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# The Chapman rearrangement in a continuous-flow microreactor†

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The Chapman rearrangement is of practical significance in pharmaceutical and fine chemical industries. It is a high temperature reaction with an exothermic nature in numerous cases. The conventional batch-wise synthesis is limited by its operational complexities, temperature control difficulties and scale-up hurdles. In this work, a microreactor-based continuous-flow approach was developed to perform the rearrangement in a highly controlled and safer manner. High conversions were obtained within short residence times ( $\leq 20$  minutes). The detailed kinetics of this reaction, using 2,6-dichloro-phenyl *N*-phenyl benzimidate and 2-carbomethoxy-phenyl *N*-phenyl benzimidate as the representative reactants, was explored at varying temperatures to understand the intensified reaction behavior, and was modelled based on the obtained experimental data. The continuous process was scaled up to a 16-fold larger reactor volume by increasing the diameter of the microreactor while maintaining the residence time without further optimization. A very slight variation was observed in the conversion for the larger-sized flow system. Upscaling the batch reaction to a 10 times larger volume, by contrast, resulted in a dramatic decrease in the conversion. The simplicity of scaling up continuous-flow system was clearly demonstrated. A CFD model coupled with the obtained rearrangement kinetics was developed and well validated against the experimental data, which provided a robust platform for guiding the relevant process design and optimization of the continuous-flow processes. The results presented shed new light on the developments and applications of continuous-flow method for the classical Chapman rearrangement that require harsh high temperatures.

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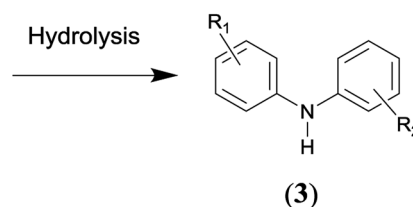
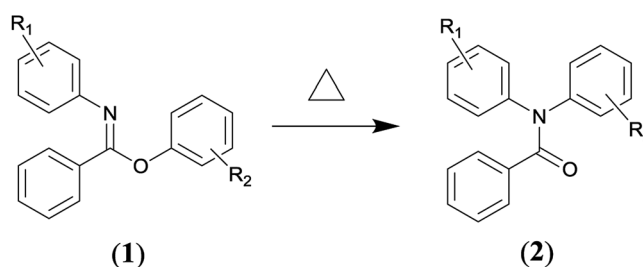
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## 1. Introduction

The Chapman rearrangement of aryl-*N*-arylbenzimidates (1) to *N,N*-diarylbenzamides (2) (Scheme 1) is of high synthetic significance in pharmaceutical and fine chemical industries, since it provides a useful approach for preparing *N,N*-diarylbenzamides (2) and/or diphenylamines (3) (*via* facile subsequent hydrolysis of (2)) that can otherwise be difficult to access.<sup>1–6</sup> *N,N*-diarylbenzamides and diphenylamines are found in a variety of medicinally active compounds<sup>7,8</sup> and among the most important building blocks for a host of chemotherapeutic drugs such as quinacrine,<sup>9,10</sup> fenbendazole,<sup>11</sup> chlorpromazine<sup>12</sup> and diclofenac sodium,<sup>13,14</sup> *etc.*

Other methods for the preparation of *N,N*-diarylbenzamides generally involve C–N cross-coupling of acyclic secondary

amides with aryl halides,<sup>15</sup> and the Ullmann-type cross-coupling reactions between aryl halides and anilines typically represents the alternative route to afford diphenylamines.<sup>16</sup> However, the cross-coupling methods often require metal-catalysts,



Scheme 1

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sophisticated ligands, high temperatures and long reaction times.<sup>15,16</sup> These factors are undesirable from economic, environmental and operational safety viewpoints considering the cost of noble metal catalysts (*e.g.*, palladium) and sophisticated ligands as well as the strict regulations to remove trace amounts of metal species in the synthesis of medicinally active molecules. What is more, only a limited substrate scope can be effected *via* cross-coupling reactions.<sup>17</sup> Therefore, the Chapman rearrangement is the method of choice in numerous synthetic routes of practical relevance.

It is an intramolecular reaction *via* four-membered transition state, as confirmed by previous experimental studies,<sup>18,19</sup> in which a 1,3 shift of an aryl group from oxygen to nitrogen occurs. The appealing usefulness of the rearrangement specifically lies in several aspects. Firstly, it is a unimolecular reaction, only the desired product is resulted as the end product. Hence, the operation and work-up procedures involved are simple. Secondly, it has been carried out successfully with a wide substrate scope, and the yields have generally been high.<sup>20</sup> Thirdly, the reactant (**1**) can be readily prepared by the utilization of simple as well as widely accessible starting materials.<sup>21</sup>

Whereas, the main concern is that a high temperature (*e.g.*, typically 473.15–573.15 K) is required to facilitate the aromatic migrating process.<sup>22</sup> While if the temperature is too high, which is far above the temperature needed to provide the activation energy, it would decompose the reactant or product in a large number of cases.<sup>23,24</sup> Furthermore, the situation becomes complex for the cases that are markedly exothermic. For example, the temperature was observed to have risen as much as 30 K for the reactant  $R_1=O-COOMe$ ,  $R_2=H$  (in Scheme 1) when operating the rearrangement at 543.15 K on a very small laboratory scale.<sup>24</sup> More importantly, the temperature increase depends partly on the scale of the operation, which is especially true for batch-wise processes.<sup>24</sup> Consequently, the Chapman rearrangement ideally needs to be run at an optimal temperature in a well-controlled manner.

