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# Linking interfacial work of deformation from deconvoluted macro-rheological spectrum to early stage healing in selected polyurethanes†

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The use of rheology and terminal flow relaxation times to predict healing behavior at long healing times is by now quite well accepted. In this work we go one step further and explore the use of macro-rheology (in particular the stored work of deformation) to predict the early stage interfacial healing properties (fracture resistance) of a set of self-healing polyurethanes. The interfacial healing is measured by single edge notch fracture experiments, using short healing times and a low healing temperature to exclude the effect of long range molecular motion on mechanical properties restoration. The systems based on aromatic diisocyanates show high fracture resistance after healing, while very limited restoration of the mechanical properties is observed for aliphatic and cycloaliphatic based polyurethanes. Linear sweep rheology and time-temperature-superposition allow obtaining the macro-rheological master curve and the mechanical relaxation spectra ( $H(t)$ ). The application of a recently established deconvolution protocol to the  $H(t)$  gives the characteristic relaxation times and stored works of deformation associated to individual dynamic processes such as segmental motion, reversible bonds, and terminal flow. It is found that the calculated stored works of deformation related to the reversible bond relaxation reproduce the trend observed by fracture resistance at healed interfaces and reveal a qualitative correspondence between reversible bonds work of deformation and interfacial healing fracture resistance. Moreover, the method seems to point to the existence of a threshold interfacial work of deformation below which no efficient load transfer can be observed.

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## 1. Introduction

The field of self-healing polymers has rapidly grown in recent times driven by increasing environmental concerns related to plastic overconsumption that boost the scientific research towards the development of alternatives to current commodities polymers, including functional and self-healing systems.

Many proofs of concepts have been presented exploiting the intrinsic healing approach. Intrinsic healing is addressed by the molecular design of the network in opposition to extrinsic systems which rely on the present of discretely dispersed carriers containing the healing agent.<sup>1,2</sup> In order to exploit the intrinsic self-healing ability two requirements have to be fulfilled: (i) high density of reversible bonds to deconstruct and reconstruct the broken interface and (ii) sufficient chain

mobility to facilitate local flow at the damage site. A number of reviews summarize how the incorporation of different reversible chemical and physical bonds can successfully lead to the production of self-healing polymers.<sup>3–6</sup> A careful analysis of these works evidences that the use of van der Waals,<sup>7,8</sup>  $\pi$ - $\pi$  stacking<sup>9</sup> and/or microphase separation<sup>10</sup> could be used to turn commodity-like systems into self-healing variants without the introduction of severe chemical modifications.

The healing action in intrinsic systems occurs in two successive stages: initial interface restoration by reversible bonds swapping and subsequent interphase healing by macromolecular diffusion.<sup>11</sup> In this work we aim to clarify the contribution of non-covalent reversible bonds to the initial recovery of interfacial strength. In a previous study we showed evidences that the incorporation of multiple reversible moieties (namely hydrogen bonding and disulphide exchange) with different association/dissociation kinetics strongly influence the early steps of healing, in which fast hydrogen bonding relaxation dynamics determines initial tack, and affect long term healing, when the opening of sulphur-sulphur bonds allows long range motion.<sup>12</sup> This issue is critical because it defines the design

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boundaries between systems with a very high density of reversible bonds but a sluggish terminal relaxation and polymers with fast terminal relaxation but a sparse physical network. Macro-rheology has been used to estimate the timescale of interphase diffusion and macroscopic crack closure by comparing the kinetics of these processes to the supramolecular bond lifetime ( $\tau_b = 2\pi/\omega_{cr}$ ) of embedded reversible interactions.<sup>7,13</sup> However, this method does not offer insights on the processes that govern the initial interface strength restoration. In this work we try to bridge this gap and explore how to extract more information from the rheological tests that can be used to predict early stage macroscopic healing strength. To do this we extend our deconvolution protocol of the mechanical relaxation spectrum constructed by rheology that allow to isolate the dynamics of individual molecular features,<sup>14</sup> including the calculation of the stored work of deformation.

We explore the use of this approach to predict early stage interfacial healing properties of a set of polyurethanes, for which the recombination of reversible bonds at the deconstructed interface defines the initial tack. To this purpose, we use four diisocyanates (diphenylmethane 4,4' diisocyanate **MDI**, 1,4-phenylene diisocyanate **PPDI**, hexamethylene diisocyanate **HDI**, 4,4'-methylenebis(cyclohexyl isocyanate **HMDI**) of increasing aromaticity to selectively incorporate multiple reversible interactions in the network (hydrogen bonding from the urethane linkage and aromatic interactions from the isocyanates) and to study the effect of the monomer symmetry on the fracture resistance restoration using the single edge notch tensile (SENT) protocol.<sup>15–17</sup>

## 2. Experimental section

### 2.1. Materials

2-Ethyl-1,3-hexanediol (EHD, 99%), diphenylmethane 4,4' diisocyanate (MDI, 98%), 1,4-phenylene diisocyanate (PPDI), hexamethylene diisocyanate (HDI, >98%), 4,4'-methylenebis(cyclohexyl isocyanate) (HMDI, mixture of isomers 90%), dibutyltin dilaurate (DBTDL, 95%) were purchased from Sigma-Aldrich. CroHeal 2000 (equivalent molecular weight 2000 g mol<sup>-1</sup>) was kindly provided from Croda Nederland B.V.

### 2.2. Synthesis of segmented polyurethanes

Four polyurethanes were synthesized by single shot technique reacting CroHeal 2000, EHD and different diisocyanates (MDI, PPDI, HDI, HMDI). The diisocyanates were selected considering increasing level of aromaticity HMDI = HDI < PPDI < MDI, and symmetry HMDI  $\cong$  MDI < PPDI  $\cong$  HDI. For all the polymers the molar ratio of the hydroxyl chemical functionalities OH (CroHeal2000):OH (EHD) was kept fixed at 1:0.6. 10% molar excess of NCO was used to carry the reaction to full completion. Samples are coded by the name of the isocyanate used followed by the addition '-p' to distinguish the polymer from the monomer (e.g. MDI based polymer is coded as MDI-p). Below we report the synthesis of polymer MDI-p. Analogous procedures were followed for the other polymers in this study. Details on their syntheses are reported in the ESI.† The molecular structure of

the segmented polyurethanes is schematically represented in Fig. 1.

