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Mechanical improvement of calcium carbonate cements by *in situ* HEMA polymerization during hardening†

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Calcium carbonate cements are a promising alternative for calcium phosphate cements. Due to the higher solubility of calcium carbonate compared to apatite, it is expected to have an improved biodegradation rate; a clear advantage for prospective biomedical applications in a clinical context. As of yet, the poor mechanical performance of calcium carbonate cements precludes their exploitation as a bioceramic. Herein, we report a mechanically enhanced calcium carbonate cement, formulated of vaterite and magnesium-doped amorphous calcium carbonate, which was strengthened by *in situ* polymerization of incorporated 2-hydroxyethylmethacrylate (HEMA) during setting in simulated body fluid (SBF). This approach allowed us to generate a pronouncedly strengthened polymer-ceramic composite whose mechanical properties can be tuned by the monomer fraction. Varying cement compositions were characterized with respect to their mechanical performance, morphology, and quantitative phase composition. HEMA polymer reinforcement strengthened the calcium carbonate cement distinctly in four-point bending test while, in stark contrast, the brittleness of the polymer-free cement simply made such tests impossible. Our results demonstrate that the chosen polymer-reinforcement strategy is an efficient and straightforward approach and allows for tuning the mechanical properties of an otherwise brittle and thus unusable calcium carbonate cement towards biomedical application.

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Introduction

The development of biomaterials, which are suitable for filling bone defects and which feature tailored properties concerning biodegradability, osteoconductivity, and osteoinduction, is a prevailing challenge in the field of orthopaedic and dental surgery. Hetero- or autografts or implants of natural origin (*e.g.* calcareous corals) are often used,^{1,2} however, they come with major drawbacks, such as biological variability and risk of viral or bacterial contaminations. In a warming world, we even may have to face an increasing uncertainty in supply when it

comes to corals.^{3–5} To address these problems which are associated with biogenic calcareous biomaterials, suitable synthetic materials are needed but their synthesis and design protocols have to meet the demands and requirements of clinical applications. In this context, fast-setting ionic cements are an attractive material class for bone filling. In the last several years, a range of calcium phosphate (CaP) cements have been developed which are suitable as a bone replacement material due to their biocompatibility and bioactivity.⁶ However, it is still a challenge to further augment the rates of bioresorption of such cements to improve bone formation and regeneration.^{7–9}

The biological resorption of bone replacement materials depends on the solubility of their constituting mineral phases. Since calcium carbonate shows higher solubility than apatite, turning from calcium phosphate-based to calcium carbonate-based cements is an auspicious approach to manufacture cements with improved and tuneable biodegradation rates.^{10,11} Cements composed of a blend of calcium carbonate and calcium phosphate have already been tested,^{12,13} but only a marginal number of studies focussed on cements which contain calcium carbonate as the only mineral component.¹⁴ Exploitation of such

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calcareous cements is, as of yet, impaired by their inferior mechanical properties. In this contribution, we explore a strategy to augment the mechanical performance of calcium carbonate cements by *in situ* polymerization during setting of the cement.

Calcium carbonate occurs in three anhydrous crystalline phases: calcite, aragonite and vaterite. It also exists in form of an extremely reactive and unstable amorphous calcium carbonate (ACC) which plays a fundamental role in biogenic and biomimetic calcification processes.^{10,15–18} In the biosphere, calcium carbonate is near-to omnipresent and is precipitated by a wide range of organisms in which it serves as load-bearing skeleton or damage-tolerant weapon. In these biogenic ceramics, the brittleness of pure calcium carbonate is overcome by a hybrid and composite material approach which grants strength and toughness at the same time to the biomineral. For more than two decades, nacre- and coral-based substitutes are already exploited as bioactive and biocompatible biomaterials, *e.g.* as powders and pseudomorphically transformed porous ceramics or in the form of mineral-enhanced gels.^{2,19,20} *In vivo* studies have demonstrated that calcium carbonate-based bioceramics derived from corals promote bone ingrowth and resorption.^{21,22} However, the mechanical properties of such coral-based grafts are poor.³ Moreover, sintering of calcium carbonate bioceramics is challenging since calcium carbonate requires very low sintering temperatures due to its low thermal decomposition temperature.²³ In this context, calcium carbonate cements are promising for designing calcareous bioceramics *via* low-temperature routes.²⁴ Combes and co-workers have recently studied the feasibility of preparing an initially biphasic calcium carbonate cement.¹⁴ Employing one highly reactive amorphous phase and a metastable crystalline calcium carbonate phase, this first calcareous cement recrystallized – fully in agreement with Ostwald step rule – during setting.¹⁴ The calcium carbonate cement was shown to be non-toxic for human osteoprogenitor cells suggesting good cytocompatibility. However, the inferior mechanical properties of their cement effectively impeded clinical application; the compressive strength of the cement was below 13 MPa. To push the mechanical properties of calcium carbonate cements into the range at which a clinical application is feasible and reasonable, we take inspiration from biominerals and reinforce the brittle cement with a ductile polymeric phase which shall provide similar toughness like the intracrystalline biopolymers in biominerals. This method is already established strategy in the field of calcium phosphate cements.^{25,26} Here, we add a monomeric substance, 2-hydroxyethylmethacrylate (HEMA), to the unsettled cement powder and allow polymerization during cement hardening.²⁵ HEMA is one of the most common polymers in biomedical applications which renders it suitable for this feasibility study.²⁷

