



Cite this: *RSC Adv.*, 2019, 9, 21844

# Development of core–sheath structured smart nanofibers by coaxial electrospinning for thermo-regulated textiles

Liqiang Yi,<sup>†a</sup> Yan Wang,<sup>†a</sup> Yini Fang,<sup>a</sup> Ming Zhang,<sup>●</sup>\*<sup>a</sup> Juming Yao,<sup>a</sup> Lina Wang<sup>a</sup> and Jaromir Marek<sup>b</sup>

It is of great significance to develop phase change materials (PCMs) with high performance. The reported PCMs usually possess serious defects like low heat capacity and poor thermal stability. Here, core–sheath structured nanofibers with polyvinyl butyral (PVB) as the sheath and octadecane as the core were fabricated by melt coaxial electrospinning. Pure octadecane without any solvents was used as the core solution, thus, the optimal sample possessed very high latent heat up to 118 J g<sup>-1</sup>. We studied the influence of core feed rate and PVB solution concentration on the encapsulation rate, and the highest encapsulation rate was found when the PVB concentration was 10% and core feed rate was 0.08 mL h<sup>-1</sup>. And hexagonal cesium tungsten bronze (Cs<sub>x</sub>WO<sub>3</sub>, a near infrared absorber) was introduced into the optimal sample partly to improve its conversion efficiency of solar to thermal energy, and partly absorb uncomfortable infrared light; the composite phase change material also possessed high latent heat up to 96.9 J g<sup>-1</sup>. In addition, 100 thermal cycle test proved that with a minor latent heat decrease, the prepared core–sheath structured smart nanofibers had good thermal stability, which overcomes the leakage problem of pure octadecane. Additionally, the 9 wt% Cs<sub>x</sub>WO<sub>3</sub>-loaded sample had an increase in tensile strength and elongation compared with the sample without Cs<sub>x</sub>WO<sub>3</sub>, indicating the good compatibility between Cs<sub>x</sub>WO<sub>3</sub> and PVB.

Received 20th May 2019  
 Accepted 1st July 2019

DOI: 10.1039/c9ra03795k

[rsc.li/rsc-advances](http://rsc.li/rsc-advances)

## 1. Introduction

Smart fibers are fabricated by incorporating functional materials into artificial fibers, which can respond to various external stimuli, such as mechanical forces, electricity, light, heat and so on.<sup>1–4</sup> Various smart fibers have been reported to be used in fields such as skin care products, wound dressing products, physiological parameter monitoring, deodorant fabrics and energy storage.<sup>5–9</sup> Particularly, energy storage fibers have attracted the attention of many researchers.

Phase change material is a substance able to provide latent heat during phase transition at a constant temperature.<sup>10</sup> As renewable energy sources, PCMs has great application prospect in solving energy crisis and environmental pollution<sup>11,12</sup> and has been applied in solar energy storage, textile garment, food packaging, buildings, industrial waste heat recovery and other fields.<sup>13–17</sup> PCMs include inorganic, organic compounds and

mixture of organic and inorganic. Some PCMs, such as inorganic compounds, are limited by their defects like high supercooling degree, phase segregation and corrosion potential.<sup>18,19</sup> Moreover, organic compound such as polyethylene glycol (PEG) has high water solubility,<sup>20</sup> which limits its development. Octadecane is a good candidate of thermo-regulated material because of its high latent heat and low supercooling degree, though, like other solid–liquid PCMs, the leakage during phase change process is unavoidable, which block its application in energy storage.<sup>21,22</sup>

According to previous research, form-stable PCMs can be obtained by many approaches, such as microencapsulate, filling porous nanofibers,<sup>23</sup> sol–gel<sup>24</sup> and electrospinning. The size of PCMs capsule has a great influence on their melting behavior. For large-size capsule, the temperature between boundary and core part may not be the same, thus restraining the heat transfer.<sup>25</sup> Therefore, nanofibers with small diameter can improve the thermal permeability of low-thermal conductivity PCMs. Electrospinning is a convenient and simple way to get ultrafine fibers, and the fibers have great advantages like small diameter, light weight and high specific surface area.<sup>26</sup> Conventional electrospinning of a PCM/polymer blend solution<sup>27</sup> may cause a removal of PCMs in the blended fiber by washing and wiping,<sup>28</sup> but coaxial electrospinning, using in-line needles to feed different solutions, which can receive core–sheath structured nanofibers and perform good thermal stability. For example, Wan *et al.* chose isopropyl palmitate

<sup>a</sup>Silk Institute, College of Materials and Textiles, Zhejiang Sci-Tech University, Hangzhou 310018, China. E-mail: ylq1615642853@outlook.com; amywang1021@hotmail.com; 2016339901214@mails.zstu.edu.cn; zhangming@zstu.edu.cn; yaoj@zstu.edu.cn; lniwang@zstu.edu.cn; Tel: +86-571-86843871

<sup>b</sup>Institute for Nanomaterials, Advanced Technologies and Innovations, Technical University of Liberec, Czech Republic. E-mail: jaromir.marek@tul.cz

<sup>†</sup> Liqiang Yi and Yan Wang contributed equally.



as core material and polyacrylonitrile as sheath material, while the latent heat was  $30.8 \text{ J g}^{-1}$ .<sup>29</sup> Do *et al.* prepared eicosane-loaded nanofibers, the latent heat was  $77 \text{ J g}^{-1}$ .<sup>30</sup> Wilson *et al.* fabricated PVOH/PCM nanofibers, and the latent heat was just  $48.6 \text{ J g}^{-1}$ .<sup>31</sup> Apparently, the latent heat of all the above prepared nanofibers are not very high, thus, there is great potential for development in the fabrication of core–sheath structured fibers with higher latent heat.