CroHeal 2000 was heated for 1 hour at 90 °C to reduce the intrinsic viscosity of the monomer (melting the crystalline domains). Subsequently 90.0 g (45.0 mmol) were transferred to a 300 mL polypropylene cup. 3.95 g of EHD (27.0 mmol) were then added to the cup. 31.64 g (79.20 mmol) of MDI were weighted in a separate 25 mL polypropylene cup, purged under nitrogen inert environment and heated 1 hour at 60 °C to reduce its intrinsic viscosity (melting crystalline domains). The MDI was rapidly poured into the main reaction cup (containing CroHeal 2000 and EHD). The mixture was sheared under vacuum at 2300 rpm for 135 seconds using a vacuum assisted high speed mixer (SpeedMixer™ DAC 400.2 VAC-P). The application of high vacuum (pressure below 100 mbar) turned out to be critical for the formation of bubble-free polymers. The mixture was then transferred to a 20 × 20 × 0.2 cm PTFE mold, equilibrated for 30 minutes at ambient conditions and subsequently cured overnight at 60 °C. The obtained bulk polymers were then equilibrated for 1 week at ambient conditions before testing.

The degree of completion of the polyurethane synthesis was monitored by Attenuated Total Reflectance Fourier transform Infrared (ATR-FTIR) analysis by monitoring the appearance of the characteristic carbonyl stretching absorption peak at  $\approx 1700$  cm<sup>-1</sup> and the disappearance of isocyanate absorption peak at about  $\approx 2270$  cm<sup>-1</sup>. ATR-FTIR spectra of all synthesized polymers are shown in Fig. S1 (ESI†).

### 2.3. Characterization methods

**2.3.1. Rheology and mechanical relaxation spectrum deconvolution protocol.** Temperature sweep and frequency sweep tests were performed to build the rheological master curves, applying the time-temperature-superposition principle (TTS). A Haake Mars III rheometer (ThermoScientific) was used, employing a parallel plate geometry (plate diameter = 8 mm). The data obtained at different temperatures were shifted using Reptate software (University of Leeds, gplv3 license). On the basis of preliminary strain amplitude sweep measurements the shear strain amplitude was set to 0.1%. Frequency sweep experiments from 10 to 0.1 Hz were performed with steps of  $T = 10$  °C over the temperature range from -20 to 200 °C for MDI-p and PPDI-p, steps of  $T = 10$  °C were used for HDI-p in the range -20 to 170 °C and steps of  $T = 10$  °C were used for HMDI-p in the range -20 to 70 °C. The isotherms were shifted to the reference temperature  $T_R = 30$  °C, corresponding to the temperature at which interfacial healing was observed and tested for all systems.

The mechanical relaxation spectrum  $H(t)$  was constructed applying the non-linear regression method developed by Honerkamp and Weese.<sup>18,19</sup> The source code of the algorithm can be found in the CPC Program library.<sup>20</sup> In this protocol, the minimum and maximum relaxation times are pre-selected by the user. In our case we simply set  $\tau_{min} = \frac{1}{\omega_{max}}$  and  $\tau_{max} = \frac{1}{\omega_{min}}$  where  $\omega_{max}$  and  $\omega_{min}$  are the highest and the lowest angular frequency in the modulus data, as suggested in the library user manual. The deconvolution protocol was performed following the procedure



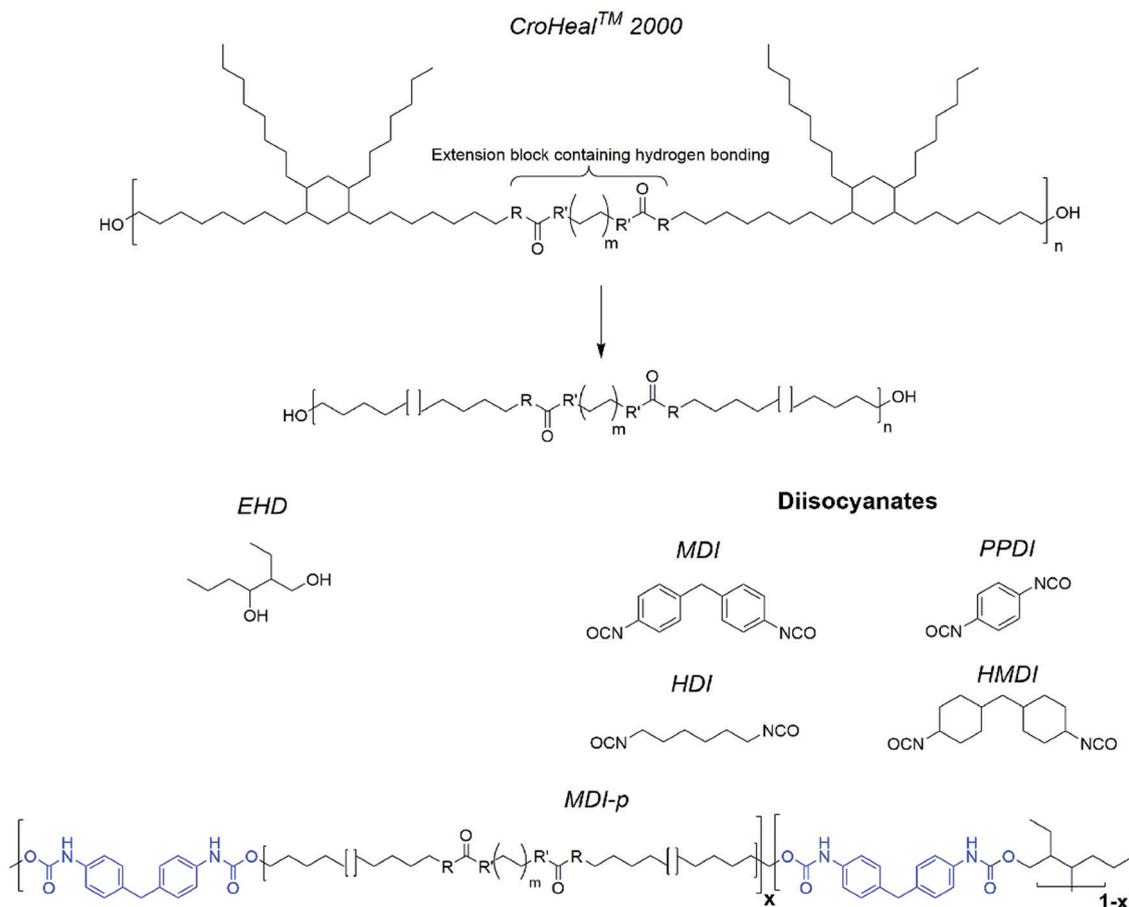


Fig. 1 Monomers used and molecular structure of synthesized segmented polyurethanes (MDI-p is showed as mode of example).

reported in ref. 14. For all the deconvoluted spectra the coefficients of determination of the reconstructed mastercurve ( $|r_G^{-2}|$  and  $|r_G^{-2}|$ ) exceed 0.9 confirming the high quality of the fit. Details of the protocol, including the calculation of stored work of deformation ( $W$ ) are reported in the ESI.†

**2.3.2. Extension dynamic mechanical analyses (DMA).** Dynamical mechanical experiments were carried out on a strain-controlled Q800 (TA Instruments) in tension mode. The gauge length used was  $\approx 10$  mm. The sample thickness was uniform per sample but varied between polymer grades between 0.45 to 1.0 mm. Temperature sweep analyses were carried out over the temperature range from  $-50$  °C to 80 and 120 °C (depending on the thermal stability of the polymer) using a heating rate of  $2.0$  °C  $\text{min}^{-1}$ . All the tests were run at the fixed amplitude of  $10$   $\mu\text{m}$ , which falls within the linear viscoelastic regime as established by the preliminary strain amplitude analyses.