It is worth noting that the Chapman rearrangement reactions are still overwhelmingly carried out in batch-wise operations. From an operational viewpoint, it is difficult to operate and manage high temperature reactions in batch reactors, in particular for large scale applications. In industrial practices, reaction temperatures over 473.15 K are generally outside of normal operating ranges for most standard batch reactors in pharmaceutical production facilities.<sup>25</sup> Large-volume high-temperature/high-pressure customized reactors, on the other hand, are very bulky as well as costly.<sup>25</sup> In spite of the continuous innovations in batch reactors, precise thermal control to ensure a spatially uniform temperature environment remains a big challenging problem for conventional batch reactors,<sup>26</sup> particularly when high temperature reactions of exothermic nature are considered because of the strong nonlinear dynamics and the intrinsically unsteady behavior of batch reactors.<sup>27</sup> Since the spatial temperature gradients are unlikely to be completely eliminated, the long-time exposure of reaction mixture to inhomogeneous heating is problematic, and may cause severe decrease in the yields. Worse still, the scale up of batch processes from laboratory size to commercial scale is non-trivial, which comprises complicated,

painfully long, case specific and expensive procedures.<sup>13</sup> When upscaling a batch reactor to larger sizes, the volume increases much faster than the external surface area, so if a small reactor is operated under an isothermal condition, increasing its volume would move the reactor towards adiabatic operational regime.<sup>28</sup> In this case, safety concerns would be raised as a result. It is thus highly desired that the Chapman rearrangement could be alternatively carried out in a more convenient, efficient, controllable and safer approach without scale-up hurdles.

Fortunately, the rapid development of micro-reaction technology (MRT) has provided new alternatives for synthetic organic chemistry and the chemical industry.<sup>25</sup> Chemical reactions could be conveniently performed in continuous-flow microreactors. Due to the high surface-to-volume ratio, exceptional heat and mass transfer efficiencies are enabled for microreactors, in which the temperatures can be uniformly and accurately controlled in a timely manner.<sup>29</sup> Besides, the closed system combined with small hold-up volume provide an inherently safe environment to implement high temperature, exothermic, hazardous and even explosive reactions.<sup>25</sup> Moreover, scale up can be straightforward for microreactors *via* the numbering-up strategy or simply adopting longer channels while maintaining the same dimensionless transport characteristics or running for an extended period of time to increase throughput.<sup>30,31</sup> Accordingly, the continuous-flow microreactors have attracted a great deal of attention in organic chemistry community.

The process design and optimization of continuous-flow processes can be effectively accelerated with the help of detailed knowledge of the fluid flow dynamics, heat and mass transfer characteristics including chemical kinetics. Conventionally, the employment of exhaustive experiments to assess the importance of various parameters in large scale applications is a tedious, time-intensive as well as costly task, especially for those cases in which the reactants/reagents/catalysts are not commercially available on the market, but needs to be in-house prepared. For this reason, computational fluid dynamics (CFD) technique can be employed as a powerful tool to acquire an in-depth understanding on the processes as well as to identify the crucial parameters for the highly efficient design and optimization of large-scale applications.

Many synthetic reactions requiring high temperatures have been successfully implemented in continuous-flow microreactors.<sup>32,33</sup> However, to our best knowledge, the Chapman rearrangement has never been attempted in continuous-flow microreactors in the open literature, despite of all the potential benefits. Ergo, the Chapman rearrangement was carried out in continuous-wise microreactors in this work in order to explore its performance and behavior in this new reaction fashion. Although rearrangement of this type has been heavily investigated in batch processes since its discovery, its reaction performance and behavior in microreactors were never discussed and analyzed before. As is often the case, continuous-wise reaction behaviors are prone to deviate substantially from the batch-wise counterparts. With this in mind, it becomes necessary to study the detailed continuous-wise reaction behaviors in order to provide new knowledge and insights into the rearrangement performed in continuous manner, and thus improve upon the conventional



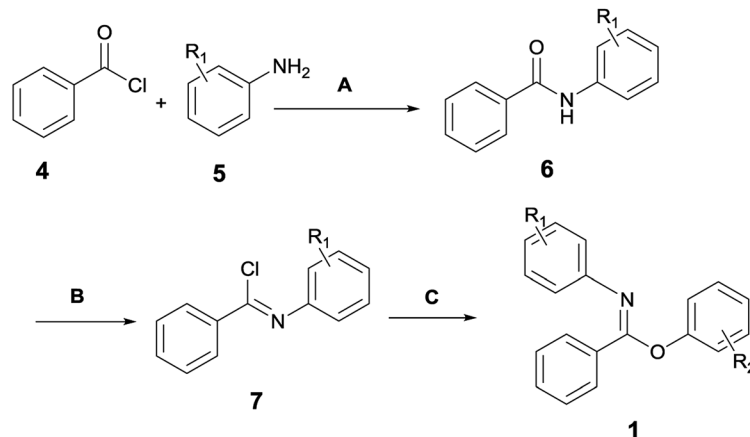
batch mode as well as define the optimal operating regimes in the continuous-flow processes. In addition, chemical kinetics could be coupled with the CFD model, thus allowing the development of a robust predictive platform for further reliable process design and optimization.

In this work, an initial understanding on the Chapman rearrangement was first obtained by examining the effects of temperature and reaction time. Then, the performance of this rearrangement in a continuous-flow microreactor was investigated for a number of reactants. Subsequently, the reaction behavior was detailedly explored and the corresponding kinetic model was formulated to describe the reaction process in a quantitative way. Following that, scale up of both the continuous-flow and batch-wise approaches was discussed in order to showcase the easy scale-up of flow devices. A CFD model coupled with the obtained chemical kinetics was developed to aid the analysis of transport characteristics of the continuous-flow processes finally. The results reported would shed new lights on the developments and applications of continuous-flow method for the classical Chapman rearrangement that requiring harsh high temperatures.

## 2. Experimental

### 2.1 Materials and analytics

Since the reactants used in this work were not commercially available, they were in-house prepared according to Scheme 2.



Scheme 2 General procedure for preparing the Chapman rearrangement reactants.

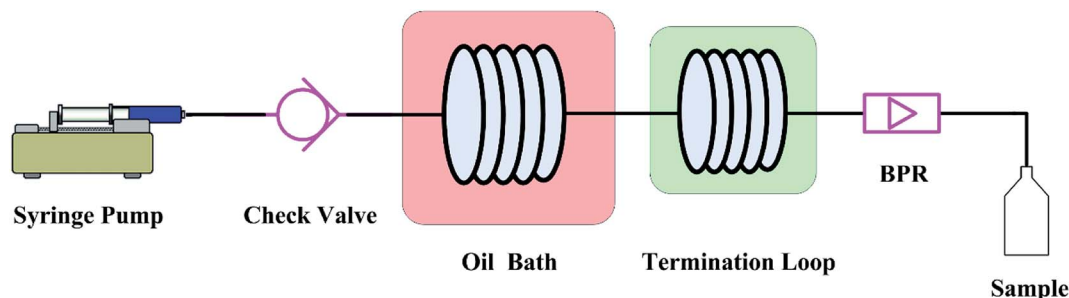


Fig. 1 Schematic overview of the experimental system for the Chapman rearrangement.