The work presented herein studies a new type of bone cement solely made of calcium carbonate serving as the inorganic/ceramic majority component. The quality and purity of the initial calcium carbonate powders was characterized by a series of techniques, *i.e.*, X-ray diffraction (XRD), Fourier transform infrared (FTIR) spectroscopy, Raman spectroscopy, and

scanning electron microscopy (SEM). The setting of calcium carbonate cement was triggered by the presence of water. Simulated body fluid was used to account for the distinct ion composition in human body fluids and to assure comparable conditions to hardening *in vivo*. The mechanical characteristics of the cement were enhanced by *in situ* polymerization of HEMA during setting of the cement paste, generating a mechanical stable polymer-ceramic composite. We compared the mechanical properties and quantitative phase composition of the HEMA-enhanced cements to a non-reinforced and polymer-free calcium carbonate cement with otherwise identical composition and hardening conditions.

Materials and methods

Synthesis of CaCO₃ powders

Synthesis of vaterite. Vaterite was prepared by double decomposition of calcium chloride and sodium carbonate at room temperature. For this, analytical grade sodium carbonate of >99% purity was purchased from Sigma-Aldrich (St. Louis, USA), and 1.0 M calcium chloride solution (volumetric standard) was obtained from Fluka Analytical (Bucharest, Romania). While stirring at 450 rpm, 50 mL of 1.0 M calcium chloride solution was added to 50 mL of 0.1 M sodium carbonate solution at a rate of 3.33 mL min⁻¹. The supernatant was removed by vacuum filtration, and the precipitate was thoroughly washed three times with water and subsequently with ethanol, before it was dried in a desiccator. The pH of the solution was measured by a hand-held pH meter (HI-98140 Hanna Instruments, Vöhringen, Germany). While the pH of the initial solution was 11.7, the pH decreased to 8.4 after completion of the precipitation reaction.

Synthesis of Mg-doped amorphous calcium carbonate. Pure amorphous calcium carbonate (ACC) crystallizes extremely fast. In order to reduce the transformation rate, ACC was precipitated in presence of magnesium, which essentially acts as crystallization inhibitor and ACC stabilizer.²⁸ In the present study, 0.5 M sodium carbonate solution (volumetric standard), was purchased from Thermo Fisher Scientific (Massachusetts, USA), and 1.0 M calcium chloride solution (volumetric standard) and magnesium chloride were purchased from Fluka Analytical (Bucharest, Romania). A series of calcium chloride solutions with 10 wt%, 20 wt% and 40 wt% magnesium content was prepared by mixing solutions of 0.2 M calcium chloride and 0.2 M magnesium chloride. While stirring at 750 rpm, 20 mL of 0.2 M sodium carbonate solution was poured rapidly into the respective metal chloride solution. After 5 s, the supernatant was removed by vacuum filtration, the precipitate was washed once with deionized water and once with ethanol in sequence and dried at a temperature of 60 °C for 2 h. The pH of the initial metal chloride solution was 7.5, 8.0, and 9.0 of 10 wt%, 20 wt% and 40 wt% Mg, respectively. After precipitation, the pH increased to 10.1 in each case. The pH was measured by a handheld pH meter (HI-98140, Hanna Instruments, Vöhringen, Germany).



Synthesis of Aragonite. Phase-pure aragonite was prepared by mixing solutions of calcium nitrate (0.1 mol L^{-1} ; Sigma-Aldrich, St. Louis, USA) and sodium carbonate (1 mol L^{-1} ; Sigma-Aldrich, St. Louis, USA) at $75 \text{ }^\circ\text{C}$ under constant agitation. The precipitate was filtered, washed three times with water and ethanol and then was dried in a desiccator.

Cement preparation. The cement pastes were prepared by mixing the powder ($\text{ACC}_{20}\text{Mg/vaterite} = 1/2$) with an appropriate amount of liquid phase (SBF) for 5 minutes at a liquid to powder ratio (LPR) of 1 mL g^{-1} . Polymer modified cements were prepared by adding the appropriate amount (10, 25, 50 wt%) of 2-hydroxyethylmethacrylate (HEMA, Merck, Darmstadt, Germany) to the SBF solution. To initiate polymerization upon cement preparation, 0.75 wt% ammonium persulfate (APS, Sigma Aldrich, Steinheim, Germany) was added to the cement powder and 0.125 wt% N,N,N',N' -tetramethylethylenediamine (TEMED, Sigma Aldrich, Steinheim, Germany) to the cement liquid prior cement preparation.

Cement and powder characterization

Fourier transform IR spectroscopy. Fourier transform infrared (FTIR) spectrometry was done with an IRAffinity-1S (Shimadzu, Japan) equipped with an ATR cell. Samples were gently ground to ensure homogeneity. All spectra are the average of two independent measurements with 32 scans each at a resolution of 4 cm^{-1} .

Scanning electron spectroscopy (SEM). The microstructure of the synthesized powders was characterized using a Carl Zeiss Auriga. All samples for SEM analysis were uncoated and observed at a working distance of 3.0 mm and an accelerating voltage of 1.0 kV.

Raman spectroscopy. Raman spectroscopy measurements were accomplished by using a LabRAM HR800, Horiba JobinYvon (Tokyo, Japan).