Lu *et al.* have prepared core–sheath structured nanofiber with PW as core and PAN as sheath, and  $\text{Cs}_x\text{WO}_3$  was loaded into the fiber,<sup>32</sup> but they just studied the influence of core feed rate on the morphology, and kerosene solution of PW was used as the core solution, so the latent heat of the final composite phase change material was only  $60.31 \text{ J g}^{-1}$ . In this study, the core–sheath structured nanofibers was fabricated by melt coaxial electrospinning, and we studied the influence of core feed rate and PVB solution concentration on the encapsulation rate. Pure liquid octadecane was used as core solution, so the final latent heat of the composite phase change material can be as high as  $96.9 \text{ J g}^{-1}$ . As we all know, near-infrared light accounts for more than half of solar energy, to improve the efficiency of converting solar energy to thermal energy,  $\text{Cs}_x\text{WO}_3$  was successfully incorporated into it. In addition, 100-thermal cycle test on the optimized sample was performed and the conclusion demonstrated the prepared core–sheath structured smart nanofibers had good thermal stability. Additionally, the 9 wt%  $\text{Cs}_x\text{WO}_3$ -loaded sample has an increase in tensile strength and elongation compared with the sample without  $\text{Cs}_x\text{WO}_3$ . This study has certain reference for the synthesis of comfortable thermo-regulated textiles.

## 2. Experimental

### 2.1. Materials

Polyvinyl butyral (PVB, B-98,  $M_w = 40\,000\text{--}70\,000$ ) and petroleum ether were purchased from Aladdin Chemistry Co., Ltd. Octadecane (99%, melting point is about  $28.2 \text{ }^\circ\text{C}$ ) was purchased from Macklin Biochemical Technology Co., Ltd. Ethanol was purchased from Hangzhou Gaojing Fine Chemical Industry Co., Ltd.  $\text{Cs}_x\text{WO}_3$  was supplied by Shanghai Buwei Applied Material Technology Co., Ltd.

### 2.2. Fabrication of the core–sheath structured smart nanofibers

To obtain the sheath solution, PVB with different concentrations of 10, 12 and 14 wt% was added into ethanol with magnetic stirring for 24 h.  $\text{Cs}_x\text{WO}_3$  was added into 10% PVB solution with concentration 3, 6 and 9 wt%, followed by ultrasonic for 2 h and magnetic stirring for 24 h. The concentric stainless-steel needles were consisted of an outer needle and an inner needle. For the outer needle, outer/inner diameters were 1.49/1.01 mm and for the inner needle, outer/inner diameters were 0.72/0.41 mm. The sheath feed rate was  $0.5 \text{ mL h}^{-1}$ , and the core feed rate was adjusted as 0.06, 0.08, 0.1,  $0.12 \text{ mL h}^{-1}$  respectively. The applied voltage was 16.3–18.9 kV and the distance from tip to collector was about 11 cm. To melt octadecane, the ambient temperature

was controlled at  $50 \text{ }^\circ\text{C}$ . Finally, the prepared samples were dried at room temperature for 24 h to remove the remaining solvent.

### 2.3. Thermal cycle test

100-thermal cycle test in a thermostatic oven between 25 and  $50 \text{ }^\circ\text{C}$  was performed to investigate the thermal stability of the smart fibers. The films were first heated to  $50 \text{ }^\circ\text{C}$  to melt octadecane, and then cooled down to room temperature.

### 2.4. Characterization methods

The morphologies of the prepared nanofibers were observed by field emission scanning electron microscope (FE-SEM, ULTRA55, Zeiss), and the acceleration voltage was 3 kV. Before observation, all the samples were pre-soaked in petroleum ether for 24 h and then coated with a thin layer of gold. To obtain cross-sectional FE-SEM image of PVB@Octa (PVB@Octa means core–sheath structured, with PVB sheath and octadecane core fibers), the samples were soaked in liquid nitrogen for a while to make it brittle, then cut with a sharp knife, and soaked in petroleum ether for 24 h and then coated with a thin layer of gold. The diameters of 30 random fibers were measured by ImageJ software, and their mean values were calculated. Transmission electron microscope (TEM, JEM-2100, JOEL) was used to investigate the core–sheath structure of the prepared nanofibers and the acceleration voltage was 200 kV. The TEM samples were prepared by depositing nanofibers onto 400-mesh carbon-coated Cu grids and then soaking in petroleum ether for 24 h. Differential scanning calorimetry (DSC, Q2000) was implemented in nitrogen flow, the samples were heated from 0 to  $50 \text{ }^\circ\text{C}$  and then cooled from 50 to  $0 \text{ }^\circ\text{C}$ , the heating and cooling rate were  $10 \text{ K min}^{-1}$ . UV/VIS/NIR spectrophotometer (UH4150) was used to study the light transmittance of the samples. PVB, PVB@Octa, PVB@Octa@Cs9% (PVB means pure electrospinning PVB film, PVB@Octa@Cs9% means  $\text{Cs}_x\text{WO}_3$ -loaded PVB@Octa, all PVB concentration was 10%) were photographed by infrared imager after 20 s irradiation by an IR lamp to directly see the absorption of near-infrared light by the samples. (The samples were put on a glass slide and the distance from samples to bulb was about 10 cm and the samples were cut into about  $0.5 \text{ cm} \times 0.5 \text{ cm} \times 0.04 \text{ cm}$  pieces.) Tensile property was measured by multifunctional mechanical tester (KES-G1) with extension rate of  $0.1 \text{ cm s}^{-1}$  at  $25 \text{ }^\circ\text{C}$ . The samples were cut into  $0.5 \times 2 \text{ cm}$  pieces, the thickness of the membrane was measured separately and accurate to  $1 \text{ }\mu\text{m}$ . Each sample was tested in triplicate.

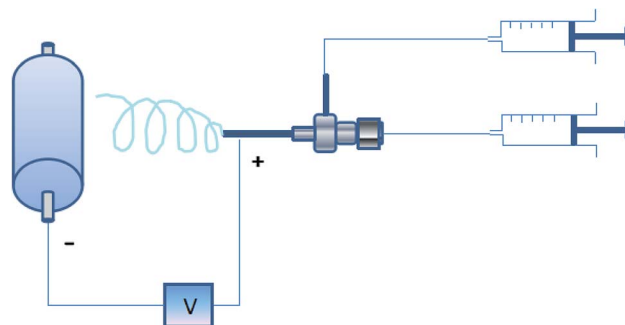


Fig. 1 Schematic illustration of the coaxial electrospinning technique.