The detailed preparation procedures are elaborated in the ESI (Pages S2–S8).†

Melting points were measured on a WRS-1B digital melting-point apparatus. HRMS was measured by the Bruker micrOTOF spectrometer. HPLC analysis was performed on an Agilent 1200 HPLC system with UV detector and PHENOMENEX OOG-4375-E0 column (250 mm × 4.6 mm). Eluents were composed of H<sub>2</sub>O (A) and CH<sub>3</sub>CN (B) with  $V_A/V_B = 40 : 60 - 10 : 90$ . Peaks were found at  $\lambda$  220 nm with a flow rate of 1.0 ml min<sup>-1</sup>. <sup>1</sup>H (400 MHz) and <sup>13</sup>C (100 MHz) NMR were analyzed on a Bruker Avance 400 spectrometer in *d*<sub>6</sub>-DMSO using tetramethyl silane (TMS) as the internal standard. The chemical shifts were given in  $\delta$  (ppm) units relative to TMS. Coupling constant (*J*) values were given in Hz. Multiplicities were designated by the following abbreviations: s, singlet; d, doublet; t, triplet; q, quartet; br, broad; m, multiplet. Products were purified by flash column chromatography on silica gel purchased from Qingdao Haiyang Chemical Co., Ltd.

### 2.2 Experimental setup and method

The graphic representation of the flow system is shown in Fig. 1. Unless otherwise specified, the adopted microreactor consisted of a 250  $\mu$ l piece of stainless steel coil with an internal diameter (*d*) of 0.588 mm and a length (*L*) of 920 mm. In the experiments, the reactant in tetraethylene glycol dimethyl ether (tetraglyme) was introduced into the microreactor by a syringe pump (Fusion 400, Chemyx). A check valve was installed between the pump



and the microreactor in order to prevent the reverse flow. The microreactor was immersed in an oil bath to ensure the required reaction temperature. A stainless termination loop with an internal diameter of 0.588 mm at room temperature was connected to the microreactor. Because the Chapman rearrangement required a certain high temperature, so it stopped proceeding once the reaction mixture flowing into the termination loop. The whole system was pressurized by a back pressure valve to avoid boiling point limitations. The use of high-boiling solvent tetraglyme (bp 548.15 K) could make the operation safer by considerably decreasing the pressure needed to overcome the boiling point limitations.

The reaction time inside the microreactor was accurately controlled *via* varying the flow rate. The quenched effluent was collected after a period of the corresponding residence time in the flow system. The collected samples were subject to further purification and quantitative analysis.

Additionally, unless otherwise stated the relevant batch-wise syntheses were carried out in a 25 ml standard round-bottomed flask with reaction volume of 10 ml in order to compare the two methods. The analytical and spectral data for all the obtained reactants and products are given in the ESI (Pages S2–S8 and S13–S18 for the reactants; Pages S9–S11 and S19–S24 for the products).†

## 3. Results and discussion

### 3.1 The Chapman rearrangement

The continuous-flow microreactor provided a convenient means to conduct high temperature reactions. In this approach, the reactant was continuously delivered into the microreactor with a pump, then it flowed through the reaction channel set at the desired temperature with chemical transformation occurred during the course. After a period of the residence time, the reaction mixture was collected when it exited the system. No external intervention was needed after the system started up.

The continuous-flow process allows this rearrangement to operate in a safer and more controllable manner. The effects of temperature ( $T$ ) and reaction time ( $t_R$ ) were first examined to have an initial understanding on this reaction based on the reactant 2,6-dichloro-phenyl *N*-phenyl benzimidate.

Fig. 2(a) reveals the temperature dependence of this rearrangement operated in a microreactor. It is of interest to note that a temperature increase from 493.15 to 533.15 K resulted in about 4.5 times higher conversion ( $X$ ), but the increase in conversion slowed down with further increase in the temperature. It is worth pointing out that over 92% conversion was achieved within only 5 min at 533.15 K, and over 99% conversion was realized in just 2.5 min at 553.15 K.

Fig. 2(b) shows the reaction time dependence of the rearrangement in both the microreactor and the batch reactor. As can be seen, more than 94.42% reactant was quickly converted into product within 20 min in continuous-flow approach, but the batch-wise reaction was much slower. Approximately, it took about 3 times more time for the batch-wise reaction to reach the similar final conversion.

Following the initial examination of the reaction conditions (Fig. 2), a group of reactants was tested as shown in Table 1 to evaluate the performance of the continuous-flow method.

It appears that high conversions were achieved in only 20 min in the continuous-flow microreactors compared to that many hours were consumed in batch-wise approaches.<sup>2,19,21,34</sup> In addition, it is important to emphasize that no by-products were found in these tested reactions. The results shown in Table 1 illustrate that the Chapman rearrangement could be efficiently performed in continuous-flow microreactors.

### 3.2 Chemical kinetics

Although chemical kinetics is useful to understand the reaction behavior as well as plays a significant role in process design and optimization, the detailed kinetics of this

