\text{NiO}_x$  was reported by Liu *et al.*, where the metal oxide nanoparticles were capped with stearate ligand and dispersed in a non-polar solvent chlorobenzene.<sup>85</sup> However, the p-i-n devices with such  $\text{NiO}_x$  layer have shown better PCE than the n-i-p devices due to remaining ligands at the perovskite/HSL interface, hindering the hole-extraction. Cao *et al.* have demonstrated another low-temperature method to deposit  $\text{NiO}_x$  on top of perovskite, which provided higher thermal stability of the PSC, in comparison to cells with spiro-OMeTAD and copper thiocyanate (CuSCN).<sup>86</sup> Thermally-induced degradation in the samples with spiro-OMeTAD was attributed to the formation of morphological defects at the perovskite/HSL interface, whereas the reaction between perovskite and CuSCN at increased

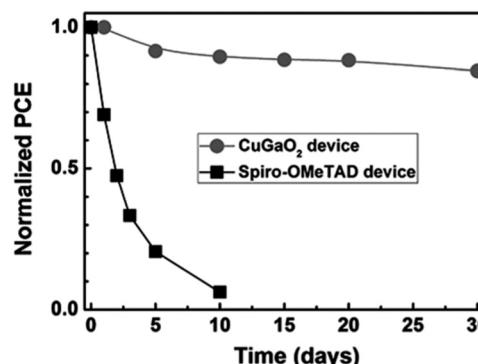


Fig. 4 Normalized PCE of PSCs with  $\text{CuGaO}_2$  and spiro-OMeTAD as HSLs measured under an ambient environment (RH = 30–55%, T = 25 °C). Adapted and reproduced with permissions from ref. 87.

temperatures was found to jeopardize the cell stability. Zhang *et al.* have proposed the use of  $\text{CuGaO}_2$  as an efficient and stable HSL, which can be deposited on top of perovskite, resulting in a better device PCE and stability than that of devices with spiro-OMeTAD (Fig. 4).<sup>87</sup> The suppressed interfacial recombination and lower dark saturation current ( $J_0$ ) were determined to be the origins of the PCE improvement, whereas the stability enhancement was attributed to less hydrophilic properties of the  $\text{CuGaO}_2$ .

The reported findings in the literature show that, as anticipated, some inorganic HSLs exhibit higher stability than the organic ones, because of their lower affinity for water and higher structural robustness in an ambient environment.<sup>45</sup> Moreover, inorganic materials typically exhibit higher thermal stability<sup>30</sup> as well as the ability to retard sublimation of volatile perovskite components (e.g. HI and  $\text{CH}_3\text{NH}_2$ ) and layer decomposition.<sup>88</sup> This is an important note, as in n-i-p cells the HSLs should protect the moisture- and oxygen-sensitive perovskite photoabsorber and not accelerate its deterioration.

**2.1.3. Intrinsic and moisture stability of metal-based electrodes.** Metal-based layers such as gold (Au), silver (Ag) and copper (Cu) are generally favored as a back-electrode in perovskite solar cells, due to their high conductivity. Unfortunately, they are often a source of degradation phenomena in PSCs, decreasing the cell stability. It was found that ions from a Au layer can diffuse through the HSL producing shunts and deep trap states (Fig. 5).<sup>89,90</sup> This ion diffusion can be alleviated to a limited extent by inclusion of a chromium (Cr) or  $\text{Cr}_2\text{O}_3$  buffer layer between the HSL and Au contact.<sup>89,91</sup> In addition to ion migration, Au electrodes show capability of moisture trapping and hinder the release of  $\text{H}_2\text{O}$  molecules from perovskite.<sup>46,92</sup>

Multiple studies have shown that PSCs with silver contact degrade due to the tendency of  $\text{Ag}^+$  ions to diffuse towards perovskite and due to the formation of silver halides, arising from an oxidation reaction with migrated  $\text{I}^-$  ions or with volatile perovskite degradation products (e.g. HI) as depicted in Fig. 6.<sup>90,93-96</sup> The Cu electrode can be easily oxidized in the presence of air and moisture, leading to increased series resistance losses in PSCs.<sup>30</sup> Also, its oxidation products can

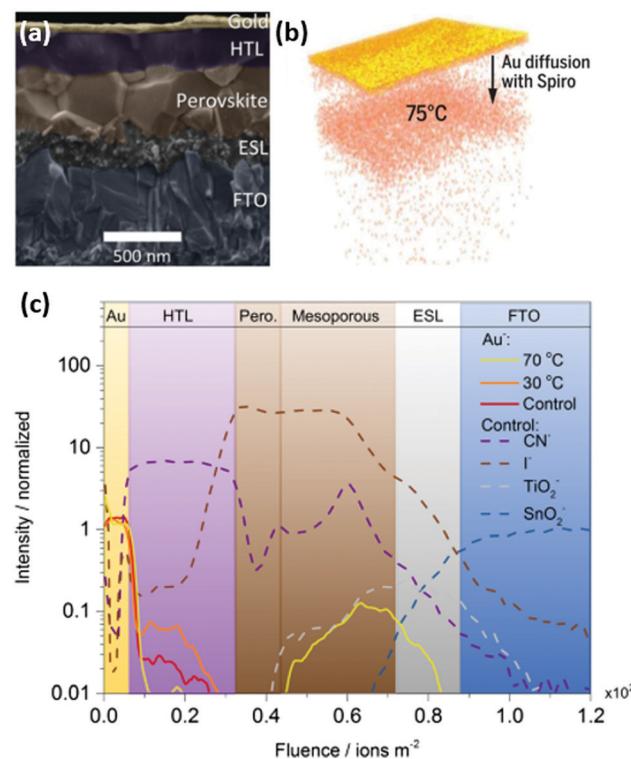


Fig. 5 (a) Solar cell stack with *m*-TiO<sub>2</sub> (ESL), perovskite, spiro-OMeTAD (HTL) and gold cathode. (b) Reconstructed 3D map of gold diffusion towards the perovskite, accelerated by higher temperatures. (c) Time-of-flight SIMS profile of the aged cell-stack. Adapted and reproduced with permission from ref. 22 and 89.

react with perovskite decomposition products such as HI, which further deteriorates the perovskite.<sup>97</sup> Notably, over the last few years, more materials such as reduced graphene oxide,<sup>98</sup> bismuth<sup>99</sup> and transparent conductive oxides<sup>95</sup> have been implemented as barrier layers to reduce the metal-electrode induced degradation. Nevertheless, the fundamental mechanisms inducing water- and metal-induced degradation remain and even in the presence of interfacial modifications, there remains a risk that future barrier development will not enable long term stabilities in the order of decades, as currently warranted for silicon PV modules. This suggests that, regarding the current research status, metal-electrode based PSCs might not be able to achieve long-term device stabilities.<sup>100</sup> Indeed, to the best of our knowledge, today the longest demonstrated operational stability of metal-based PSCs is 5000 h (illuminated with intensity of 13 mW cm<sup>-2</sup>, which is almost 1/8 of the Sun irradiation intensity, under relative humidity of 70%), which is still too low for passing international PV standards of long-term stability.<sup>24,47,101</sup>

**2.1.4. Encapsulation of PSCs.** Considering that often PSC stability measurements are carried out in an inert atmosphere to avoid degradation from moisture and air,<sup>102</sup> the ability to reach the IEC61215:2016 standard is still not on the horizon for unencapsulated cells with metal-based electrodes. This fundamental obstacle of long-term stability must be addressed and changing the electrode material is one way to bring the perovskite PV closer towards its commercialization. Moreover,

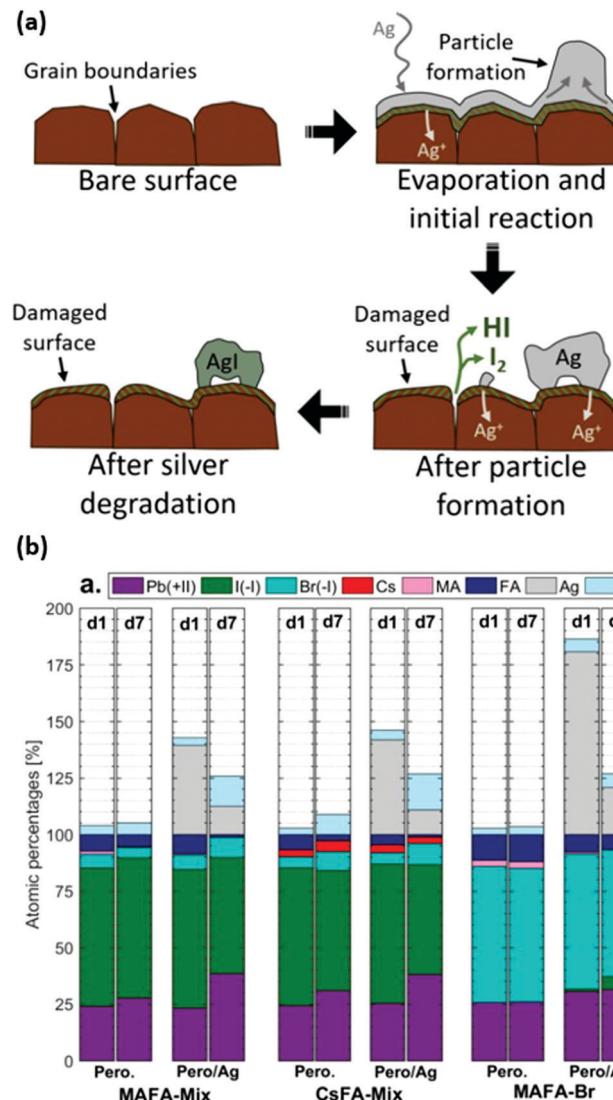


Fig. 6 (a) Model of the silver degradation in the presence of mobile volatile species (e.g. HI, I<sub>2</sub>) and I<sup>-</sup> and Ag<sup>+</sup> ions in perovskite. (b) The relative elemental percentage of each species at the surface, determined from core level XPS analysis of the pure perovskite (noted as Pero.) and when the Ag is deposited on top (Pero/Ag) for different perovskite cation compositions on day 1 (d1) and day 7 (d7). Adapted and reproduced with permission from ref. 93.

the stability tests should be carried out under similar, standardized conditions in order to unify the stability assessment between various reports and develop a deeper understanding of the degradation pathways in photovoltaic devices.<sup>42</sup>

It needs to be mentioned that despite strong stability disadvantages of organic HSLs and metallic contacts, there has been tremendous progress in developing encapsulation techniques to bring the decomposition reactions to equilibrium and prevent the PCE deterioration of such devices. Glass-glass encapsulation as well as the use of edge-seal technology have been proposed, although low perovskite decomposition temperature presents a challenge for selecting a benign sealant. The authors demonstrated how such encapsulation provides a

sufficient protection against the ambient environment and improves cell stability, namely, the fabricated encapsulated PSCs could withstand damp heat, dry heat and thermal cycling tests.<sup>103</sup> Recently Shi *et al.* reported how encapsulation with polyisobutylene provided an effective moisture barrier, surpassing over 1800 h of damp-heat test and over 70 humidity-freeze test cycles, meeting the requirements set by the IEC61215:2016 standard.<sup>104</sup>

Although, undoubtedly, encapsulation helps to reduce the moisture ingress into the photovoltaic device, the stability of the photoabsorber, selective layers and cathode materials still needs to be considered and effective strategies to passivate perovskite and mitigate decomposition reactions need to be developed besides encapsulation. For example, Liu *et al.* have demonstrated implementation of interfacial engineering in perovskite solar modules, which provided a moderate operational stability. Although the encapsulated device retained 86% of the initial PCE after 2000 h of operation under AM1.5G illumination,<sup>105</sup> the authors noted that the modules without encapsulation had a similar operational stability, highlighting that encapsulation can only partially prevent the deterioration of the perovskite photovoltaic device and the main stability improvements should be achieved *via* PSC architecture modification, for example by replacing metallic electrodes with the carbon-based ones.

**2.1.5. Stability improvements using hydrophobic carbon-based electrodes.** At the moment, a carbon-based hydrophobic electrode is the only counter electrode material that does not have any intrinsic and moisture-induced degradation. It is chemically stable with halides,<sup>30,93</sup> shows highly hydrophobic properties<sup>31,34,106–108</sup> and exhibits a very high thermal stability,<sup>109–111</sup> which provides strong protection from the environment to the sensitive layers underneath.

Deposition of the carbon-based contact on top of the monolithic cell stack is one of the most promising routes to prolong the lifetime of a perovskite PV device. In this case, carbon-based electrodes are typically  $>5$   $\mu\text{m}$  thick, meaning that the over-excess of perovskite can be applied in its porous structure, which makes it more tolerant against the decomposition in the photo-absorber. In 2014, Mei *et al.* employed a mixed-dimensional perovskite of  $(5\text{-AVA})_x(\text{MA})_{1-x}\text{PbI}_3$  into mesoscopic carbon-based HSL-free perovskite solar cells, resulting in a stable certified PCE of 12.8% ( $>1000$  h) under ambient air and full sunlight without encapsulation.<sup>32</sup> Notably, Grancini *et al.*, in collaboration with the company Solaronix, reported an outstanding 10 000 h stability (Fig. 7a) with the same device structure, whereas the PCE of the n-i-p cell (with the same photoabsorber layer) with the spiro-OMeTAD layer and Au electrode, decreased by almost 40% relatively to the initial value after only 300 h of continuous 1 Sun illumination.<sup>112</sup> Zhou *et al.* have shown how a low-temperature processed carbon layer is able to repel water better than Au and Ag metal electrodes, resulting in a better overall performance stability without encapsulation.<sup>107</sup> Ye *et al.* have shown how a planar cell with Zn-doped  $\text{SnO}_2$  as ESL, CuPc as HSL and a carbon electrode gave a stable PCE close to 18% for 1200 h without

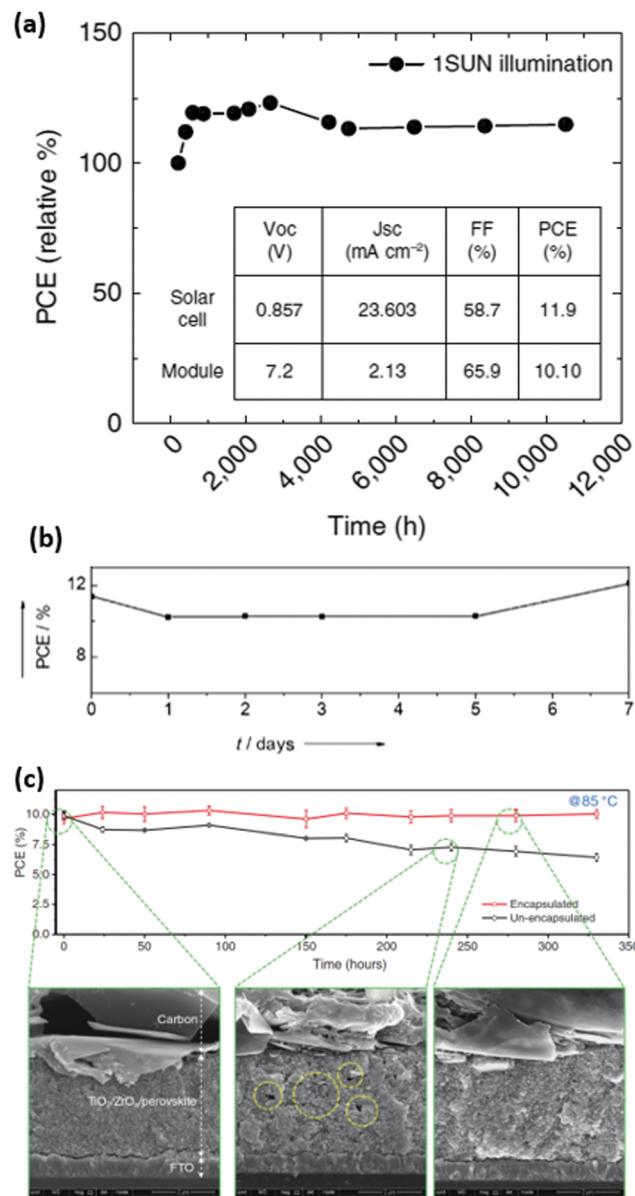


Fig. 7 (a) Long-term stability measurement of carbon-based perovskite solar cells and  $10 \times 10 \text{ cm}^2$  modules with IV-parameters shown in the inset. (b) Outdoor stability tests of a HSL-free C-PSC in Jeddah, Saudi Arabia. (c) Thermal stability measurement of encapsulated and non-encapsulated  $10 \times 10 \text{ cm}^2$  modules with SEM images right after the encapsulation and after thermal stress. Adapted and reproduced with permission from ref. 112, 109 and 118.

encapsulation.<sup>113</sup> Zhang *et al.* have demonstrated a cell with 19.2% PCE with 1000 h stability, where a carbon-based electrode was deposited on top of the HSL by press-transferring a self-adhesive carbon film.<sup>114</sup>

In addition, Li *et al.* have conducted for the first-time extensive stability tests under outdoor conditions with increased temperatures (Fig. 7b) and long-term light soaking as well as thermal stress at 80–85 °C during 3 months on the carbon-based HSL-free perovskite solar cells.<sup>109</sup> Remarkably, the device performance does not present significant degradation under those

stability test conditions, providing a promising pathway towards stable perovskite solar cells with carbon contact. Emami *et al.* have implemented a laser-sealed glass-frit encapsulation on the C-PSCs which allowed for the cells to withstand damp-heat and thermal cycling tests (although they were carried out for less than 1000 h).<sup>115</sup> Wu *et al.* have also conducted damp-heat tests on the non-encapsulated C-PSCs, where the authors observed that such cells are able to retain 77% of the initial PCE after such an intensive test.<sup>116</sup> Furthermore, due to the ease of carbon-based electrode deposition, large sized modules of 70 cm<sup>2</sup> have been fabricated, showing an extraordinary stable performance of perovskite modules even in humid environments.<sup>117</sup> More recently, by encapsulating carbon-based HSL-free printable PSC submodules (substrate area 100 cm<sup>2</sup>) with polyurethane (PU) at a mild temperature of 80 °C, the thermal stability of the cell was dramatically enhanced.<sup>118</sup> The submodules can still maintain over 97% of the initial PCE after over 2000 h under outdoor conditions (Fig. 7c), which provides potential for commercial viability of the carbon-based perovskite solar cells with excellent stability under suitable encapsulation. As clearly shown in these reports, in comparison to devices with metallic electrodes, carbon-based cells show very stable operation, providing strong arguments for it to be used as a stable back contact in perovskite solar cells and modules.