Differential thermal analysis (DTA) and thermogravimetric analysis (TGA). Simultaneous DTA/TGA were performed by means of an SDT 2960 DTA/TGA (TA Instruments, New Castle) using platinum crucibles; corundum powder was used as an inert reference. A heating rate of $5 \text{ }^\circ\text{C min}^{-1}$ was applied; samples were heated up to a maximum temperature of $1000 \text{ }^\circ\text{C}$.

X-ray diffraction (XRD). Phase identification was carried out using a Siemens Kristalloflex D500 (Karlsruhe, Germany). A $\text{Cu K}\alpha$ source was used over a 2θ range of 20° to 60° ; a step size of 0.02° and a dwell time 0.05 were applied. Phase analysis was done using MATCH! (Crystal Impact, Bonn, Germany).

Quantitative XRD analysis. The quantitative phase composition of the starting powders and the hardened cement samples was determined by powder X-ray diffraction (XRD). Additionally, samples of pure calcite (purity >99%), purchased from Sigma-Aldrich (St. Louis, USA) and aragonite (prepared as described above) were measured as reference for the quantitative evaluation and lattice parameters. In order to obtain hardened samples for XRD measurements, the carbonate samples were first mixed with the corresponding mixing liquid for at least 1 min until a pasty consistence was reached. A liquid to powder ratio of 1 g mL^{-1} was used. The paste was filled into plastic

crucibles which were closed by a lid and tightly sealed with Parafilm. The samples were allowed to harden for 24 h at $37 \text{ }^\circ\text{C}$ in a drying oven (Memmert, Schwabach). Afterwards they were dried in a vacuum drying chamber (Binder, Tuttlingen) at $40 \text{ }^\circ\text{C}$ for 24 h. The dried samples were carefully ground using an agate mortar to obtain fine powders suitable for XRD measurements and to ensure un-biased sampling. For each HEMA concentration, XRD analyses were performed in triplicate. XRD measurements were performed with a D8 Advance with DaVinci design diffractometer (Bruker AXS, Karlsruhe). The following parameters were applied: angle range $10\text{--}70^\circ 2\theta$; step size $0.0112^\circ 2\theta$; integration time 0.2 s; divergence slit 0.3° ; sample rotation with 0.5 s^{-1} . Qualitative evaluation of the diffraction patterns was performed with the software package EVA v.4.1 (Bruker AXS, Karlsruhe). For Rietveld refinements, the software package TOPAS v.4.2 (Bruker AXS, Karlsruhe) was used. The structures given below were used in combination with a Chebychev polynomial of third order. Lattice parameters were refined for all samples. Crystallite sizes and microstrain were refined as far as reasonable values were obtained. Preferred orientation was refined for calcite in (1 0 4) direction and for vaterite in (0 0 1) direction.

Phase	ICSD #	Space group	Authors
Calcite	80 869	$R\bar{3}c$	Maslen <i>et al.</i> ²⁹
Aragonite	15 198	$Pm\bar{c}n$	Dal Negro <i>et al.</i> ³⁰
Vaterite	424 574	$C\bar{1}$	Mugnaioli <i>et al.</i> ³¹
NaCl	61 662	$Fm\bar{3}m$	Nickels <i>et al.</i> ³²

The absolute quantities of the crystalline CaCO_3 phases were then determined by the G-factor method, an external standard method. The G-factor, a device specific calibration constant, is obtained from measurement of an appropriate external standard according to eqn (1).³³

$$G = S_s \frac{\rho_s V_s^2 \mu_s^*}{c_s} \quad (1)$$

A quartzite slice was applied as secondary standard which was calibrated with fully crystalline silicon powder (NIST Si Standard 640d) as primary standard. The mass attenuation coefficients μ_s^* of quartzite and the carbonate samples investigated was calculated from the mass attenuation coefficients of the elements involved.³⁴ The quantities c_j of the crystalline phases j of interest were then calculated according to eqn (2), where μ_{sample}^* was calculated from the mass attenuation coefficients of the elements involved.¹¹

$$c_j = S_j \frac{\rho_j V_j^2 \mu_{\text{sample}}^*}{G} \quad (2)$$

Isothermal calorimetry. Calorimetry measurements of cements were performed by means of a TAM Air isothermal calorimeter (TA Instruments) with integrated thermostat at $37 \pm 0.02 \text{ }^\circ\text{C}$. The cements were mixed by internal stirring using a self-devised injection and mixing device which allows



internal paste preparation (InMixEr, FAU Erlangen, Mineralogy). Stirring was performed for 2 min with an external motor at a constant stirring rate of 858 rpm. Equilibration of carbonate powders and mixing liquid was directly performed inside the calorimeter. The heat flow curves were corrected for the calibration constant of the InMixEr mixing device and the time constant of the calorimeter.³⁵ The total heat release was then determined by integrating the heat flow over time.

Mechanical testing. The cement paste, which showed good workability, was transferred into cuboid silicon rubber moulds in order to prepare samples for compressive strength ($12 \times 6 \times 6$ mm) or 4-point bending strength ($5 \times 5 \times 30$ mm) testing and allowed to set at 37°C for time periods of 2 h, 4 h, 6 h, 24 h, 3 d, 7 d and 14 d in a sealed container saturated with water. Wet samples ($n = 5$ per condition) were tested for compressive strength and 4-point bending strength (Instron 5565, Darmstadt, Germany).