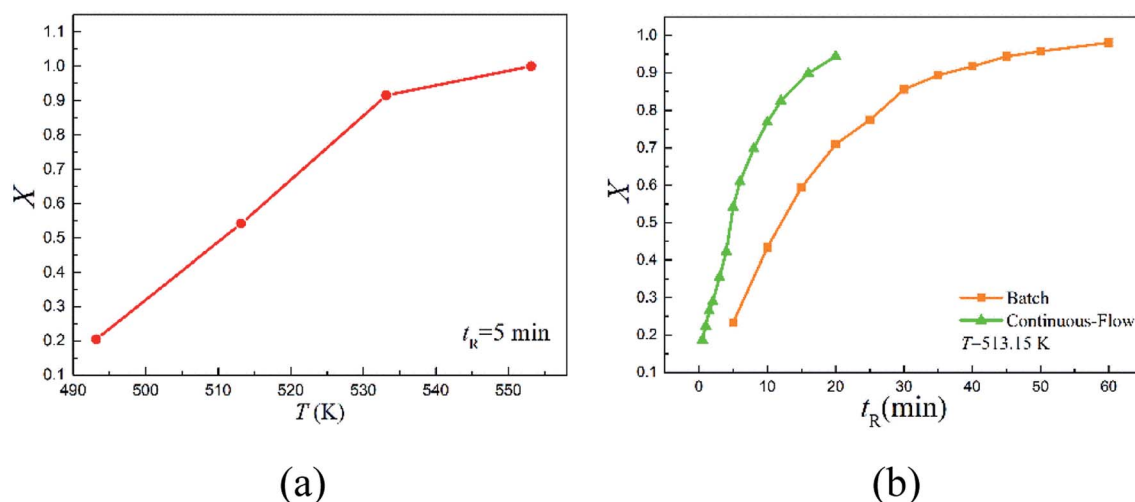
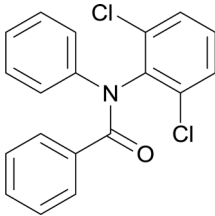
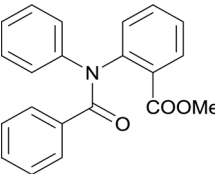
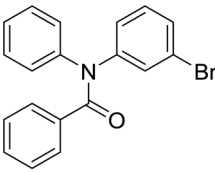
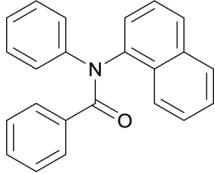
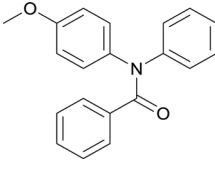
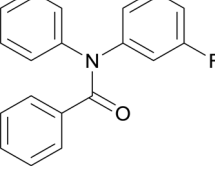


Fig. 2 Effects of temperature and reaction time on the conversion for 2,6-dichloro-phenyl *N*-phenyl benzimidate. (a) Effect of temperature in a microreactor for  $t_R = 5$  min. (b) Effect of reaction time in a microreactor and a batch reactor.



Table 1 The Chapman rearrangement for varying reactants in a continuous-flow microreactor ( $C_r = 0.3 \text{ mol L}^{-1}$ )

Entry	Product	$t_R$ (min)	$T$ (K)	Conversion <sup>a</sup>	Isolated yield
1		20	513.15	94.42%	81%
2		20	513.15	>99%	82.8%
3		20	563.15	92%	73.8%
4		20	563.15	78.5%	67.4%
5		20	563.15	72.4%	65.9%
6		20	563.15	83.3%	53.8%

<sup>a</sup> Conversion was quantified by offline HPLC analysis of aliquots of reaction mixture with internal standard of diphenyl ether (bp 531.7 K).

continuous-flow Chapman rearrangement has never been reported. Efforts were thus undertaken in the present study to explore the intensified kinetic behavior. Since it is a unimolecular reaction,<sup>18,19</sup> the rate of transformation of the reactant was derived as

$$-\frac{\partial C_r}{\partial t} = k_r C_r \quad (1)$$

where  $C_r$  is reactant concentration ( $\text{mol L}^{-1}$ ),  $k_r$  the reaction rate constant (1/s) and  $t$  time (s).

Integrating and applying the condition that at  $t = 0$  s,  $C_r = C_{r,0}$  (initial reactant concentration), we arrived at

$$C_r = C_{r,0} e^{-k_r t} \quad (2)$$

In order to determine the value of  $k_r$  from the experimental data, taking the natural log of eqn (2) led to

$$\ln(C_r) = \ln(C_{r,0}) - k_r t \quad (3)$$

As is known, the Arrhenius equation quantitatively correlates the reaction rate constant with the corresponding energy of activation ( $E_a$ ,  $\text{kJ mol}^{-1}$ ) and pre-exponential factor ( $A$ , 1/s) as

$$\ln k_r(T) = -\frac{E_a}{RT} + \ln(A) \quad (4)$$



The kinetic parameters were calculated from the equations below<sup>35,36</sup>

$$\Delta H^\ddagger = E_a - RT \quad (5)$$

$$k_r = \frac{k_B T}{h} e^{-\frac{\Delta G^\ddagger}{RT}} \quad (6)$$

$$\Delta S^\ddagger = \frac{\Delta G^\ddagger - \Delta H^\ddagger}{T} \quad (7)$$

where  $R$  is the universal gas constant ( $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ ),  $T$  the absolute temperature (K),  $\Delta G^\ddagger$  the Gibbs energy of activation ( $\text{kJ mol}^{-1}$ ),  $\Delta H^\ddagger$  the enthalpy of activation ( $\text{kJ mol}^{-1}$ ),  $\Delta S^\ddagger$  the entropy of activation ( $\text{J mol}^{-1} \text{ K}^{-1}$ ),  $h$  Planck's constant and  $k_B$  the Boltzmann's constant.

The typical reactants 2,6-dichloro-phenyl *N*-phenyl benzimidate and 2-carbomethoxy-phenyl *N*-phenyl benzimidate were employed to study the detailed kinetics because they are of practical importance in the syntheses of diclofenac sodium<sup>13</sup> and quinacrine,<sup>9,10</sup> respectively. A series of kinetic experiments were conducted in the microreactor at 493.15, 513.15, 533.15, and 553.15 K with the reactant concentration of  $0.3 \text{ mol L}^{-1}$ . Reactant concentrations over time were closely followed in order to obtain the corresponding reaction rate constants. Fig. 3 shows the variations of reactant concentrations over time. Obviously, the rearrangement is highly temperature-dependent, and increasing temperature would dramatically facilitate the transformation.

