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# Manganese–cerium mixed oxides supported on rice husk based activated carbon with high sulfur tolerance for low-temperature selective catalytic reduction of nitrogen oxides with ammonia†

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A rice husk-derived activated carbon supported manganese–cerium mixed oxide catalyst (Mn–Ce/RAC) was prepared by an impregnation method and tested for the selective catalytic reduction of nitrogen oxides with ammonia (NH<sub>3</sub>-SCR). 5 wt% Mn–Ce/RAC catalyst showed the highest activity, yielding nearly 100% NO<sub>x</sub> conversion and N<sub>2</sub> selectivity at 240 °C at a space velocity of 30 000 h<sup>–1</sup>. Compared with commercial activated carbon supported manganese–cerium mixed oxide catalyst (Mn–Ce/SAC), a higher SCR performance with good SO<sub>2</sub> tolerance could be observed in the tested temperature range over the Mn–Ce/RAC catalyst. The characterization results revealed that the Mn–Ce/RAC catalyst had a higher Mn<sup>4+</sup>/Mn<sup>3+</sup> ratio, amount of chemisorbed oxygen and more Brønsted acid sites than the Mn–Ce/SAC catalyst. The XRD analysis indicated that Mn–Ce oxides were highly dispersed on the RAC support. These properties of Mn–Ce/RAC assisted the SCR reaction. Moreover, *in situ* DRIFTS results demonstrated that sulfate species formation on Mn–Ce/RAC was much less in the presence of SO<sub>2</sub> than that of Mn–Ce/SAC, which might be ascribed to the reduced alkalinity of the catalyst by the presence of SiO<sub>2</sub> in RAC.

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## Introduction

Nitrogen oxides (NO<sub>x</sub>) emitted from power plants and diesel engines are major air pollutants, which can result in acid rain, photochemical smog, and ozone destruction. Selective catalytic reduction (SCR) with NH<sub>3</sub> is the most widely used technology for post-NO<sub>x</sub> removal, and V<sub>2</sub>O<sub>5</sub>–WO<sub>3</sub>(MoO<sub>3</sub>)/TiO<sub>2</sub> has been commonly used with high catalytic activity at 300–400 °C.<sup>1–3</sup> However, several shortcomings of V<sub>2</sub>O<sub>5</sub>-based catalysts still need to be addressed, including the toxicity of vanadium, SO<sub>2</sub> oxidation to SO<sub>3</sub>, and the poor low-temperature SCR activity. Therefore, it is extremely desirable to develop environment-friendly non-vanadium-based catalysts with high catalytic activity, and high SO<sub>2</sub>-tolerance within low-temperature regions.

On the basis of the good low-temperature activity and their inherent environmentally benign characters, Mn-based

catalysts have been widely developed for SCR of NO with NH<sub>3</sub>.<sup>4–6</sup> Unfortunately, Mn-based catalysts are very sensitive to the presence of SO<sub>2</sub> in the feed gas, which can induce a severe deactivation.<sup>7,8</sup> Based on its high oxygen storage capacity and unique redox properties, ceria has been investigated extensively, which is usually introduced as a promoter for enhancing SO<sub>2</sub> resistance of Mn-based catalysts due to the interaction between MnO<sub>x</sub> and CeO<sub>x</sub>, leading to the inhibition of formation of ammonium sulfates and MnSO<sub>4</sub> on the catalyst surface.<sup>9–14</sup> Fan *et al.*<sup>13</sup> reported that a strong synergistic effect existed in Mn–Ce/CeAPSO-34 catalyst, which showed outstanding SO<sub>2</sub> tolerance and H<sub>2</sub>O resistance. Jin *et al.*<sup>14</sup> studied the role of ceria in the improved resistance for a Ce-modified Mn/TiO<sub>2</sub> catalyst. In their investigation, the introduction of Ce lessened the sulfation of the main active phase (MnO<sub>x</sub>) during low-temperature SCR processes in the presence of SO<sub>2</sub>. Nevertheless, it is still necessary to further improve the resistance of SO<sub>2</sub> for Mn–Ce binary metal oxide catalysts.

Generally, supports play an important role in SCR reaction. Proper supports not only can provide a huge surface to disperse the active components and prevent the formation of large crystalline particles but can also affect the sulfur tolerance. Carbon materials (*i.e.*, activated carbon (AC),<sup>15</sup> activated coke<sup>16</sup> and carbon fiber<sup>17</sup>) are widely used as supports for NH<sub>3</sub>-SCR reaction and exhibit a high NO<sub>x</sub> removal efficiency at low

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† Electronic supplementary information (ESI) available: Characteristics of raw biomasses, Raman spectra of different samples, Si 2p XPS spectra of Mn–Ce/RAC and Mn–Ce/SAC catalysts and FT-IR spectra of Mn–Ce/RAC and Mn–Ce/SAC catalysts before and after pretreatment with a flow of 800 ppm NO-800 ppm NH<sub>3</sub>-3% O<sub>2</sub>-300 ppm SO<sub>2</sub>-10 vol% H<sub>2</sub>O are shown. See DOI: 10.1039/c9ra03937f



temperatures (100–250 °C). Zhu *et al.* reported that activated carbon supported vanadium oxide catalyst showed high activity in presence of SO<sub>2</sub> at 180–250 °C due to formation of SO<sub>4</sub><sup>2-</sup>.<sup>15,18</sup> In addition, SiO<sub>2</sub> was proposed to be a structural promoter to enhance the SO<sub>2</sub> resistance of catalyst.<sup>19–21</sup> Liu *et al.*<sup>19</sup> observed that the addition of SiO<sub>2</sub> improved SCR performance of Ce/TiO<sub>2</sub> catalyst. They reported that the introduction of SiO<sub>2</sub> could weaken the alkalinity over the surface of Ce/TiO<sub>2</sub>-SiO<sub>2</sub> catalyst, which resulted in sulfate not easily accumulating on the surface of the Ce/TiO<sub>2</sub>-SiO<sub>2</sub> in comparison with the Ce/TiO<sub>2</sub>. From the research by Kobayashi *et al.*,<sup>20</sup> the SO<sub>2</sub> tolerance was found to be more excellent over vanadia loaded on TiO<sub>2</sub>-SiO<sub>2</sub> than over that on pure TiO<sub>2</sub>, which was ascribed to the increased acidity of the former. However, it should be noted that the SiO<sub>2</sub> precursors usually used were commercially made alkoxy silane compounds such as tetraethylorthosilicate, colloidal silica and tetramethylorthosilicate. Nakashima *et al.*<sup>22</sup> reported that acute exposure to tetraethylorthosilicate can lead to death. Thus, there is a need to find a safer and less expensive silica source.