**2.3.3. Single edge notch tensile (SENT) fracture test.** SENT fracture experiments were performed using an Instron Universal Tensile Testing machine equipped with a 1 kN load cell. Rectangular samples ( $70 \times 20$  mm) were cut with a die from 2 mm thick polymer sheets. A sharp pre-notch with length of 10 mm was made from the middle of the longest edge, perpendicularly to it, using a razor blade. The polymers were cooled for 1 hour at  $2$  °C prior to the damaging procedure, in order to produce sharp cut surfaces.

The mechanical tests were performed at a cross-head speed of  $0.5$   $\text{mm s}^{-1}$ , allowing detailed observation of crack tip opening. The testing temperature was controlled using an environmental chamber (Instron) with a glass window using evaporating liquid nitrogen and was set at  $10$  °C. Optical snapshots at a frequency of 10 Hz were taken during testing using an Optomotive Velociraptor camera in order to observe crack opening and propagation. The camera was placed on a vibration damping tripod at  $\approx 50$  cm of distance from the sample.

The fracture properties were determined using the J-integral analysis method, as described elsewhere.<sup>12,15,21</sup> Critical fracture resistance values,  $J_C$  were calculated as:

$$J_C [\text{kJ m}^{-2}] = \frac{\eta U_C}{b(w-a)} \Big|_{u_C}$$

where  $U_C$  is the energy calculated as the area under the load-displacement curves at the terminal displacement  $u_C$  when the samples fail,  $\eta$  is the proportionality factor (a value of 0.9 was selected according to literature<sup>21</sup>);  $b$ ,  $w$ ,  $a$  are the sample thickness, sample width and pre-crack length respectively.

**2.3.4. Preparation of healed specimens.** Specimens for healing experiments were taken from pre-notched  $70 \times 20$  mm samples used for SENT testing. The samples were completely



fractured following a trajectory extending the pre-notch path, perpendicularly to the longest edge of the rectangular specimen. The fractured samples were immediately positioned in a PTFE mold and healed using a recirculating furnace for  $\approx 3.6 \times 10^3$  s (1 hour),  $8.64 \times 10^4$  s (1 day) and  $1.2 \times 10^6$  (2 weeks) at 30 °C. During the healing procedure the actual pre-notch area was prevented to heal by placing a thin PTFE foil in between the broken surfaces, to avoid cross interface contact being re-established.

The healed samples were mechanically tested following the SENT procedure described in Section 2.3.3 to obtain a value for the critical fracture resistance after healing  $J_C^{\text{interfacial}}$ .

**2.3.5. Preparation of healed specimens.** Thermal properties were determined by thermogravimetric analysis (TGA) and differential scanning calorimetry (DSC). TGA analyses were performed from room temperature to 600 °C, under dry nitrogen atmosphere at 10 °C min<sup>-1</sup> heating rate using a PerkinElmer TGA 4000. DSC measurements were performed under dry nitrogen atmosphere at 10 °C min<sup>-1</sup> heating and cooling rates over the range from -40 °C to 200 °C using a PerkinElmer Pyris Sapphire DSC. The glass transition temperature ( $T_g$ ) was determined using the inflection point method.

Table 1 reports the results of TGA analyses and the DSC- $T_g$  (glass transition). All polymers reported a high thermal stability (5% weight loss at  $T > 350$  °C).

All systems showed a single endothermic peak in the DSC curve located between -5 and 10 °C which is attributed to the main chain segmental mobility. The relatively low content of EHD monomer feed is responsible for the absence of a high temperature first order thermal transition, generally attributed to the melting of the hard segment (chain extender + isocyanate).<sup>22,23</sup>

**2.3.6. Attenuated total reflectance infrared spectroscopy (ATR-FTIR).** Attenuated total reflectance Fourier transform infrared spectroscopy was used to follow synthesis completion and to study the state of hydrogen bonding in the proposed segmented polyurethanes. Each reported ATR-FTIR spectrum is the average of 32 scans over the wavenumber region 4000–500 cm<sup>-1</sup> with resolution of 1 cm<sup>-1</sup>. All the spectra are available in Fig. S1 (ESI†).

**2.3.7. Micro-attenuated total reflectance FTIR ( $\mu$ ATR-FTIR).**  $\mu$ ATR-FTIR spectra were recorded using a PerkinElmer Spotlight 200i FTIR microscope system. A diamond ATR crystal was utilized. The spectra were collected with a 4 cm<sup>-1</sup> spectral resolution and 16 accumulations, scanning an area of 300 to 500  $\mu\text{m}^2$ , in the wavenumber region 4000–750 cm<sup>-1</sup>. The analysis was performed

at a constant contact pressure between the ATR crystal and the sample. The spectral density was set at 1.56  $\mu\text{m}$  allowing the imaging of  $\mu$ -size network heterogeneities.

Principal component analysis (PCA) was applied to identify spectral heterogeneities. The PCA is based on the generation of 8 principal spectral scores. The analysis was performed using the built-in function of the ImageSpectra software (PerkinElmer).