The conversions with time are depicted in Fig. 4. Specifically, 2,6-dichloro-phenyl *N*-phenyl benzimidate reached only about 50.73% conversion at 493.15 K within 20 min of reaction time,

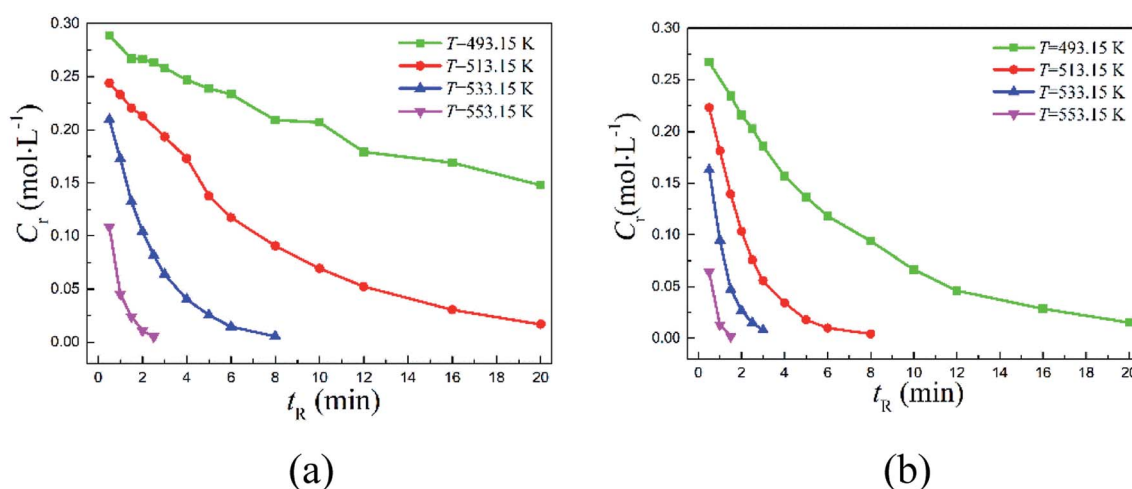


Fig. 3 Measured reactant concentrations vs. residence time in a continuous-flow microreactor at varying temperatures for (a) 2,6-dichloro-phenyl *N*-phenyl benzimidate, (b) 2-carbomethoxy-phenyl *N*-phenyl benzimidate.

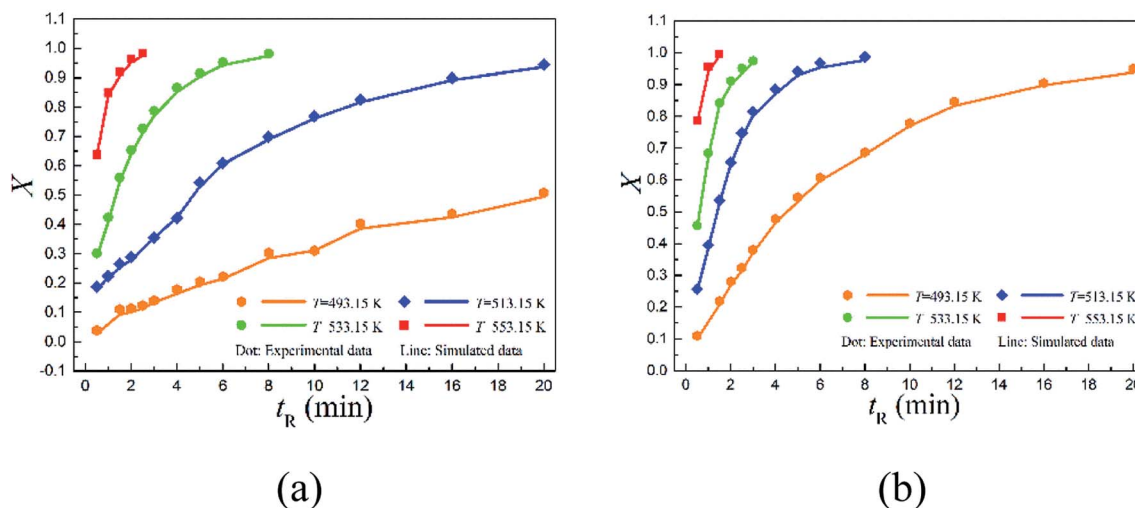


Fig. 4 Comparison of measured and simulated conversions vs. reaction time in a continuous-flow microreactor at varying temperatures for (a) 2,6-dichloro-phenyl *N*-phenyl benzimidate, (b) 2-carbomethoxy-phenyl *N*-phenyl benzimidate (scattered dots: experimental data; solid lines: CFD simulated data).



but over 94.42% reactant was successfully converted within the same period of reaction time (20 min) when increasing the temperature to 513.15 K. Further increasing it to 553.15 K, the conversion was complete in 2.5 min. Note that over 95% conversion was realized in 20 min at 493.15 K for 2-carbomethoxy-phenyl *N*-phenyl benzimidate, and almost complete conversion was reached in 1.5 min at 553.15 K.

The data shown in Fig. 4 offers valuable information for aiding the choices of optimum operating variables including the residence times and reaction temperatures. Because in practical process design, it is often challenging to define the optimal operating conditions. Higher temperature means more energy consumption. It might not be the best practice to simply select the highest possible temperature for large scale applications, as conversion need to be trade-off with energy consumption and the overall operating cost.

The reaction rate constants at varying temperatures were obtained *via* fitting eqn (3) to the experimental data. The rate constants of reaction as well as the corresponding kinetic parameters ( $\Delta G^\ddagger$ ,  $\Delta H^\ddagger$  and  $\Delta S^\ddagger$ ) are tabulated in Tables 2 and 3.

Arrhenius correlations between reaction rate constants and inverse temperatures are plotted in Fig. 5. The energy of activation  $E_a$  and pre-exponential factor  $A$  were obtained from the slope and intercept, respectively (Tables 2 and 3).

Fig. 5 quantitatively indicates that the higher the temperature, the larger the reaction rate constant for the Chapman rearrangement. Note that the reaction rate constants of 2-carbomethoxy-phenyl *N*-phenyl benzimidate are larger than the counterparts of 2,6-dichloro-phenyl *N*-phenyl benzimidate. This fact justifies the better conversions of 2-carbomethoxy-phenyl *N*-phenyl benzimidate compared to those of 2,6-dichloro-phenyl *N*-phenyl benzimidate at the same operating conditions as shown in Fig. 4.

Table 2 Kinetic rate constants and kinetic parameters for continuous-flow transformation of 2,6-dichloro-phenyl *N*-phenyl benzimidate<sup>a</sup>

$T$ (K)	$k_r$ (1/s)	$\Delta G^\ddagger$	$\Delta H^\ddagger$	$\Delta S^\ddagger$
493.15	0.0337	136.739	139.657	-5.918
513.15	0.1389	136.412	139.491	-6.000
533.15	0.4893	136.317	139.325	-5.642
553.15	1.51	136.417	139.159	-4.956

<sup>a</sup>  $E_a = 143.757 \text{ kJ mol}^{-1}$ ,  $A = 5.826 \times 10^{13} \text{ (1/s)}$ .