Rice husk is a major agriculture by-product in several parts of Asia, mainly in China and India. This biomass waste possesses unique properties, such as high SiO<sub>2</sub> content, high porosity and large external surface area.<sup>23</sup> In addition, biomass has proven to be a promising type of raw material for producing activated carbon with high adsorption capacity.<sup>24,25</sup> These properties make the rice husk an idea biomass waste for use as an alternative silica source, a catalyst or a catalyst support for pollutant removal. Inspired by those mentioned points, it is speculated that rice husk might be a good option to be used as precursor for producing activated carbon, which could be used as supports for SCR processes and exhibit a good SO<sub>2</sub> tolerance at low temperatures.

In this paper, activated carbon was prepared from rice husk and subsequently impregnated with MnO<sub>x</sub> and CeO<sub>x</sub> for SCR of NO with NH<sub>3</sub>. The attempt was to develop low-temperature deNO<sub>x</sub> catalyst having good SO<sub>2</sub> tolerance. For comparison purposes, the catalytic activity of commercial activated carbon catalyst with the same active composition was investigated under the same working conditions.

## Experimental

The rice husk of the most widely grown variety of rice in China was chosen for this study. After receiving, it was thoroughly washed to remove impurities and then dried at 110 °C for 24 h. After drying, the sample was cut in uniform lengths of ≤5 mm. The proximate and elemental analysis of raw rice husk was in Table S1 in ESI.† It could be found that the raw sample showed a higher volatile and low N and S content, and the heating value was about 15 MJ kg<sup>-1</sup>. It was an ideal renewable energy resource, with minor environmental pollution.

### Chemically activated carbon

A known mass of rice husk was immersed in 100 ml of activating agent which comprised of H<sub>3</sub>PO<sub>4</sub> and H<sub>2</sub>O. The mixture was continuously stirred for 2 h, and then it was oven dried at

120 °C for 48 h. The activation of the mixture was performed in a fixed bed reactor. The reactor was heated to 800 °C at a heating rate of 5 °C min<sup>-1</sup> and maintained for 2 h in N<sub>2</sub> (200 ml min<sup>-1</sup>). Then, the sample was cooled down to room temperature under an N<sub>2</sub> atmosphere. The resulting activated carbon sample was washed with NaOH solution, followed by distilled water until the wash water reached a pH of 6–7 to remove residual PO<sub>4</sub><sup>3-</sup>. The final activated carbon sample was dried and sieved to obtain a particle size range of 40–60 mesh.

### Catalyst

The chemically activated carbon was supported with Mn and Ce using impregnation methods, where Mn and Ce nitrates (Mn/Ce molar ratio, 2 : 1) were dissolved in deionized water, and certain amount of the chemically activated carbon was added. The mixture of metal nitrates and carbon was heated and continuously stirred for 2 h. Then, the sample was dried for 12 h at 110 °C in a drying oven. After drying, the sample was calcined for 5 h at 500 °C in tubular furnace with heating rate of 10 °C min<sup>-1</sup> under N<sub>2</sub> atmosphere. Finally, the sample was cooled down to room temperature with protection of N<sub>2</sub>. Mn–Ce/activated carbon (with commercial activated carbon as the support) was also prepared through the same method for comparison. The commercial activated carbon made from sawdust was purchased from Sinopharm Chemical Reagent limited corporation. The resulting catalyst is denoted as Mn–Ce/XAC (X represents the initial raw material for the activated carbon preparation, X = R and S). For example, Mn–Ce/RAC and Mn–Ce/SAC indicate the rice husk-based activated carbon supported Mn–Ce catalyst and the sawdust-based activated carbon supported Mn–Ce catalyst, respectively.

### SCR activity measurements

NH<sub>3</sub>-SCR activity measurements were carried out in a fixed-bed quartz flow reactor (i.d. 9 mm) containing 0.5 g of catalyst. The reactor was electrically heated, which was described in detail in our previous study.<sup>26</sup> The typical composition of the reactant gas was: 1000 ppm NO, 1000 ppm NH<sub>3</sub>, 3 vol% O<sub>2</sub>, 200 ppm SO<sub>2</sub> (when needed), and N<sub>2</sub> as the balance gas. The total flow rate was 500 ml min<sup>-1</sup> (refers to 1 atm and 298 K) which corresponded to a gas hourly space velocity (GHSV) of 30 000 h<sup>-1</sup>. Before entering the reactor, the reactant gases were mixed in a mixing tubing, but NH<sub>3</sub> was fed directly into the reactor by passing the mixing tubing to avoid possible reaction between SO<sub>2</sub> and NH<sub>3</sub> before the catalyst bed. Water vapor was generated by passing N<sub>2</sub> through a gas-wash bottle containing deionized water. The tubings of the reactor system were heated to prevent the formation and deposition of ammonium sulfate/bisulfate and ammonium nitrate. The NO, NO<sub>2</sub>, NH<sub>3</sub>, SO<sub>2</sub> and N<sub>2</sub>O concentrations were measured online with a Fourier transform infrared (FTIR) analyzer system (GASMET DX-4000) produced by Gasmet Technologies, Inc. in Finland. The O<sub>2</sub> concentrations were measured *via* an electrochemical gas analyser (Testo 340). The reaction system was kept for 1 h at each reaction temperature to reach a steady state before the analysis of the product



was performed. The  $\text{NO}_x$  conversion and  $\text{N}_2$  selectivity were calculated as follows:

$$\text{NO}_x \text{ conversion} = \left(1 - \frac{[\text{NO}_x]_{\text{out}}}{[\text{NO}_x]_{\text{in}}}\right) \times 100\%$$

$\text{N}_2$  selectivity

$$= \frac{[\text{NO}_x]_{\text{in}} + [\text{NH}_3]_{\text{in}} - [\text{NO}_x]_{\text{out}} - [\text{NH}_3]_{\text{out}} - 2[\text{N}_2\text{O}]_{\text{out}}}{[\text{NO}_x]_{\text{in}} + [\text{NH}_3]_{\text{in}} - [\text{NO}_x]_{\text{out}} - [\text{NH}_3]_{\text{out}}} \times 100$$

where  $[\text{NO}_x] = [\text{NO}] + [\text{NO}_2]$ ,  $[\text{NO}_x]_{\text{in}}$  and  $[\text{NO}_x]_{\text{out}}$  were the concentrations of  $\text{NO}_x$  at the inlet and outlet of the tube, respectively. In order to confirm that the decrease of  $\text{NO}_x$  was not caused by the adsorption of  $\text{NO}_x$  at the beginning of each experiment, the catalyst was purged with the reactant gas until there was no difference between the inlet and the outlet gas.