## 3. Results and discussion

### 3.1 Deconvolution protocol to unveil individual relaxations and related work of deformation

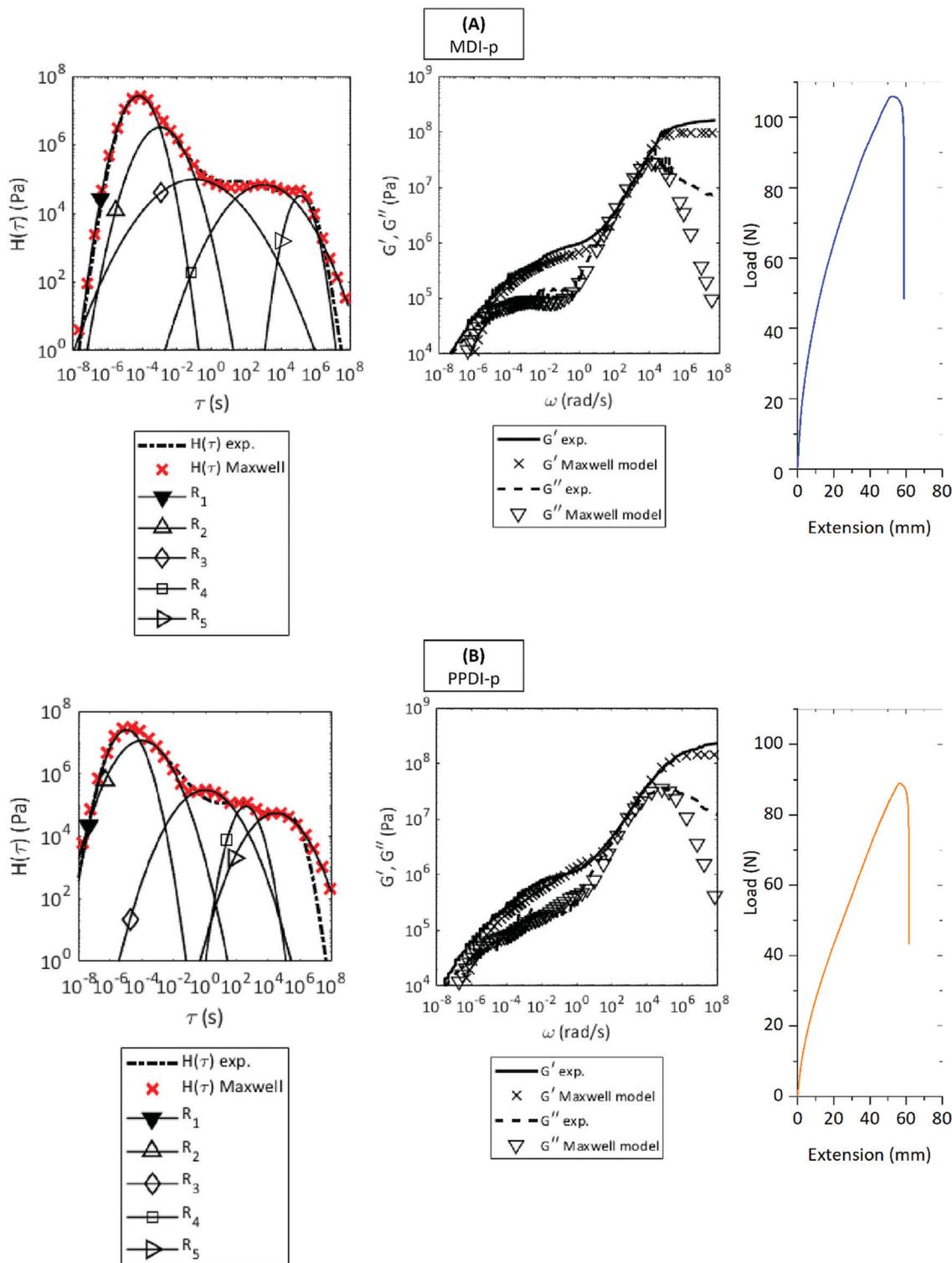
The first step to establish the relationship between the dynamics and energy storage of individual relaxation processes and the interfacial healing fracture resistance is the application of the deconvolution protocol to the mechanical relaxation spectrum following previous reports.<sup>14</sup>

The resulting deconvoluted  $H(t)$  with identified individual time constants are shown in Fig. 2 for the aromatic-based polyurethanes (MDI-p and PPDI-p) and in Fig. 3 for the aliphatic-based polyurethanes (HDMI-p, HDI-p). Starting from a known polymer architecture the method allows to assign physical meaning to the relaxation mechanism identified through the deconvolution. Fig. 2A shows that five dominant relaxation mechanisms are obtained for MDI-p. Polyurethanes synthesized from a mixture of a high molecular weight diol (polyol), a low molecular weight diol (chain extender) and a diisocyanate may present a segmented structure. The segmented structure is physically described as hard phase regions, enriched with chain extender + diisocyanate segments, intercalated in a soft matrix, enriched of polyol + diisocyanate segments.<sup>24,25</sup> The phase separated architecture is responsible for the elastomeric properties of this class of material, where the hard phase works as stable physical crosslinks of the polymer network. These preliminary considerations are essential to infer the physical meaning of the five relaxation mechanisms deconvoluted for MDI-p. The first dynamic event ( $R_1$ ) is associated to main chain segmental motion occurring in the soft matrix of the segmented polyurethane microstructure. As inferred from the molecular structure of this system, reversible bonds (hydrogen bonding and aromatic  $\pi$ - $\pi$  stacking) are present in the soft phase. They are responsible of the second relaxation event ( $R_2$ ). The transition part of the spectrum ( $10^3$  s  $< \tau < 10^5$  s) is dominated by relaxation of the hard blocks dispersed in the segmented microstructure. Hard blocks segmental motion ( $R_3$ ) is followed by hydrogen bonds and aromatic  $\pi$ - $\pi$  stacking relaxations ( $R_4$ ). Thermoplastic elastomers present a strong but transient cross-linked network, therefore terminal relaxation can be observed but is very sluggish ( $R_5$ ). The elastomeric nature of MDI-p is confirmed by its mechanical behaviour, tested by SENT in the pristine state and shown as auxiliary data in Fig. 2A. Analogous arguments follow the deconvolution of PPDI-p (Fig. 2B) which shows five dominant relaxation mechanisms and mechanical features typical of a thermoplastic elastomer.