We have mentioned some of the reported stability tests in the literature on C-PSCs and conventional PSCs in Table 1 for comparison. From these results, it can be observed that most of the reported C-PSCs remain stable under an ambient environment without encapsulation for over 1000 h, whereas the conventional devices with metallic electrodes remain stable in most cases only when they are encapsulated or measured under an inert gas atmosphere. However, to the best of our knowledge, so far there has been no systematic study performed comparing the cell stack with a carbon-based back-contact *versus* a metallic one in terms of stability (thermal, humidity, oxygen *etc.*) under the exact same conditions. We would like to invite researchers in the perovskite community to address this issue and quantitatively compare the precise effect of applying a carbon-based electrode instead of metallic ones on the stability of PSCs.

## 2.2. Low-cost

Perovskite PV has a chance to be a disruptive technology, promising low fabrication costs and therefore final product price. However, several studies have revealed that material and processing costs of metal electrodes like gold and HSLs (*e.g.* spiro-OMeTAD and P3HT) as currently employed in many laboratory-scale devices together with the TCO account for the highest costs in the total module price. To decrease the cost further, this mandates to either reduce the usage of these materials or to replace them with cheaper alternatives.

According to a report by Chang *et al.*, in devices with evaporated Au-electrodes, more than 90% of the total device costs are attributed to material costs, 76.6% of which come from gold, contributing to 74.7% of the total fabrication costs (including materials, evaporation process *etc.*).<sup>119</sup> The authors

estimated the cost of a module of FTO/c-TiO<sub>2</sub>/m-TiO<sub>2</sub>/Perovskite/P3HT/Au to be around 330 \$US m<sup>-2</sup>, which was significantly more expensive than the CdTe (86 \$ m<sup>-2</sup>) and c-Si (136 \$ m<sup>-2</sup>) modules at that time (in 2017). In addition, the study suggested that replacing Au with Ag would decrease the price to a comparable value of 102 \$ m<sup>-2</sup> or it can even be reduced to 90 \$ m<sup>-2</sup> if one avoids using a sacrificial metal mask during spray deposition of c-TiO<sub>2</sub> and uses laser patterning instead.

The cost of roll-to-roll manufactured flexible perovskite PV devices has also been investigated by Chang *et al.* in a later report. They found that using screen-printing for back contact metallization strongly reduces the capital costs of the final module, in comparison to metal evaporation deposition.<sup>120</sup> Considering that with higher web-speeds the manufacturing costs decrease, the material costs become more and more dominant in the total module fabrication costs. Therefore, cheaper HSLs and back-contacts such as carbon-graphite are vital for the further reduction of the module price in industrially relevant high/throughput fabrication methods.

Song *et al.* have investigated the material and manufacturing costs of industrially fabricated modules with inorganic selective layers and Al back electrode in a p-i-n configuration.<sup>121</sup> Notably, the authors found that depositing such inexpensive materials by industry-scale deposition techniques (screen-printing and sputtering) leads to very low material costs of the functional layers of a PV device (ESL, perovskite, HSL), accounting for only 1.1% of the total material cost of a module. Interestingly, when the employed functional layers are so low-priced, 93.5% of the total material costs come from the balance of the system/module, which includes glass substrates, interconnection busbars, sealant, lamination film, edge-sealing frame, a junction-box and wiring. These results show that using up-scalable deposition techniques for fabricating back-electrodes results in reasonable module prices (unlike evaporation of noble metals), which serves as a further motivation towards printable PSCs with carbon-based contacts, due to higher long-term stability than the metal-based ones.

All of the studies mentioned above have been conducted *via* a bottom-up cost calculation approach, which considers the cost and its uncertainty at each manufacturing step.<sup>120</sup> In summary, we postulate that in order to reach perovskite module prices lower than that of c-Si or thin-film technologies, one needs to implement low-cost materials, which can be easily applied on an industrial scale. An example of such module cost reduction may be replacement of the metal electrode with a carbon-based contact in a perovskite PV device stack.

## 2.3. Up-scaling

An increasing number of companies, such as Microquanta Semiconductor, Saule Technologies and Toshiba, have recently started to develop large-scale single-junction perovskite PV modules.<sup>122</sup> However, for the large-scale applications it is still challenging to accurately control layer deposition to form homogeneous pin-hole-free films.<sup>20</sup> Most of the record-breaking perovskite solar cells or modules utilize a metal evaporation step in the device fabrication process, which requires high vacuum



Table 1 Reported stability tests on PSCs with metallic, HTCB- and LTCB-electrodes

	Device structure (perovskite)	Champion cell PCE (%)	Ageing conditions	Relative PCE retained after ageing (%)	Duration	Ref.
PSCs with metallic electrodes	ITO/NiO <sub>x</sub> /PVSK/LiF/C <sub>60</sub> /SnO <sub>2</sub> /Ag (FA <sub>0.83</sub> CS <sub>0.17</sub> PbI <sub>2.4</sub> Br <sub>0.51</sub> )	~14	Encapsulated, damp-heat test (85 °C, RH = 85%)	~99	1000 h	103
		~14	Encapsulated, dry-heat test (85 °C, RH = 25%)	~97	1000 h	
		~14	Encapsulated, thermal cycles (−40 to 85 °C)	~103	200 cycles	
		~11	Non-encapsulated, N <sub>2</sub> atmosphere, 85 °C	~80	1000 h	
		~12	Encapsulated, N <sub>2</sub> atmosphere, 85 °C	97	1000 h	
		14.6	Laminated, 25 °C, continuous MPP-tracking	~100	93 h	172
	ITO/SnO <sub>2</sub> /PVSK/PTAA/NiO <sub>x</sub> /Au/PEN (CS <sub>0.1</sub> MA <sub>0.83</sub> Br <sub>0.83</sub> Br <sub>0.17</sub> )	19	Non-encapsulated, RH = 40–50%, 60–65 °C	86	100 h	
	ITO/NiO <sub>x</sub> /PVSK/PCBM/BCP/Cr/Cr <sub>2</sub> O <sub>3</sub> /Au (FA <sub>0.83</sub> MA <sub>0.17</sub> Br <sub>0.95</sub> CS <sub>0.05</sub> PbI <sub>2.0</sub> ) <sub>3</sub> with BMIMBF <sub>4</sub> <sup>−</sup>	18.45	Encapsulated, 70–75 °C	95	1885 h	
	ITO/NiO <sub>x</sub> /PVSK/PCBM/BCP/Al <sub>2</sub> O <sub>3</sub> (CS <sub>0.05</sub> MA <sub>0.95</sub> PbI <sub>3</sub> )		Non-encapsulated, 1 sun illumination with UV filter, 85 °C	86.7	500 h	88
	<i>m</i> -TiO <sub>2</sub> /PVSK/CuSCN/rGO/Au [(FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> CS <sub>0.05</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	20	1 sun illumination with UV filter, N <sub>2</sub> atmosphere, 60 °C	95	1000 h	98
	<i>m</i> -TiO <sub>2</sub> /PVSK/spiro-OMeTAD/Au [(5AVA) <sub>1-x</sub> MA <sub>x</sub> PbI <sub>3</sub> )	14.6	1 sun illumination, under Ar atmosphere	60	300 h	112
	<i>m</i> -TiO <sub>2</sub> /ZrO <sub>2</sub> /C [(5AVA) <sub>1-x</sub> MA <sub>x</sub> PbI <sub>3</sub> )	11.4	Encapsulated, at 80–85 °C, dark	92.5	3 months	109
			Encapsulated, outdoor illumination, non-continuous measurement	~105.2	7 days	
		12.7	Encapsulated, Indoor, 1 sun illumination with UV filter	~115	10 000 h	112
			Non-encapsulated, indoor, 1 sun illumination Indoor, 1 sun illumination	>95	2000 h	117
		10.74	Non-encapsulated, indoor, 1 sun illumination	>100	1008 h	32
		12.8	Non-encapsulated, dark	>93	1000 h	136
		14.9	Non-encapsulated, dark at 60 °C	79.7	1000 h	
			Non-encapsulated, RH = 55–75%, dark	~100	3500 h	173
		15.9	Encapsulated, at 85 °C, dark	91	1000 h	137
		17.02	Encapsulated, damp-heat test (85 °C, RH = 85%)	100.9	50 h	115
		~11	Encapsulated, thermal cycles (−40 to 85 °C)	97.0	70 cycles	
		~11	Encapsulated, RH = 80%, dark	~110	500 h	
			Non-encapsulated, dark	91.5	600 h	142
		18.1	Non-encapsulated, RH = 50%, dark	97	1680 h	146
			Encapsulated, 1 sun illumination without UV and IR, indoor	89	600 h	
			Non-encapsulated, RH = 30–40%, dark	97	1200 h	157
			Non-encapsulated, RH = 30%, dark	95	1000 h	114
			Non-encapsulated, RH = 20%, dark	100	1200 h	113
			Non-encapsulated, outdoor illumination	82.6	30 days	140
		15.5	Non-encapsulated, dark	>90	1500 h	174
		18.56	Non-encapsulation, damp-heat test (85 °C, RH = 85%)	77	192 h	116
			Non-encapsulation, damp-heat test (85 °C, RH = 85%)			
PSCs with LTCB-electrodes	<i>m</i> -TiO <sub>2</sub> /PVSK/CuPe/C (MAPbI <sub>3</sub> )	16.1				
	SnO <sub>2</sub> @TiO <sub>2</sub> /PVSK/P3HT-graphene/C (FA <sub>0.3</sub> MA <sub>0.7</sub> PbI <sub>3</sub> )	18.1				
	Ni:TiO <sub>2</sub> /PVSK/CuPe/C (CS <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	17.46				
	<i>m</i> -TiO <sub>2</sub> /PVSK/spiro-OMeTAD/C (FA <sub>1-x</sub> MA <sub>x</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	19.2				
	Zn:SnO <sub>2</sub> /PVSK/CuPe/C (CS <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	17.8				
	<i>m</i> -TiO <sub>2</sub> /PVSK/TPDI/C (MAPbI <sub>3</sub> )	15.5				
	SnO <sub>2</sub> /PVSK/spiro-OMeTAD/C/graphite paper (CS <sub>0.05</sub> (FA <sub>0.83</sub> MA <sub>0.15</sub> ) <sub>0.95</sub> PbI <sub>2.55</sub> Br <sub>0.45</sub> )	18.56				
	FTO/ <i>m</i> -TiO <sub>2</sub> /PVSK/PEO/C (FA <sub>0.8</sub> CS <sub>0.2</sub> PbI <sub>2.64</sub> Br <sub>0.36</sub> )	14.9				

conditions, making it difficult and costly to upscale, in addition to the high CO<sub>2</sub> footprint of such modules. Carbon pastes can be solution-processed with a variety of fast, large area-compatible, and low-cost deposition techniques. Moreover, low-temperature pastes (which will be discussed in Section 3) can be processed on top of the perovskite photovoltaic stack, which makes these materials one of the most up-scalable back contact electrode options for perovskite technology.

Over the last few years multiple large-area perovskite PV modules utilizing carbon electrodes were reported. In 2016, Priyadarshi *et al.* reported carbon-based PV modules yielding 10.74% PCE (70 cm<sup>2</sup> active area) and good ambient stability (less than 5% drop over more than 2000 h).<sup>117</sup> Subsequently, Grancini *et al.* demonstrated 11.2% PCE for the perovskite module of the same architecture (47.6 cm<sup>2</sup> active area out of 100 cm<sup>2</sup> module area).<sup>112</sup> Already in 2016, the swiss-based company Solaronix demonstrated an HSL-free 500 cm<sup>2</sup> carbon-based perovskite module with a PCE of 12%, produced by a drop-casting method.<sup>122</sup> Recently, Xu *et al.* reported modules with an area of 60.08 cm<sup>2</sup>, having PCE of 12.87%, infiltrated with perovskite solution using slot-die coating.<sup>123</sup> The group of Hongwei Han from Huazhong University of Science and Technology showed large-area perovskite solar panels of 7 m<sup>2</sup>, which were fully fabricated with printing techniques.<sup>118</sup> Weihua Solar, a Chinese perovskite PV manufacturer, demonstrated a power station made out of 32 carbon-based, perovskite panels of 45 × 65 cm<sup>2</sup> area.<sup>124</sup> Cai *et al.* printed carbon back contact on top of a perovskite layer, delivering 10.6% PCE for the HSL-free architecture (FTO/ZnO/MAPbI<sub>3</sub> perovskite/Carbon), with an active area of 17.6 cm<sup>2</sup> (module area: 5 × 5 cm<sup>2</sup>).<sup>124</sup>

These examples highlight significant progress in the scalable manufacturing of carbon-based perovskite PV modules, and big potential for large-scale industrial deployment.

#### 2.4. Sustainability: CO<sub>2</sub>-footprint and resource consumption

The motivation behind the development of every renewable energy generation has been mainly attributed to decreasing green-house-gas emissions (e.g. CO<sub>2</sub>, CH<sub>4</sub>) and preventing the depletion of fossil energy sources. Therefore, even though the CO<sub>2</sub>-footprint of the photovoltaics is much lower than that of fossil fuel energy generation, based on global PV installation projections until 2050, the total CO<sub>2</sub>-emissions from Si PV manufacturing could have a substantial share on global greenhouse gas emissions.<sup>125</sup> Such projection displays how crucial it is to continuously develop the PV sector, aiming at technologies with lower CO<sub>2</sub> footprint.

Soon after perovskite PV emerged as a booming research field, there have been several extensive life-cycle assessments of perovskite solar cells.<sup>126–128</sup> The authors found that among the manufacturing processes of each cell layer, the primary energy consumption of cathode evaporation is the highest and Au has the highest embedded energy – the energy required to extract this material from the ore. More importantly, the gold cathode has the highest impact on the environmental profile of the cell (Fig. 8) and its replacement would greatly reduce the environmental harm during the PSC manufacturing process. Notably, a recent study conducted by our group revealed that the CO<sub>2</sub> footprint of some high-temperature carbon-based perovskite modules can be as low as 4.7% of that of c-Si PV modules.<sup>125</sup> In addition to the scarcity of noble metals, it is strongly suggested that, to minimize the environmental impact of perovskite PV,

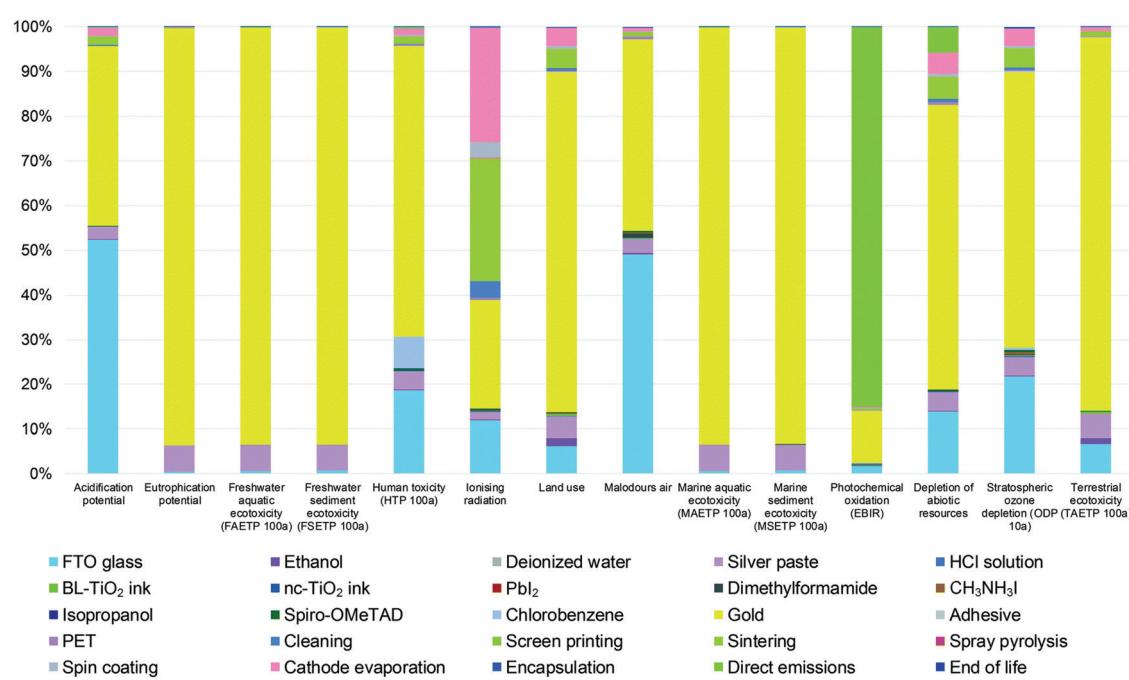


Fig. 8 Environmental profile of 1 m<sup>2</sup> FTO/c-TiO<sub>2</sub>/m-TiO<sub>2</sub>/MAPbI<sub>3</sub>/spiro-OMeTAD/Au perovskite PV device. Adapted and reproduced with permission from ref. 126.



another type of cathode material that can be deposited with less energy consumption needs to be developed, such as carbon-based electrodes.

For a truly sustainable global society, a circular economy needs to be implemented where resources are not lost, but recycled or based on renewable sources. Metals are a group of materials well-suited for recycling. However, their recycling efficiencies are governed by the second law of thermodynamics,<sup>129,130</sup> where the created entropy across the chains of circular economy dictates the inevitable energy losses. Especially for highly technological electronic devices, this implies that fine distributions of different materials such as a hundred nanometer thin metal back electrode of a perovskite solar module inevitably leads to dissipation and thus loss of at least a part of these metals from the circular economy. Graphite, although today mainly extracted from fossil resources, can already be produced from renewable, plant-based resources such as coconut shells<sup>131</sup> and aloe vera.<sup>132</sup>

One step towards designing a more sustainable energy harvesting technology can be reached by replacing the metal back electrode with a stable, organic matter-based materials like graphite.