### Catalyst characterization

The specific surface areas of the catalysts were measured by nitrogen adsorption using the Brunauer–Emmett–Teller (BET) method (Quadrasorb SI). Powder X-ray diffraction (XRD) measurements were carried out on a Rigaku D/MAX-2400 X-ray diffractometer with Cu K $\alpha$  radiation. X-ray photoelectron spectroscopy (XPS) was implemented on a surface analysis system (Thermal ESCALAB 250) using Al K $\alpha$  radiation. The C 1s line at 284.6 eV was considered as a reference for the binding energy calibration. The peak fitting was carried out using a XPSPEAK41 processing program. Temperature-programmed reduction ( $\text{H}_2$ -TPR) was performed on a ChemBET PULSAR TPR/TPD instrument. Prior to TPR experiments, the catalysts were pretreated at 400 °C for 2 h under helium flow, then cooled down to room temperature. Finally, the reactor temperature was raised to 700 °C at a constant heating rate of 10 °C min<sup>-1</sup> in a flow of  $\text{H}_2$  (5 vol%)/He. Temperature-programmed desorption (TPD) experiments of  $\text{NH}_3$  and  $\text{SO}_2$  were performed on the same ChemBET PULSAR TPR/TPD instrument. The experiment consisted of four stages: (i) degasification of the sample in He at 400 °C for 2 h, (ii) adsorption of  $\text{NH}_3$  (300 ppm  $\text{SO}_2$  + 3%  $\text{O}_2$ ) at room temperature for 1 h, (iii) isothermal desorption under He until no  $\text{NH}_3$  ( $\text{SO}_2$ ) was detected, and (iv) temperature-programmed desorption under He at 10 °C min<sup>-1</sup> to 500 °C or 800 °C. *In situ* diffuse reflectance infrared Fourier transform spectroscopy (*in situ* DRIFTS) was performed on a FTIR spectrometer (Bruker Vertex 70) equipped with a high sensitivity MCT detector cooled by liquid  $\text{N}_2$ . An approximately 12 mg sample was finely ground and pressed into a self-supported wafer. Mass flow controllers and a sample temperature controller were used to simulate the real reaction conditions. Prior to each experiment, the wafer was heated to 350 °C in  $\text{N}_2$  (99.999%) for 1 h and then cooled down to the desired reaction temperature. The background spectrum was collected in flowing  $\text{N}_2$  and automatically subtracted from the sample spectrum. The reaction conditions were controlled as follows: 500 ml min<sup>-1</sup> total flow rate, 500 ppm NO, 500 ppm  $\text{NH}_3$ , 3%  $\text{O}_2$ , (100 ppm  $\text{SO}_2$  when used) and  $\text{N}_2$  balance. All spectra were

recorded by accumulating 100 scans with a resolution of 4 cm<sup>-1</sup>.

## Results and discussion

### Effect of the loading amounts of Mn–Ce on SCR activity

Fig. 1 displays  $\text{NO}_x$  conversion and  $\text{N}_2$  selectivity at various temperatures for the Mn–Ce/RAC-catalyzed  $\text{NH}_3$ -SCR reaction with varying Mn–Ce loadings. The SCR activity of the RAC were quite low in the whole temperature range, with  $\text{NO}_x$  conversions less than 9%. After Mn–Ce oxide species were loaded onto the RAC, the  $\text{NO}_x$  conversion of Mn–Ce/RAC was greater than 80% at 240 °C. It demonstrated that Mn–Ce based catalyst could exhibited high SCR activity at relatively low temperature range as the literatures reported.<sup>27</sup> As the Mn–Ce loading increased from 1 wt% to 5 wt%, the  $\text{NO}_x$  conversion improved gradually. At a Mn–Ce loading of 5 wt%, for example, the  $\text{NO}_x$  conversion was 99.4% at 240 °C. Further increase of the Mn–Ce loading from 5 wt% to 10 wt% led to certain decline in  $\text{NO}_x$  conversion at both low and high temperatures, which might be ascribed to aggregation of active component on the surface of RAC.<sup>27,28</sup> All of the catalysts exhibited high  $\text{N}_2$  selectivity (>95%) across tested temperature ranges (as shown in inset of Fig. 1). The formation of  $\text{N}_2\text{O}$  was less than 5 ppm. Since the 5 wt% Mn–Ce/RAC catalyst showed the highest SCR activity, all of the Mn–Ce/RAC catalysts that appeared below had a Mn–Ce loading of 5 wt%.

### Comparison with Mn–Ce/SAC catalyst

In order to test the effect of the support, the  $\text{NO}_x$  conversion and  $\text{N}_2$  selectivity over Mn–Ce/RAC and Mn–Ce/SAC catalysts were compared, and the results are shown in Fig. 2. The active component loading and the experimental conditions were the same. The Mn–Ce/RAC catalyst showed a higher SCR activity in the whole temperature range than Mn–Ce/SAC, together with much better  $\text{N}_2$  selectivity. It indicated that the activity of Mn–Ce/RAC catalyst was significantly improved in comparison with Mn–Ce/SAC catalyst by taking the RAC as support.

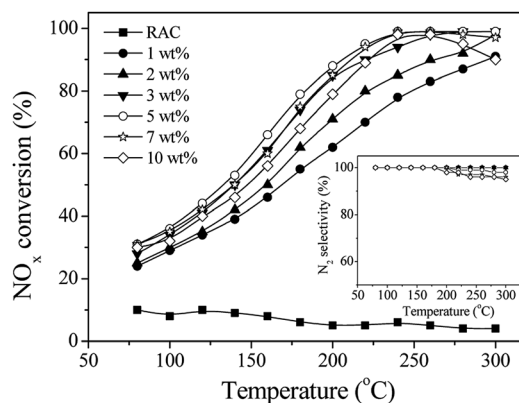


Fig. 1  $\text{NO}_x$  conversion during the SCR reaction over Mn–Ce/RAC catalysts with different Mn–Ce loadings. Reaction conditions: 800 ppm NO, 800 ppm  $\text{NH}_3$ , 3%  $\text{O}_2$ ,  $\text{N}_2$  as balance gas, and GHSV = 30 000 h<sup>-1</sup>. Inset:  $\text{N}_2$  selectivity during the SCR reaction.