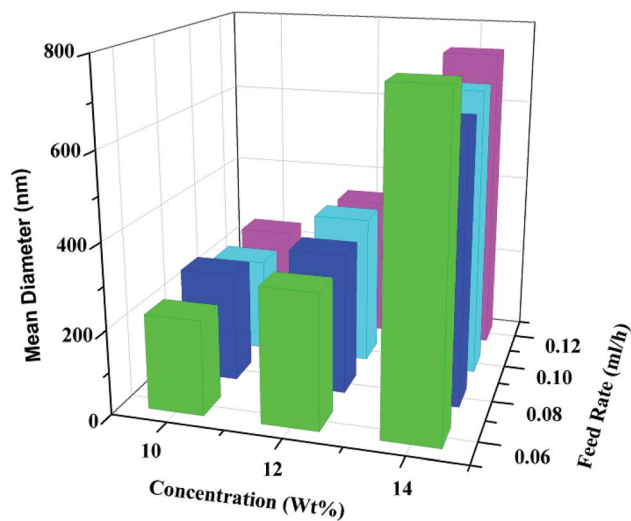


Fig. 2 Three dimensional histogram of mean fiber diameter at different PVB concentration and core feed rate.

### 3. Results and discussion

Briefly, the core–sheath structured smart fibers were fabricated *via* coaxial electrospinning technique, as shown in Fig. 1, sheath

solution and core solution were poured into two individual 10 mL plastic syringe connected to two in-line stainless-steel needles. The sheath solution was connected with the outer needle, and the core solution was connected with the inner needle. When a high voltage was applied, the tension generated by the charges that accumulated on the surface of the polymer solution caused the polymer solution to form a jet with the core solution. During the jet process, the solvent vaporized and the fibers could be obtained on the roller collector.

Fig. 2 shows the mean diameter of fibers with different PVB solution concentration and core feed rate. It clearly shows that the diameter of the fibers gradually increases with the increase of PVB solution concentration, this is because that the viscosity of PVB solution increases with the increase of PVB solution concentration, and high viscosity results in big diameter. When the concentration is constant, the increase of core feed rate has no great influence on the diameter.

As shown in Fig. 3, PVB solution concentration and core feed rate have a great influence on the morphology of the fibers. The fibers show a cylindrical and bead-free morphology with PVB concentration of 10% and core feed rate of  $0.08 \text{ mL h}^{-1}$ . While when the core feed rate increases to  $0.1$  and  $0.12 \text{ mL h}^{-1}$ , the fibers become uneven, and spindle-like beads appear. Similarly, at concentration of 12 and 14%, the fibers are cylindrical and