### 3. High-temperature carbon vs. low-temperature carbon

Carbon electrodes in perovskite solar cells can be prepared through two main routes: high- and low-temperature curing (Fig. 9). A typical high-temperature carbon-based (HTCB) cell is

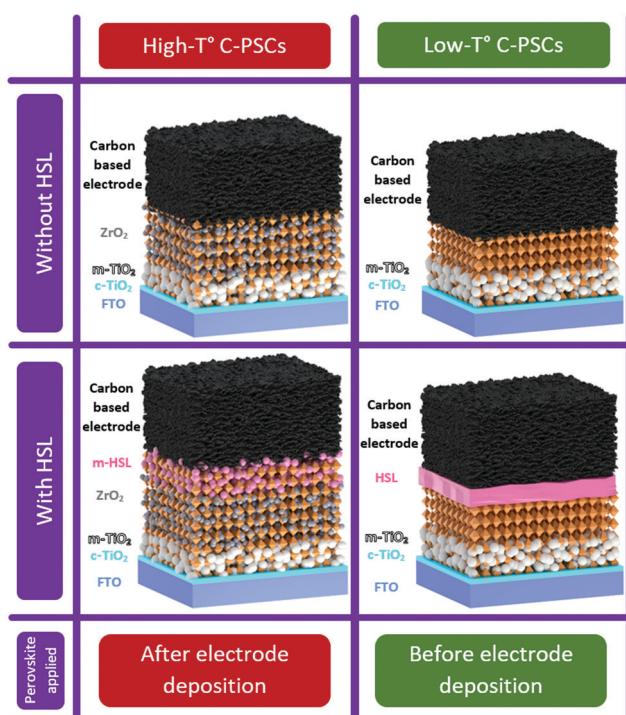


Fig. 9 Schematics of perovskite solar cells with high- and low-temperature carbon-based electrodes with and without HSL.

fabricated by depositing mesoscopic selective and electrode layers, which are usually printable (*e.g.* by screen-printing) and require high-temperature pyrolysis of the organic binders and solvents in them. Therefore, a processing temperature of 400–500 °C during layer deposition is needed,<sup>133</sup> meaning that perovskite precursor solution can be only added afterwards.

On the other hand, in low-temperature carbon-based (LTCB) cells, the electrode layer is fabricated at temperatures below the irreversible perovskite degradation, allowing for the deposition of perovskite before the back-electrode.

Both strategies can be implemented with or without HSL. However, as will be noted later in this work, the LTCB-cells allow for an easier integration of the HSL than the high-temperature treated ones.

#### 3.1. Cell structures

**3.1.1. High temperature carbon-based electrodes.** Since the perovskite precursor solution is added after all the cell layers are fabricated, most of them need to be highly porous and no planar configurations can be implemented.

The overall structure of a typical HTCB-cell without a hole-selective layer consists of a front FTO/Glass substrate, a mesoporous inorganic electron-selective layer, an insulating layer and a mesoporous HTCB-electrode. In order to improve the efficiency by avoiding non-radiative recombination at the front-electrode, a compact hole-blocking layer (*e.g.* c-TiO<sub>2</sub>) has proven to be essential for reaching high PCEs.

Emerging from the dye-sensitized solar cells, an anatase mesoporous TiO<sub>2</sub> layer has been widely used as an electron-selective layer not only in the traditional mesoscopic n-i-p cells,<sup>30,134</sup> but also in HTCB-cells. The insulating layer was found to be crucial, in order to avoid ohmic shunts *via* contact between the counter electrode and front electrode or ESL. Metal oxides with suitable valence and conduction bands are commonly employed as ESLs and insulating layers in HTCB-cells. Porous dielectric oxide layers of ZrO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> have been mainly used as insulators, due to their ability to avoid direct shunts and inability to extract charge carriers.<sup>31,33</sup> Sputtered layers of Al<sub>2</sub>O<sub>3</sub> as thin as 10 nm, which can also electrically isolate electrons in the conduction band of m-TiO<sub>2</sub> from reaching the back-contact and the respective electrodes against pin-holes to the TCO layer have been demonstrated by us earlier.<sup>135</sup> The latter advantage is particularly useful for large-area device fabrication, to avoid the shunted regions in the modules. Because of the nature of the sputtering process, the inner surface (*i.e.* inside the pores) of the m-TiO<sub>2</sub> is not covered and therefore accessible for electrons extracted from the perovskite.

After the insulator layer is fabricated, the mesoporous cell stack is completed by depositing a HTCB-layer and drop-casting the perovskite solution. The concept of a fully-printable triple-layer carbon-based (TiO<sub>2</sub>/ZrO<sub>2</sub>/Carbon) perovskite solar cell (Fig. 9) has gained wide attention after Mei *et al.* displayed an exceptional stability and strong upscaling potential of such devices.<sup>32</sup> Since then, the development of such HTCB cells has been rapid, resulting in an extensive list of reports demonstrating large area devices with moderate efficiencies. In 2018 a

company called Wonder Solar launched a 110 m<sup>2</sup> PV system based on a triple-layer architecture.<sup>20</sup> Also a double-mesoscopic layer structure was proposed by replacing the thick porous spacer layer with a sputtered ultra-thin pseudo-porous Al<sub>2</sub>O<sub>3</sub> layer.<sup>135</sup> However, the absence of hole-selective contacts in such PV devices results in excessive surface recombination at the counter electrode and limits the open-circuit voltage of the device.<sup>133</sup> To overcome this issue in HTCB-cells, Xu *et al.* proposed to use a mesoporous NiO<sub>x</sub> layer as a hole-selective material.<sup>136</sup> The HTCB-cells with TiO<sub>2</sub>/NiO<sub>x</sub>/Carbon layers have been found to have a slightly higher PCE than that of the standard triple-layer configuration, but the strong recombination at the TiO<sub>2</sub>/NiO<sub>x</sub> interface poses a problem for reaching high efficiencies in such devices.<sup>136</sup> In fact, the highest reported PCE of 17.02% (non-certified) for the HTCB-cell to date was achieved by Liu *et al.* *via* integration of mixed absorber Cs<sub>0.05</sub>(FA<sub>0.4</sub>MA<sub>0.6</sub>)<sub>0.95</sub>Pb<sub>2.8</sub>Br<sub>0.2</sub> into the TiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>/NiO<sub>x</sub>/Carbon structure (mesoscopic cell with HSL, as well as *J-V* and EQE measurements are shown in Fig. 10). Although, the *V<sub>oc</sub>* in these cases was still below 1.01 V, highlighting that the implementation of NiO<sub>x</sub> (as a mesoporous or thin layer) into the C-PSCs is still an ongoing research topic. Apparently, there is still large room to further improve the efficiencies of these devices; however, it is limited by the compatibility of HSLs with the sintering process of such mesoscopic structures under high temperatures.

**3.1.2. Low temperature carbon-based electrodes.** The most common architecture of cells with the LTCB-electrode consists of the n-i-p structure, where the n-region is usually *m*-TiO<sub>2</sub><sup>31</sup> or SnO<sub>x</sub><sup>113</sup> and FTO is implemented as a front-electrode. PSCs

with a carbon-based back electrode cured at low temperatures can consist of the same functional layers as the traditionally (layer-by-layer deposited) processed cells, where LTCB-layer is used to directly replace the metal-based back electrode. Here, the carbon-electrode can be cured at temperatures lower than the hybrid perovskite decomposition temperatures. Thus, it allows for an easier integration of the perovskite into the layer stack without the need of infiltrating the precursor solution through a carbon-based electrode and a spacer layer (e.g. ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>) between the back electrode and ESL, unlike in HTCB-cells. Such properties allow the production of not only mesoscopic LTCB-cells, but also planar ones.<sup>113</sup> Generally, we can distinguish between two types of such PSC architectures that are reported to date: with and without HSLs.

After the deposition of hole-blocking layer and ESL, the perovskite photoabsorber layer is deposited straight away.<sup>31</sup> In contrast to high-temperature processed cells, here perovskite can have large crystals, that are not constrained by the pore size as in a triple-layer porous structure. Also, it provides a wide range of opportunities for solvent engineering and crystallization control techniques that are often challenging in the cells with a HTCB-electrode.<sup>31</sup> When the perovskite layer is crystallized, the carbon layer completes the HSL-free cell architecture, followed by mild annealing (in most cases <120 °C).

In the cells where the hole-selective layer is present it can be added either as a dense film between the perovskite and carbon (before electrode deposition) or it can be added directly to the LTCB-paste prior to the paste manufacturing process.<sup>138</sup> In the latter case, the HSL is formed directly at the perovskite/carbon interface upon the curing process of the electrode.

### 3.2. Key advantages of the low-temperature processed electrodes

The low-temperature C-PSC concept has several important advantages depicted in Fig. 11 in comparison to the high-temperature one, such as ability to easily integrate a planar hole-(or electron-) selective layer, a higher control over the perovskite crystallization, compatibility with flexible substrates and higher processing speed, without requiring high-temperature sintering.

**3.2.1. Easier integration of HSLs.** The LTCB-cells with a hole-selective layer represent a promising route towards higher efficiencies for C-PSCs due to a potentially improved hole-extraction rate and lower non-radiative recombination at the perovskite/carbon interface, which should be prevented by hindering electrons from reaching the carbon surface. Therefore, the main requirements for every HSL is to block the electrons from reaching this contact and to allow fast hole-transport.

In the state-of-the-art PSCs, the organic HSLs with suitable valence bands are implemented, although, the drawback of this strategy is the layer stability. As mentioned before, there are few choices of materials which do not have a hygroscopic nature, do not degrade perovskite and meet the demands of high hole mobility and suitable valence band. Nevertheless, a lot of research in the past few years was focused on improving the cell efficiency by the introduction of HSLs described below.

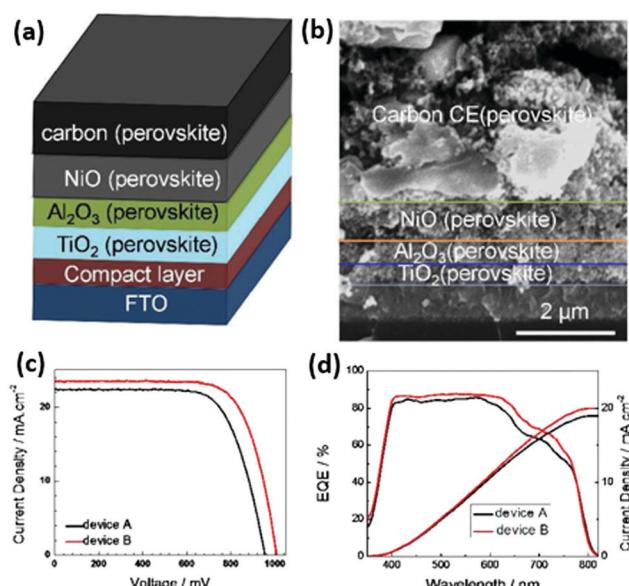


Fig. 10 (a) Schematic cell architecture of the HTCB-cell with the highest PCE reported to date. (b) Cross-section SEM image of the device. (c) *J-V* curves of the devices with such architecture, including different absorbers: device A – FA<sub>0.4</sub>MA<sub>0.6</sub>PbI<sub>2.8</sub>Br<sub>0.2</sub>, device B – Cs<sub>0.05</sub>(FA<sub>0.4</sub>MA<sub>0.6</sub>)<sub>0.95</sub>PbI<sub>2.8</sub>Br<sub>0.2</sub>. (d) External quantum efficiency and integrated current density of devices A and B. Adapted and reproduced with permission from ref. 137.



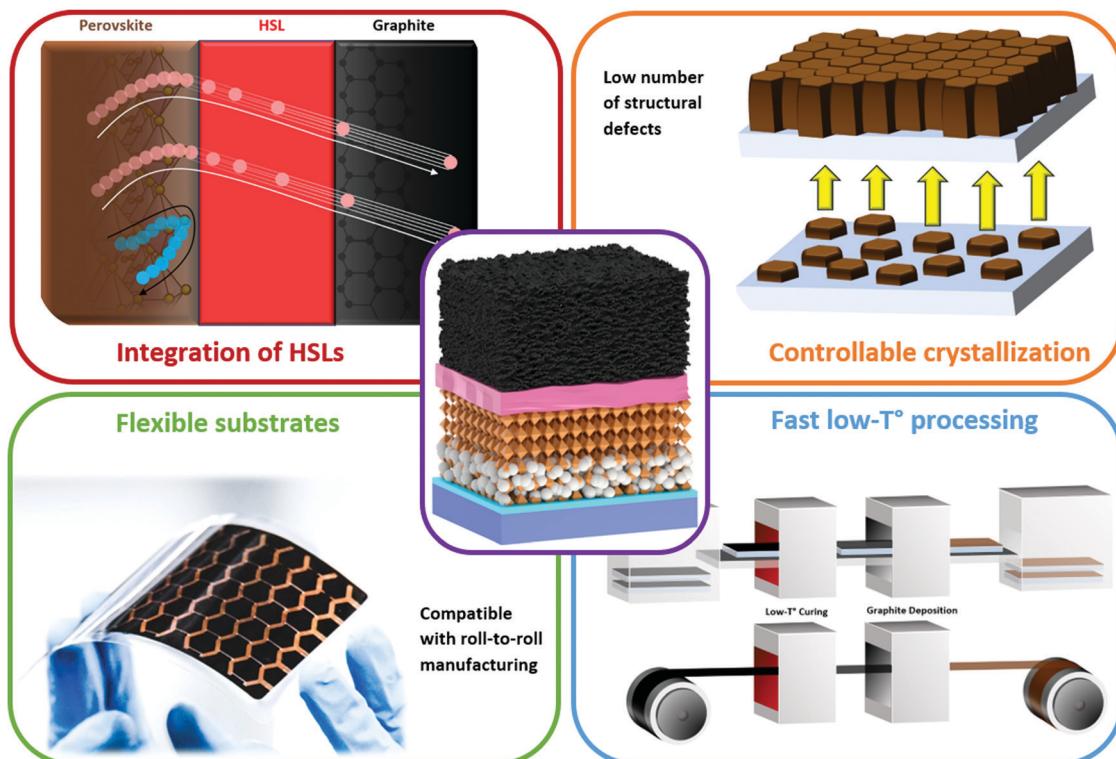


Fig. 11 Key advantages of the low-temperature carbon-based concept: (1) ability to integrate various planar HSLs (or ESL in p-i-n configuration) into the cell stack, (2) better control over the crystallization in planar perovskite films, (3) processability of the carbon-based module on flexible polymeric substrates (reproduced with permission. Copyright 2020, Saule Technologies), (4) faster processing at lower temperatures due to faster solvent evaporation and binder removal.

According to a recent report from Ren *et al.*, a layer of fluorinated small molecules based on difluorobenzene, benzene-[1,2-*b*:4,5-*b'*]dithiophene (BDT) and 4,4'-dimethoxydiphenylamine (DPA) – BDT2FMeDPA can be used as a dopant-free hydrophobic HSL. In particular, the authors have deposited this novel HSL in between the perovskite and LTCB-electrode achieving PCE of 14.5%, keeping 90% of the initial value after 30 days.<sup>139</sup> As an alternative HSL with improved thermal stability, hole mobility, valence band alignment and cost-effectiveness, a 5,10,15-triphenyl-5H-diindolo[3,2-*a*:3',2'c]carbazole (TBDI) was proposed.<sup>140</sup> Implementation of this layer resulted in reduction of the perovskite/carbon interface energy barrier, comparable PCE with cells containing spiro-OMeTAD and a much higher stability. Deposition of PEDOT:PSS in cells with an LTCB-electrode appears to improve this contact, thereby decreasing the hysteresis.<sup>141</sup>

Integration of copper phthalocyanine (CuPc) nanorods as the HSL in the LTCB-cell (Fig. 12a) yielded a similar hole-extraction ability to spiro-OMeTAD and decreased charge carrier recombination at the back electrode, resulting in an impressive PCE of 16.1%.<sup>142</sup> A commonly used electron-donor layer in organic PV – poly(3-hexyl thiophene) (P3HT), has also been employed as an HSL, not only in standard PSCs, but also in LTCB-cells.<sup>143–145</sup> By adding graphene to the pristine P3HT (Fig. 12b), Chu *et al.* were able to enhance the hole mobility of the HSL by almost two orders of magnitude.<sup>146</sup> With the help of this composite

P3HT/Graphene layer, the authors reported an outstanding certified efficiency of the LTCB-cell, which is the highest at the moment for C-PSCs – 17.8%.

Another inorganic HSL that has been often exploited in perovskite and dye-sensitized solar cells, CuSCN, has been implemented by Baranwal *et al.* to enhance the FF and slightly improve the  $V_{oc}$  of LTCB-cells.<sup>110</sup> However, it was found that over a long time, degradation at the CuSCN/perovskite interface occurs, mediated by the loss of SCN group, leading to an interdiffusion between the perovskite and HSL. A similar result on the poor long-term stability of the pristine CuSCN/perovskite interface was also noted by Arora *et al.*<sup>98</sup>

Several studies have highlighted the enhanced hole-extraction and reduced recombination at the back electrode of LTCB-cells by addition of mesoporous  $\text{NiO}_x$  into the cell stack.<sup>136,137,147,148</sup> Peiris *et al.* have demonstrated how an LTCB-electrode can be applied on top of a fully-printed  $m\text{-TiO}_2/\text{ZrO}_2/\text{NiO}_x$  stack with a minimized perovskite capping layer *via*  $\text{N}_2$  blow drying.<sup>149</sup> Although, planar  $\text{NiO}_x$ , which is often used in p-i-n and n-i-p PSCs with a metal electrode, can also be implemented in LTCB-cells, there were no reports of such cell configuration, according to our knowledge.

**3.2.2. Higher control over perovskite crystallization.** In HSL-free carbon-based PSCs, perovskite not only acts as a light absorber to generate electron and hole pairs under illumination, but is also responsible for hole-transport to the cathode.