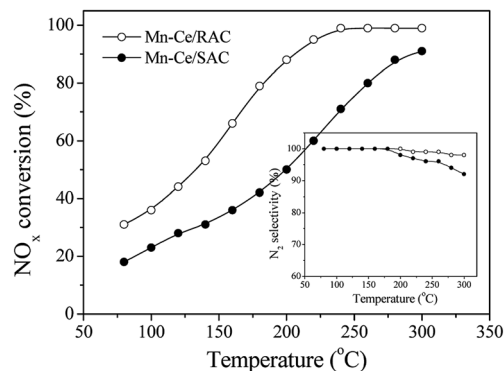


Fig. 2  $\text{NO}_x$  conversion during the SCR reaction over Mn–Ce/RAC and Mn–Ce/SAC catalysts. Reaction conditions: 800 ppm NO, 800 ppm  $\text{NH}_3$ , 3%  $\text{O}_2$ ,  $\text{N}_2$  as balance gas, and GHSV = 30 000  $\text{h}^{-1}$ . Inset:  $\text{N}_2$  selectivity during the SCR reaction.

### Effects of $\text{SO}_2$ and $\text{H}_2\text{O}$

The emissions of  $\text{SO}_2$  and  $\text{H}_2\text{O}$  are unavoidable in exhaust and flue gases, and the investigation of the impact of  $\text{SO}_2$  and  $\text{H}_2\text{O}$  on the SCR activity of catalysts is therefore important. Fig. 3A shows the SCR activity over the Mn–Ce/RAC and Mn–Ce/SAC catalysts in the presence of 10 vol%  $\text{H}_2\text{O}$  at 240 °C. When the steam was added to the reaction system, the  $\text{NO}_x$  conversions of the two catalysts were little changed within 10 h. This suggested that individual  $\text{H}_2\text{O}$  in the feed gas at 240 °C had nearly no influence on the SCR activity of Mn–Ce/RAC and Mn–Ce/SAC catalysts.

Fig. 3B depicts the  $\text{SO}_2$  tolerance tests of the catalysts in the presence of 300 ppm  $\text{SO}_2$  at 240 °C. The  $\text{NO}_x$  conversion over Mn–Ce/RAC decreased slightly after  $\text{SO}_2$  was added to the reaction gas, and it then reached a steady state. After switching  $\text{SO}_2$  off, the activity was restored. In contrast, in the case of Mn–Ce/SAC, the introduction of  $\text{SO}_2$  induced a dramatic drop from 80% to 63% after 10 h, and the  $\text{NO}_x$  conversion of Mn–Ce/SAC only returned to 70%, far from the initial level. These results demonstrated that the Mn–Ce/RAC catalyst presented

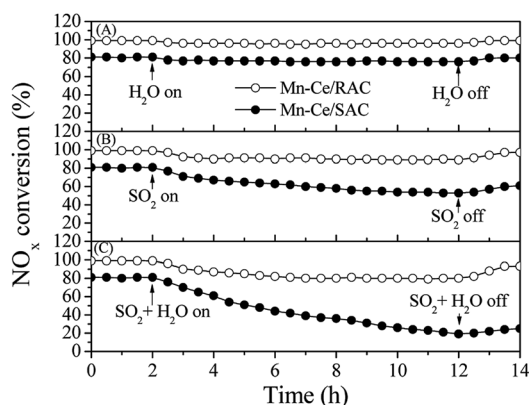


Fig. 3 (A)  $\text{H}_2\text{O}$  resistance, (B)  $\text{SO}_2$  tolerance, (C)  $\text{SO}_2$  and  $\text{H}_2\text{O}$  synergistic effect study of the catalysts at 240 °C. Reaction conditions: 800 ppm NO, 800 ppm  $\text{NH}_3$ , 300 ppm  $\text{SO}_2$  (when used), 10 vol%  $\text{H}_2\text{O}$  (when used), 3%  $\text{O}_2$ ,  $\text{N}_2$  as balance gas, and GHSV = 30 000  $\text{h}^{-1}$ .

advantages in  $\text{SO}_2$  tolerance over the Mn–Ce/SAC catalyst. According to literatures,<sup>8,18</sup> the deactivation of the catalyst caused by  $\text{SO}_2$  was related with the formation of  $(\text{NH}_4)_2\text{SO}_4$  or  $\text{NH}_4\text{HSO}_4$ , which deposited on the surface of catalyst and blocked the partial active sites.

The combined impact of  $\text{SO}_2$  and  $\text{H}_2\text{O}$  on SCR activity were also investigated (Fig. 3C). The introduction of  $\text{SO}_2$  and  $\text{H}_2\text{O}$  induced a 18% decrease in the  $\text{NO}_x$  conversion over Mn–Ce/RAC. But the  $\text{NO}_x$  conversion gradually recovered to 93% after shutting off the supply of  $\text{SO}_2$  and  $\text{H}_2\text{O}$ . However, the conversion of  $\text{NO}_x$  on Mn–Ce/SAC decreased quickly from 80% to 35% and barely recovered even though  $\text{SO}_2 + \text{H}_2\text{O}$  was eliminated. It indicated that there was a synergistic inhibition effect between  $\text{SO}_2$  and  $\text{H}_2\text{O}$  in the SCR reaction. When  $\text{SO}_2$  and  $\text{H}_2\text{O}$  were added simultaneously, water would make the formation of the ammonium sulfate species more rapid, resulting in a dramatic decrease in  $\text{NO}_x$  conversion.<sup>29</sup> It could be concluded from the above results that Mn–Ce/RAC were highly sulfur-tolerant and water-resistant, and RAC presented a positive role in the sulfur and water tolerance of the catalyst.