**Table 1** Thermal analyses results. The increase in the aromatic character of the diisocyanate monomer provokes an increase in thermal stability and retards main chain segmental mobility

Polymer	TGA-5% weight loss (°C)	DSC- $T_g$ (°C)
MDI-p	353	5.2
PPDI-p	361	10.0
HMDI-p	353	-5.5
HDI-p	344	0.4



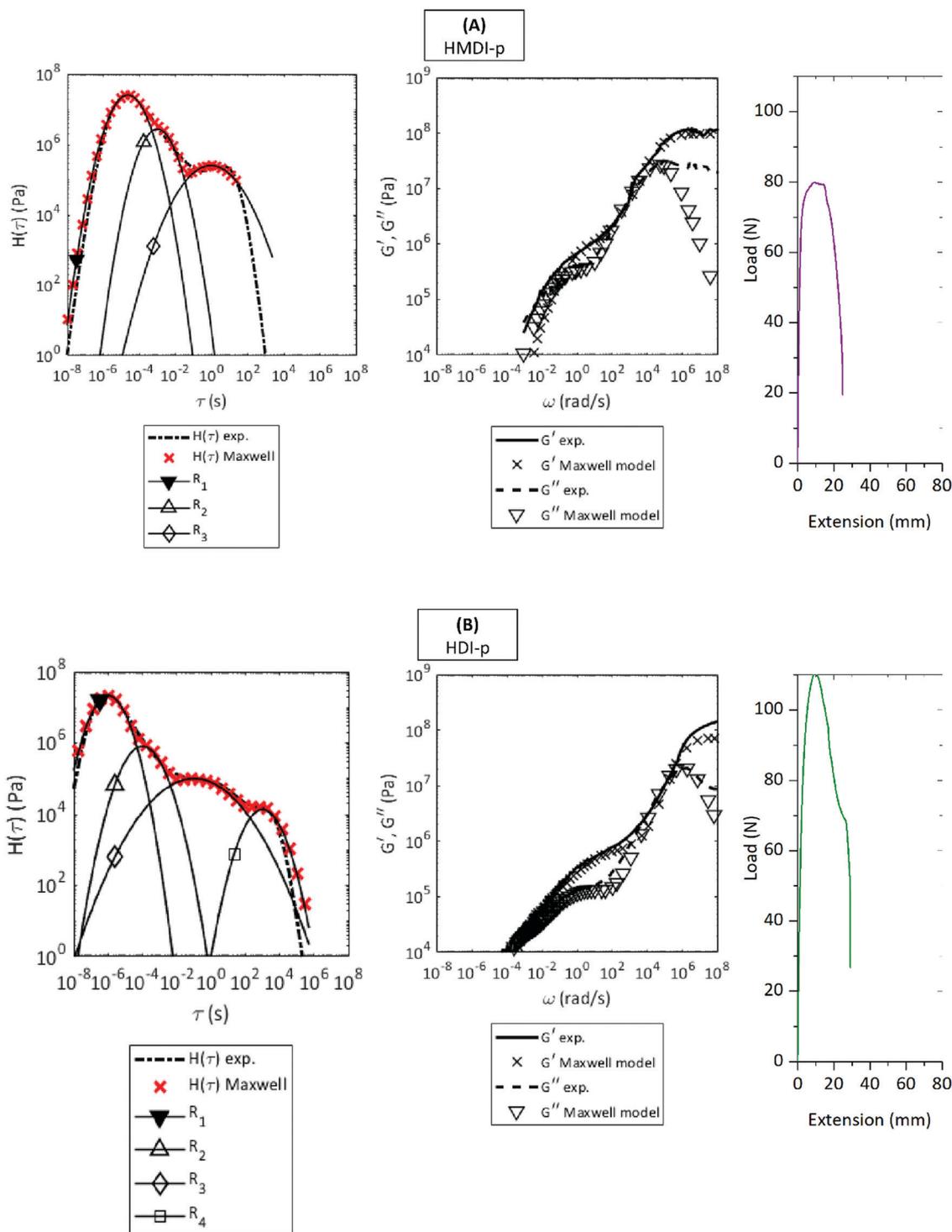


**Fig. 2** Deconvoluted relaxation spectra, mastercurve reconstruction and SENT load–displacement data of MDI-p and PPDI-p. (A) MDI-p (B) PPDI-p. For both polymers the method identifies five dominant relaxation mechanisms.  $R_1$  = soft phase segmental mobility.  $R_2$  = soft phase reversible bonds disjunction.  $R_3$  = hard phase segmental mobility.  $R_4$  = hard phase reversible bonds disjunction.  $R_5$  = terminal relaxation. Mechanical properties are typical of thermoplastic elastomers. The mastercurves are shifted at the reference temperature  $T_R = 30$  °C.

The deconvolution procedure applied to HMDI-p results in a radically different outcome (Fig. 3A). In this case only three main relaxation mechanisms can be identified with a complete

disappearance of the wide transient region previously observed for MDI-p and PPDI-p. The deconvolution spectrum resembles the one of lightly crosslinked systems reported elsewhere.<sup>14</sup>





**Fig. 3** Deconvoluted relaxation spectra, mastercurve reconstruction and SENT results of HMDI-p and HDI-p. (A) HMDI-p. The deconvolution method identifies three dominant relaxation mechanisms.  $R_1$  = main chain segmental mobility.  $R_2$  = reversible bonds disjunction.  $R_3$  = terminal relaxation. (B) HDI-p. The deconvolution method identifies three dominant relaxation mechanisms.  $R_1$  = main chain segmental mobility.  $R_2$  and  $R_3$  = reversible bonds disjunction and quasi-crystalline melting.  $R_4$  = terminal relaxation. The mechanical properties are typical of thermoplastic polymers.

The first dynamic process is attributed to main chain segmental motion ( $R_1$ ), followed by a temporary restriction of mobility associated to entanglements and/or physical interactions ( $R_2$ ) (e.g. hydrogen bonds) and rapid terminal relaxation ( $R_3$ ). The

absence of segmented structure and rubbery elasticity for HMDI-p is confirmed from static mechanical properties (auxiliary data in Fig. 3A). Moreover, extensional DMA data for HMDI-p (Fig. S4, ESI<sup>†</sup>) show a complete absence of the rubbery



plateau and terminal flow occurring at  $\approx 60$  °C, a typical feature of linear unentangled/lightly entangled networks.<sup>9,26</sup> A similar description applies to the deconvolution of HDI-p, for which an optimal fit is found when assuming four relaxation mechanisms (Fig. 3B). The additional relaxation mechanism located in the transient regime is related to the stacking of highly linear and symmetric HDI segments that determines crystalline-like ordered structures.<sup>27</sup> Nevertheless in analogy with HMDI-p, because of no aromatic entities being present there is no segmented microstructure. In parallel with HMDI-p, the mechanical SENT data of the pristine HDI-p sample shows the typical behaviour of linear networks and appearance of terminal flow in DMA analysis at about  $\approx 100$  °C (Fig. S5, ESI†).