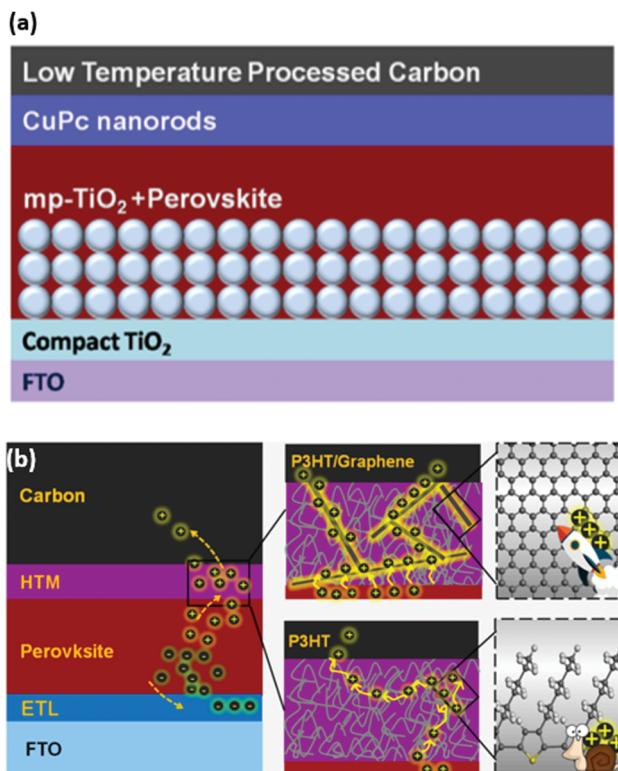


Fig. 12 (a) Schematic structure of the LTB-cell with CuPc nanorods as the HSL. (b) Schematic structure of the LTB-cell with P3HT as the HSL (HTM), illustrating how incorporation of graphene results in higher hole mobility and better charge transport. Adapted and reproduced with permission from ref. 142 and 146.

Therefore, the quality of the perovskite layer is critical in order to achieve efficient charge transportation and reduced recombination for highly efficient perovskite solar cell devices. However, important differences between the perovskite crystallization kinetics in HTCB-cells with highly porous layers and LTB-cells are the interface-energetics and crystallization constraints. Since porous layers provide multiple nucleation sites, the crystallization is highly heterogeneous. In addition, the pores confine the crystals during the perovskite formation, resulting in additional pressure exerted on a crystal which normally does not occur in planar cells.<sup>150</sup> Moreover, the evaporation of solvent, driving the crystallization, also occurs at different rates in HTCB- and LTB-cells due to different diffusion paths. Considering that multiple advanced crystallization control mechanisms were developed for traditional cells with metal-based electrodes, the same methods can be easily implemented for planar cells with an LTB-electrode, but not for HTCB-cells.

An example of carefully controlled crystallization in LTB-cells was given by Chen *et al.*, who obtained an outstanding result of 14.38% PCE with a  $V_{oc}$  above 1 V on 0.07 cm<sup>2</sup> active area and 10% PCE on 1 cm<sup>2</sup> devices.<sup>151</sup> The high-quality perovskite film was obtained *via* a 2-step approach, where the solvent of MAI in the second step was changed from isopropanol (IPA) to a mixed

solvent of IPA/Cyclohexane (CYHEX) (Fig. 13). This mixed-solvent strategy has been proved not only to accelerate the conversion of PbI<sub>2</sub> to MAPbI<sub>3</sub>, but also to effectively suppress the Ostwald ripening process, which eventually provided a pure high-quality perovskite layer with a uniform surface and compact capping layer structure.<sup>151</sup> The similar method of solvent engineering was realized later by the same group to deposit a more thermally stable MAPbBr<sub>3</sub> perovskite through the addition of non-polar CYHEX into the second step solvent of IPA, leading to a LTB-cell with a PCE of 8.09%.<sup>152</sup> In addition, the perovskite composition with a mixed cation of methylammonium (MA) and formamidinium (FA) has been explored by Bai *et al.* in order to enhance the light harvesting capability. The synthesized cubic: column composite structure of (FA)<sub>x</sub>(MA)<sub>1-x</sub>PbI<sub>3</sub> has been demonstrated to broaden the light harvesting area and reduce the probability of electron recombination.<sup>153</sup>

Furthermore, in 2016, Chang *et al.* implemented a colloidal engineering approach, where the authors controlled the crystallization *via* formation of PbI<sub>2</sub>(DMSO)-adducts dispersed in DMF (Fig. 14).<sup>154</sup> The resulting film shows an impressive perovskite layer homogeneity, leading to a better interfacial contact at the perovskite/carbon interface. The renowned anti-solvent engineering techniques, which are widely used nowadays to prepare high-quality dense perovskite crystals,<sup>150</sup> have also been realized in LTB-cells, by adding chlorobenzene during the precursor deposition process.<sup>155</sup> Zhou *et al.* have demonstrated how the incorporation of amino-group functionalized ionic liquid to the precursor solution, yields highly crystalline perovskite with large grains and hydrophobic surface, promoting even higher stability in HSL-free LTB-cells.<sup>156</sup> As can be seen from multiple reports on the topic, the mixed-cation, mixed halide hybrid perovskite films with high crystallinity can be easily manufactured in LTB-cells,<sup>113,114,146,157</sup> since the processing conditions are identical to conventional cells with metallic electrodes, which provides a strong foundation for C-PSCs reaching high PCEs. C-PSCs with inorganic CsPbBr<sub>3</sub> perovskite, having an LTB-electrode were reported as well, which had an outstanding stability in a humid environment (90–95% RH) for over 3 months, in addition to stable performance even under harsh temperature conditions (100 °C to –22 °C).<sup>158</sup> By introducing small amounts of Sn into the perovskite structure, Liang *et al.* fabricated mixed CsPb<sub>0.9</sub>Sn<sub>0.1</sub>Br<sub>2</sub> all-inorganic perovskite solar cells, covered with an LTB-electrode, which exhibited an impressive PCE of 11.33%.<sup>159</sup> LTB-cells with a Mn-doped all-inorganic perovskite absorber have also been reported, displaying a moderate stability, thanks to the inorganic nature of the perovskite and stable LTB-electrodes.<sup>160</sup> In addition to all these crystallization-controlling techniques, which were already applied in LTB-cells, many more effective methods coming from traditional PSCs with metal electrodes can be implemented. We also note that passivation and interface engineering plays a crucial role in enhancing the PCE and stability can also be easily realized in cells with LTB-electrodes, as was recently demonstrated by Di Carlo *et al.*<sup>161</sup>

**3.2.3. Compatible with flexible substrates.** In most of the perovskite solar cells produced today, glass is used as a cell



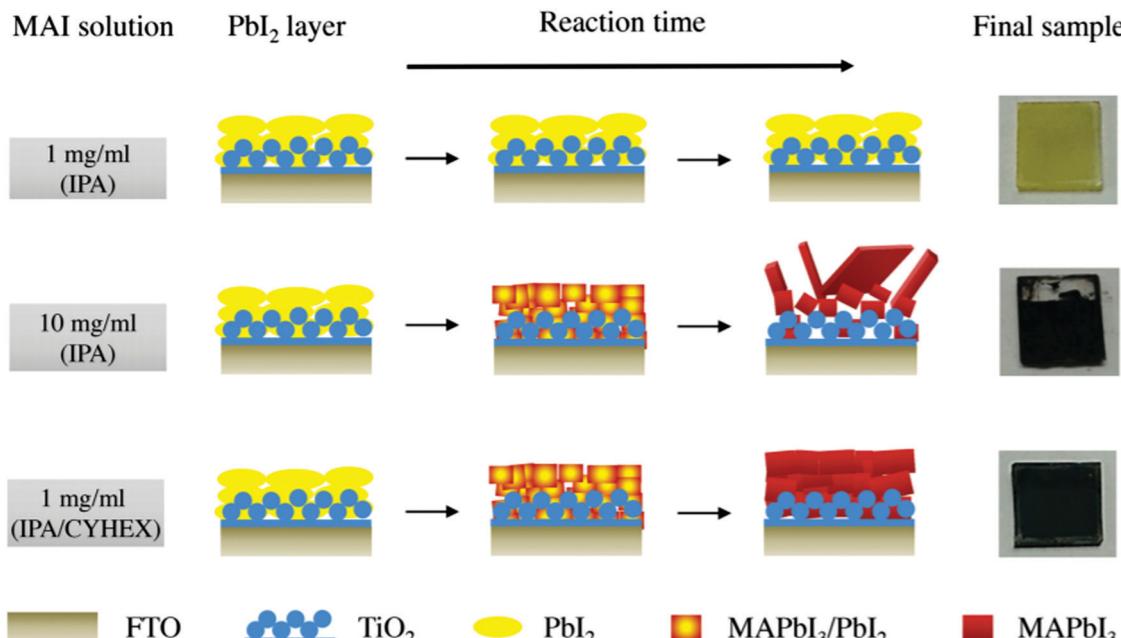


Fig. 13 Illustration of crystallization dynamics where MAI in IPA and augmented IPA/CYHEX mixed solvents are added to the PbI<sub>2</sub> layer. Adapted and reproduced with permission from ref. 151.

substrate, which is coated with a conducting oxide layer. However, they can also be manufactured on flexible polymeric substrates, which provide several benefits, such as light device weight, while maintaining comparable power output, high mechanical flexibility, compatibility with roll-to-roll processing and low-cost manufacturing. Unfortunately, the thermal stability of such substrates remains one major concern for fabrication at higher temperatures. Ordinary plastic substrates, especially transparent ones like polyethylene terephthalate (PET), polyimide (Kapton™), and polyethylene naphthalate (PEN) can only withstand temperatures up to 200 °C.<sup>162</sup> This drawback highlights that carbon-based electrodes in such flexible PSCs can only be deposited using low-temperature carbon pastes, giving it a unique advantage over HTCB-cells.

Using this advantage of low-temperature processing, Zhou *et al.* have applied this layer on a flexible substrate showing

potential for producing flexible PSCs with a hydrophobic carbon-based electrode.<sup>107</sup> In manufacturing flexible PSCs, mechanical integrity after multiple bending cycles is an important consideration. Wang *et al.* have tested the durability of their LTCB-cell and showed that it could keep 70% of its initial PCE even after 1000 bending cycles (Fig. 15).<sup>141</sup>

To date, there are few published studies of carbon-based PSCs on flexible substrates. Chu *et al.* fabricated LTCB-cell (n-i-p configuration) with graphene-doped P3HT as the HTL.<sup>146</sup> The devices on PEN foil delivered an efficiency of 12.4% with only 3% drop after storage under ambient conditions (humidity: *ca.* 50%) for 1680 h. Recently, Babu *et al.* demonstrated carbon-based flexible perovskite solar cells in the p-i-n configuration on PET foil.<sup>163</sup> The devices with an active area of 1 cm<sup>2</sup> delivered an efficiency of 15.18% and excellent operational (MPPT) and thermal (85 °C) stability over 1000 h of ageing.

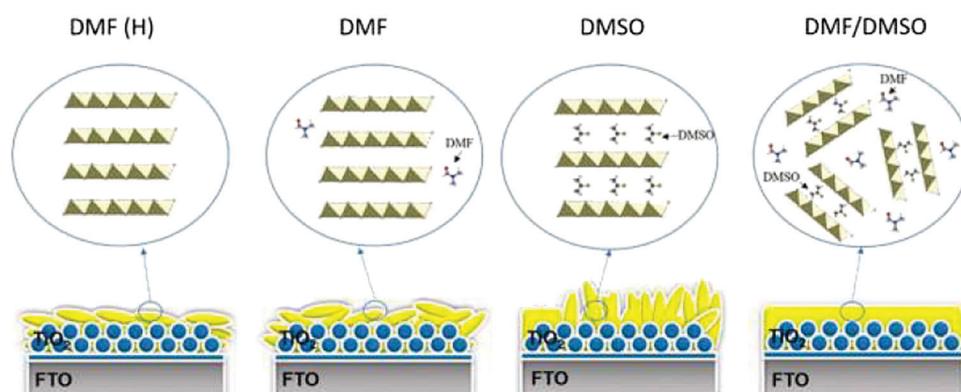


Fig. 14 Illustration of the role of DMF and DMSO solvents in the crystallization and how PbI<sub>2</sub>(DMSO) adducts dispersed in DMF yield a superior film morphology. Adapted and reproduced with permission from ref. 154.



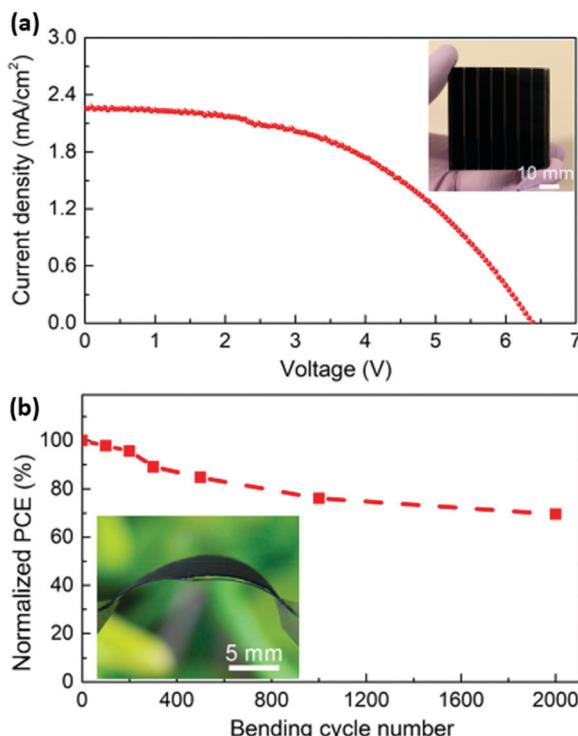


Fig. 15 (a)  $J$ – $V$  curve of the as-prepared flexible  $5 \times 5 \text{ cm}^2$  LTCB-minimodule. (b) PCE change of the LTCB-minimodule after multiple bending cycles (photograph of the minimodule in a bent state is shown in the inset). Adapted and reproduced with permission from ref. 138.

In one of the studies by integrating copper phthalocyanine (CuPc) as an interface modifier and dopant, He *et al.* demonstrated an LTCB module with an active area of  $22.4 \text{ cm}^2$ . The module retained 75% of its initial PCE of 6% after 2000 bending cycles.<sup>138</sup>

One of the key problems of flexible PSCs is the use of expensive conductive metal oxides, such as ITO, which significantly hinders the full commercialization potential. In other thin-film technologies, the front-contact materials such as Al-doped zinc oxide (AZO) and thin transparent Ag are not chemically compatible with perovskite in the long-term. Therefore, we suggest that cheaper and long-term stable alternatives (*e.g.* using titanium foil<sup>164</sup> or “wrap-through” concept<sup>165</sup>) for transparent front-contact are essential for the development of flexible PSCs.

**3.2.4. Fast processing.** Sintering high-temperature carbon-paste normally adds a considerable additional time during cell/module processing, although it could be alleviated by such techniques as heating up the glass substrates *via* near-infrared processing.<sup>166</sup> Regardless of the sintering method, the low-temperature carbon paste is annealed at much lower temperatures, which reduces the energy consumption and processing speed, positively affecting the potential for upscalability in terms of higher throughput.<sup>110</sup> Dou *et al.* have demonstrated 19.6% efficient flexible PSCs manufactured by roll-to-roll fabrication, which significantly reduces the processing time, allowing for web-speeds up to 3 m/min.<sup>167</sup> The combination of

such high efficiency and high-throughput fabrication process is crucial for having lower PV module costs and levelized cost of electricity. Notably the authors implemented a rapid methylamine-induced liquefaction and re-crystallization process to manufacture perovskite photoabsorber in record short times (<2 min). As recently demonstrated by Bogachuk *et al.* in this process, methylamine ( $\text{MA}^0$ ) molecules bind with  $\text{Pb}^{2+}$  and  $\text{MA}^+$  forming  $\text{PbI}_x\text{MA}^{6-x}$  liquefied complex and  $\text{MA}^+-\text{MA}^0$  dimers, which can rapidly rearrange back to  $\text{CH}_3\text{NH}_3\text{PbI}_3$  upon removal of highly volatile  $\text{MA}^0$ .<sup>168</sup> Even higher speeds of  $3\text{--}5 \text{ m min}^{-1}$  on 30 cm wide flexible webs have been reported by Galagan *et al.* by using slot-die coating deposition.<sup>169</sup> Although these publications on roll-to-roll manufacturing have displayed strong up-scalability potential of such PV devices, both back-contacts were deposited by evaporation of a noble metal and replacing it with an efficient low-temperature carbon contact would yield an ultimate combination of low-cost, more stable, moderately efficient and more environment-friendly perovskite PV modules.

### 3.3. Low-temperature carbon-based electrodes offer to close the efficiency gap between G-PSCs and traditional cells

To date most of the high-efficient HTCB-cells have open circuit voltages around 1 V,<sup>135,137,170,171</sup> despite tremendous efforts to boost this value closer to the cells with HSL and the metallic electrode. In contrast, the versatility of implementation of the LTCB-layer is the most attractive advantage of this approach, as the layer can be simply used to replace the costly metal-based electrodes on top of the HSL to improve cell stability at low cost.

As mentioned earlier, the multiple crystallization control and passivation techniques, which were implemented in traditional PSCs, can also be applied here, which can allow growth of high-quality crystals with less grain boundaries as well as less structural and electronic disorder. In addition, implementing selective layers in LTCB-cells with high carrier-mobilities and favorable band alignment will provide much higher PCEs than the standard HTCB-cells can offer. One can notice from Table 1 and Fig. 16 that since 2018 LTCB-cells went beyond 17% PCE (with 17.8% certified PCE), bridging closer to the record-breaking cells with metallic electrodes. Therefore, replacing metal electrodes with more moisture-resistant and chemically stable low-temperature carbon-based electrodes is the most promising route to mitigate the efficiency gap between standard perovskite cells and carbon-based ones.