### Characterization of supports and catalysts

**BET.** The BET surface, pore volume and pore size of the catalysts are summarized in Table 1. It could be seen that the surface area and total pore volume of the catalysts decreased after the impregnation process, which might be resulted from the clogging of pores by the impregnated metallic oxides.<sup>30,31</sup> Mn–Ce/RAC showed a smaller loss of BET surface area than Mn–Ce/SAC after loading with the Mn and Ce oxides. In addition, compared with the Mn–Ce/SAC, the Mn–Ce/RAC had lower surface area and total pore volume, but a higher activity towards  $\text{NO}_x$  reduction. This agreed with previous findings that the catalytic activity was more dependent on surface chemistry than surface area.<sup>32</sup>

**XRD.** The XRD patterns of various samples are displayed in Fig. 4. A broad diffraction peak was observed at  $\sim 24.5^\circ$  for all the samples, which indicated that the activated carbon sample had a low graphitization structure.<sup>33</sup> After introducing Mn and Ce oxides, no visible phase of manganese oxides and ceria could be observed on Mn–Ce/RAC, but the  $\text{Mn}_2\text{O}_3$  (JCPDS 06-0540),  $\text{MnO}_2$  (JCPDS 30-0820) and cubic  $\text{CeO}_2$  (JCPDS 43-1002) phases could be detected on Mn–Ce/SAC. These results indicated that the active components Mn and Ce oxides were highly dispersed on the surface of the RAC support. In combination with XPS results in the following section, the reason for the high dispersion of Mn and Ce oxides on RAC might be that a large amount of surface oxygen groups on RAC could accelerate the

Table 1 Physical properties of various samples

Sample	BET surface area ( $\text{m}^2 \text{g}^{-1}$ )	Total pore volume ( $\text{ml g}^{-1}$ )	Average pore diameter (nm)
RAC	291.6	0.18	2.79
Mn–Ce/RAC	249.5	0.13	3.87
SAC	382.9	0.24	2.14
Mn–Ce/SAC	265.8	0.14	2.51





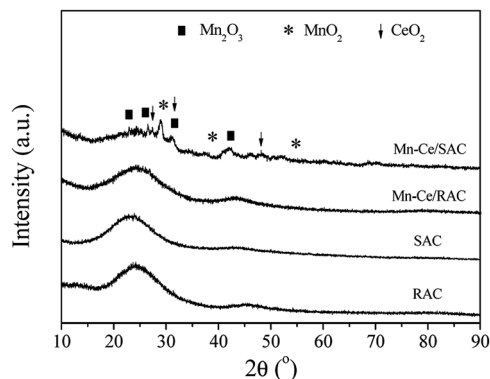


Fig. 4 The XRD patterns of various samples.

diffusion of Mn and Ce ions into the inner pores of RAC by the interaction between Mn and Ce precursors and surface oxygen groups, resulting in an improvement of the dispersion of Mn and Ce oxides.<sup>34</sup> The highly dispersed active phases were demonstrated to improve the surface properties of catalysts, resulting in an enhancement of the catalytic activity,<sup>16</sup> which was in accordance with the SCR activity results. Fig. S1† compares the Raman spectra of RAC and SAC based catalysts. Three characteristic peaks at about  $1350\text{ cm}^{-1}$  (D band),  $1590\text{ cm}^{-1}$  (G band) and  $2700\text{ cm}^{-1}$  (2D band) in the graphitized structures were observed in the Raman spectrum of all the samples.<sup>35</sup>

**XPS.** The catalysts were further analyzed using XPS to identify the surface nature and content of the active species. Surface atomic contents of Mn, Ce, O and Si are summarized in Table 2, and photoelectron spectra of Mn 2p, Ce 3d and O 1s levels are displayed in Fig. 5. As listed in Table 2, the Mn and Ce concentrations on Mn-Ce/RAC were higher than those on Mn-Ce/SAC. And the results of Fig. 4 indicated that the enrichment of Mn and Ce on the surface of the Mn-Ce/RAC catalyst did not lead to the crystallization in the catalyst. These implied that Mn-Ce/RAC had a higher ability to disperse Mn and Ce oxides than Mn-Ce/SAC. In addition, on the Mn-Ce/SAC catalyst no obvious Si 2p band was detected, while an evident band attributed to Si 2p was observed on the Mn-Ce/RAC catalyst (Fig. S2 in ESI†). The binding energies of this Si 2p was  $103.8\text{ eV}$ , which was consistent with the Si(IV) oxidation state and assigned to the  $\text{SiO}_2$  species.<sup>36</sup>

In Fig. 5A, two main peaks of Mn  $2p_{3/2}$  and Mn  $2p_{1/2}$  were observed in the binding energy range from  $636\text{ eV}$  to  $660\text{ eV}$ . The asymmetric Mn  $2p_{3/2}$  peak confirmed the existence of mixed valence of manganese states. Thus, the Mn oxide states were further analyzed by deconvolution and curve fitting procedures.

Table 2 XPS results of Mn-Ce/RAC and Mn-Ce/SAC catalysts

Catalyst	Surface atomic content (%)				$\text{Mn}^{4+}/\text{Mn}^{3+}$	$\text{Ce}^{3+}/(\text{Ce}^{3+} + \text{Ce}^{4+})$ (%)	$\text{O}_\alpha/(\text{O}_\alpha + \text{O}_\beta)$ (%)
	Mn	Ce	O	Si			
Mn-Ce/RAC	11.2	4.2	48.5	5.1	3.35	40.5	48.5
Mn-Ce/SAC	8.7	3.8	44.2	0.9	2.07	20.9	32.6

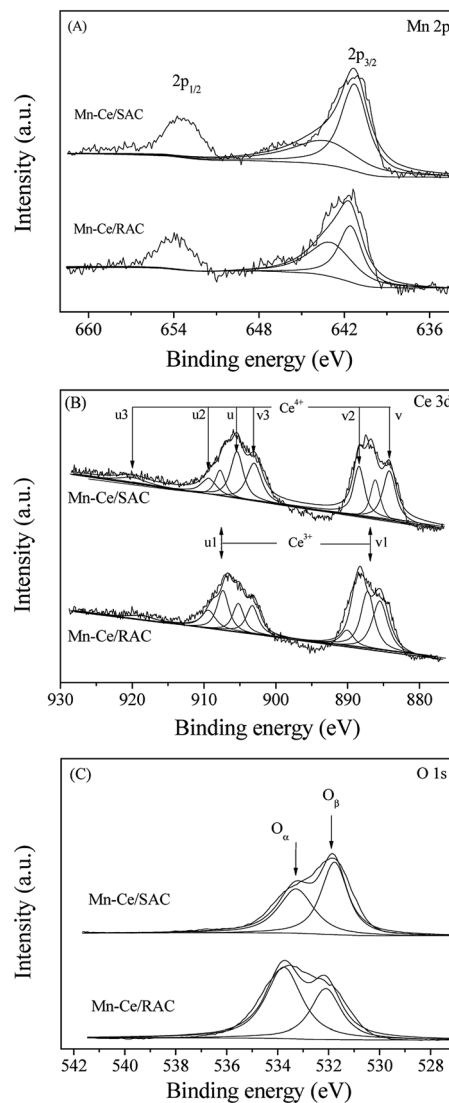


Fig. 5 (A) Mn 2p, (B) Ce 3d and (C) O 1s XPS spectra of Mn-Ce/RAC and Mn-Ce/SAC catalysts.