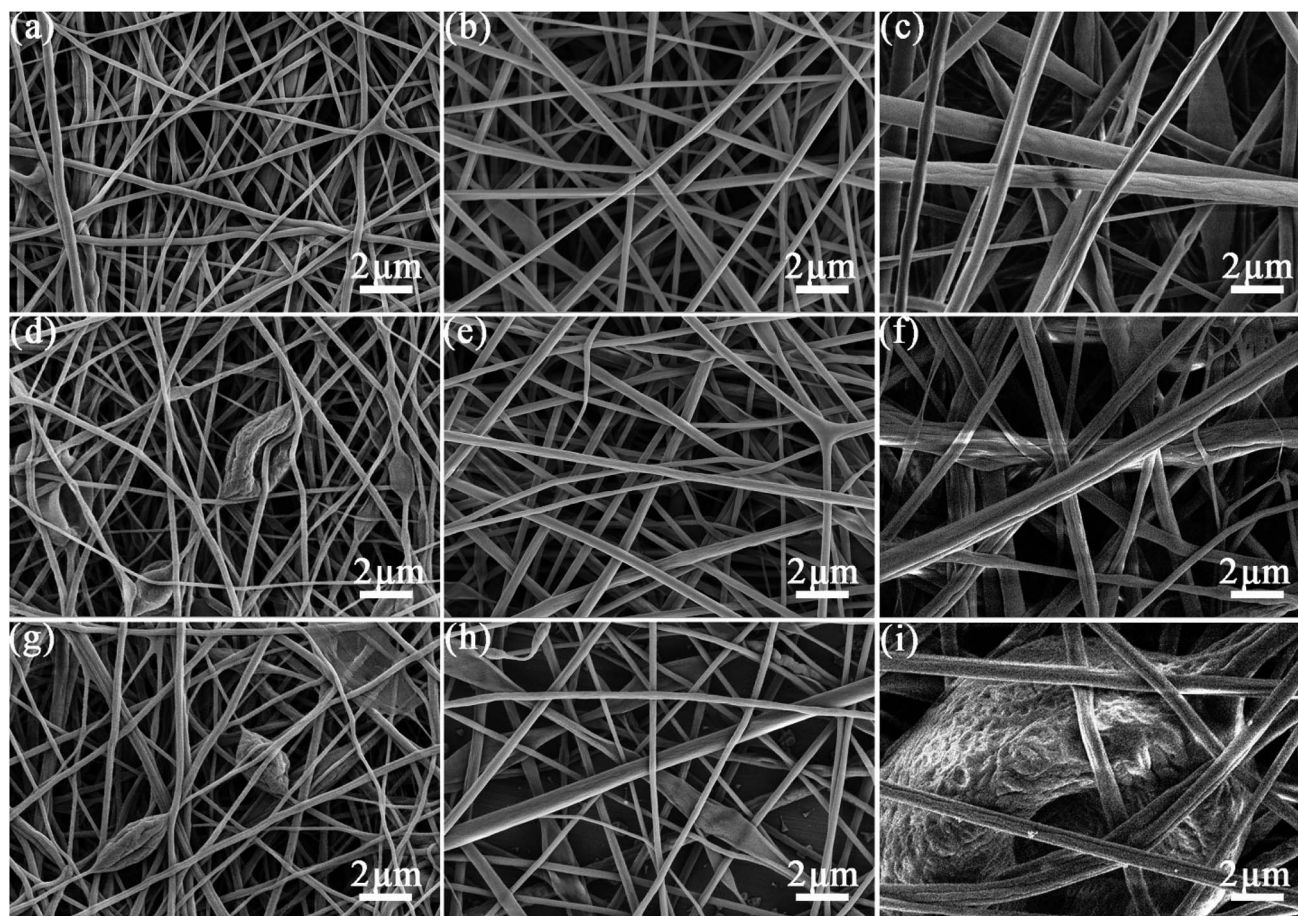


Fig. 3 FE-SEM images of the electrospun core–sheath structured nanofibers with different core feed rates: (a–c)  $0.08 \text{ mL h}^{-1}$ ; (d–f)  $0.1 \text{ mL h}^{-1}$ ; (g–i)  $0.12 \text{ mL h}^{-1}$ ; samples with different PVB concentration (wt%): (a, d and g) 10%; (b, e and h) 12%; (c, f and i) 14%.



bead-free when the core feed rates are 0.08 and 0.1 mL h<sup>-1</sup>, but when the core feed rate increases to 0.12 mL h<sup>-1</sup>, spindle-like structure appears. This may be due to the fact that as the core feed rate increases, there is too much core material inside the fibers, and the viscosity of the polymer solution is not high enough, resulting in this uneven structure, and part of the octadecane has not been incorporated, which can be proven by DSC analyses. The solution to this problem is to increase the concentration of the polymer solution, as shown in Fig. 3d-f. When the core feed rate is 0.1 mL h<sup>-1</sup> and the concentration is

10%, the fibers have spindle-like beads, as the concentration increases to 12 and 14%, the fibers become rod-shaped. This is because the viscosity of the solution increases with the increase of PVB solution concentration, which makes it easier for the sheath to remain uniform when the core layer is stretched. The increase of the concentration will also increase the diameter of the fibers, which to some extent also makes the spindle-like structure not easy to appear.

Table 1 is the DSC analyses data of samples with different PVB solution concentration and core feed rate and Fig. 4 is the DSC

Table 1 DSC analyses data of samples with different PVB concentration and core feed rate

Concentration (wt%)	Feed rate (mL h <sup>-1</sup> )	<i>T</i> <sub>onset</sub> (°C)	$\Delta H_m$ (J g <sup>-1</sup> )	<i>T</i> <sub>onset</sub> (°C)	$\Delta H_c$ (J g <sup>-1</sup> )
10	0.06	26.36	94.89	25.92	95.77
	0.08	26.89	118	25.67	120.1
	0.1	25.76	128.6	25.11	135.1
	0.12	28.04	128.7	24.77	127.4
12	0.06	26.61	50.24	25.83	50.85
	0.08	27.01	100.7	26.09	103.5
	0.1	26.31	126.7	25.39	132
	0.12	26.51	133.6	25.72	139.3
14	0.06	26.45	51.2	25.61	35.64
	0.08	26.66	82.02	26.03	69.36
	0.1	26.84	114.8	25.89	114.7
	0.12	26.95	126.9	26.24	128.3

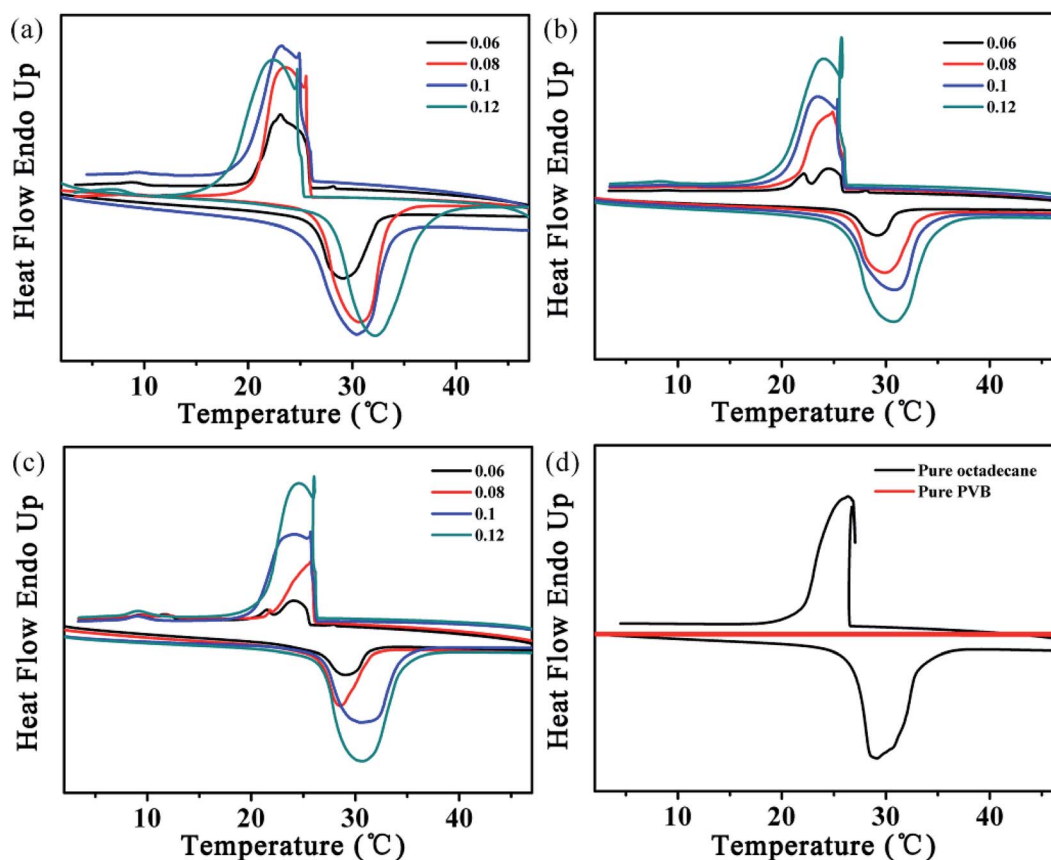


Fig. 4 DSC curves of samples with different PVB concentration: (a) 10%; (b) 12%; (c) 14% and (d) pure PVB and octadecane.