## 4. Low-temperature carbon paste composition

The composition of the carbon paste plays an important role in the device performance and stability of the carbon-based perovskite solar cells. Typically, the composition of carbon paste includes carbon-based materials, organic solvents or/and organic binders in different ratios, which could be deposited by solution processable methods, such as doctor-blading and screen printing.<sup>133</sup> Carbon black, graphite, graphene and carbon nanotubes are



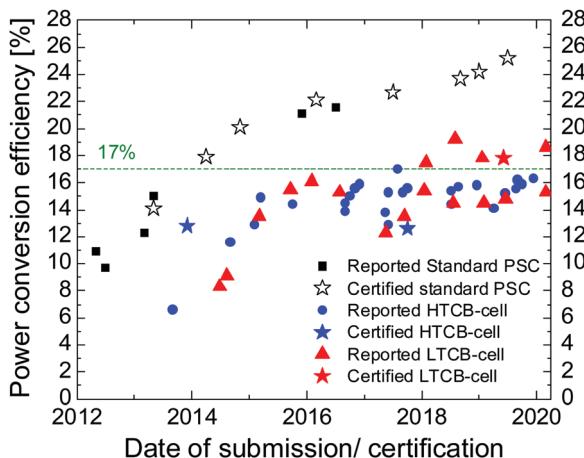


Fig. 16 Development of reported PCEs of perovskite solar cells over the last few years.

commonly used materials for carbon paste. Wei *et al.* have shown that a carbon-based electrode composed of pure carbon black particles deposited by the “candle soot” method can be employed as the counter electrode for PSCs yielding an impressive PCE of 11.02%.<sup>175</sup> In order to further improve the conductivity of the carbon electrode, in further studies graphite was introduced to the carbon paste to reduce the resistive losses. High conductivity of graphite is associated with a high number of delocalized  $\pi$  electrons, meaning that increasing the graphite content in the layer decreases its sheet resistivity.<sup>176</sup> Ku *et al.* have shown how the graphite shape (e.g. spheroidal, flaky) affects the photovoltaic properties of the solar cell devices.<sup>29</sup> To make the resulting electrode more porous, normally carbon black particles are added to the carbon paste, which creates space between the flakes.<sup>33</sup> The main roles of carbon black particles are to adjust the paste processability and facilitate an efficient interconnection between graphite flakes<sup>177</sup> as well as between the perovskite layer and graphite flakes.<sup>178</sup>

In order to form a continuous electrode layer, an organic binder such as ethyl cellulose is normally used.<sup>176</sup> Since such a binder has to be removed before the introduction of perovskite solution into the cell layers, the carbon-based layer has to be sintered at temperatures over 400 °C. This introduces a serious obstacle for the traditional layer-by-layer deposition method that is predominant in the perovskite community. Therefore, in high temperature carbon-based cells, the perovskite solution is drop-casted on the monolithic cell stack after all the functional layers are manufactured and sintered. This highlights that the porosity of the carbon-based electrode (enhanced by carbon black particles) is essential for allowing the complete cell infiltration with solution. Once the cell is impregnated with it, the annealing removes the solvent, causing the crystallization of perovskite inside the cell stack.

Since the low-temperature carbon-based layer, *a priori* does not need to be annealed at high temperatures to remove the binder, it can be deposited on top of perovskite or charge-selective layer directly. The paste in this case can be composed

of carbon powder, a moderate solvent and curing resin or a binder that can be annealed at temperatures less than the decomposition temperatures of HSL and perovskite. Zhou *et al.* demonstrated how a simple dispersion of dried carbon powder (obtained from commercial paste) with a small portion of  $ZrO_2$  particles can be dispersed in chlorobenzene to produce an LTCB ink.<sup>107</sup> A similar approach was later implemented by Gholipour *et al.* except for the absence of  $ZrO_2$  particles.<sup>111</sup> Liu *et al.* have produced an LTCB paste using carbon powder, and polyvinyl acetate (PVAc) as a binder with a small portion of hydroxypropyl cellulose to adjust the viscosity of carbon paste, which were dispersed in ethyl acetate.<sup>179</sup> Dileep *et al.* implemented carboxy-methylcellulose, which could be used as a low-temperature curable binder.<sup>176</sup> Adding a carbon powder, they were able to get a paste curable at room temperature. Recently, Han’s group has successfully developed an LTCB paste, with the help of titanium(IV) isopropoxide and acetic acid acting as low-temperature binders dispersed in terpineol.<sup>180</sup> The peculiar interaction between the binders was attributed to the separation of the acetate group from acetic acid and formation of ligands with  $Ti^{4+}$  in bidentate and bridging binding modes. The resultant polymeric  $Ti-O-Ti$  species encapsulate the graphite and slightly permeate carbon-black particles, producing a strong inter-particle connection, responsible for the layer robustness and conductivity. The resulting LTCB-layer showed an exceptionally low sheet resistance, even lower than that of an HTCB-layer. The same group later demonstrated how such paste can form cracks on top of a perovskite layer after deposition, unless an anti-solvent like chlorobenzene is dripped upon the cell.<sup>141</sup> Later the cell can be annealed at 100 °C for 20 min to completely evaporate chlorobenzene.

Zhang *et al.* have implemented a solvent-exchange process, shown in Fig. 17, where ethanol was added to the paste in order to suppress excessive curing to avoid densification of the carbon-film.<sup>114</sup> However, since ethanol can partially dissolve perovskite (but not  $PbI_2$ ), the carbon layer had to be transferred on top of the cell layers by a press-transfer technique using another substrate. A notable perovskite-friendly approach has been proposed by Chu *et al.*, where the authors produced their LTCB-paste based on propylene glycol monomethyl ether acetate (PGMEA) and polyacrylic resin binder and directly applied it on the perovskite layer.<sup>171</sup>

This myriad of different LTCB-paste compositions shows that there are a lot of alternative routes to produce high quality and conductive pastes through composition engineering, giving a large space for researchers in the perovskite community to explore.

## 5. Deposition methods of low-temperature carbon-based electrodes

The reported deposition techniques of low-temperature carbon-based electrodes, based on liquid processing include: blade coating, press transfer and screen printing. Despite high potential of slot-die coating for large area films, there were no

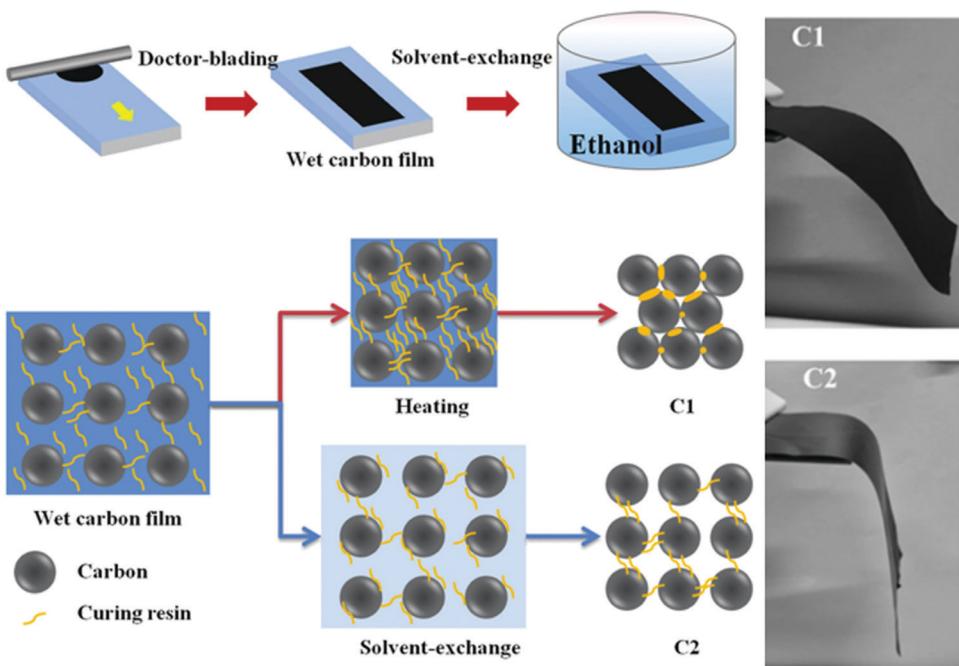


Fig. 17 Schematic diagram of room-temperature solvent-exchange (C2) LTCB-electrode preparation vs. the standard low-temperature annealing method (C1). Photographs of the differences in mechanical flexibility between both preparation methods. Adapted and reproduced with permission from ref. 114.

perovskite solar devices with a slot-die coated LTCB-electrode reported, according to our knowledge. Also, since in the past few years most of the record-breaking cells were produced using spin-coating and metal evaporation, less attention was given to the aforementioned up-scalable methods. Naturally, this influenced the rate of development of these strategies, which currently lags behind the conventional ones. Although there have been slightly more reports on HTCB-cells and modules, due to strong advantages of the LTCB-concept discussed earlier (to reach efficiencies comparable to the ones with metal electrodes), we strongly encourage scientists and engineers in the perovskite community to explore this option.

### 5.1. Blade-coating

Blade-coating (or doctor-blading) is an up-scalable layer deposition technique where solution/paste is dropped on a substrate and then spread by sweeping a blade across the substrate at a fixed height. The resulting thin layer can have comparable heights (controllable by blade height and speed) to spin-coating, allowing for swift solvent evaporation and uniform, dense film deposition. This promising technique has the potential to be implemented for LTCB-manufacturing in an ambient environment on a large scale and it is also compatible with roll-to-roll manufacturing.

In the first reports on an LTCB-electrode in PSCs, the authors used blade coating to deposit carbon and achieved PCEs of 8–9%.<sup>107,140</sup> Over the years, many of the LTCB-electrodes demonstrated in the literature were manufactured this way and remarkable power conversion efficiencies over 17% (Table 2) have been achieved in PSCs.

Chu *et al.* have implemented a “fast drying” process (Fig. 18) to show that a blade-coated carbon paste can be dried by mild annealing at 100 °C and exposure to vacuum for a short amount of time.<sup>181</sup> Since the paste is directly applied on the cell layer, it should not contain solvents that can dissolve the layers underneath. The speed and pressure applied on top of the blade play a critical role in deposition of homogeneous LTCB-layers with a tight connection to the layers beneath it.

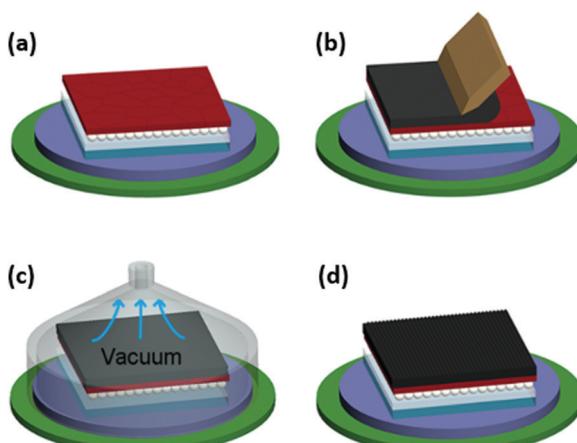
### 5.2. Press-transfer

Due to the often-occurring issue of poor contact between the perovskite or HSL and carbon electrode, the cells often have high series resistance at the carbon/perovskite or carbon/HSL interfaces. A press-transfer technique has been praised by being able to partially minimize this problem. Additionally, this technique is well-compatible with fast roll-to-roll production. The first step of this method is deposition of an LTCB-layer on a substrate (*e.g.* by blade-coating) followed by subsequent solvent removal. Then, the substrate with a carbon-based layer is pressed against the remaining cell layers leading to an improved adhesion and interfacial contact.

As of today, some of the highest efficiency PSCs with a carbon-based electrode (not only among low-temperature processed ones) have been realized *via* the press-transfer approach. Zhang *et al.* proposed an impressive approach – to reduce the number of agglomerated carbon blocks during film curing by a solvent-exchange process instead of common annealing. After removing the solvent in the paste, the LTCB-layer was deposited on top of the cell stack by a press-transfer method. The combination of high film compressibility (thanks to avoidance

**Table 2** Summary of PCEs of C-PSCs with a low-temperature carbon-based electrode described in recent reports, with the corresponding electrode deposition methods

Carbon deposition method	Cell structure (perovskite composition)	PCE (%)	Year	Ref.
Blade-coating	<i>m</i> -TiO <sub>2</sub> /PVS/C (MAPbI <sub>3</sub> )	9	2015	107
Blade-coating	<i>m</i> -TiO <sub>2</sub> /PVS/TPDI/C (MAPbI <sub>3</sub> )	15.5	2015	140
Blade-coating	<i>m</i> -TiO <sub>2</sub> /PVS/CuPc/C (MAPbI <sub>3</sub> )	16.1	2015	142
Blade-coating	<i>m</i> -TiO <sub>2</sub> /PVS/C (MAPbI <sub>3</sub> )	12.3	2017	181
Blade coating	<i>m</i> -TiO <sub>2</sub> /PVS/C (MAPbI <sub>3</sub> )	13.5	2018	171
Blade-coating	<i>m</i> -TiO <sub>2</sub> -SnO <sub>2</sub> /PVS/CuPc/C (Cs <sub>0.05</sub> (MA <sub>0.17</sub> FA <sub>0.83</sub> ) <sub>0.95</sub> Pb(I <sub>0.83</sub> Br <sub>0.17</sub> ) <sub>3</sub> )	15.4	2018	186
Blade-coating	<i>m</i> -TiO <sub>2</sub> /PVS/BDT2FMeDPA/C ((FAPbI <sub>3</sub> ) <sub>0.85</sub> (MAPbBr <sub>3</sub> ) <sub>0.15</sub> )	14.5	2018	139
Blade-coating	Ni:TiO <sub>2</sub> /PVS/CuPc/C (Cs <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	17.46	2018	157
Blade-coating	<i>m</i> -TiO <sub>2</sub> /PVS/CuPc/C (MAPbI <sub>3</sub> )	14.8	2019	138
Blade-coating	Zn:SnO <sub>2</sub> /PVS/CuPc/C (Cs <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	17.8	2019	113
Press-transfer	<i>m</i> -TiO <sub>2</sub> /PVS/spiro-OMeTAD/C (FA <sub>1-x</sub> MA <sub>x</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	19.2	2017	114
Press-transfer	SnO <sub>2</sub> /PVS/spiro-OMeTAD/C/graphite paper (Cs <sub>0.05</sub> (FA <sub>0.85</sub> MA <sub>0.15</sub> ) <sub>0.95</sub> PbI <sub>2.55</sub> Br <sub>0.45</sub> )	18.6	2019	174
Hot-press	<i>m</i> -TiO <sub>2</sub> /PVS/spiro-OMeTAD/C (Cs <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	15.3	2016	111
Hot-press	SnO <sub>2</sub> /PVS/CuSCN/C (Cs <sub>1-x</sub> (FA <sub>0.83</sub> MA <sub>0.17</sub> ) <sub>x</sub> PbI <sub>2.53</sub> Br <sub>0.47</sub> )	15.3	2020	182
Screen-printing	<i>m</i> -TiO <sub>2</sub> /PVS/C (MAPbBr <sub>3</sub> )	8.1	2016	152
Screen-printing	<i>m</i> -TiO <sub>2</sub> /PVS/C (MAPbI <sub>3</sub> )	14.4	2016	151
Screen-printing	<i>m</i> -TiO <sub>2</sub> /PVS/PEDOT:PSS/C (Cs <sub>0.05</sub> (FA <sub>0.83</sub> MA <sub>0.17</sub> ) <sub>0.95</sub> Pb(I <sub>0.83</sub> Br <sub>0.17</sub> ) <sub>3</sub> )	14.5	2019	141
Screen-printing	SnO <sub>2</sub> /MOH/PVS/C (CsPbIBr <sub>2</sub> )	11.8	2019	187
Ink-jet printing	<i>m</i> -TiO <sub>2</sub> /PVS/C (MAPbI <sub>3</sub> )	11.6	2014	184
Spraying	SnO <sub>2</sub> /PVS/spiro-OMeTAD/C-carbon black (Cs <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	14.1	2019	185
	SnO <sub>2</sub> /PVS/spiro-OMeTAD/C-graphite (Cs <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	9.9		
	SnO <sub>2</sub> /PVS/spiro-OMeTAD/C-graphene (Cs <sub>0.05</sub> (FA <sub>1-x</sub> MA <sub>x</sub> ) <sub>0.95</sub> PbI <sub>3-x</sub> Br <sub>x</sub> )	18.7		



**Fig. 18** Schematic diagram of the fabrication process of the LTCB-electrode using blade coating and subsequent drying, which can be vacuum-assisted. Adapted and reproduced with permission from ref. 181.

of carbon-agglomerations) and pressing technique (which improves the interface between carbon and layer underneath) resulted in achieving a record PCE of 19.2%.<sup>114</sup> Later, the same group modified their novel deposition method by using a highly conductive transferring substrate in order to successfully implement it on a large area (1 cm<sup>2</sup>) device, reaching a PCE above 17%.<sup>174</sup>

The so-called “hot-press” approach (in the context of PSC manufacturing) is a press transfer method carried out at increased temperatures (Fig. 19). Interestingly, Yang *et al.* have found how applying higher temperatures during the

press-transfer method improves  $J_{sc}$ , FF and  $V_{oc}$ .<sup>182</sup> Meng *et al.* have demonstrated a cell with a coal-based low-temperature processed electrode fabricated by a hot-press approach, as an example of an ultralow-cost perovskite solar cell.<sup>183</sup> Using such a technique, Wei *et al.* reached an impressive 13.5% PCE on a HSL-free cell with a performance drop of only 5% after 20 days under ambient conditions.<sup>177</sup>

### 5.3. Screen-printing

Similarly to the most C-PSCs with high-temperature carbon-based electrodes reported in literature, LTCB-electrodes can also be deposited by screen-printing. This printing method is based on moving a blade across the screen to fill a fine aperture mesh with a paste and then a squeegee applies a pressure on the screen, while moving backwards. In such way, the pressure applied by the squeegee pushes the ink through the aperture area, which touches the substrate only in the locations corresponding to the aperture area, while the rest of the ink is blocked by stencils. Consequently, the resulting print area is fully defined by the screen aperture area, whereas its thickness depends on mesh properties and printing parameters. A big advantage of a screen-printing technique, in comparison, for instance, to blade-coating, is the ability of precise layer patterning (without the use of masks), at an accuracy which is defined by the screen fineness. Notably, it can also be applicable to roll-to-roll manufacturing.