Table 2 shows the quantitative data extracted from the deconvolution protocol in terms of kinetics of the relaxation transition ( $\tau$ ) and stored work of deformation ( $W$ ). The information regarding the physical nature of the individual relaxation mechanisms is conveyed through the parameters subscript and superscripts:  $W_{sp}^{seg}$  (soft phase segmental mobility)  $W_{sp}^{rev}$  (soft phase reversible bonds)  $W_{hp}^{seg}$  (hard phase segmental mobility)  $W_{hp}^{rev}$  (hard phase reversible bonds)  $W_t$  (terminal relaxation).  $W_{interfacial}$  corresponds to the sum of all the works of deformation associated to reversible ligands relaxation ( $W_{interfacial} = W_{sp}^{rev} + W_{hp}^{rev}$ ). This choice is based on the assumption that segmental motion/short range conformational re-arrangements do not contribute to the reconstruction of the broken interface. MDI-p and PPDI-p present comparable soft and hard segmental relaxation timescales. The slightly lower values for the kinetic parameters of PPDI-p are attributed to the higher rigidity and symmetry of the PPDI diisocyanate monomer when compared to MDI. The work of deformation related to reversible bonds in the soft phase ( $W_{sp}^{rev}$ ) is higher for PPDI-p. Such an increase can be explained considering the rigid segment design and in particular to the reduced periodic distance among reversible bonding moieties (aromatic units and urethane linkages).

Beyond the reduced number of relaxation mechanisms obtained by the deconvolution process, HMDI-p deviates from MDI-p and PPDI-p in its rapid terminal relaxation kinetics ( $\tau_t \cong 1$  s) and the reduced interfacial work of deformation ( $W_{interfacial}$ ), an expected result when considering the absence of  $\pi$ - $\pi$  stacking interactions among aromatics and therefore the formation of a weaker transient network. For the second aliphatic polyurethane (HDI-p), as qualitatively discussed in the previous paragraph, the slower terminal relaxation ( $\tau_t \cong 10^3$  s) when compared to HMDI-p is attributed to HDI monomer stacking and the strong chemical compatibility between HDI monomer

and the CroHeal 2000 segment, which yields a denser transient network (higher chain packing and friction). Nevertheless, the two aliphatic systems maintain comparable levels of  $W_{interfacial}$  indicating that the physically crosslinked networks constituted by fully aliphatic chains are able to store similar amount of energy related to reversible interactions.

The effect of the diisocyanate chemistry on the macromolecular segmentation in turn responsible for microphase separation in polyurethanes was further investigated by dedicated  $\mu$ ATR-FTIR analysis. Fig. 4 reports the infrared spectra maps obtained upon application of principal component analysis of the four polyurethanes. The aromatic-based polyurethanes (MDI-p and PPDI-p) show a continuous phase (reported in grey color) intercalated by a micron-sized dispersed phase (yellow color). The aliphatic and linear polyurethane (HDI-p) presents a homogeneous microstructure (no dispersed phase is probed), while HMDI-p shows some phase separation, yet to a lower extent and smaller dimension than in the case of MDI-p and PPDI-p. The analysis of the infrared spectra traces corresponding to the continuous (points numbered as '1' in Fig. 4) and the dispersed phases (points numbered as '2' in Fig. 4) gives insights into the molecular differences between the two probed regions. All shifts and intensity variations point towards a microstructure composed of a soft continuous phase (enriched in CroHeal + MDI segments) and hard and urea-rich heterogeneities (enriched in EHD + MDI segments). For MDI-p the carbonyl band (C=O) probed for the continuous phase at  $1695\text{ cm}^{-1}$  shifts to  $1643\text{ cm}^{-1}$  due to increase in bidentate urea ligands and aromatic conjugation.<sup>28</sup> The N-H band located at  $3324\text{ cm}^{-1}$  broadens and shifts to  $3274\text{ cm}^{-1}$  indicating a stronger hydrogen bonding state. The aliphatic C-H bands at  $2852$  and  $2919\text{ cm}^{-1}$  undergo a strong decrease in intensity due to the scarcity of highly aliphatic branch in the hard heterogeneities. The C-O-C stretch peak loses intensity and shifts from  $1220\text{ cm}^{-1}$  to  $1234\text{ cm}^{-1}$  as result of loss of urethane linkages in favor of formation of urea units. The C-H stretch in the aromatic rings clearly visible for the soft phase at  $1600\text{ cm}^{-1}$ , only appear as a shoulder of the intense and broader main carbonyl peak in the hard phase spectrum. For HDI-p no substantial shift is observed when scanning through the probed infrared map. Only a slight shoulder of the carbonyl C=O peak located at  $1680\text{ cm}^{-1}$  appears at about  $1630\text{ cm}^{-1}$  as a sign of a possible increase in the hydrogen bonding strength in the small (size  $< 2\text{ }\mu\text{m}$ ) yellow-grey regions. HMDI-p presents similar spectral feature when compared to MDI-p and PPDI-p, yet the band associated to the C-O-C stretch at

**Table 2** Time constants and work of deformations associated to individual relaxation mechanisms. Note that in bold we report the parameters related to the relaxation of reversible moieties. These contribute to the calculation of interfacial work of deformation ( $W_{interfacial}$ )

	$\tau_{sp}^{seg}$ (s)	$\tau_{sp}^{rev}$ (s)	$\tau_{hp}^{seg}$ (s)	$\tau_{hp}^{rev}$ (s)	$\tau_t$ (s)	$W_{sp}^{seg}$ (kJ m <sup>-3</sup> ) $\times 10^{-1}$	$W_{sp}^{rev}$ (kJ m <sup>-3</sup> ) $\times 10^{-1}$	$W_{hp}^{seg}$ (kJ m <sup>-3</sup> ) $\times 10^{-1}$	$W_{hp}^{rev}$ (kJ m <sup>-3</sup> ) $\times 10^{-1}$	$W_t$ (kJ m <sup>-3</sup> ) $\times 10^{-1}$	$W_{interfacial}$ (kJ m <sup>-3</sup> ) $\times 10^{-1}$
MDI-p	$6.2 \times 10^{-5}$	<b><math>1.1 \times 10^{-5}</math></b>	0.1	<b><math>1.0 \times 10^3</math></b>	$1.3 \times 10^5$	579	<b>120</b>	9.6	<b>12.9</b>	3.4	<b>132.9</b>
PPDI-p	$1.1 \times 10^{-5}$	<b><math>1.0 \times 10^{-4}</math></b>	1.0	<b><math>0.3 \times 10^3</math></b>	$3.1 \times 10^4$	481	<b>407</b>	25.1	<b>6.5</b>	11.8	<b>413.5</b>
HMDI-p	$2.3 \times 10^{-5}$	<b><math>1.0 \times 10^{-3}</math></b>	—	—	0.92	512	<b>73.1</b>	—	—	19.5	<b>73.1</b>
HDI-p	$1.0 \times 10^{-6}$	<b><math>1.0 \times 10^{-4}</math></b>	—	<b>0.10</b>	$1.0 \times 10^3$	356	<b>23.6</b>	—	<b>12.2</b>	1.5	<b>35.8</b>