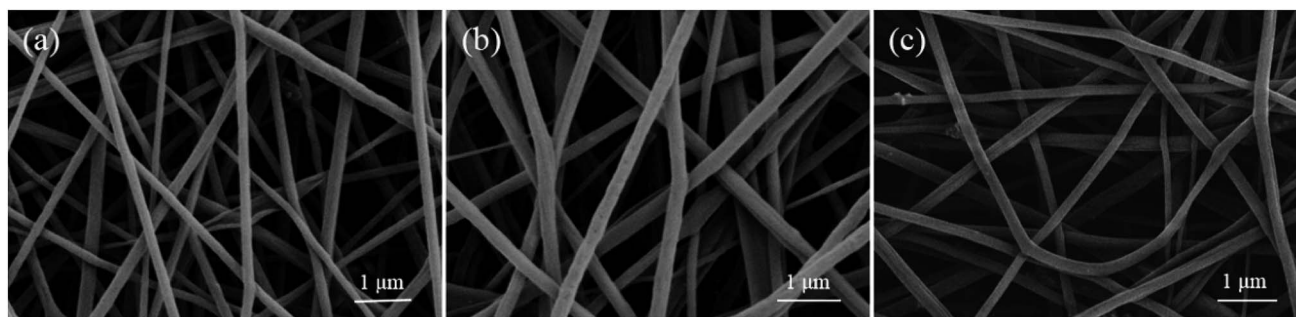


Fig. 5 FE-SEM image of PVB@Octa@Cs3%; PVB@Octa@Cs6% and PVB@Octa@Cs9%.

Table 2 DSC analyses of PVB@Octa@Cs3%; PVB@Octa@Cs6% and PVB@Octa@Cs9%

Samples	$T_{\text{onset}}$ (°C)	$\Delta H_m$ (J g <sup>-1</sup> )	$T_{\text{onset}}$ (°C)	$\Delta H_c$ (J g <sup>-1</sup> )
PVB@Octa@Cs3%	26.65	104.8	25.76	102.9
PVB@Octa@Cs6%	26.57	101.9	25.55	100.6
PVB@Octa@Cs9%	26.63	96.9	25.44	98.61

curves of all PVB@Octa samples, pure PVB and pure octadecane. We can get the conclusion that at a certain concentration, the latent heat increases with the increase of core feed rate, and finally it will reach a plateau, which may be the highest encapsulation rate under this experimental condition. For example, at concentration of 12%, the latent heat increases a lot when core feed rate goes up from 0.06 mL h<sup>-1</sup> to 0.1 mL h<sup>-1</sup>, while when the core feed rate rises from 0.1 mL h<sup>-1</sup> to 0.12 mL h<sup>-1</sup>, the latent heat increases only a little, similar situation happens when PVB concentrations are 10% and 14%, with the increase of core feed rate, the latent heat of the fibers at various concentrations will reach to around 130 J g<sup>-1</sup> and be stable, but the morphologies of the fibers those at the highest latent heat are spindle-like. At a certain core feed rate, the latent heat generally decreases with the increase of the PVB solution concentration. This is because that with the increase of PVB solution concentration, the component of PVB in the core-sheath structured fibers rises, while PVB only contributes to the increase in weight and no phase transition occurs. Therefore, the latent heat of the entire fibers decreases. Finally, we can get the optimized sample: PVB solution concentration is 10% and core feed rate is 0.08 mL h<sup>-1</sup>. The latent heat is up to 118 J g<sup>-1</sup>, and the morphology of the fibers are cylindrical and bead-free. For pure PVB, there was no phase transition according to Fig. 4d, and the latent heat of pure octadecane was about 242.2 J g<sup>-1</sup>.

Fig. 5 is the SEM image of PVB@Octa@Cs with different mass fraction of Cs<sub>x</sub>WO<sub>3</sub>. The addition of Cs<sub>x</sub>WO<sub>3</sub> has no great influence on the morphology of fibers, the surface is smooth, and there are only a few bulges. As shown in Table 2, the  $T_{\text{onset}}$  points are almost the same before and after loading Cs<sub>x</sub>WO<sub>3</sub>, and different concentrations of Cs<sub>x</sub>WO<sub>3</sub> have no effect on  $T_{\text{onset}}$  point. While the latent heat of the fibers after adding Cs<sub>x</sub>WO<sub>3</sub> has a decline which is caused by the density difference of

Cs<sub>x</sub>WO<sub>3</sub> and PVB, the density of Cs<sub>x</sub>WO<sub>3</sub> is higher than PVB. So with a similar diameter, higher weight of PVB@Octa@Cs results in a lower latent heat in its calculation. And the fibers with 9% Cs<sub>x</sub>WO<sub>3</sub> still possess a very high latent heat up to 96.9 J g<sup>-1</sup>.

Fig. 6 shows the DSC curves of PVB@Octa@Cs9% before and after 100 thermal cycles. The areas of two peaks are almost the same, and the latent heat after thermal cycle test is 95.73 J g<sup>-1</sup>, which is very close to 96.9 J g<sup>-1</sup>, so we can get the conclusion that the core-sheath structured smart nanofibers have good thermal stability.

Fig. 7a and b clearly show the core-sheath structure of the fibers, indicating that octadecane is successfully encapsulated into PVB. Fig. 7c and d are the TEM images of smart fibers. The black dots in the image indicate that cesium tungsten bronze is successfully incorporated into the fibers.