### 5.4. Other deposition methods

The ink-jet printing technique was demonstrated as a deposition method for fabricating a low temperature nanocarbon



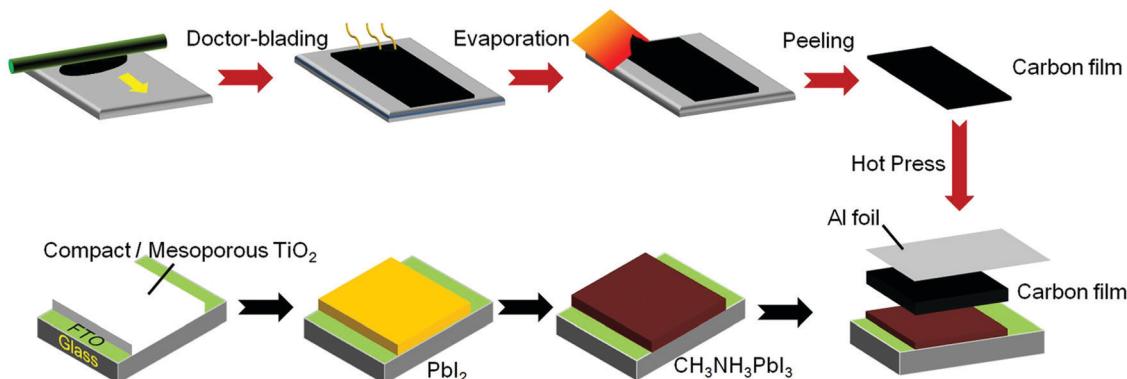


Fig. 19 Schematic diagram of the LTCB-cell assembly process using a hot-press approach. Adapted and reproduced with permission from ref. 177.

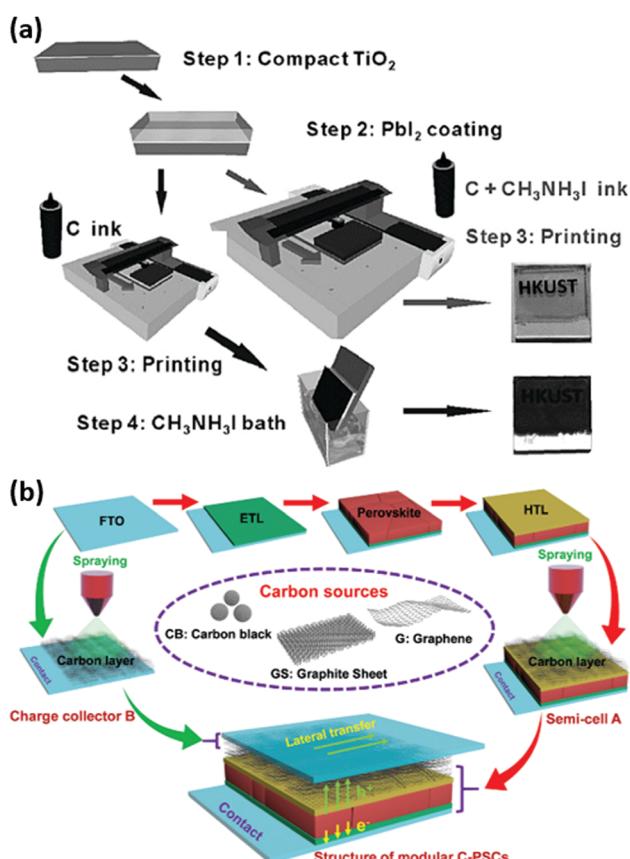


Fig. 20 (a) Schematic demonstration of the process flow for fabricating perovskite solar cells with an ink-jet printed carbon electrode (two alternative routes are shown). (b) Overview of the fabrication process of the LTCB-cells with a sprayed carbon electrode. Adapted and reproduced with permissions from ref. 184 and 185.

electrode in HSL-free mesoscopic PSCs. The carbon ink was formulated with the addition of  $\text{CH}_3\text{NH}_3\text{I}$ , which allowed *in situ* transformation of a  $\text{PbI}_2$  layer into  $\text{CH}_3\text{NH}_3\text{PbI}_3$  perovskite (Fig. 20a).<sup>184</sup> With this strategy, improved characteristics of perovskite/carbon interface were obtained, reaching 11.60% efficiency. Furthermore, the ink-jet technique allowed the production of precisely controlled patterns of carbon electrode.

In the work of Zhang *et al.*, three commercialized carbon sources (graphene, carbon black, graphite sheet) have been tested as back electrodes in an innovative modular PSC design, where the carbon materials were sprayed upon the HTM (Fig. 20b).<sup>185</sup> Remarkably, the sheet resistance and thickness were dramatically reduced by covering the cell with an additional carbon-coated FTO glass with applied pressure. Among different carbon sources, graphene provided the best performance for a carbon-based PSC with an impressive PCE of 18.65%. The device performance could maintain 90% of its initial PCE after ageing at 85 °C for 1000 h without encapsulation. Notably, the optimized graphene-based PSCs exhibited excellent structural flexibility with negligible degradation in PCE with multiple re-assembling (detaching the substrate with a half-cell and re-attaching it back) for more than 500 cycles, providing a promising strategy for facile repair and maintenance of the PSC through modular interconnections.

## 6. Strategies to reach high efficiencies using a low-temperature carbon electrode

As demonstrated earlier, the cells with a low-temperature carbon-based electrode have already shown superior PCEs to the ones produced by a high-temperature method. However, to our knowledge, they still have not surpassed a PCE of 20%. Despite the physical limitations of LTCB-materials for PSCs, we are confident that there are still multiple ways to improve them and bring the power-conversion efficiencies of C-PSCs closer to the ones with metal-electrodes. In Fig. 21 we highlight that the main properties that need to be optimized in order to close this efficiency gap are conductivity, charge selectivity and perovskite/carbon contact.

### 6.1. Increase of conductivity

By definition, metals are materials where the Fermi level of electrons lies within the conduction band of this material. This leaves electrons free to travel through the lattice. Due to highly periodic lattice in noble metals, the mobility of free charge



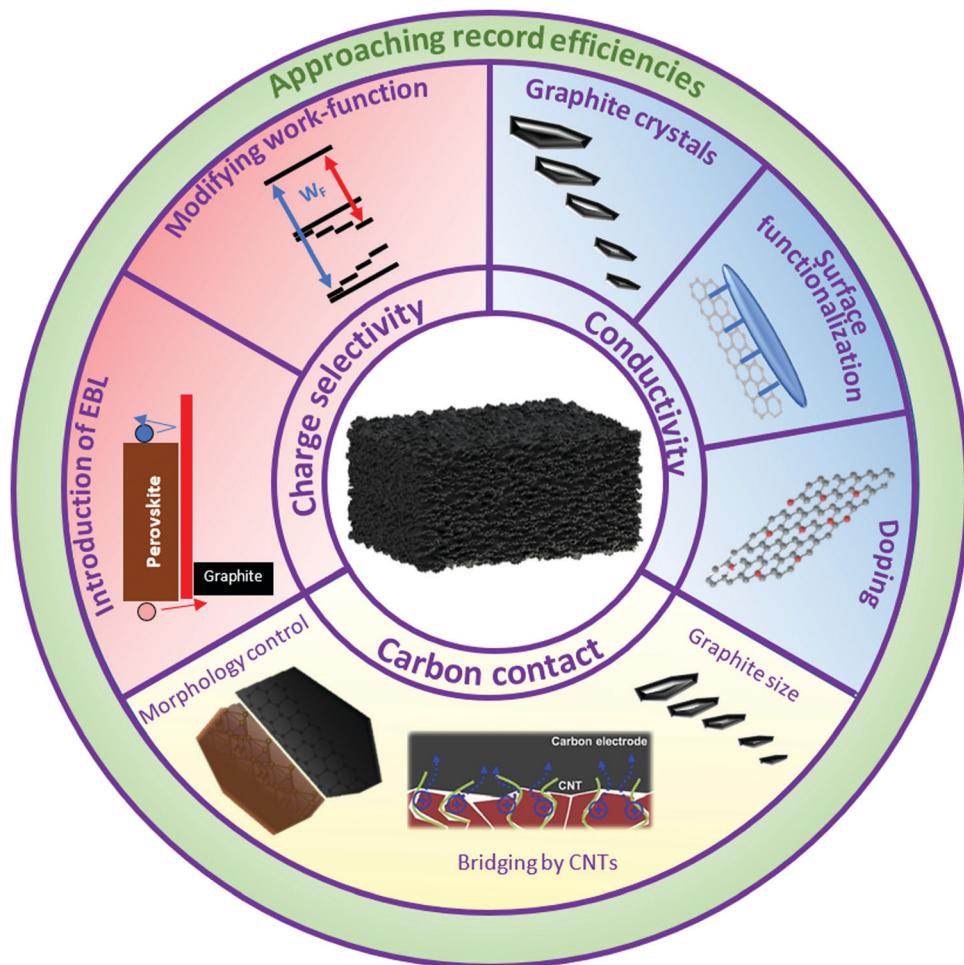


Fig. 21 Proposed approaches to improve the PCE of low-temperature carbon-based cells. Partially adapted and reproduced with permissions from ref. 188 and 189.

carriers is generally higher than in semiconductors and most of the carbon-based materials.

Graphite particles (which are present in most of the carbon-based electrodes) consist of stacked graphene sheets.<sup>190,191</sup> Graphene has a hexagonally close packed crystal structure and is a 2D layer of periodically arranged carbon atoms interconnected by covalent bonds.<sup>192</sup> These graphene sheets can be AB stacked upon each other by weak van der Waals forces to form graphite or can be wrapped into a tube shape, which would form a carbon nanotube (CNT). Graphene is formed by  $sp^2$  hybridization of carbon with neighboring three carbon atoms, while the fourth valence electron ( $2p_z$ ) is delocalized and forms a  $\pi$ -orbital.<sup>191</sup> These delocalized  $\pi$ -electrons have ultra-high mobility along the sheet and are responsible for such low resistivity of graphene, which is even lower than silver. Since graphite consists of stacked graphene sheets it has high conductivity in the direction along the carbon-sheets, but worse conductivity between the sheets, leading to anisotropic electrical nature of graphite.<sup>191</sup> Since carbon-based electrodes in PSCs consist not only of multiple graphite flakes, but also carbon black particles, the layer conductivity is severely decreased. Nevertheless, there were several effective strategies suggested to enhance

this property by doping, altering graphite size and functionalization of the carbon surface.

**6.1.1. Increase of conductivity by doping.** One of the proposed methods to improve the conductivity of a carbon-based layer is to dope the graphite with boron atoms. Duan *et al.* added boron carbide to coke powder prior to the carbonization process (Fig. 22). After the graphitization, it was mixed together with carbon black in terpineol solution. The introduction of boron atoms was found to decrease the interlayer distance along the (002) plane, leading to improved graphitization degree, crystallinity and conductivity (Fig. 23a).<sup>189</sup> Doping techniques that improve the conductivity of graphene might also be applicable for doping graphite flakes (as in the case of B-doping). Another report shows that the sheet resistance can be tuned to  $8.41 \Omega \text{ cm}^{-2}$  and  $7.98 \Omega \text{ cm}^{-2}$  for the B-doped and P-doped carbon layers, respectively, compared to  $14.75 \Omega \text{ cm}^{-2}$  of pure carbon. This improvement subsequently led to an increase in the overall performance of the PSCs, allowing for the PCE to almost double, compared to the ones obtained with a pure carbon electrode.<sup>193</sup> However, relatively few studies in the perovskite research field have been focused on graphite-doping and more on doping of graphene-based electrodes and CNTs.



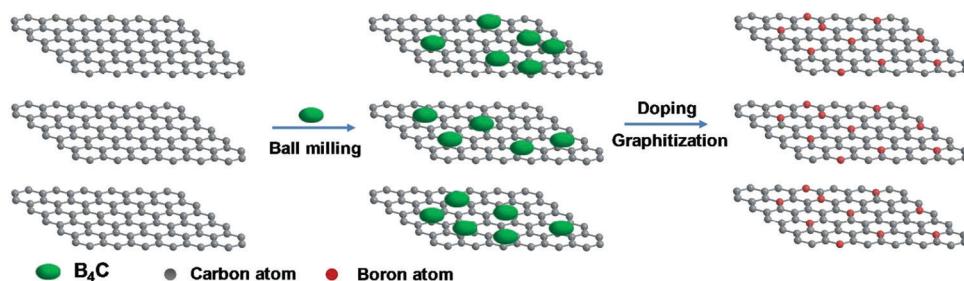


Fig. 22 Schematic of the boron-doped graphite preparation process. Reproduced with permissions from ref. 189.

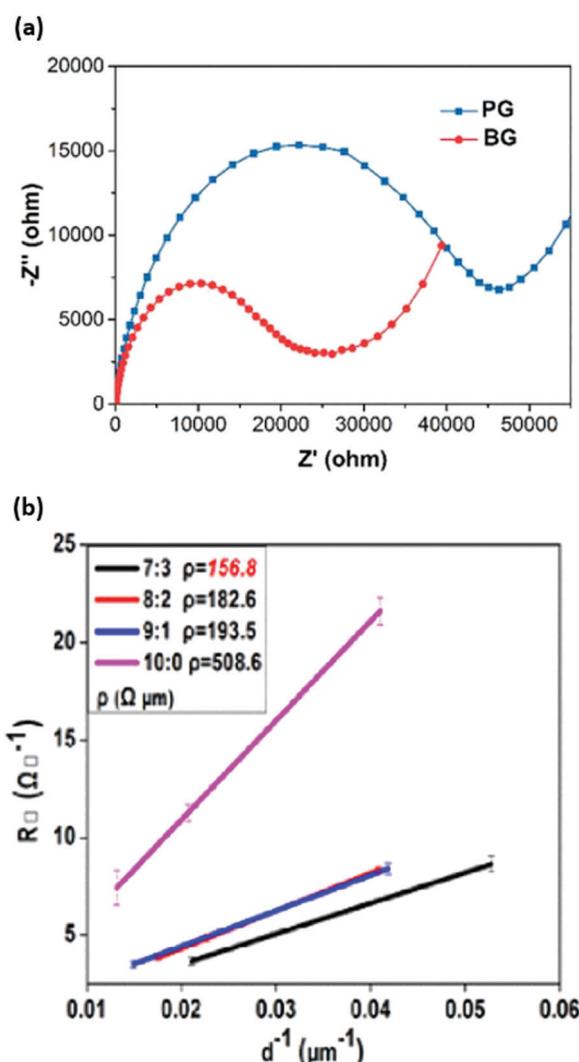


Fig. 23 (a) Nyquist plots of the PSCs with boron-doped (BG) and boron-free (PG) carbon-based electrodes. (b) Square resistance measurements of LTCB-electrodes with varied graphite to carbon-black ratio (G : CB). Adapted and reproduced with permissions from ref. 189 and 180.

One of the first studies investigating the increase of CNT conductivity by boron doping on the electrical behavior of CNTs was conducted by Liu *et al.*<sup>194</sup> Moreover, Zheng *et al.* have achieved noticeably higher PCEs through the incorporation of boron doped multi-walled carbon nanotubes (MWCNTs) in

their PSC structure as back contact electrodes.<sup>195</sup> The authors demonstrated that boron doping MWCNTs through thermal annealing allows an increase in their work function, carrier concentration and conductivity, enhancing their hole extraction and transport properties and therefore the performance of the PSC, with a PCE improvement from around 10.7% with undoped MWCNTs to approximately 14.6% with B-doped MWCNTs with a relatively insignificant hysteresis and an efficiency of over 15.2% with an added aluminum oxide (Al<sub>2</sub>O<sub>3</sub>) as an insulating layer.

The impact of vapor assisted trifluoromethanesulfonic acid (TFMS) *ex situ* doping was investigated by Lee *et al.* Such doping was performed through exposing self-standing CNT sheets to TFMS vapor.<sup>196</sup> The authors found that it effectively improved the conductivity of CNTs and their performance in PSCs, reaching an outstanding PCE of 17.6%, with 72% fill factor. The TFMS-doped CNT-based devices have also shown a better stability compared to undoped devices.

We expect that the methods of CNT doping presented above can also be applied to the carbon-based electrodes, in order to decrease the series resistance losses and enhance the power conversion efficiency of the PV device.

**6.1.2. Increase of conductivity by adjusting graphite size and its portion in the paste.** Most of the graphite materials consist of aggregates of smaller graphite crystallites forming a polycrystalline structure. The crystallite size (perpendicular to the basal plane) can vary from a few to hundreds of nanometers, depending on the graphite type, which is determined by the carbon precursors and fabrication methods.<sup>197,198</sup> Larger crystallites, their improved alignment and lower number of structural defects (*e.g.* vacancies, stacking faults, dislocation and disinclinations) will have a strong impact on the layer conductivity<sup>191,198</sup> (as in the case of pyrolytic graphite) and can reduce the series resistance losses in C-PSCs.

The graphite particle size has been found to play a role in the conductivity of the layer, where lower square resistance can be achieved with larger flakes.<sup>199</sup> The size distribution as well as contact area between the graphite flakes directly affect the interparticle resistance and represent a critical parameter to consider during the manufacturing process of the carbon-based paste.<sup>180</sup> Notably, the ratio of graphite to carbon-black particles is another factor that requires fine-tuning to reach the highest conductivity of the carbon-based layer. Despite the fact that graphite is more conductive than carbon-black, the latter



particles serve as a crucial inter-particle medium for graphite and a significant portion of it is required to obtain highly conductive carbon-based electrodes.<sup>180</sup> Based on the studies from Jones *et al.*<sup>200</sup> and Jiang *et al.*<sup>180</sup> the optimal ratio of graphite to carbon-black was found to be (7:3) as shown in Fig. 23b; however, reports with various ratios have been shown in the literature,<sup>201</sup> which is probably related to the disparity between the used graphite and carbon-black powders.