Results and discussion

Powder synthesis and characterization

In order to prepare the calcium carbonate-based cements, phase-pure calcium carbonate polymorphs were freshly synthesized. Phase-pure vaterite was synthesized by a double-composition technique which yielded polycrystalline and ellipsoidal aggregates with particle sizes ranging from $1\ \mu\text{m}$ to $6\ \mu\text{m}$ and a diameter of about $2.5\ \mu\text{m}$.^{36–38} At higher magnification, micrographs show that these ellipsoidal particles are composed of aligned needle-like nanocrystallites with a mean length of $200\ \text{nm}$ (Fig. 1A). Further analytical details, especially on the phase purity and composition of the synthesized starting material is given in the ESI† (Fig. S1).

Pure amorphous calcium carbonate (ACC) is unstable and transforms to a crystalline phase when brought into contact with water so fast that it is not suitable for a reasonable cement formulation. Hence, we adjusted the rate of ACC phase transformation by using magnesium as phase stabilizer and crystallization inhibitor. Mg-ACC powders were prepared with varying magnesium content, *i.e.*, with 10% of Mg (ACC_10Mg), with 20% of Mg (ACC_20Mg) and 40% of Mg (ACC_40Mg). The morphology of the Mg-ACC powder varies only marginally as a function of magnesium content (Fig. 1B). All variants of Mg-doped ACC consist of spheroidal and aggregated nanoparticles whose average size ranges from 120 to $200\ \text{nm}$ and are X-ray amorphous (Fig. S2A, ESI†). After preparation, Mg-ACC slowly recrystallizes to calcite even when stored dry, as evidenced by a representative XRD pattern recorded 7 days after a sample of ACC_10Mg was prepared (Fig. S2B, ESI†). After 31 days of storage in a desiccator, this specific sample had completely transformed to crystalline calcite whereas samples of ACC_20Mg and ACC_40Mg were still amorphous (Fig. S2C, ESI†). ICP measurements showed that the rate of Mg^{2+} incorporation does not mirror the exact Mg/Ca ratio of the mother solution but increases with increasing Mg concentration (Fig. S2D, ESI†). A further DTA-TGA is given in the ESI† which further corroborates the purity of the synthesized phase (Fig. S3, ESI†).

Cement preparation and characterization

Cement pastes were prepared by mixing the powders of Mg-doped ACC and vaterite in a ratio of 1 to 2 with an appropriate amount of liquid phase (SBF) to give a liquid to powder ratio (LPR) of $1\ \text{mL g}^{-1}$. To mechanically enhance the cements by *in situ* HEMA polymerization during cement setting,

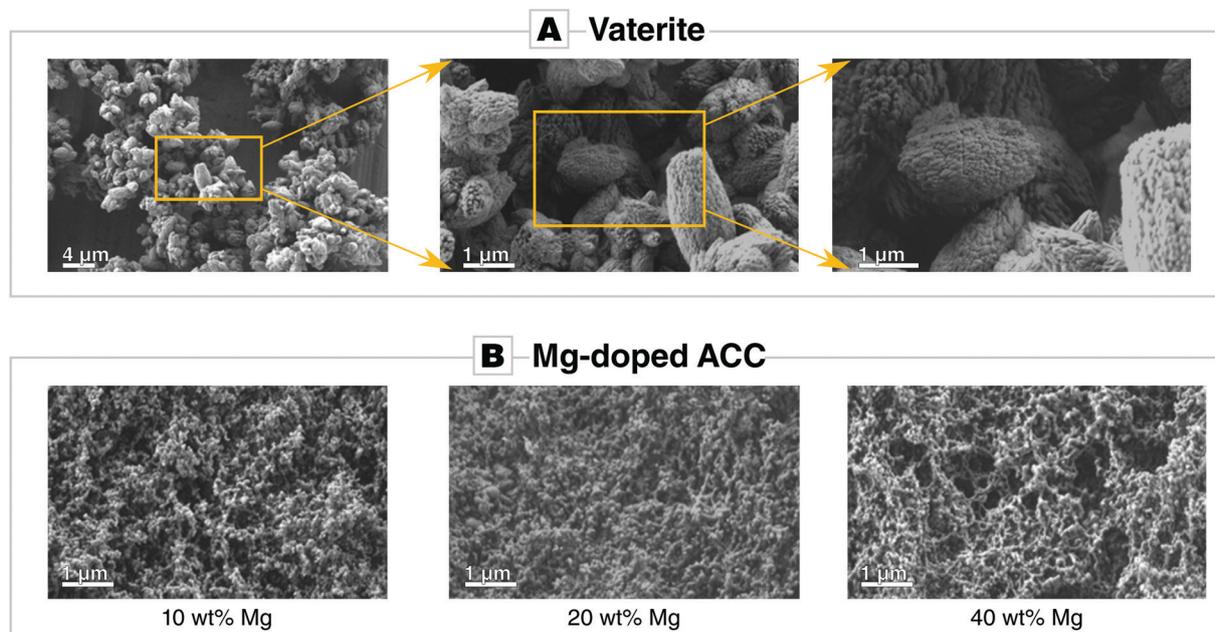


Fig. 1 Scanning electron micrographs of synthesized (A) vaterite and (B) Mg-doped amorphous calcium carbonate (ACC).