Table 3 Kinetic rate constants and kinetic parameters for continuous-flow transformation of 2-carbomethoxy-phenyl *N*-phenyl benzimidate<sup>a</sup>

$T$ (K)	$k_r$ (1/s)	$\Delta G^\ddagger$	$\Delta H^\ddagger$	$\Delta S^\ddagger$
493.15	0.1471	130.697	114.823	32.188
513.15	0.5515	130.529	114.657	30.931
533.15	1.2172	132.277	114.491	33.360
553.15	3.7164	132.275	114.325	32.451

<sup>a</sup>  $E_a = 118.923 \text{ kJ mol}^{-1}$ ,  $A = 6.126 \times 10^{11} \text{ (1/s)}$ .

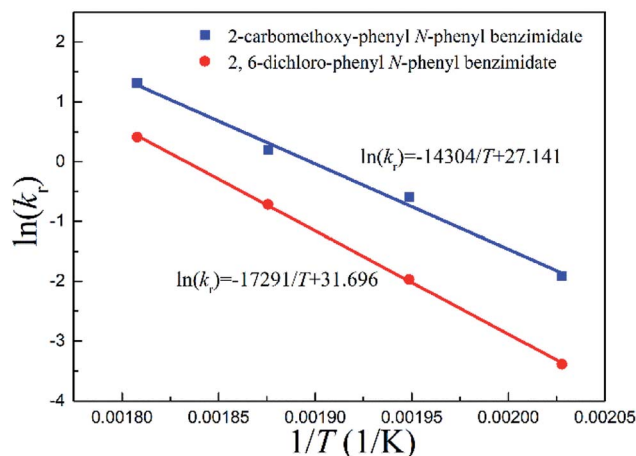


Fig. 5 Arrhenius correlations between reaction rate constants and inverse temperatures for continuous-flow processes.

### 3.3 Scale-up

The throughput of a single channel on sub-millimeter scale is often too low to supply large amounts of materials to meet commercial needs. The straightforward approaches to increase the throughput involve numbering up the flow devices or adopting longer channels while maintaining the same dimensionless transport characteristics or simply running the reaction for an extended period of time. However, numbering-up of sub-milliliter volume microreactor is not industrially preferred taking into account the complexity of simultaneously controlling flows and temperatures in numerous microreactors in parallel. On the other hand, the exceedingly long microchannel results in a very high pressure drop. Alternatively, it was suggested to first scale the microchannel to a larger size while maintaining transport characteristics and then number up a smaller number of flow devices.<sup>37</sup>

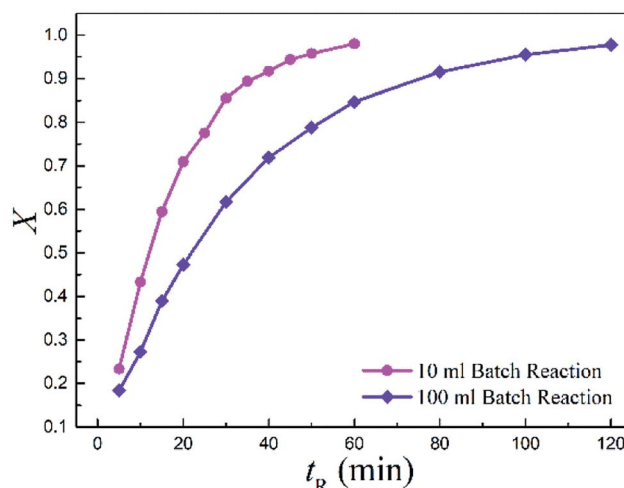


Fig. 6 Measured conversions vs. reaction time for the two batch reactors ( $T = 513.15 \text{ K}$  and  $C_r = 0.3 \text{ mol L}^{-1}$ ).