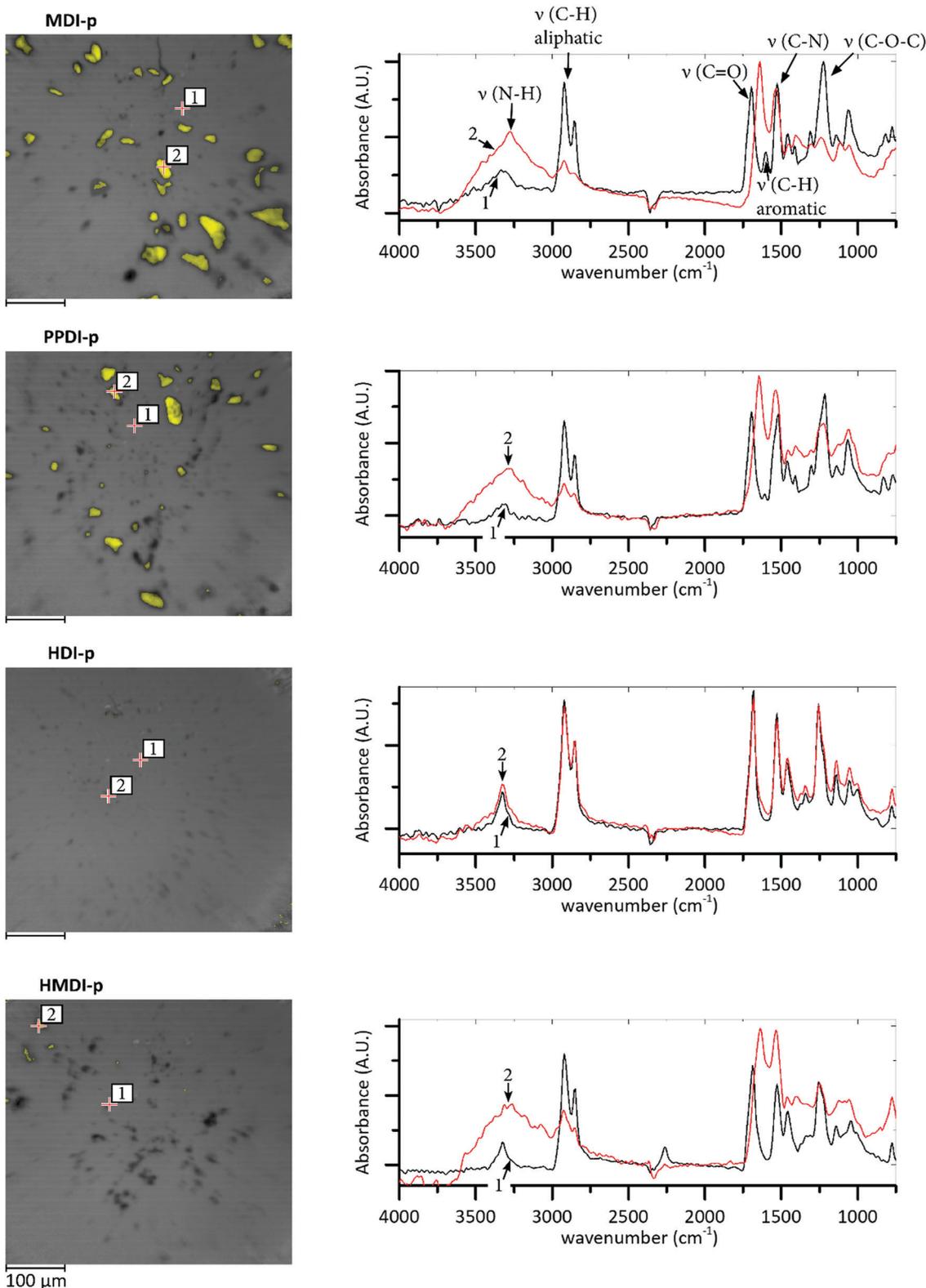


Fig. 4  $\mu$ ATR-FTIR mapping of self-healing polyurethane elastomers. Principal component analysis reveals a phase separated microstructure consisting in a continuous matrix (grey color) intercalated by heterogeneities (yellow color). Right figures show the local IR spectra of locations 1 (homogeneous) and 2 (dispersoids).



$1253\text{ cm}^{-1}$  does not undergo any shift nor decrease in intensity suggesting a minimal difference in the urethane linkages content. The higher content in bidentate urea and the stronger hydrogen bonded state of the segregated phase might be responsible for a slower molecular reorganization which, in turn, determines a local higher  $T_g$ .<sup>29</sup>

### 3.2. Interfacial work of deformation relation to early-stage healing fracture resistance

The deconvolution results were not only used to obtain information on the physical state of the network. Starting from the hypothesis that interfacial healing is governed by the reconstruction of reversible bonds at the broken interface and using SENT data collected for all the polymers in the early stage of healing, we explore the existence of a relationship between the interfacial work of deformation (obtained by melt rheology) and fracture resistance (a mechanical measure of interfacial healing obtained by SENT analysis). All the mechanical raw data and optical snapshots used for fracture resistance calculation are reported in the ESI† (Fig. S6 MDI-p, Fig. S7 PPDI-p, Fig. S8 HDMI-p and Fig. S9 HDI-p). Fig. 5 displays the relation between the calculated interfacial work of deformation ( $W_{\text{interfacial}}$ ) from rheology and  $J_C^{\text{interfacial}}$  from the SENT tests of the polymers healed for  $3.6 \times 10^3\text{ s}$  (1 h) at  $30\text{ }^\circ\text{C}$ . A closer look to the data (Table 2) reveals that higher  $W_{\text{interfacial}}$  of the PPDI-p and MDI-p samples is mainly related to the higher work of deformation assigned to the relaxation of the reversible ligands (concurrent relaxation of hydrogen bonds and aromatics) in the soft phase ( $W_{\text{sp}}^{\text{ev}}$ ). Since the soft phase undergoes fast conformational rearrangements, its reversible bonds reshuffling are expected to be the main contributors to the reconstruction of the broken interface at short healing times.<sup>10,11,30</sup> In this framework the use of the deconvolution protocol offers a critical advance to the understanding and optimization of interfacial healing, since its results are successfully sensitive to the incorporation of multiple reversible ligands, their symmetry and their energetic contribution to the reconstruction of the broken interface.