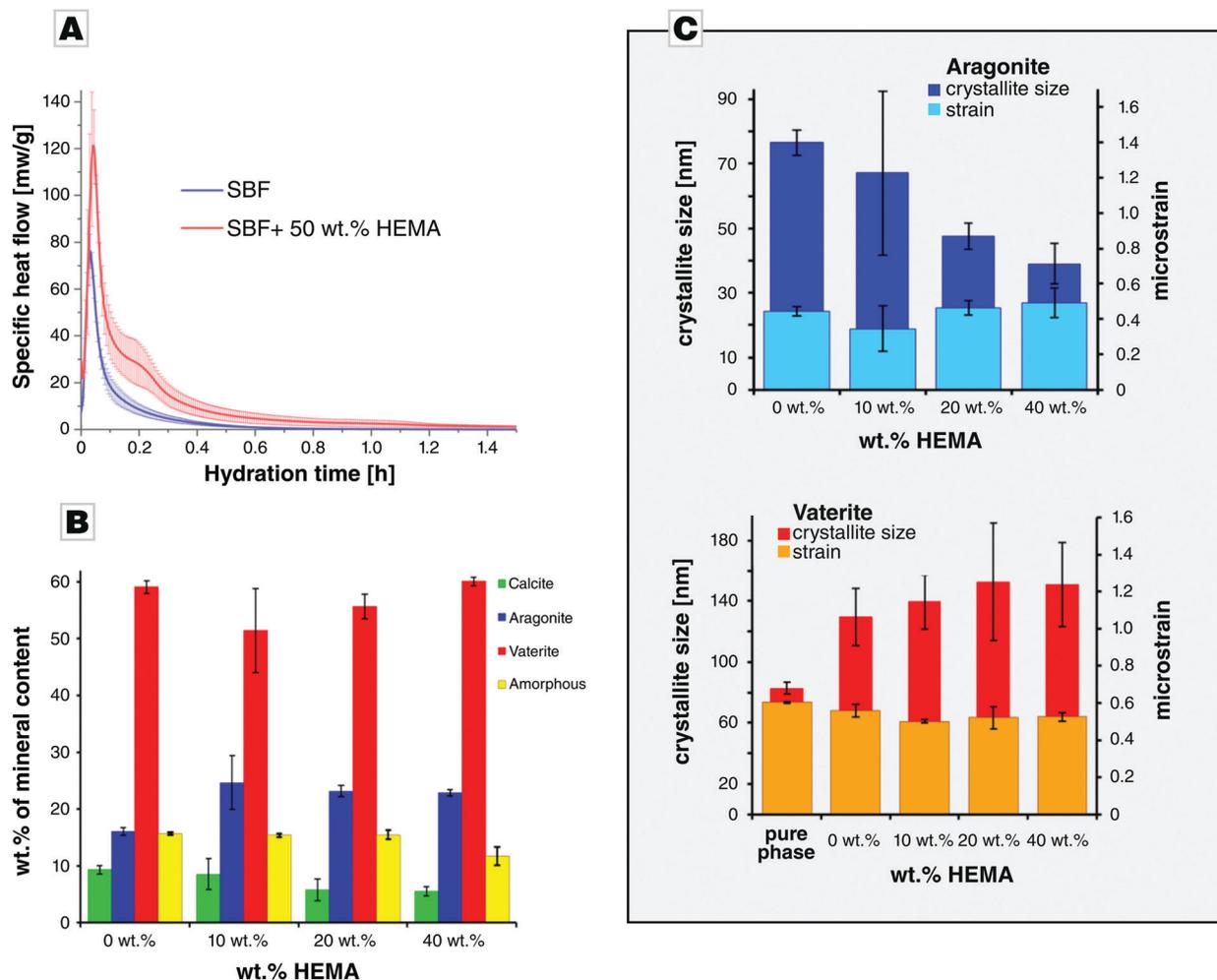


Fig. 2 Characterization of the cement setting. (A) Calorimetry of a cement prepared of ACC_Mg20/vaterite in a ratio of 1 : 2, prepared in absence and in presence of 50 wt% HEMA; the mean values of three independent measurements are presented and the error bars give the standard deviation. (B) Phase analysis of cements (ACC_Mg20/vaterite = 1/2) after 24 h, as a function of HEMA content; mean values of three independently prepared measurements are shown. (C) Crystallite sizes and microstrain analysis of aragonite and vaterite in cements (ACC_Mg20/V = 1/2, LPR = 1 mL g⁻¹) prepared at different HEMA concentrations after 24 h of hardening at 37 °C; the mean values of three independently prepared measurements are shown.

2-hydroxyethylmethacrylate (HEMA) was added in varying amounts (10, 25, and 50 wt%) to the SBF solution. Polymerization was triggered by addition of APS and TEMED to the cement mixture. We followed the reaction *in situ* by isothermal calorimetry which demonstrated that the hardening reaction proceeded very rapidly for both the reference sample in absence of HEMA and a sample containing 50 wt% HEMA. Major heat release is only observed in the first hour of hardening (Fig. 2A) and, for both samples, a single and sharp heat flow maximum occurred already after some few minutes of reaction time. This pronounced heat maximum was significantly higher for the polymer-containing sample, for which the over-all reaction time also lasted distinctly longer. Thus, the total heat release during setting and hardening was significantly higher for the samples containing 50 wt% HEMA in comparison with those without polymer which we attribute to an additional heat release as a result of polymerization.