The binding energy for  $\text{Mn}^{4+}$  is approximately  $643.1\text{ eV}$ , whereas the binding energy for  $\text{Mn}^{3+}$  is approximately  $641.7\text{ eV}$ .<sup>37,38</sup> As observed in Table 2, the  $\text{Mn}^{4+}/\text{Mn}^{3+}$  ratio for Mn-Ce/RAC was higher than Mn-Ce/SAC. This suggested a higher average valence state of Mn ions on the surface of Mn-Ce/RAC than that on Mn-Ce/SAC. It is well known that  $\text{Mn}^{4+}$  species is more active than  $\text{Mn}^{3+}$  species, and the  $\text{Mn}^{4+}$  can enhance the NO to  $\text{NO}_2$  oxidation and as a result of this promoting the SCR reaction through the “fast SCR” pathway. Therefore, Mn-Ce/RAC exhibited higher  $\text{NO}_x$  conversion than Mn-Ce/SAC, as shown in Fig. 2.

The Ce 3d XPS spectra of Mn-Ce/RAC and Mn-Ce/SAC catalysts (Fig. 5B) were fitted into two bands (u and v). The bands labeled u1 and v1 represent the  $3d^{10} 4f^1$  initial electronic state, corresponding to  $\text{Ce}^{3+}$ , whereas the peaks labeled u, u2, u3, v, v2 and v3 represent the  $3d^{10} 4f^0$  state of  $\text{Ce}^{4+}$  ions.<sup>39</sup> The intensities of  $\text{Ce}^{3+}$  characteristic peaks over Mn-Ce/RAC were more intense than those over Mn-Ce/SAC. The  $\text{Ce}^{3+}$  ratio,



calculated by  $\text{Ce}^{3+}/(\text{Ce}^{3+} + \text{Ce}^{4+})$ , of Mn–Ce/RAC (40.5%) was higher than that of Mn–Ce/SAC (20.9%), as listed in Table 2. It indicated that Ce was in a partially reduced state on the surface of the Mn–Ce/RAC catalyst, which might be attributed to the presence of  $\text{SiO}_2$  in RAC.<sup>19</sup> Some researchers have reported that the presence of  $\text{Ce}^{3+}$  could induce charge imbalance, more vacancies and unsaturated chemical bonds on the catalyst surface, and thus lead to the increase of surface chemisorbed oxygen.<sup>40,41</sup>

Fig. 5C reveals the fitted O 1s peaks for lattice oxygen  $\text{O}^{2-}$  at 529.5–529.8 eV (denoted as  $\text{O}_\beta$ ) and chemisorbed oxygen at 531.0–531.4 eV (denoted as  $\text{O}_\alpha$ ), such as  $\text{O}_2^{2-}$  and  $\text{O}^-$  belonging to defect-oxide or hydroxyl-like group.<sup>42</sup> As shown in Table 2, the  $\text{O}_\alpha$  of Mn–Ce/RAC (48.5%) calculated by  $\text{O}_\alpha/(\text{O}_\alpha + \text{O}_\beta)$  was much higher than that of Mn–Ce/SAC (32.6%). Surface chemisorbed oxygen ( $\text{O}_\alpha$ ) has been reported to be more active than lattice oxygen ( $\text{O}_\beta$ ) due to its higher mobility and plays an important role in oxidation reactions.<sup>43</sup> Therefore, the higher  $\text{O}_\alpha$  on Mn–Ce/RAC was beneficial for the NO oxidation to  $\text{NO}_2$  in the SCR reaction, and thereby facilitated the “fast SCR” reaction and enhanced de $\text{NO}_x$  efficiency. On the other hand, a larger amount of surface hydroxyl groups could act as Brønsted acid sites to enhance the  $\text{NH}_3$  adsorption.<sup>2,3</sup> The enhancement of  $\text{NH}_3$  adsorption over the Mn–Ce/RAC catalyst would be discussed later.

**$\text{H}_2$ -TPR and  $\text{NH}_3$ -TPD.** The redox properties of the Mn–Ce/RAC and Mn–Ce/SAC catalysts are examined using  $\text{H}_2$ -TPR experiment (as shown in Fig. 6). It could be seen that there was one broad peak on these two catalysts. This suggested that the reducible metal oxide species might exist in a mixed valence. As for Mn–Ce/SAC catalyst, the TPR profile was fitted into two reduction peaks: the peak at 452 °C was ascribed to the reduction of  $\text{MnO}_2$  to  $\text{Mn}_2\text{O}_3$ , while the peak at 497 °C was attributed to the reduction of  $\text{Mn}_2\text{O}_3$  to MnO and surface cerium oxides.<sup>44</sup> In terms of Mn–Ce/RAC catalyst, the TPR profile was also fitted into two peaks corresponding to the reduction of Mn and Ce oxide species. Compared with Mn–Ce/SAC, the reduction peaks of Mn–Ce/RAC shifted toward a lower temperature region. As reported in the literature,<sup>5</sup> the lower reduction temperature for the catalyst indicated better redox characteristics. The redox character for the Mn–Ce/RAC catalyst seemed to be better than the Mn–Ce/SAC catalyst.

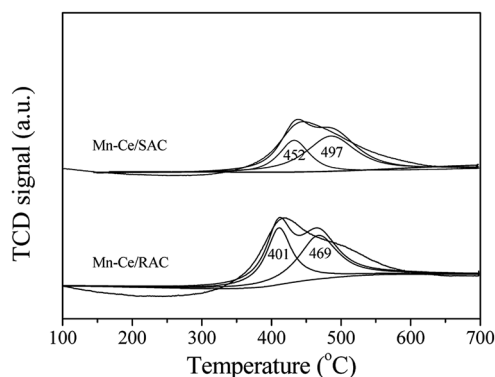


Fig. 6  $\text{H}_2$ -TPR profiles of Mn–Ce/RAC and Mn–Ce/SAC catalysts.