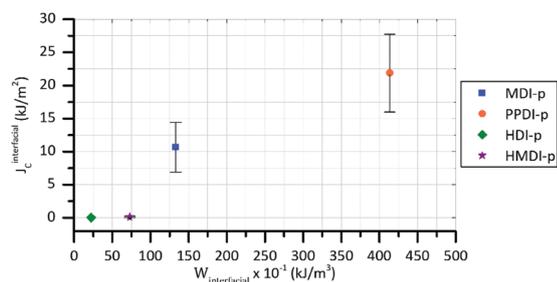


Fig. 5 Comparison between interfacial healing fracture resistance and interfacial work of deformation as obtained by macro-rheology. While qualitatively an increase in  $W_{\text{interfacial}}$  corresponds to higher  $J_C^{\text{interfacial}}$ , from a quantitative point of view the work of deformation does not capture the dramatic drop of fracture resistance for the aliphatic polyurethanes (HDI-p, HDMI-p). HDI-p point data does not include error bars due to immediate breakage of the samples tested upon application of the minimal sample alignment load of 3 N.

Quantitatively, for short healing times (3600 seconds at  $30\text{ }^\circ\text{C}$ ), both the aliphatic systems (HMDI-p and HDI-p) show a virtual absence of tensile fracture resistance ( $J_C^{\text{interfacial}}$  HMDI-p =  $0.18\text{ kJ m}^{-2}$ ,  $J_C^{\text{interfacial}}$  HDI-p =  $0.03\text{ kJ m}^{-2}$ ), as can be easily inferred from optical snapshots acquired during SENT testing (Fig. S8 and S9, ESI†). In this sense the data provided by macro-rheology seems to point to the existence of a limiting  $W_{\text{interfacial}}$  that must be surpassed to get sufficient recovery of fracture resistance upon interfacial healing. However, more systems, ideally incorporating different types and numbers of reversible ligands, should be tested in a wide range of  $W_{\text{interfacial}}$  to confirm and locate the presence of such threshold.

Another possible explanation to absence of fracture resistance for HMDI-p and HDI-p at the early stage of healing can be found in the characteristics of the different polyurethanes microstructures. The aromatic polymers present a segmented microstructure and, as probed by  $\mu\text{FTIR-ATR}$ , show some high  $T_g$  segregated heterogeneities at the microscale (Fig. 4 and Table S1, ESI†). The high  $T_g$  of these segregates implies, locally, a much slower reorganization and an improved directionality of the reversible ligands. This effect, when occurring at a damage site, leads to a more efficient interfacial re-bonding/healing. The lack of such structures in the aliphatic polymers causes a dramatic drop of  $J_C^{\text{interfacial}}$ . In a recent work Yang *et al.*<sup>31</sup> show similar beneficial effects of micro-segregated structures on scratch-healing behavior of PU coatings, attributing the healing enhancement to a more efficient entropic energy storage during local deformation. Furthermore, Chen *et al.*<sup>10</sup> have shown that a multiphase microstructure in self-healing thermoplastic elastomers is crucial to the rapid re-arrangement of the polymer soft phase leading to high healing.

Long range dynamics is expected to determine interphase randomisation and to lead the system to higher degree of property restoration at longer healing times. The deconvolution procedure provides kinetics of terminal relaxation in the range  $\tau_t = 10^0$  to  $10^3\text{ s}$  for HDI-p and HMDI-p and very sluggish terminal flow for MDI-p and PPDI-p ( $\tau_t > 10^5\text{ s}$ ). Fig. 6 shows a quantitative impression of the effect of long term healing on the polyurethane systems used for this study. The aliphatic polymers show a significant recovery of fracture resistance going from being virtually absent for short healing times ( $3.6 \times 10^3$  seconds) to a moderate mechanical stability at longer

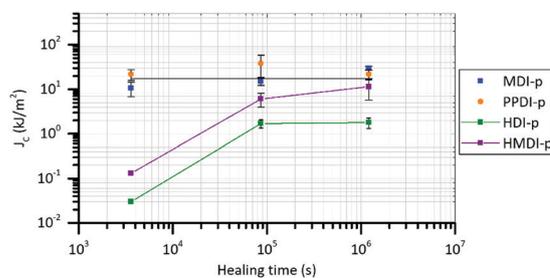


Fig. 6 Long range dynamics effect on fracture resistance recovery. In accordance with time constants obtained from deconvolution, the beneficial effect of long range dynamics is only observed for aliphatic polyurethanes (HDI-p, HMDI-p). Healing temperature is  $30\text{ }^\circ\text{C}$ .



healing times (after  $10^6$  seconds  $J_C$  HMDI-p =  $11.4 \text{ kJ m}^{-2}$ ,  $J_C$  HDI-p =  $1.8 \text{ kJ m}^{-2}$ ). An immediate feedback regarding the increase in fracture properties when going from short to longer healing times can be obtained when looking at the optical snapshots acquired during SENT testing and used for  $J_C$  calculation (Fig. S8 and S9, ESI<sup>†</sup>), in which a higher deformation can be seen before fracture at the healed interface. Moreover, in accordance with kinetics predictions obtained by rheology deconvolution, MDI-p and PPDI-p do not show any significant improvement in the fracture resistance which remains virtually constant over long holding times at the healing temperature of  $30 \text{ }^\circ\text{C}$ .

## 4. Conclusions

In this work we demonstrate that the intelligent use of macro-rheology data can provide semi-quantitative information on the degree of interfacial healing in polymers. In this framework, we apply a deconvolution protocol of the mechanical relaxation spectrum derived from macro-rheology to a set of self-healing polyurethanes and explore the relation between the derived stored work of deformation and the degree of mechanical restoration in the early stage of polymer healing.

The deconvolution protocol is found to be sensitive to the variations in the polymer architecture and in particular to the addition of multiple reversible ligands, to the symmetry of the rigid backbone segments and to their individual energetic contribution to the relaxation process.

The work of deformation associated to the disjunction of reversible moieties reflects in a semi-quantitative way the recovery of fracture resistance in the early stage of healing. It results higher for polymers endowed of multiple reversible ligands that coherently show a higher degree of mechanical restoration. The results points at the existence of a so far unidentified threshold of interfacial work of deformation marking the transition between healing (*i.e.* sufficient reversible bonds at interface to transfer load along the fracture plane) and no healing. Furthermore, the time constants capture the kinetics of the entire healing process, predicting the access to long range motion for less physically crosslinked systems.

These insights on the relation between polymer structure, rheology and interfacial healing benefit the design of novel systems showing high mechanical restoration in the early stage of healing.

## Conflicts of interest

The authors report no conflicts of interest.

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