In all hardened cement samples investigated by XRD, vaterite was the main phase, while calcite and aragonite were present in

smaller amounts along with traces of sodium chloride present in all samples. G-Factor quantification indicated the presence of a residual amorphous fraction. In order to compare the changes of CaCO₃ phase composition as a function of HEMA content, the data was normalized to the sum of carbonate phases, including the amorphous content (Fig. 2B). While the vaterite content was practically identical for all samples within the error range, the amount of aragonite was significantly higher for the HEMA containing samples, compared to the reference. Accordingly, calcite content significantly decreased in case of 25% HEMA and 50% HEMA, compared to the reference. The normalized amorphous content was nearly identical to the reference except for 50% HEMA, which had a slightly smaller amorphous fraction. The crystallite size of aragonite decreased in presence of HEMA, compared to the reference samples hardened in absence of HEMA (Fig. 2C). In contrast to aragonite, the crystallite size of vaterite increased slightly in presence of HEMA but was unaffected by a change in HEMA content. The initial crystallite



size of vaterite was lower than that of the vaterite present in the hardened cement samples, while its microstrain decreased during hardening, indicating crystal growth. The crystallite size of calcite exceeded the range in which reliable interpretation on basis of the Scherrer equation is possible.

For calcite, both the cell parameters for the *a*- and *c*-axes were significantly larger in case of the calcite standard, compared to the calcite that formed from reaction of the carbonate cements (Fig. S4A, ESI†). For aragonite, no variation in cell parameters was observed (Fig. S4B, ESI†). The cell parameters for the *a*- and *b*-axes of vaterite did not vary significantly, while the *c* parameter was significantly higher in case of pure vaterite (Fig. S4C, ESI†). The shorter cell parameters of calcite formed during hardening might indicate that Mg was incorporated into the calcite lattice. Mg²⁺ has a smaller ionic radius of 0.72 Å compared to Ca²⁺ with 1.00 Å (both values given for six fold coordination)³⁹ and thus would lead to a reduction in cell parameters. Since aragonite did not show a change in cell parameters, it is plausible to assume that Mg²⁺ was incorporated into the calcite lattice or remained in the residual amorphous phase. ACC phases are well-known to be stabilized by Mg incorporation which also accounts for the unexpected long-time stability of a residual amorphous phase.⁴⁰ Moreover, magnesium is known to impede calcite growth while favouring aragonite formation which explains the presence of aragonite in the hardened cements.^{41,42}

From the phase analysis combined with the results of the crystal size determination, we can infer that calcite and aragonite formation was driven by vaterite transformation only to a minor extend. Instead, ACC redissolution mainly fed the formation and growth of aragonite and calcite. The slight increase in the average crystallite size of vaterite indicates that the vaterite fraction of lower crystallinity has transformed to either aragonite or calcite, leading to an overall increase of the average crystallite size. From the cement's phase composition, one may conclude that the polymer addition slightly influences the crystallization pathway. Higher polymer content seems to impair formation of calcite; higher amounts of HEMA lead to a preferred aragonite formation.

The morphological evolution in time of samples which contain 50 wt% of HEMA is shown in Fig. 3. It demonstrates that, in the first 6 hours of hardening, the cement appears to be composed of poorly crystalline phases. After 6 h of hardening, rhombohedral calcite and ellipsoidal vaterite crystals appeared; thus, the overall fraction of crystalline phases increased with time. EDS analysis showed that a calcareous precipitate had formed (Fig. S5, ESI†).

The compressive strength of the calcium carbonate cements (Fig. 4A) increased with HEMA content. Reference samples, which contained no polymer and were hardened for 6 hours were still too brittle to perform any measurements; only reference