As shown in Fig. 8a, the EDS elemental analysis shows Cs and W, which belongs to Cs<sub>x</sub>WO<sub>3</sub>. Fig. 8b is the UV-VIS-NIR transmission diagram of smart fibers with different Cs<sub>x</sub>WO<sub>3</sub> concentration and PVB@Octa. Cs3%, Cs6%, Cs9% represents the concentration of Cs<sub>x</sub>WO<sub>3</sub> is 3, 6, 9 wt%, respectively. Visible light has a wavelength range of 380–780 nm, and the peaks of the Cs<sub>x</sub>WO<sub>3</sub>-loaded samples in the figure correspond to this value, indicating that cesium tungsten bronze does not absorb

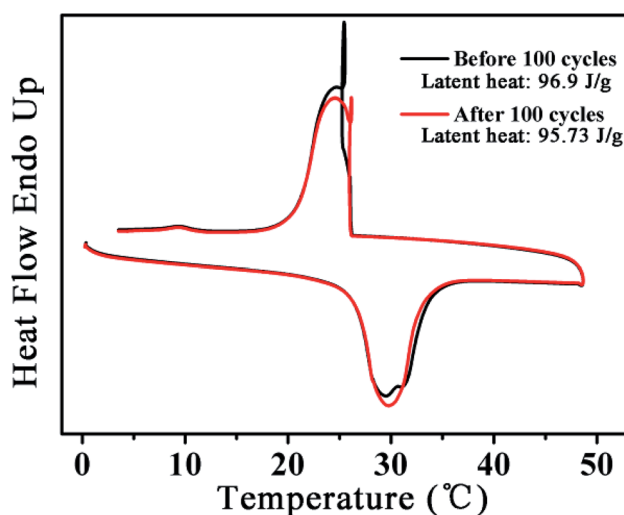


Fig. 6 DSC curves of PVB@Octa@Cs9% before and after 100 cycles.



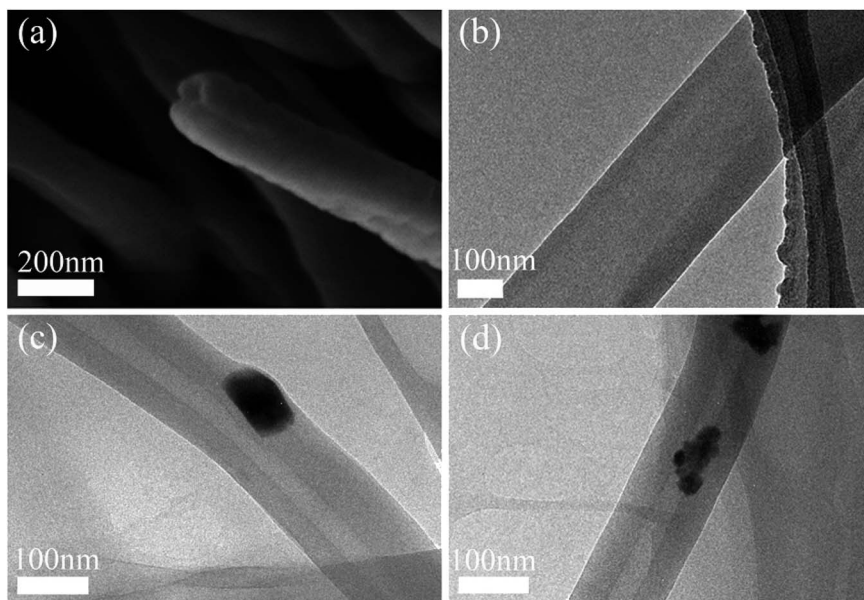


Fig. 7 (a) Cross-sectional SEM image of PVB@Octa; (b) TEM image of PVB@Octa; (c and d) TEM image of PVB@Octa@Cs.

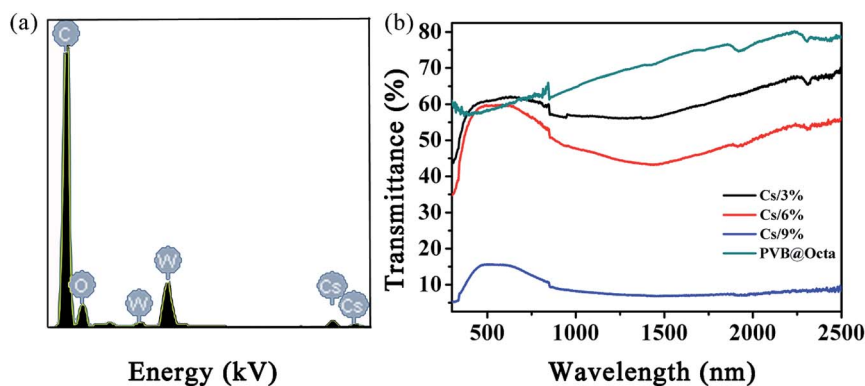


Fig. 8 (a) EDS curve of PVB@Octa@Cs; (b) UV-VIS-NIR spectroscopy of PVB@Octa and PVB@Octa@Cs with different  $\text{Cs}_x\text{WO}_3$  concentration.

much visible light, while for PVB@Octa sample, there is no peak at this range, and the sample has highest transmissivity compared with the  $\text{Cs}_x\text{WO}_3$ -loaded samples. It can also be seen from the figure that with the increase of the concentration of  $\text{Cs}_x\text{WO}_3$ , the transmissivity gradually decreases, as the transmissivity even goes as low as about 5% when  $\text{Cs}_x\text{WO}_3$  concentration is 9%, which means that the smart fiber has good performance of NIR absorption. Hence, the addition of  $\text{Cs}_x\text{WO}_3$  is helpful to improve the heat storage performance of the smart fiber.