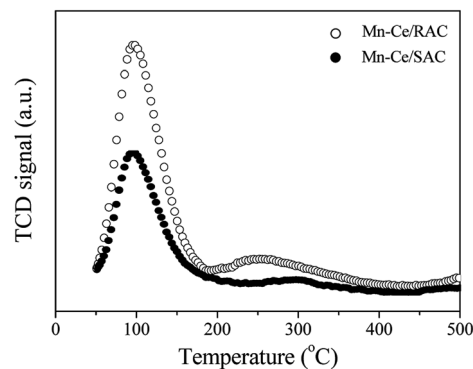


Fig. 7  $\text{NH}_3$ -TPD profiles of Mn–Ce/RAC and Mn–Ce/SAC catalysts.

The  $\text{NH}_3$ -TPD profiles of the Mn–Ce/RAC and Mn–Ce/SAC catalysts are shown in Fig. 7. The desorption peaks of these two catalysts appeared primarily in the temperature range of 50–150 °C (weak acid sites) and 220–360 °C (medium acid sites), respectively.<sup>45</sup> It was found that the intensities of desorption peaks (weak and medium acid sites) on the surface of the Mn–Ce/RAC catalyst were obviously higher than those on the Mn–Ce/SAC catalyst, especially for the desorption peak belonging to weak acid sites. This result implied that the Mn–Ce/RAC catalyst had more acidic sites than the Mn–Ce/SAC catalyst. Many research showed that the surface acidity played a critical role in SCR reaction.<sup>4–6</sup> Consequently, the increased acidic sites might represent one of the most important reasons for the higher catalytic activity of the Mn–Ce/RAC catalyst than that of the Mn–Ce/SAC catalyst.

**$\text{SO}_2$ -TPD.**  $\text{SO}_2$ -TPD experiments over Mn–Ce/RAC and Mn–Ce/SAC catalysts pretreated with a  $\text{SO}_2$ - $\text{O}_2$  coexisting feed gas were performed to determine adsorption/desorption characteristics of  $\text{SO}_2$  over the catalysts. The catalysts for the TPD experiments were treated with a flow of 300 ppm  $\text{SO}_2$  + 3%  $\text{O}_2$  at 240 °C, as shown in Fig. 8. One major  $\text{SO}_2$  desorption peak was found for Mn–Ce/RAC and Mn–Ce/SAC at around 460 °C, which could be ascribed to the decomposition of sulfate species on the surface of the catalyst.<sup>46,47</sup> The  $\text{SO}_2$  desorption peak for the Mn–Ce/RAC catalyst was obviously smaller than that for the Mn–Ce/SAC catalyst, demonstrating that the Mn–Ce/RAC was more  $\text{SO}_2$  resistance and with less  $\text{SO}_2$  adsorption on its surface. It was

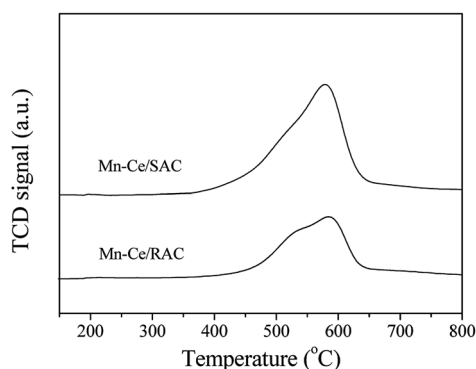


Fig. 8  $\text{SO}_2$ -TPD profiles of Mn–Ce/RAC and Mn–Ce/SAC catalysts.



found by Liu *et al.*<sup>19</sup> that the addition of SiO<sub>2</sub> to SCR catalyst could weaken the alkalinity of the catalyst, which resulted in sulfate species not easily adsorbing on the surface of the catalyst. Hence, the presence of SiO<sub>2</sub> in RAC support reduced the alkalinity on the surface of Mn–Ce/RAC catalyst, thereafter suppressing the formation of sulfate species. This might represent a significant factor for the high activity of the Mn–Ce/RAC in the presence of SO<sub>2</sub> + H<sub>2</sub>O (as shown in Fig. 3).

**In situ DRIFTS study.** To further distinguish between the different acid types (Lewis or Brønsted acid sites on the catalyst surface), *in situ* DRIFTS experiments were employed to study the NH<sub>3</sub> adsorption/desorption behavior of the catalysts. The DRIFTS spectra of NH<sub>3</sub> over Mn–Ce/RAC and Mn–Ce/SAC catalysts at 240 °C are shown in Fig. 9. After samples were exposed to NH<sub>3</sub> in N<sub>2</sub> for 60 min and purge with N<sub>2</sub>, the bands at 1685 cm<sup>−1</sup> and 1410 cm<sup>−1</sup> were assigned to the symmetric and asymmetric bending vibrations of NH<sub>4</sub><sup>+</sup> species on Brønsted acid sites,<sup>48,49</sup> while the bands at 1602 cm<sup>−1</sup>, 1245 and 1180 cm<sup>−1</sup> were attributed to symmetric and asymmetric bending vibrations of the N–H bonds in NH<sub>3</sub> coordinated to Lewis acid sites.<sup>48,50</sup> Obviously, the stronger NH<sub>4</sub><sup>+</sup> (1671 and 1428 cm<sup>−1</sup>) bands were observed on Mn–Ce/RAC, despite its low surface area, than those on Mn–Ce/SAC, indicating that the Brønsted acid sites was enhanced on the Mn–Ce/RAC catalyst. Some researchers showed that the presence of SiO<sub>2</sub> could enhance surface acidity of the catalyst, especially the number of Brønsted acid sites.<sup>19,51</sup> Thus, the enhanced Brønsted acid sites of Mn–Ce/RAC, compared with that of Mn–Ce/SAC, should be ascribed to the presence of SiO<sub>2</sub> in RAC support.