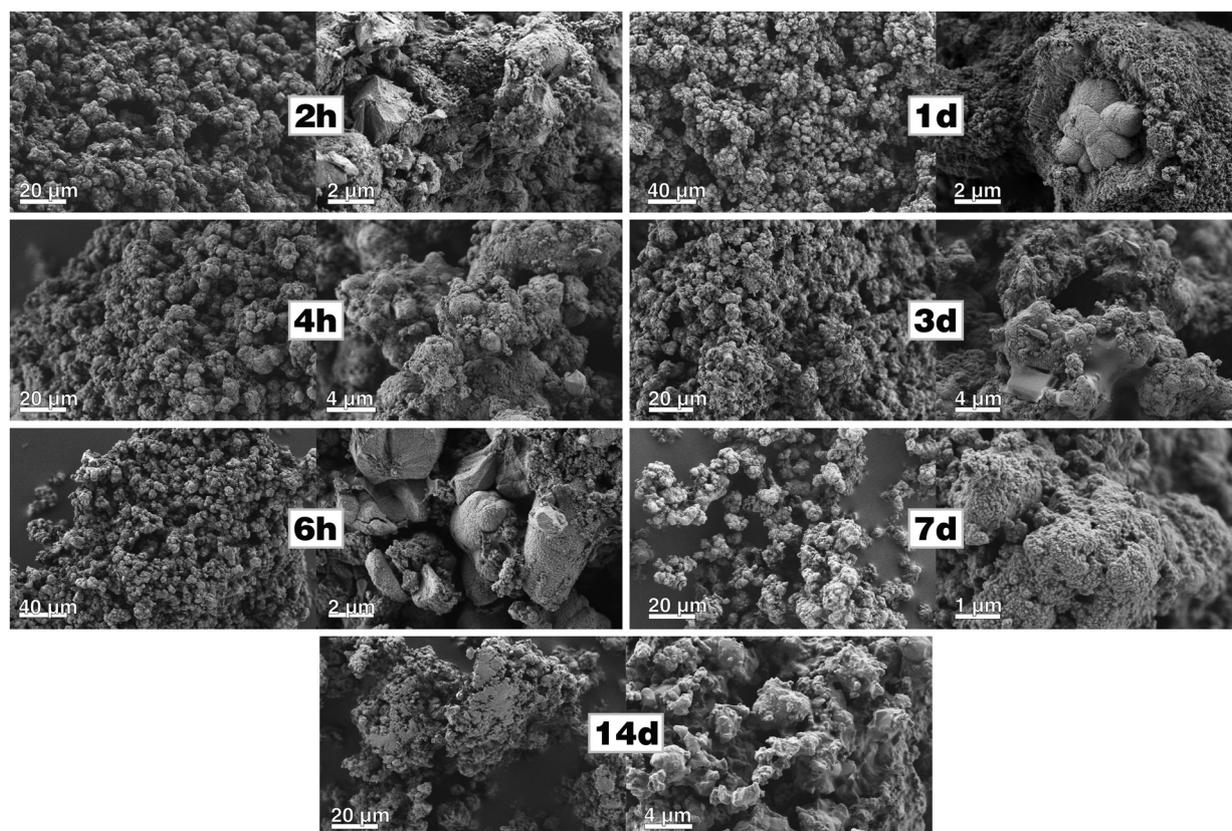


Fig. 3 SEM micrographs of fracture surfaces of cements (ACC_Mg20:V = 1:2, LPR = 1 mL g⁻¹, 50 wt% HEMA) after different times of setting. The samples were gently crushed so that individual particles and crystallites can be easily distinguished. Since the polymerized HEMA produces only a low contrast in comparison to the mineral matrix, the polymer matrix is barely visible.



samples hardened for longer periods of time could be evaluated. Even after a hardening period of 14 days, the compressive strength of the reference samples was very weak (below 1 MPa). In contrast, the addition of 10 and 25 wt% of HEMA already improved the compressive strength of the calcium carbonate cements considerably. For hardening periods not longer than 6 hours, the determined compressive strength was below 1 MPa, and, after 1 day of setting, the samples with 10 wt% HEMA already reached a compressive strength of 2 MPa which further increased to 4 MPa after 14 days. By increasing the content of HEMA to 25 wt%, the compressive strength was essentially increased by a twofold; after 14 days a compressive strength of approx. 9 MPa was determined. The addition of 50 wt% HEMA strengthened the cement most pronouncedly. Already after 2 hours of setting, the compressive strength was already at 14 MPa, and it slowly increased reaching a value of about 25 MPa within a week's time. After two weeks of hardening, the compressive strength of the enhanced cement rose to 33 MPa. Overall, it seems clear that strengthening by addition of 50 wt% HEMA polymer to the cement remarkably improves the compressive strength of our calcium carbonate cement.

The mechanical performance was further tested by means of four-point bending tests and showed that incorporation of HEMA improved also the cement's bending strength at the

same time (Fig. 4B). HEMA-free reference samples were too brittle to perform such measurements, whereas samples enhanced with 10 wt% HEMA already showed a bending strength of approx. 0.1 MPa after 2 hours of hardening which further increased to 0.9 MPa after 14 days of hardening. Addition of 25 wt% HEMA further enhanced the cement's bending strength: after 2 hours of setting, the bending strength was 0.3 MPa and increased by a six-fold within the next two hours, to reach a value of about 2.5 MPa after 6 hours of hardening. Increasing the HEMA content even further to 50 wt%, the four-point bending strength rose from about 1 MPa after 2 hours of hardening, to about 13 MPa after 14 days of hardening. While cements with a HEMA content of 10 and 25 wt% still showed the characteristic brittle fracture of ceramics and a maximum bending deformation of the samples of less than 0.8 mm (Fig. 4B), samples with 50 wt% of polymer exhibited pronounced flexibility as bending up to 4 mm was possible before fracture (see Fig. S6 in the ESI†). In fact, Christel and co-workers obtained similar bending strength values by adding 50 wt% HEMA to α -tricalcium phosphate cements. These cements showed a maximum bending displacement of 0.4–1.5 mm.²⁶ In contrast, our calcium carbonate cement with 50 wt% polymer was much more flexible, as bending was possible for 2–4 mm before the samples underwent