In order to directly observe the infrared light absorption performance of the smart fibers, the infrared lamp is used to irradiate the fibers, and the thermographic images are made. Fig. 9 is the thermographic images of PVB (left), PVB@Octa (middle), and PVB@Octa@Cs (right), (a), (b), (c) and (d) are the images with different duration time of 1, 5, 13, and 18 s after 20 s irradiation respectively. Fig. 8a shows that one second later after 20 s irradiation, the temperature of PVB@Octa@Cs is

39.3 °C, while the temperature of PVB@Octa and PVB are only 31.1 °C and 29 °C, which are almost the same as the ambient temperature. The temperature difference between PVB@Octa@Cs and PVB can be as high as 10 °C. Fig. 9b–d show that after 5, 13 and 18 s, the temperature of the three samples all decreases, and PVB@Octa@Cs shows the highest temperature which is always higher than the ambient temperature. Therefore, the results show that the addition of  $\text{Cs}_x\text{WO}_3$  can improve the efficiency of converting solar energy to thermal energy.

Fig. 10 is the stress–strain curves of PVB@Octa and PVB@Octa@Cs. Generally, all samples have a low elongation because of the load of brittle octadecane. With the increase of mass fraction of  $\text{Cs}_x\text{WO}_3$ , the tensile strength of PVB@Octa@Cs gradually increases. PVB@Octa has a higher tensile strength compared to PVB@Octa@Cs3% and PVB@Octa@Cs6%, but PVB@Octa@Cs9% has a highest tensile strength and elongation which even higher than PVB@Octa, indicating that there is good compatibility between PVB and  $\text{Cs}_x\text{WO}_3$ .



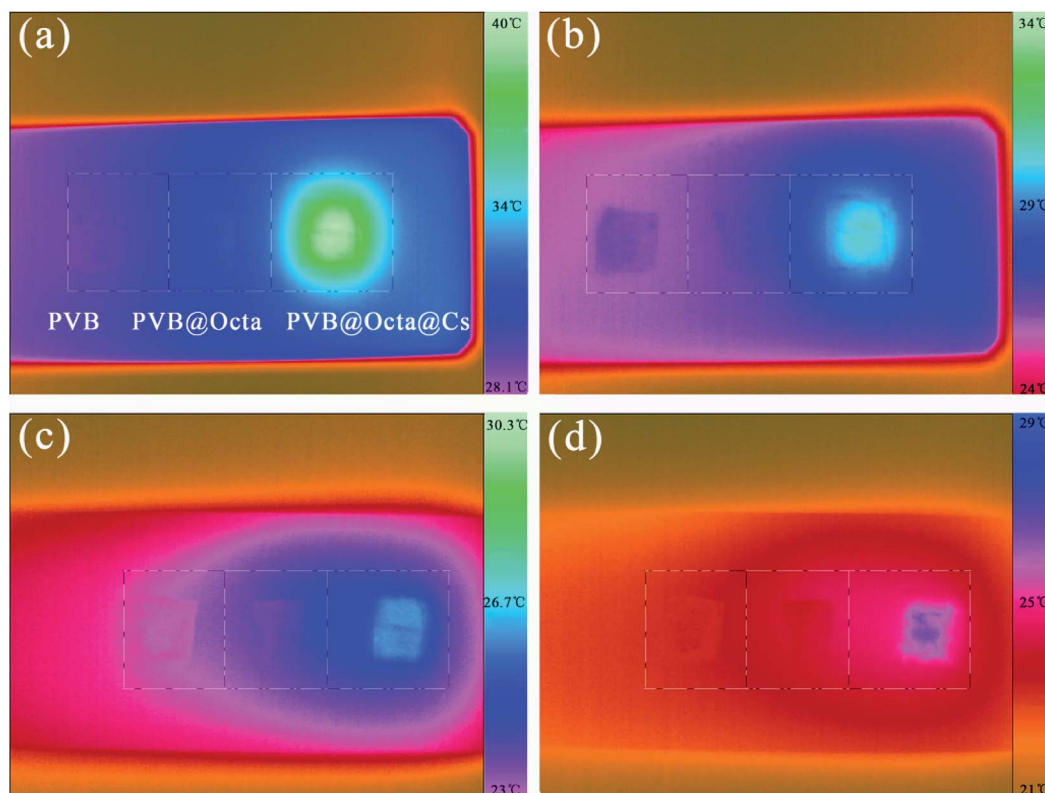


Fig. 9 Thermographic images of PVB; PVB@Octa; PVB@Octa@Cs with different durable time of (a) 1 s; (b) 5 s; (c) 13 s and (d) 18 s after 20 s irradiation by an IR lamp.

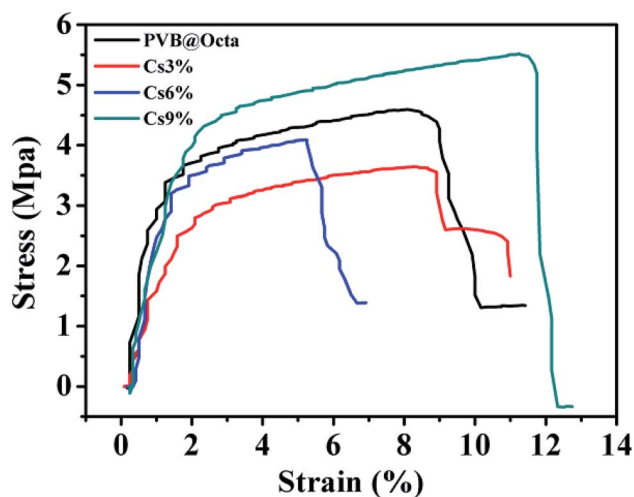


Fig. 10 Stress–strain curves of PVB@Octa and PVB@Octa@Cs.