To understand deactivation mechanism of Mn–Ce/RAC and Mn–Ce/SAC by SO<sub>2</sub> for the NH<sub>3</sub>-SCR, the DRIFTS spectra of catalysts in a flow of NH<sub>3</sub> + NO + O<sub>2</sub> before and after the addition of 100 ppm SO<sub>2</sub> at 240 °C were recorded. Fig. 10A shows the DRIFTS spectra of Mn–Ce/SAC catalyst. When a mixture of NH<sub>3</sub>, NO, O<sub>2</sub> and N<sub>2</sub> were flowed over the catalyst for 30 min, the bands ascribed to ionic NH<sub>4</sub><sup>+</sup> (1670 cm<sup>−1</sup>) and coordinated NH<sub>3</sub> (1245 cm<sup>−1</sup>) showed up.<sup>48,49</sup> The band at 1258 cm<sup>−1</sup> might be attributed to nitrate species.<sup>52</sup> After SO<sub>2</sub> was flowed for 5 min, the intensity of the band at 1258 cm<sup>−1</sup> due to nitrate species increased obviously, and its position moved to high wavenumber at 1262 cm<sup>−1</sup>. According to the reported literature,<sup>53</sup> we

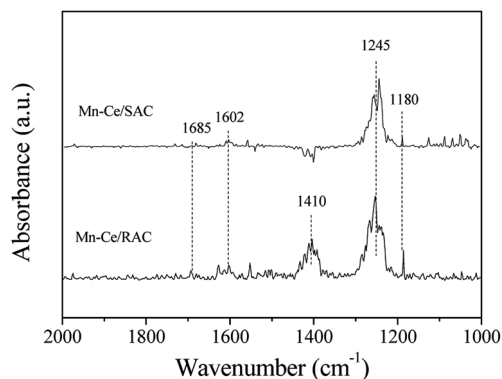


Fig. 9 DRIFTS spectra of NH<sub>3</sub> adsorption over Mn–Ce/RAC and Mn–Ce/SAC catalysts at 240 °C.

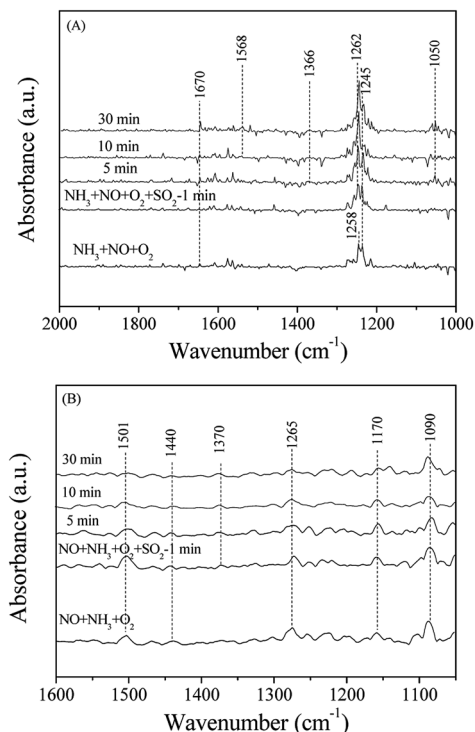


Fig. 10 DRIFTS spectra of Mn–Ce/SAC (A) and Mn–Ce/RAC (B) catalysts in a flow of NH<sub>3</sub> + NO + O<sub>2</sub> before and after the addition of 100 ppm SO<sub>2</sub> at 240 °C.

could assign the bands at 1262 (overlap band) and 1366 cm<sup>−1</sup> to the deposited sulfate species. The band at 1050 cm<sup>−1</sup> might be attributed to the perturbation of sulfate species (*vs* S–O) through reaction with NH<sub>3</sub> to form ammonium sulfate.<sup>50</sup> Moreover, HSO<sub>4</sub><sup>−</sup> (1568 cm<sup>−1</sup>)<sup>54</sup> was also found to increase with SO<sub>2</sub> exposure time verifying the formation of NH<sub>4</sub>HSO<sub>4</sub>. These results suggested that the formation of (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> and NH<sub>4</sub>HSO<sub>4</sub> should be responsible for the deactivated observed for the Mn–Ce/SAC catalyst (as shown in Fig. 3), which was in agreement with a previous report.<sup>15,18</sup> From Fig. 10B, when the SCR gases were directed into the reactor for 30 min, the adsorption peaks of NH<sub>4</sub><sup>+</sup> (1440 cm<sup>−1</sup>) and coordinated NH<sub>3</sub> (1265 and 1170 cm<sup>−1</sup>) appeared on the surface of the Mn–Ce/RAC catalyst. Anionic nitrosyl NO<sup>−</sup> species have been observed by some researchers giving rise to absorption in the region of 1200–1000 cm<sup>−1</sup>.<sup>55,56</sup> So the band at 1090 cm<sup>−1</sup> could be assigned to anionic nitrosyl NO<sup>−</sup> species. Additional adsorbed species was also found, namely *cis*-N<sub>2</sub>O<sub>2</sub><sup>2−</sup> (1501 cm<sup>−1</sup>).<sup>57</sup> After the addition of SO<sub>2</sub>, no obvious change was observed on Mn–Ce/RAC, except for that a weak adsorption peak linked to sulfate species (1370 cm<sup>−1</sup>) was detected after 5 min. These results demonstrated that the Mn–Ce/SAC catalyst exhibited significant adsorption of SO<sub>2</sub> which leads to deactivation caused by (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> and NH<sub>4</sub>HSO<sub>4</sub> formation on the surface of the catalyst. Conversely, the Mn–Ce/RAC catalyst resulted in very minor formation of sulfate species after SO<sub>2</sub> exposure, demonstrating an improved SO<sub>2</sub> resistance of the catalyst. This was consistent with the Fourier transform infrared spectroscopy (FT-IR) results (Fig. S3 in ESI<sup>†</sup>) that there was little ammonium-



sulfate salts deposited on the surface of the Mn–Ce/RAC catalyst compared to that of the Mn–Ce/SAC catalyst during the pretreatment with a flow of NO–NH<sub>3</sub>–O<sub>2</sub>–SO<sub>2</sub>–H<sub>2</sub>O.

## Conclusions

This work has evaluated rice husk-derived activated carbon impregnated with the Mn–Ce as a potential catalyst in the NH<sub>3</sub>–SCR. Mn–Ce loading enhanced the SCR performance of RAC, and 5 wt% was the optimum mass ratio for the Mn–Ce/RAC catalyst. In comparison with the Mn–Ce/SAC, the Mn–Ce/RAC had a high SCR performance and a good tolerance to SO<sub>2</sub>. The XRD analysis indicated that Mn–Ce was more dispersed on the surface of RAC support than SAC support. The high Mn<sup>4+</sup>/Mn<sup>3+</sup> ratios, chemisorbed oxygen content and more Brønsted acid sites as well as the enhanced redox activity of the Mn–Ce/RAC catalyst improved its NH<sub>3</sub>–SCR activity. *In situ* DRIFTS results demonstrated that sulfate formation was suppressed on the surface of the RAC support, which might be the most significant reason that Mn–Ce/RAC maintained a high SCR activity in the presence of SO<sub>2</sub>. This study demonstrated that the rice husk might be a potential material for use as a low temperature SCR catalytic support instead of the commercial activated carbon.

## Conflicts of interest

There are no conflicts to declare.

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