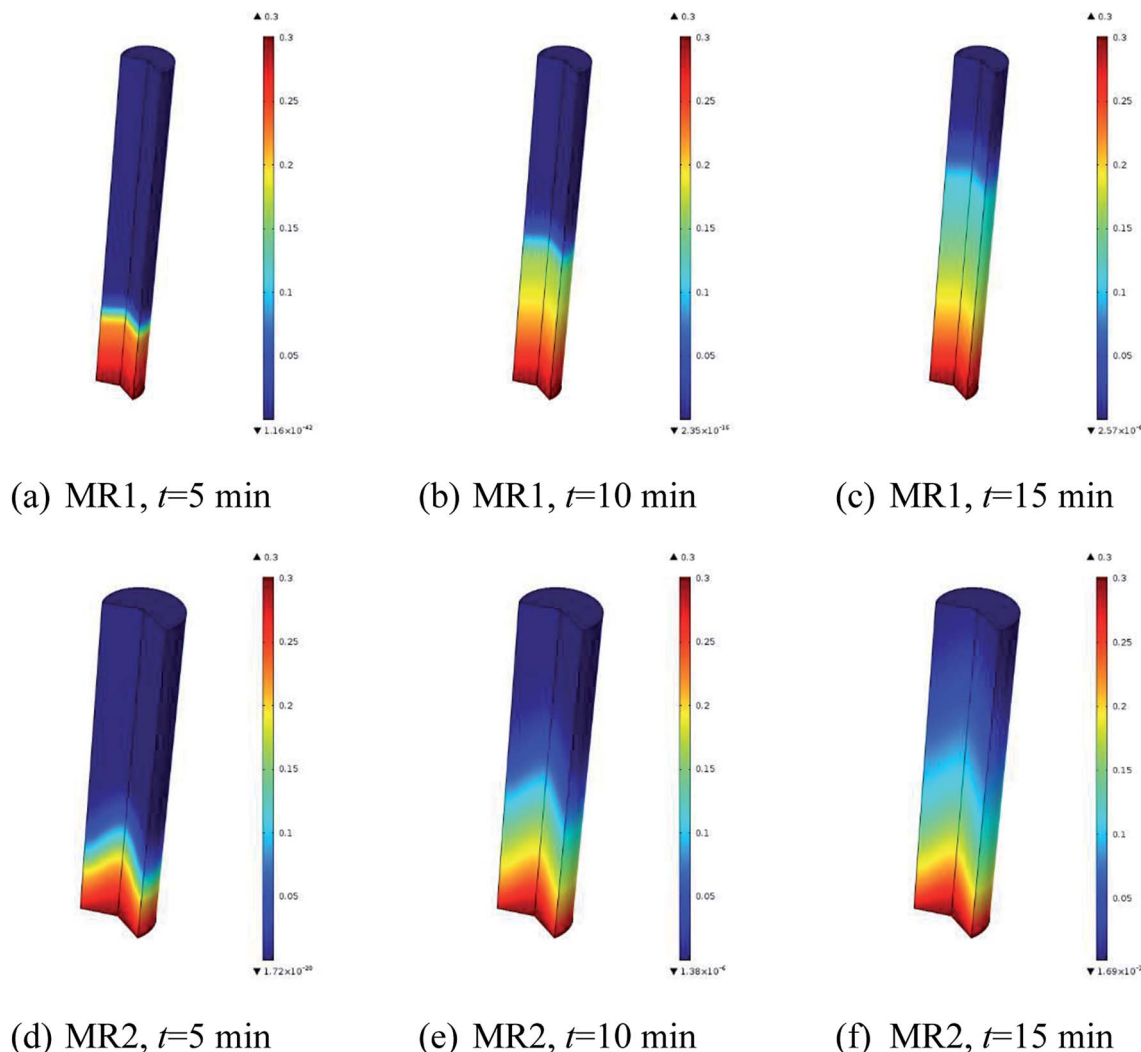


Fig. 7 Simulated reactant concentration distributions inside microreactors: (a–c) for MR1, (d–f) for MR2 (2,6-dichloro-phenyl *N*-phenyl benzimidate,  $T = 513.15$  K,  $t_r = 20$  min and  $C_r = 0.3$  mol L<sup>-1</sup>).

Based on these considerations, the sub-millimeter microreactor (MR1) was scaled up to a 16-fold larger volume by employing a larger-sized stainless steel coil (MR2). The comparison was made such that the diameter and length were changed while the residence time was retained constant.

Meanwhile, the batch-wise reaction volume was scaled from 10 (BR1) to 100 ml (BR2) as well. Notably, the conversion dramatically decreased by more than 33.3% when upscaling the batch reaction to a 10 times larger volume.

Fig. 6 displays the conversions with time for the two batch reactors. It is observed that the reaction in larger volume was much slower than in the small one, suggesting a strong scale-up effect for the conventional batch-wise synthesis.

However, in stark contrast, only a very slight decrease was found in the conversion when increasing 16-fold the reaction volume for the continuous-flow method. Clearly, it exemplified the flow system could be easily scaled to a larger dimension without palpably affecting the reaction results. More importantly, no further optimization was needed. The production

rate of MR1 was 62 mg h<sup>-1</sup>, while it reached 0.949 g h<sup>-1</sup> for MR2. The production rate of MR2 represents a 15.31-fold increase in scale, which could be translated to 22.776 g product per day. The scale-up experiments demonstrated the simplicity of scaling up continuous-flow Chapman rearrangement.

### 3.4 CFD modelling

It is difficult to experimentally measure the transport characteristics (*e.g.*, species concentration distributions, temperature distributions, *etc.*) inside the microreactor used in this work because it is made of opaque stainless steel and has a very small dimension. CFD modelling can thus be used to obtain an in-depth understanding on the transport characteristics inside the microreactors, as well as a powerful tool in the relevant process design and optimization. Since the microreactors used are circular tubes, a 2D axisymmetric computational domain was reasonably assumed to decrease the computing burden. The fluid flow inside was laminar with Reynolds number in the





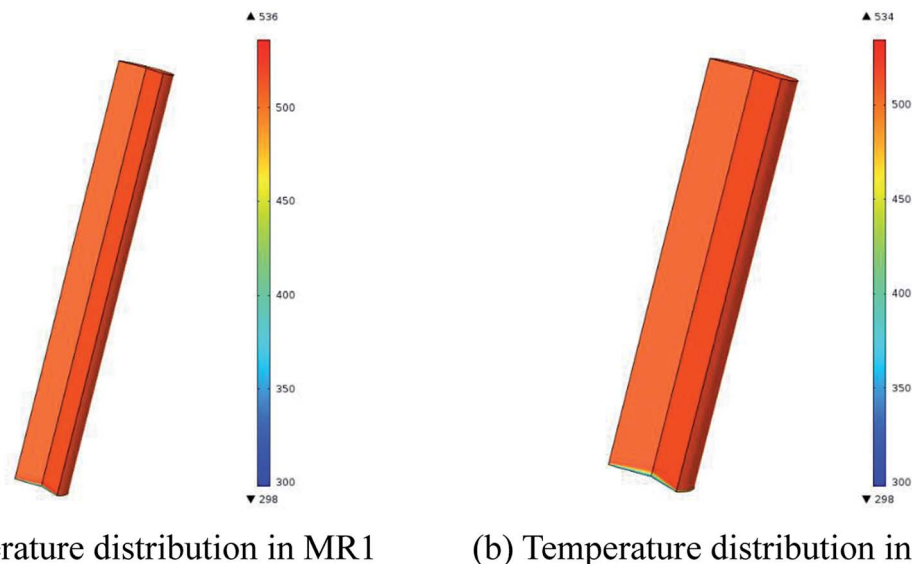


Fig. 8 Temperature distributions in MR1 and MR2 (2,6-dichloro-phenyl *N*-phenyl benzimidate,  $T = 513.15$  K,  $t_R = 20$  min and  $C_r = 0.3$  mol L<sup>-1</sup>).