## 4. Conclusions

In summary, core–sheath structured nanofibers with polyvinyl butyral (PVB) as sheath and octadecane as core was fabricated by melt coaxial electrospinning successfully. Hexagonal cesium tungsten bronze was loaded into the nanofibers to improve its converting efficiency of solar to thermal energy. The DSC results show the prepared smart fibers have an extremely high latent

heat up to  $96.9 \text{ J g}^{-1}$ . And 100 thermal cycle test shows a good thermal stability of the smart fibers, which overcome the leakage problem. Additionally, the 9 wt%  $\text{Cs}_x\text{WO}_3$ -loaded sample has an increase in mechanical properties. Hence, this work provides a strong support for the application of smart fibers in the field of thermo-regulated textiles.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

The authors acknowledge financial support from Key Program for International Cooperation Projects of China (2016YFE0131400).

## References

- 1 M. Stoppa and A. Chiolerio, *Sensors*, 2014, **14**, 11957–11992.
- 2 J. Hu, H. Meng, G. Li and S. I. Ibekwe, *Smart Mater. Struct.*, 2012, **21**, 053001.
- 3 B. Pause, *J. Ind. Text.*, 2016, **33**, 93–99.
- 4 H. Y. Jiang, S. Kelch and A. Lendlein, *Adv. Mater.*, 2006, **18**, 1471–1475.
- 5 J. Hu, W. Liu and B. Liu, *US Pat.*, US007780979B2, 2010.



- 6 H. Tamura, Y. Tsuruta and S. Tokura, *Mater. Sci. Eng. C*, 2002, **20**, 143–147.
- 7 S. Pasche, S. Angeloni, R. Ischer, M. Liley, J. Luprano and G. Voirin, *Adv. Sci. Technol.*, 2008, **57**, 80–87.
- 8 J. Hu, F. Zeng and P. Li, *US Pat.*, US007968083B2, 2011.
- 9 K. Jost, G. Dion and Y. Gogotsi, *J. Mater. Chem. A*, 2014, **2**, 10776.
- 10 B. Rezaei, M. Ghani, M. Askari, A. M. Shoushtari and R. M. A. Malek, *Adv. Polym. Technol.*, 2016, **35**, 21534.
- 11 S. K. Song, T. T. Zhao, F. Qiu, W. T. Zhu, T. R. Chen, Y. Guo, Y. Zhang, Y. Q. Wang, R. Feng, Y. Liu, C. X. Xiong, J. Zhou and L. J. Dong, *Energy*, 2019, **172**, 1144–1150.
- 12 S. K. Song, T. T. Zhao, W. T. Zhu, F. Qiu, Y. Q. Wang and L. J. Dong, *ACS Appl. Mater. Interfaces*, 2019, **11**, 20828–20837.
- 13 M. Kenisarin and K. Mahkamov, *Renewable Sustainable Energy Rev.*, 2007, **11**, 1913–1965.
- 14 G. Li, G. Hong, D. Dong, W. Song and X. Zhang, *Adv. Mater.*, 2018, **30**, 1801754.
- 15 W. Chalco-Sandoval, M. J. Fabra, A. López-Rubio and J. M. Lagaron, *Eur. Polym. J.*, 2015, **72**, 23–33.
- 16 A. K. Pandey, M. S. Hossain, V. V. Tyagi, N. Abd Rahim, J. A. L. Selvaraj and A. Sari, *Renewable Sustainable Energy Rev.*, 2018, **82**, 281–323.
- 17 S. K. Song, F. Qiu, W. T. Zhu, Y. Guo, Y. Zhang, Y. Y. Ju, R. Feng, Y. Liu, Z. Chen, J. Zhou, C. X. Xiong and L. J. Dong, *Sol. Energy Mater. Sol. Cells*, 2019, **193**, 237–245.
- 18 B. Zalba, J. M. Marín, L. F. Cabeza and H. Mehling, *Appl. Therm. Eng.*, 2003, **23**, 251–283.
- 19 S. A. Mohamed, F. A. Al-Sulaiman, N. I. Ibrahim, M. H. Zahir, A. Al-Ahmed, R. Saidur, B. S. Yılbaş and A. Z. Sahin, *Renewable Sustainable Energy Rev.*, 2017, **70**, 1072–1089.
- 20 C. Chen, L. Wang and Y. Huang, *Polymer*, 2007, **48**, 5202–5207.
- 21 M. F. Demirbas, *Energy Sources, Part B*, 2006, **1**, 85–95.
- 22 Y. Lu, X. Xiao, Y. Zhan, C. Huan, S. Qi, H. Cheng and G. Xu, *ACS Appl. Mater. Interfaces*, 2018, **10**, 12759–12767.
- 23 H. Ke and Q. Wei, *Thermochim. Acta*, 2019, **671**, 10–16.
- 24 A. Babapoor, G. Karimi, S. I. Golestaneh and M. A. Mezjin, *Appl. Therm. Eng.*, 2017, **118**, 398–407.
- 25 L. F. Cabeza, C. Castellón, M. Nogués, M. Medrano, R. Leppers and O. Zubillaga, *Energy Build.*, 2007, **39**, 113–119.
- 26 N. Zhang, Y. Yuan, X. Cao, Y. Du, Z. Zhang and Y. Gui, *Adv. Eng. Mater.*, 2018, **20**, 1700753.
- 27 C. Chen, L. Wang and Y. Huang, *Appl. Energy*, 2011, **88**, 3133–3139.
- 28 C. Cherif, N. H. A. Tran, M. Kirsten, H. Bruenig and R. Vogel, *eXPRESS Polym. Lett.*, 2018, **12**, 203–214.
- 29 Y. Wan, P. Zhou, Y. Liu and H. Chen, *RSC Adv.*, 2016, **6**, 21204.
- 30 C. V. Do, T. T. T. Nguyen and J. S. Park, *Korean J. Chem. Eng.*, 2013, **30**, 1403–1409.
- 31 W. Chalco-Sandoval, M. J. Fabra, A. López-Rubio and J. M. Lagaron, *J. Appl. Polym. Sci.*, 2016, **133**, 43903.
- 32 Y. Lu, X. D. Xiao, J. Fu, C. M. Huan, S. Qi, Y. J. Zhan, Y. Q. Zhu and G. Xu, *Chem. Eng. J.*, 2019, **355**, 532–539.