**6.1.3. Increase of conductivity by surface functionalization.** Surface chemistry can also alter the conducting properties *via* functional groups at the layer surface, which can cause electron localization, introduction/removal of electron traps and changes in conduction activation energy. Polovina *et al.* have investigated how oxidation of activated carbon cloth by air, nitric acid, hydrogen peroxide and iron-nitrate-crystallohydrates can directly affect the series resistance of carbon-based materials.<sup>202</sup> By adding highly conductive antimony-doped tin oxide nanoparticles (ATO) to the carbon precursor prior to carbonization, a carbon/ATO-decorated graphite was demonstrated with exceptionally low sheet resistance.<sup>203</sup> Oxidizing graphite with  $(\text{NH}_4)_2\text{S}_2\text{O}_8$  was also found to improve the electrode conductivity.<sup>204</sup> In the literature, CNTs functionalized with PEI have displayed an improvement in electrical conductivity and thus enhancement of solar cell PCE.<sup>205</sup> In organic photovoltaics the addition of surface functionalized carbon nanotubes and graphene nanocomposites to the electrodes has proven to improve their performance.<sup>206</sup>

We suggest that further exploration of doping techniques, careful control of graphite particle size and surface functionalization of the carbon-based layer can result in the development of effective strategies to improve the layer conductivity and enhance the FF of cells with low-temperature carbon-based contact.

## 6.2. Improve charge selectivity

As mentioned earlier, the issue of poor hole selectivity in HSL-free perovskite solar cells with a carbon-based electrode has to be solved in order to bridge closer to the high-efficiency cells above 20%. Lack of potential barrier for electrons at the perovskite/carbon interface allows electrons to recombine non-radiatively with holes, resulting in a significant drop of  $V_{\text{oc}}$ . Therefore, an excellent charge extraction and hole conductivity of the low temperature carbon counter electrode is fundamental to improve device PCE. Many attempts have been made to resolve this issue either by the introduction of an HSL into the cell stack (by adding it to the carbon paste or by depositing a planar layer) or by increasing the work function of a carbon-based electrode. In addition, the introduction of an electron-blocking layer on the LTCB-surface can also resolve the issue of electron-hole recombination at the back contact. The main advantage of the low-temperature carbon-based electrode is its compatibility with any given structure and versatility of implementation, which makes it an ideal candidate to reach comparable PCEs with record-breaking cells with metal-based electrodes, while maintaining superior stability.

**6.2.1. Modifying the work function of carbon-based electrodes.** Besides the insertion of a hole-selective layer, the LTCB-electrode

layer itself could be modified to energetically favor the hole extraction. One can shift the work function of the carbon electrode by modifying its formulation. This method is fundamentally different to integration of the HSL, since it changes the electron energy band structure of the carbon-based electrode. Additionally, it becomes not prone to degradation mechanisms induced by HSL, while having efficient hole extraction. In fact, simulations by Minemoto and Murata have shown that if the electrode work function is similar to the valence band of the perovskite, the built-in voltage can be equally high with or without HSL material.<sup>207,208</sup>

In addition to improving the conductivity, doping (*e.g.* by boron) was found to alter the work-function of the carbon-based layer (Fig. 24a).<sup>189</sup> Chen *et al.* fabricated a PSC involving boron (B) and phosphorus (P) co-doped carbon electrode through coating the B-atoms onto a hydrothermally P-doped carbon layer. The B/P-doped carbon layer showed an improved work function and electrical conductivity compared to the pristine pure carbon sample.<sup>193</sup> By adding a surface modifying layer to an electrode, it is also possible to alter its surface dipole, which has a direct influence on the material work-function.<sup>211</sup> Another carbon-layer modification by p-doping was demonstrated by Kim *et al.*, where the authors exposed a complete HSL-free cell to  $\text{C}_4\text{F}_8$  plasma treatment as a post-processing step. They found that such fluorine-based treatment was able to form various  $\text{C-F}_x$  groups, which in turn increase the work-function of the electrode (Fig. 24b).<sup>209</sup> Tian *et al.* have proposed a method to increase the work function of carbon-based electrodes by augmenting the oxygen content in them (Fig. 24c and d).<sup>210</sup> The authors attributed the increase in work function to the introduction of  $\text{sp}^3$  hybridization into the  $\text{sp}^2$  conjugated hexagonal lattice during formation of graphite, resulting in an increase of interplanar distance along the (002) plane. A similar difference in work-function between pure graphene (4.6 eV) and graphene oxide (4.9 eV) was demonstrated earlier in organic PV cells, making it a promising HTM.<sup>212</sup> Since oxygen is more electronegative than carbon, the creation of a surface dipole has been proposed as the underlying reason behind the shift in work-function of graphene oxide. TFMS acid doping of counter electrode CNTs has been proved to improve their conductivity as well as tune their work function, from 4.75 eV to 4.96 eV, subsequently enhancing the energy alignment of the cell and  $V_{\text{oc}}$ .<sup>196</sup>

Li *et al.* have shown that a device with a carbon/graphite/single-walled carbon nanotube (SWCNT) counter electrode mixture (Fig. 25) yielded an improved efficiency of 14.7% compared to devices employing pristine carbon CE.<sup>213</sup> This was attributed to the higher work function of 4.7 eV measured for carbon/SWCNT layers as well as to the longer interfacial charge recombination lifetime at the perovskite/SWCNT-carbon electrode interface.

Another strategy to modify the work function of carbon electrodes was demonstrated with a p-type material of high hole mobility blended into the carbon formulation. He *et al.* used copper phthalocyanine (CuPc) addition to change the carbon bulk properties (Fig. 26a).<sup>138</sup> The work function measured by



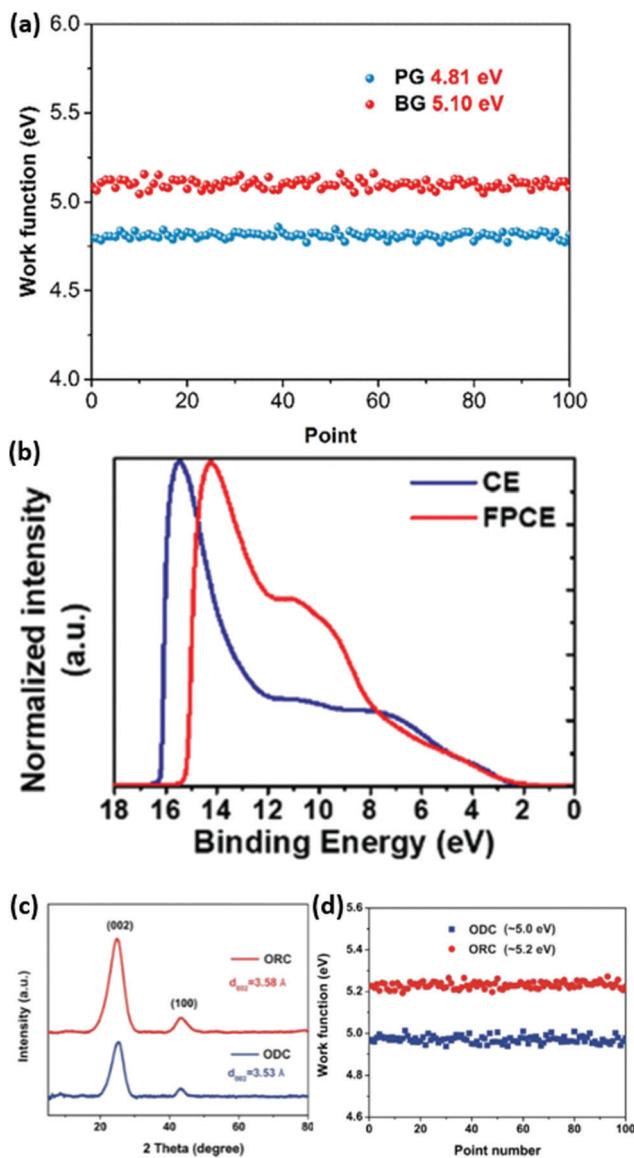


Fig. 24 (a) Work function curves of the boron-free (PG) and boron-doped (BG) carbon-based electrodes. (b) UPS spectra of standard (CE) and fluorine-plasma treated (FPCE) carbon electrodes, highlighting the higher secondary electron cut-off region and work-function in the fluorine-plasma doped electrode. (c) XRD-patterns and (d) work-function curves of oxygen-deficient (ODC) and oxygen-rich (ORC) carbon electrodes. Adapted and reprinted with permissions from ref. 189, 209 and 210.

ultraviolet photoelectron spectroscopy increased from 4.03 eV for the unmodified carbon to 4.22 eV for the paste blended with 1 wt.% of CuPc (Fig. 26b). Upward shift of the electrode work function resulted in a better hole extraction and overall PCE improvement, from 11.4% to 14.8%. The cells were fabricated in an HSL-free perovskite solar cell architecture (structure: FTO/TiO<sub>2</sub>/MAPbI<sub>3</sub>/carbon). Additionally, the authors compared the performance of CuPc-modified carbon devices with the ones where a CuPc interlayer was thermally evaporated between the perovskite and bare carbon layer. The modification of the carbon bulk properties yielded better results than the insertion of CuPc as the HSL.

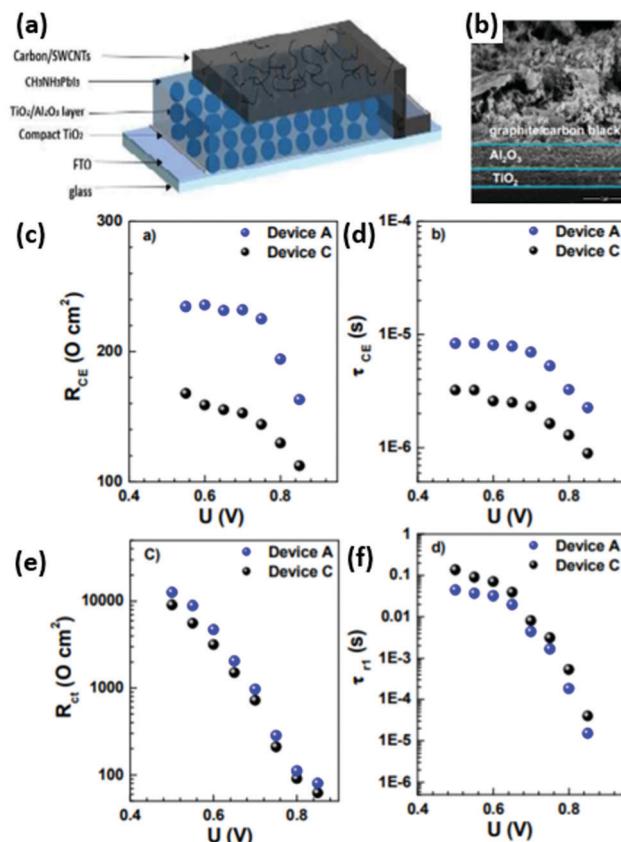


Fig. 25 (a) Schematic device architecture with SWCNTs integrated into the carbon-based counter electrode. (b) SEM image of the fabricated device. (c) Charge transfer resistance, (d) charge lifetime at the carbon-based counter electrode (CE), (e) interfacial recombination resistance, and (f) charge lifetime at the interface between perovskite and carbon-based electrode as a function of applied bias. Adapted and reprinted with permission from ref. 213.

Hu *et al.* observed that incorporating small amounts of CuS into their LTCB-layer leads to improved hole extraction and reduced recombination at the back electrode.<sup>214</sup> Similar effects were reported for different metal oxides embedded into the high temperature carbon paste. Tungsten oxide (WO<sub>x</sub>) nanoparticles were utilized to facilitate a more effective hole collection, which resulted in improved  $J_{\text{sc}}$ .<sup>215</sup> Jiang *et al.* conducted extensive research on the metal-oxide modifiers (Co<sub>2</sub>O<sub>3</sub>, CuO, MoO<sub>3</sub> and NiO) of carbon-based electrodes, which increased the work function and improved the hole selectivity at the perovskite/carbon interface.<sup>216</sup> Since these metal oxide additives are applicable for the HTCB-pastes, they can also be embedded into the LTCB-formulations.

Most of the reported perovskite solar cells with a carbon-based back contact electrode are fabricated in a “normal” configuration, which means that holes are collected at the carbon layer. The strategy of work function modification could also be extended to the upward shift (lowering work function). This could provide energetic alignment more favorable for electron extraction, and realization of “inverted” perovskite solar cell configurations.

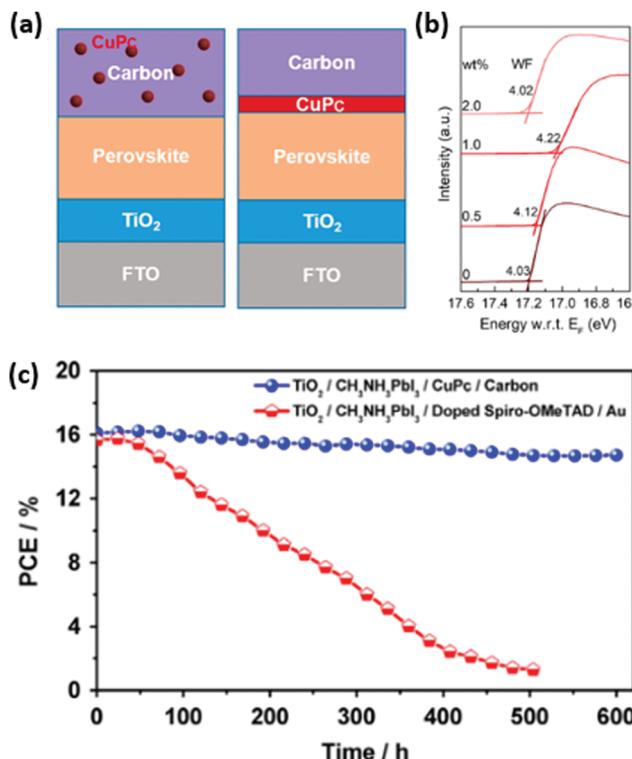


Fig. 26 (a) Schematics of integration of a copper phthalocyanine (CuPc) HSL into the cell stack by embedding it into the carbon paste and by introducing it as a planar interlayer. (b) UPS measurements of different contents of CuPc in the carbon-paste displaying ability to tune the work-function of the LTB-electrode by varying the CuPc thickness. (c) Stability tests of perovskite solar cells using CuPc and LTB-electrode vs. spiro-OMeTAD and Au-cathode. Adapted and reproduced with permissions from ref. 138 and 142.

A study conducted by Zhou *et al.* demonstrated that polyethylenimine (PEI) surface modified super-aligned cross stacked CNTs employed as counter electrodes for inverted planar PSCs allow for a better energy level alignment throughout the cell, consequently enhancing the photovoltaic performance of the cell.<sup>205</sup> These improvements were attributed to the impact of the PEI surface modification on the work function of the CNTs, which leads to reducing electron accumulation and suppressing interfacial charge recombination.

**6.2.2. Introducing an electron-blocking layer.** Poor contact between two foreign crystal lattices results in more occurring dangling bonds, causing inter-gap energy states at the perovskite surface which serve as recombination centers, lowering the quasi-Fermi level. Minimizing the surface recombination at this interface would decrease the need for high electrode work-function and, therefore needs to be pursued as a promising strategy to enhance HSL-free PSCs with a carbon-based electrode.

One way to reduce the non-radiative recombination in HSL-free cells is to introduce an electron-blocking layer at the carbon electrode surface. A blocking layer has a slightly different function from a charge-selective layer, although they often possess similar physical properties. The main requirement of a charge-blocking

layer is not to extract and conduct charges to the respective electrode, but to only effectively block the charge carriers from reaching the electrode of the opposite charge, which would otherwise result in higher recombination (*e.g.* hole-blocking c-TiO<sub>2</sub> layer). Therefore, a thin, compact, electron-blocking layer would be enough to significantly reduce surface non-radiative recombination enhancing the  $V_{oc}$  of the device.

In a recent work by Liu *et al.*, MABr was deposited on top of a MAPbI<sub>3</sub> absorber with an excess of PbI<sub>2</sub>, which predominantly located at the layer surface.<sup>217</sup> The excess of PbI<sub>2</sub> reacting with MABr can form MAPbI<sub>3-x</sub>Br<sub>x</sub> perovskite on top of MAPbI<sub>3</sub>, resulting in stacking structures. The authors found that due to the upshift of Pb 4f<sub>7/2</sub> and I 3d<sub>5/2</sub> core levels by 0.31 eV, both the valence band maximum and conduction bands were upshifted in the MAPbI<sub>3-x</sub>Br<sub>x</sub> layer (located at the MAPbI<sub>3</sub>/graphite interface) by 0.23 eV and 0.25 eV, respectively (Fig. 27). This intermediate layer facilitates easier extraction of holes, but more importantly, it forms an energy barrier for excited electrons diffusing towards the carbon-based electrode.

### 6.3. Improving contact to the perovskite

One of the strong suits of evaporated metal-electrodes is homogeneous and dense layer deposition, which facilitates efficient contact to the underlying charge selective layer. However, often the perovskite/carbon interface suffers from a low number of interfacial contact sites and poor adhesion, which seriously limits hole extraction and transport in the PV device.<sup>31</sup> Moreover, we believe that the introduction of barriers under the carbon-based electrode, that have been mentioned earlier in Section 2.1.3 will facilitate an even longer operational stability of the C-PSCs, in comparison to that of devices with metallic contacts.

Liu *et al.* found that the interfacial charge transfer between the perovskite and LTB-layer is highly influenced by the size of graphite particles.<sup>179</sup> Besides conductivity, the graphite size also has an influence on the perovskite/carbon contact area, which can be increased by decreasing the particle size (Fig. 28).<sup>178</sup> Thus, finding a careful balance between a high conductivity and an efficient hole-extraction would be optimal for reaching high PCEs with carbon-based electrodes. A poor contact between the perovskite and carbon-based electrode can also lead to larger anion migration towards the interface, which will increase hysteresis.<sup>141</sup> Addition of NiO-modifier also promoted a more intimate contact at this interface and enhanced the charge transfer rate.<sup>216</sup>

It is clear, that solvents in the LTB-pastes play a critical role in determining the properties of the final electrode and should be compatible with the perovskite and layers underneath the LTB-layer to form a smooth, intimate interface.<sup>218</sup> In contrast, there were reports that solvents present in the LTB-paste, which are not fully compatible with the perovskite layer,<sup>218</sup> can lead to significant damage of the perovskite morphology and worsen the interface characteristics. In some cases, LTB-paste can contain polar solvents (*e.g.* ethyl carbitol acetate or alcohols) that can dissolve the layers underneath, including perovskite since the paste is directly applied on top of the cell layers.