Table 4 Comparison of scale-up properties between continuous-flow and batch-wise syntheses using 2,6-dichloro-phenyl *N*-phenyl benzimidate ( $T = 513.15$  K and  $C_r = 0.3$  mol L<sup>-1</sup>)

Reactor	Geometric parameters	Reaction volume	Reaction time	Conversion <sup>c</sup>	Isolated yield
MR1	$d = 0.588$ mm <sup>a</sup> , $L = 920$ mm <sup>a</sup>	0.25 ml	20 min	94.42%	81%
MR2	$d = 1.755$ mm <sup>a</sup> , $L = 1650$ mm <sup>a</sup>	4.0 ml	20 min	92.7%	78%
BR1	$V_R = 25$ ml flask <sup>b</sup>	10 ml	20 min	70.92%	— <sup>d</sup>
BR2	$V_R = 250$ ml flask <sup>b</sup>	100 ml	20 min	47.27%	— <sup>d</sup>

<sup>a</sup> Internal diameter ( $d$ ) and length ( $L$ ) of the microreactor. <sup>b</sup> Standard round-bottomed flask,  $V_R$  is the total reactor volume. <sup>c</sup> Conversion was quantified by offline HPLC analysis of aliquots of reaction mixture with internal standard of diphenyl ether. <sup>d</sup> Not isolated.

range of 0.13–0.74. The fluid was assumed to be constant density considering that it was pressurized in the system.

The continuity and momentum equations were given by the Navier–Stokes equations

$$\nabla \cdot (\rho \mathbf{u}) = 0 \quad (8)$$

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho (\mathbf{u} \cdot \nabla) \mathbf{u} = \nabla \cdot [-p \mathbf{I} + \mu (\nabla \mathbf{u} + (\nabla \mathbf{u})^T)] \quad (9)$$

where  $\mathbf{u}$  is the flow field,  $p$  the pressure and  $\rho$  the viscosity.

The energy conservation equation in the microreactor was modelled as

$$\rho C_p \left( \frac{\partial T}{\partial t} + (\mathbf{u} \cdot \nabla) T \right) + \nabla \cdot (-k_h \nabla T) = k_r C_r \Delta H \quad (10)$$

where  $T$  is the temperature (K),  $C_p$  the specific heat,  $k_h$  the thermal conductivity and  $\Delta H$  the enthalpy of reaction.

The mass conservation of the reactant in the microreactor was formulated as

$$\frac{\partial C_r}{\partial t} + \mathbf{u} \cdot \nabla (C_r) - \nabla \cdot (D_M \nabla C_r) = -k_r C_r \quad (11)$$

where  $D_M$  is the molecular diffusivity. In the CFD modelling, the obtained kinetics eqn (4) was included into the source term of

eqn (11). The numerical details are given in the ESI (Page S12).<sup>†</sup>

The CFD simulated values of conversion are compared to the corresponding experimental data as shown in Fig. 4. As can be

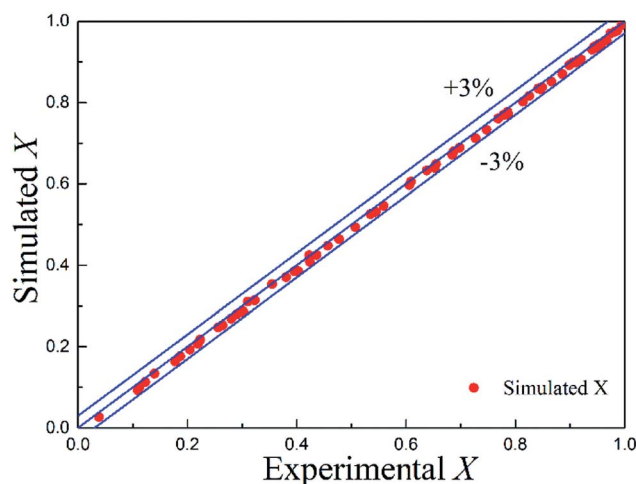


Fig. 9 Comparison of experimental and CFD simulated conversions.



seen, the simulated conversions (solid lines) matched well with the experimental data (scattered dots).

The simulated reactant concentration distributions inside MR1 and MR2 are shown in Fig. 7. Be noted that the geometries were scaled by a factor of 200 for both MR1 and MR2 as they had very large aspect ratios. Interestingly, it is noted that the plug flow pattern was very closely presented in MR1, while the flow profile obviously deviated from the ideal plug flow in MR2.

Fig. 8 exhibits the temperature distributions in MR1 and MR2. The CFD simulations revealed that the reaction fluid was heated up to 513.15 K in 4.03 seconds for MR1 and in 5.88 seconds for MR2 respectively after it was pumped into the flow system from room temperature. The similarly distributed temperatures in MR1 and MR2 ensured that the reaction results were close to each other. Nevertheless, the deviation from plug flow pattern in MR2 might be the cause for the slight variation in the conversion as compared to that of MR1 (Table 4).

The simulated values of conversion and experimental data are compared in Fig. 9 with the mean absolute error of 1.06%. Almost all the simulated data fell within 3% absolute error with the experimental data. Therefore, good agreement was obtained between the simulated values and the measured data, which confirmed that the CFD model was robust and could be further employed as a powerful predictive platform in the process design and optimization when translating the developed continuous-flow approach into industrial practices.

## 4. Conclusion

In this work, a microreactor-based continuous flow method was developed for the high temperature Chapman rearrangement. The process was found to operate in a highly controlled and safer manner as compared to the conventional batch mode. High conversions were reached for a range of reactants within short residence times ( $\leq 20$  minutes). The continuous-flow rearrangement was several times faster than the batch-wise counterpart. The detailed kinetics of this reaction, using 2,6-dichloro-phenyl *N*-phenyl benzimidate and 2-carbomethoxy-phenyl *N*-phenyl benzimidate as the representative reactants, was explored at varying temperatures to understand the intensified reaction behavior, and was modelled based on the obtained experimental data. The determined kinetic parameters indicated that the activation energy of 2,6-dichloro-phenyl *N*-phenyl benzimidate is higher than that of 2-carbomethoxy-phenyl *N*-phenyl benzimidate. The continuous-flow synthesis was scaled up 16 times in volume by increasing the diameter of the microreactor while maintaining the residence time. Only a very slight decrease was observed in the conversion for the larger-sized system. By contrast, upscaling the batch-wise reaction to a 10 times larger volume resulted in a dramatic decrease in the conversion. The simplicity of scaling up continuous-flow system was well demonstrated. A CFD model coupling with the rearrangement kinetics was developed and well validated against the experimental data, which provided a robust platform for guiding the

process design and optimization of the continuous-flow Chapman rearrangement.

## Conflicts of interest

There are no conflicts to declare.

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