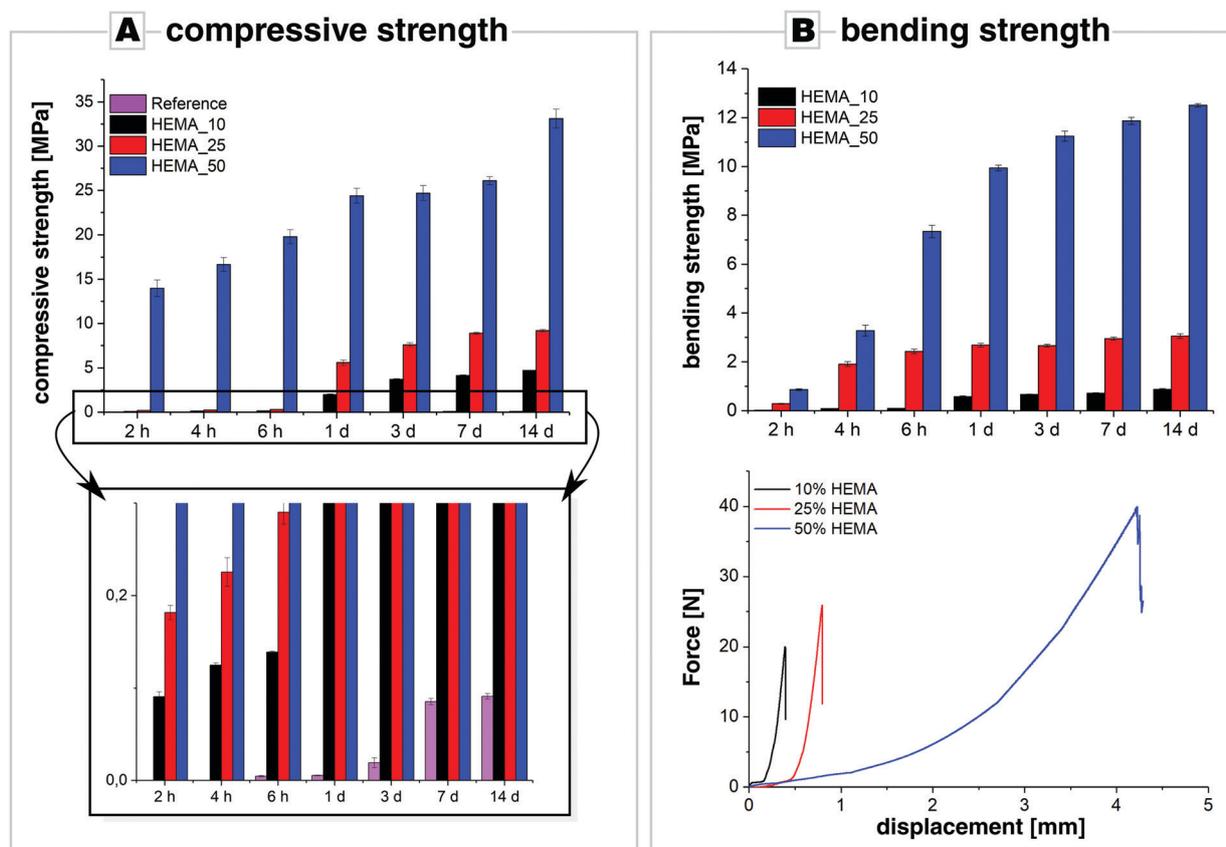


Fig. 4 (A) Compressive strength and (B) four-point bending tests along with force displacements curves of cements (ACC_20Mg/vaterite = 1/2, LPR = 1 mL g⁻¹) with various contents of HEMA (10, 25, 50 wt%) as a function of hardening time. For the most part, reference samples were too brittle to perform measurements.



fracture. This might be caused by the difference in crystal morphology as elongated aragonite crystals may reinforce the cement by fibre toughening and fibre pull-out. The large particle size distribution, which can be seen in Fig. 3 in which agglomerations of relatively large particles can be spotted, might have a similar effect by causing tortuous crack paths further augmenting the mechanical response in four-point-bending tests.

The actual role and mechanisms, by which the polymer reinforces such cements, still have to be analysed in detail. Our calorimetric analysis already an insight on how the toughening and strengthening effect might take place although HEMA polymers do not strongly bind to mineral surfaces as they lack anionic side chains. The polymerization of HEMA quickly takes place at an early stage of the cement setting, and thus the morphology of the formed HEMA polymer matrix fills the intercrystalline volume and voids of the cement. After completion of the polymerization, the setting reaction still continues so that the formed polymer strands are incorporated into the crystals while Ostwald-ripening, phase transformation, and crystal growth further proceeds. Upon loading, the intracrystalline polymer matrix can then augment the mechanical response of the reinforced cement by a range of mechanisms, e.g., by fibre pull-out, ligament formation upon crack extension, or crack bridging mechanisms and other mechanisms which enhance stress distribution.^{43,44} In order to optimize the mechanical response of the polymer-enhanced cements, detailed and ultrastructural analyses have to be carried out in future. For instance, we expect that by crosslinking of the HEMA polymer matrix and by further introduction of optimized mineral binding sites into the polymer matrix, the mechanical properties of our cements can be further increased.

Conclusions

We developed a non-brittle Mg-doped polymer-reinforced cement with appealing mechanical properties which contains only calcium carbonate as the mineral component. By taking inspiration from biogenic ceramics, we addressed the issue of the poor mechanical performance of calcium carbonate-based cements which made their broad exploitation impossible although calcareous cements represent attractive and auspicious alternatives to CaP cements due to a higher expected biodegradation rate. This feasibility study involved also the optimization of the phase transformation rate of the highly reactive component amorphous calcium carbonate by stabilization *via* Mg-doping.

Since the mechanical performance of the cement was significantly improved by adding 50 wt% of HEMA polymer, the cement-polymer composites may be suitable even for minimally invasive injection to cure bone defects. By optimizing the cement's particle size distribution, as well as the liquid to powder ratio, further improvements of the system may be achieved. For further evaluation of such polymer-enhanced calcium carbonate cements as new bioceramics, further studies to characterize cell compatibility are envisaged.

Conflicts of interest

There are no conflicts to declare.

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