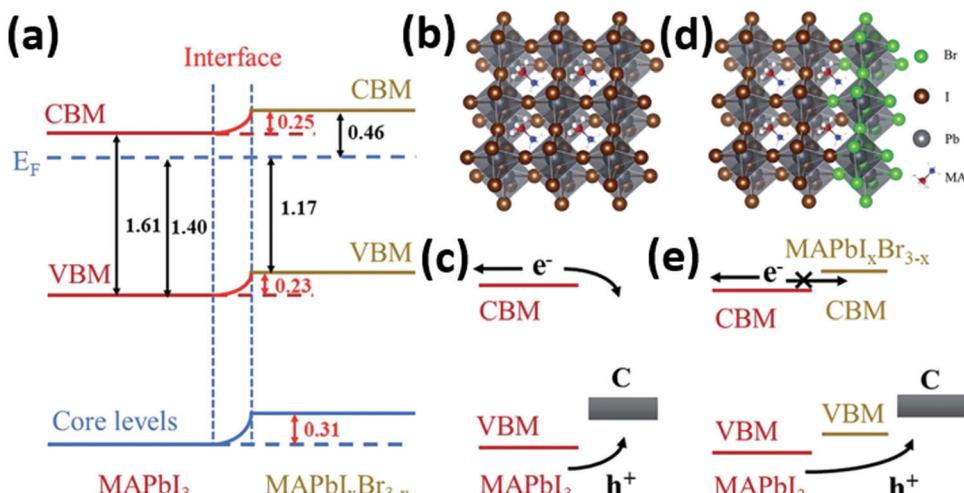


Fig. 27 (a) Energy level diagram of the stacked MAPbI<sub>3</sub>/MAPbI<sub>x</sub>Br<sub>3-x</sub> perovskite interface. (b) Crystal structure and (c) charge transfer diagram at the MAPbI<sub>3</sub>/carbon electrode interface. (d) Crystal structure and (e) charge transfer diagram of the stacked MAPbI<sub>3</sub>. Adapted and reprinted with permission from ref. 217.

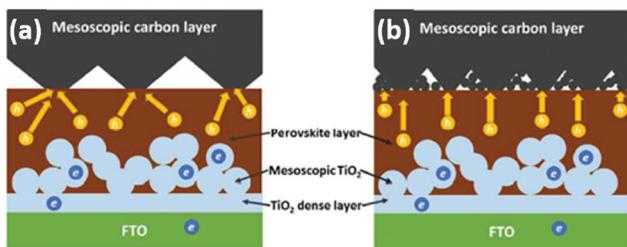


Fig. 28 Scheme of charge transfer in HTM-free CH<sub>3</sub>NH<sub>3</sub>PbI<sub>3</sub>/TiO<sub>2</sub> heterojunction solar cells with a carbon electrode, consisting of (a) large and (b) small graphite flakes. Adapted and reprinted with permission from ref. 178.

Hence, we advocate for LTCB-pastes with “harmless” solvents preserving dense and uniform morphology, resulting in lower interfacial resistance and higher stability.<sup>171</sup>

Similarly, Chen *et al.* in the work mentioned above, improved the electronic contact at the perovskite/carbon interface by growing smoother perovskite films of higher surface quality. The obtained 14.38% PCE was a record value for a HSL-free carbon-based PSC at that time.

Notably, carbon nanotubes manifest impressive electrical conductivity properties making them an excellent candidate for improving the hole conductivity of the carbon electrode and decreasing interfacial recombination resistance at the carbon/perovskite interface. In addition, many studies on C-PSCs have aimed at improving the electrical conductivity as well as enhancing the charge selectivity at the perovskite/carbon interface through the incorporation of different additives, the most promising among which are carbon nanotubes. The incorporation of CNTs in perovskite solar cells has demonstrated a noticeable improvement in device performance.<sup>219</sup>

For example, Wang *et al.* have opted for a “bridging method”, where they incorporated CNTs into both: the perovskite and

carbon electrode (Fig. 29), for the purpose of forming a better interface quality *via* CNT-bridges between these layers.<sup>188</sup> The cells showed an efficiency of over 15.7%, with a FF of around 70%.

An alternative strategy is to incorporate CNTs between the perovskite and carbon electrode layers. Ryu *et al.* introduced a MWCNT chlorobenzene dispersion into the complete LTCB-cells by a dripping method.<sup>220</sup> The MWCNTs, penetrating both the perovskite absorber and carbon electrode, created a pathway that allowed for more optimal carrier harvesting and transport properties, achieving a PCE of 13.57%.

Yet another approach for improved hole selectivity and reduced recombination could be obtained with the perovskite surface modification at the perovskite/carbon interface. Hou *et al.* applied guanidinium chloride into MAPbI<sub>3</sub> perovskite precursor solution.<sup>221</sup> The additive passivated trap states in the perovskite layer and reduced recombination rate at the perovskite/carbon interface (mesoscopic architecture, TiO<sub>2</sub>/ZrO<sub>2</sub>/carbon, infiltrated with perovskite solution). This led to *V<sub>oc</sub>* enhancement, from 0.88 V to 1.02 V. Rong *et al.* used ammonium chloride (NH<sub>4</sub>Cl) additive in the precursor solution, which also improved the optoelectronic quality of MAPbI<sub>3</sub> films.<sup>222</sup> Impressive efficiency of 15.6% was reported for the same mesoscopic, triple-layer scaffold architecture (TiO<sub>2</sub>/ZrO<sub>2</sub>/carbon).

Liu *et al.* applied cesium acetate (CsAc) treatment after the carbon deposition.<sup>223</sup> They suggested that the acetate salt could penetrate to the buried perovskite surface, modifying its composition, which grants a higher hole selectivity. The CsAc treatment improved the average PCE of HSL-free devices, from 12.6% to 15.3%, with a *V<sub>oc</sub>* value reaching 1.1 V. Another defect post-healing method was shown with dip-coating pre-fabricated carbon-based mesoscopic PSCs in trioctylphosphine oxide (TOPO) solution.<sup>224</sup> TOPO ligands act as a Lewis base, selectively adsorbing onto halide-deficient defect sites at the perovskite surface, reducing non-radiative recombination at the interface with a carbon electrode (Fig. 30). PCE improved after the treatment

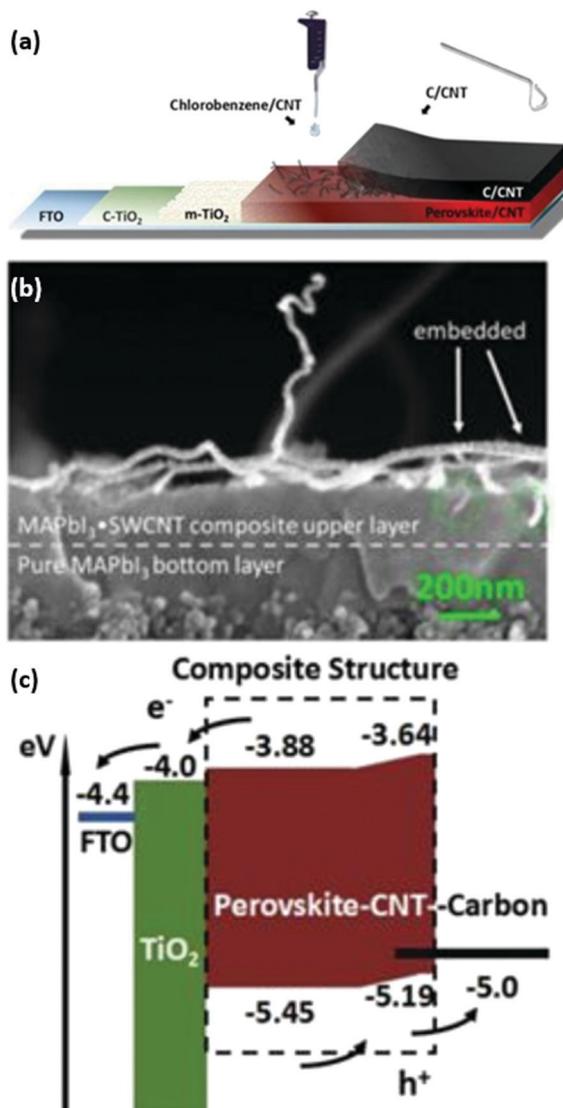


Fig. 29 (a) LTCB-device architecture with CNTs incorporated into the perovskite and electrode. (b) Cross-sectional SEM image and (c) energy band diagram of such device. Adapted and reprinted with permission from ref. 188.

from 11% to 12.8%, primarily due to the  $V_{oc}$  increase. In another example, Liu *et al.* applied polydimethylsiloxane (PDMS) encapsulant on carbon-based, HSL-free mesoscopic  $\text{MAPbI}_3/\text{TiO}_2$  heterojunction solar cells.<sup>225</sup> It was demonstrated that PDMS, during its solidification, fills the gaps in the mesoporous carbon film, which significantly improves the perovskite/carbon interface characteristics. The authors demonstrated that the charge extraction efficacy was improved and the recombination rate got reduced, which resulted in a 54% enhancement of photovoltaic performance, reaching 10.8% PCE.

Similarly, different strategies for improving electronic contact and charge selectivity at the interface with the carbon electrode were also demonstrated for the inverted perovskite solar cell architecture (p-i-n configuration). Luo *et al.* reported devices utilizing a back contact electrode based on transfer-printed

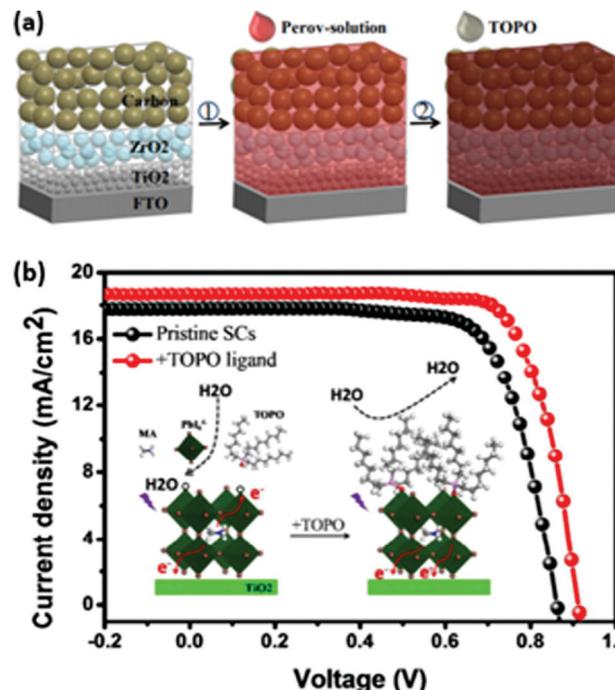


Fig. 30 (a) Schematic illustration of a mesoscopic perovskite solar cell fabrication process with a TOPO passivation step; (b) JV curves of a TOPO-passivated device and a reference cell, combined with a schematic drawing of the TOPO interaction with perovskite defects. Adapted and reprinted with permission from ref. 224.

carbon nanotubes.<sup>226</sup> In order to improve the efficacy of electron extraction from the perovskite layer, the authors applied  $\text{SnO}_2$ -coated cross-stacked carbon nanotubes ( $\text{SnO}_2@\text{CSCNT}$ ). The  $\text{SnO}_2$  coating improved the PCE from 10.7% to 14.3%, with significantly reduced hysteresis. Furthermore, flexible PSCs applying a  $\text{SnO}_2$ -modified CNT electrode were demonstrated, reaching 10.5% efficiency.

Recently, Babu *et al.* demonstrated a Cr buffer layer inserted between the electron transport layer and carbon electrode as a way to obtain Ohmic contact at that interface and efficient

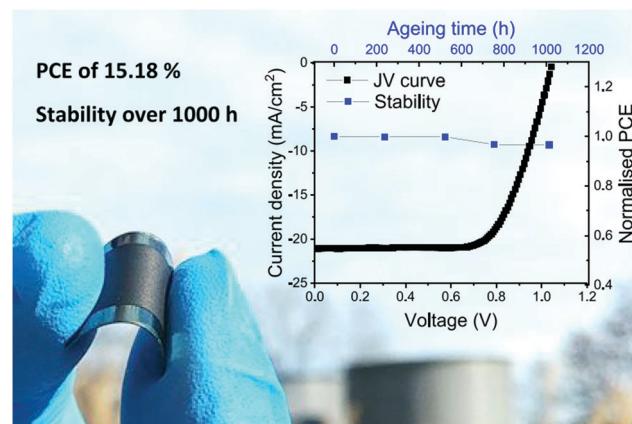


Fig. 31 J-V curve and performance evolution during aging test of a flexible inverted PSC with a carbon back contact electrode. Adapted and reprinted with permission from ref. 163.

charge collection in p-i-n devices.<sup>163</sup> They reported 15.18% PCE for a flexible perovskite solar cell (Fig. 31) with a large active area of 1 cm<sup>2</sup>. Furthermore, a Cr interlayer was also applied in n-i-p configuration, inserted between the hole transport layer and carbon electrode. It resulted in an improvement in fill factor, assigned to improved electronic contact, yielding 12.06% PCE (flexible PSC, 1 cm<sup>2</sup> active area).

## 7. Conclusions

### 7.1. Summary

Most of the state-of-the-art perovskite solar cells use metal electrodes as a back contact, attempting to bridge cell efficiencies closer to the radiative limits. However, in this review we point out that poor stability of these metallic layers, limited up-scalability potential, high costs and negative environmental impact hinder further development of perovskite PV in the direction of commercialization. Therefore, carbon-based electrodes have been proposed to alleviate these issues and to fulfill the potential of perovskite to become the next generation PV technology.

Comparing between high-temperature and low-temperature cured carbon-based layers, the latter ones come along with multiple processing advantages: (1) easier integration of hole-selective layers, owing to the electrode low curing temperature, which is compatible with perovskites and HSLs, (2) possibility to implement advanced crystallization and passivation techniques (in comparison to poorly controlled crystallization after the solution infiltration in C-PSCs with high-temperature cured electrodes), (3) applicability to flexible substrates and roll-to-roll manufacturing and (4) shorter processing time. Based on the multiple reports showing PCEs above 17% (with 17.8% certified value), we postulate that low-temperature carbon electrodes can be used to produce high-efficiency PSCs, while simultaneously being a more chemically stable, up-scalable, cost-efficient and sustainable alternative to conventional metal contacts.

We summarize different paste formulations present in the literature, displaying the effect of various additives, solvents, binders and carbon powder compositions (e.g. carbon-black to graphite ratios) on the final film properties. Literature on carbon-based electrodes suggests that they can be deposited by blade-coating, press-transfer, screen-printing methods and even ink-jet printing or spray coating all of which are up-scalable techniques and can be implemented to fabricate large area modules.

Furthermore, we propose effective strategies that have been reported for low-temperature carbon-based electrodes, to improve the layer conductivity, charge selectivity and contact between carbon and the layer underneath: (1) a higher conductivity can be reached by modification of graphite crystals and its portion in the paste, surface functionalization and foreign atom doping. (2) Enhancing charge selectivity is suggested to be improved by modification of the work-function and integration of electron-blocking layers at the perovskite/carbon interface.

(3) Finally, a better contact at the carbon surface can be obtained by producing smooth pin-hole free films, introducing carbon-nanotubes to facilitate better interfacial charge transfer and tuning the graphite size.

### 7.2. Perspective

In order to overcome the voltage loss of still 200 mV compared to the highest-efficiency cells, two conditions have to be fulfilled: non-radiative surface recombination at the back-contact has to be reduced and the valence (for n-i-p cells) or conduction (for p-i-n cells) band of the back-contact have to match the energy levels of the perovskite absorber, which can be achieved by tuning the carbon-based electrode or by adding a selective layer in between. In this review, different strategies have been proposed: to introduce an HSL as an electron-blocking and hole-conducting layer between the perovskite and carbon-based electrode or to modify the work-function of the carbon electrode itself.

To increase the photo-current and fill factor of the C-PSCs, the efficient extraction of holes from the perovskite to graphite is required, highlighting the necessity to find a method to reach this goal. The low-temperature cured carbon-based layers display clear advantages of higher flexibility in implementing the strategies mentioned above, originating from the capability of the LTCB-layer to be applied before or after the perovskite deposition. In particular, this allows for new options for functionalizing the interface at the perovskite/carbon contact. It is not surprising that in the last few years PSCs with low-temperature cured electrodes have already reached higher efficiencies than the ones with high-temperature treated contacts.

Overall, we emphasize that the vast knowledge acquired by the perovskite community on methods to fabricate high-efficiency solar cells so far can be readily transferred to low-temperature carbon-based perovskite solar cells, which represents strong potential to bring perovskite technology closer to the PV market.

## Author contributions

D. B., L. W., S. M., S. Z. and A. H. proposed the idea of summarizing the recent progress in low-temperature carbon-based electrodes in PSCs and identifying their advantages. B. Y. together with D. B. and A. H. described the stability disadvantages of conventional PSCs as well as reported stability measurements of carbon-based PSCs. S. M. together with L. W. analyzed the environmental concerns of conventional PSCs, while J. L. together with L. W. conducted a literature research on the cost analysis of PSCs. D. B., J. L. and B. Y. described the differences between the low- and high-temperature carbon based devices, as well as advantages of crystallization control, and ability to introduce a wider range of HSLs. K. W., V. B. and D. B. further elaborated how these low-temperature carbon-based electrodes can be applied on flexible substrates and allow for faster manufacturing process. B. X. and H. P. together with D. B. summarized the low-temperature carbon paste formulations.



The carbon layer deposition methods were described by K. W., V. B., D. B., B. X. and B. Y. Among the proposed strategies to improve low-temperature carbon-based electrodes, D. B., S. Z. and L. W. analyzed the conductivity improvement methods. K. W., V. B., D. B., L. W., S. Z. and A. H. contributed to the description of charge selectivity improvement strategies. K. W., V. B., S. Z. and D. B. identified effective methods to improve the perovskite/carbon interface. A. H., A. H. and D. B. summarized the findings and provided the perspective. All authors contributed to the study with valuable discussions and reviewed the manuscript. This work is a result of the well-coordinated collaboration between European Research institutes, Universities and industrial partners.

## Conflicts of interest

K. W. is an employee of Saule Tech, A. H. and H. P. are the co-founders of Dyenamo AB, Bo Xu is an employee of Dyenamo AB.

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