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# Fundamental aspects of the corrosion of N80 steel in a formation water system under high CO<sub>2</sub> partial pressure at 100 °C

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The corrosion behavior of N80 carbon steel in a simulated formation water system saturated with CO<sub>2</sub> under high pressure at 100 °C was investigated. The effect of the CO<sub>2</sub> partial pressure on the electrochemical behavior and surface morphologies of the N80 carbon steel was analyzed by *in situ* electrochemical methods and surface analysis, combined with a series of thermodynamic calculations of the potential of anodic/cathodic reactions. While an increase in the CO<sub>2</sub> partial pressure did not alter the corrosion mechanism of the N80 steel, it resulted in higher concentrations of H<sup>+</sup> and HCO<sub>3</sub><sup>−</sup> ions, thereby significantly enhancing the rate of the cathodic reactions. The precipitation rate of FeCO<sub>3</sub> increased with the CO<sub>2</sub> partial pressure, with small and fine grains nucleating and growing on the steel surface with poor protectiveness.

## Introduction

Carbon steels are widely used in the petroleum industry owing to their cost-efficiency and good mechanical properties.<sup>1,2</sup> In particular, N80 carbon steel is the most common tubing material.<sup>1</sup> Despite this wide use, carbon steels are prone to undergo corrosion. CO<sub>2</sub> corrosion has been regarded as one of the most common corrosion issues in oil- and gas-production and transportation facilities. CO<sub>2</sub> corrosion is responsible for the failure of pipelines, tubing, and equipment, resulting in great economic losses and accidents.<sup>4–6</sup> In addition, CO<sub>2</sub> corrosion results in crude oil leakage and subsequent environmental pollution, having an impact also on downstream industries.<sup>7,8</sup>

The aqueous CO<sub>2</sub> corrosion of carbon steels observed in the oil and gas industries is, by nature, a complex process involving a number of simultaneous electrochemical, chemical, and mass transport reactions taking place close to the corroding steel surface simultaneously. Carbon steel corrosion has been widely investigated over the past decades. Research has either focused on the inherent complexities of modelling the electrochemical processes, the corrosion mechanism itself, or on the numerous factors influencing the corrosion response of carbon steels.<sup>2,9–15</sup> The different reactions taking place during corrosion<sup>1,12,16–19</sup> and the corrosion behaviors are affected differently by temperature, CO<sub>2</sub> partial pressure, pH, and other operational parameters. Temperature is a primary factor that plays an important role in the performance of films generated by CO<sub>2</sub> corrosion products.<sup>20,21</sup> At room temperature, iron carbonate precipitation is very slow and

non-protective layers invariably form, even at high supersaturation values.<sup>12</sup> However, higher temperatures ( $T > 70$  °C) result in higher precipitation rates, yielding dense, well-attached protective layers and dramatically decreasing the corrosion rate.<sup>22–24</sup> The CO<sub>2</sub> partial pressure is another important factor that strongly influences corrosion processes.<sup>25,26</sup> High CO<sub>2</sub> partial pressures promote the precipitation of FeCO<sub>3</sub>. Videm<sup>27</sup> investigated that increasing the CO<sub>2</sub> partial pressure (from 1 to 10 bar) of a brine (80 °C, pH = 5) increased the film formation rate on a carbon steel significantly. Gavanluei<sup>28</sup> reported high corrosion rates upon increasing the CO<sub>2</sub> partial pressure up to 22.1 bar at 75 °C, despite the high density of the FeCO<sub>3</sub> crystals formed on the steel surface. These environmental factors influencing the iron carbonate formation and the corrosion rate have been widely investigated at relative low temperatures and/or low CO<sub>2</sub> partial pressures, while works at high temperatures and high CO<sub>2</sub> partial pressures are scarce in the literature. However, corrosion in severe CO<sub>2</sub>-containing environments under high temperature and high pressure (HTHP) is potentially important, particularly in wellbore systems.

In this paper, the corrosion behaviors of N80 steel in simulated formation water system saturated with CO<sub>2</sub> at high partial pressure and 100 °C were investigated by *in situ* electrochemical measurements. The formation of corrosion product films at different CO<sub>2</sub> partial pressures was analyzed by scanning electron microscopy (SEM) and X-ray diffraction (XRD). With the aim to determine the relationship between the corrosion rate and the electrochemical mechanism, we calculated the ionic concentrations, reaction rate constants, and equilibrium electrode potentials of the possible anodic/cathodic reactions. The effect of high CO<sub>2</sub> partial pressure on N80 steel at 100 °C was discussed. We believe that this study can provide an essential insight into the corrosion mechanism of carbon steels under HTHP CO<sub>2</sub>-containing environments.

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## Experimental

### Materials and solution

The detailed composition of the N80 low alloy steel used herein is presented in Table 1.

Immersion specimens were cut into  $20 \times 20 \times 3$  mm pieces, while the electrochemical test specimens were embedded in epoxy resin with an exposed working area of  $10 \times 10$  mm<sup>2</sup>. All specimens were mechanically ground with up to 2000-grit silicon carbide papers, washed with distilled water, and degreased with acetone prior to testing.

A test solution simulating the formation water was prepared from deionized water and analytical grade chemicals (Tianjin Guangfu Technology Development Co., Ltd.). The chemical composition of the formation water is shown in Table 2. The experiments were conducted for dissolved O<sub>2</sub> contents lower than 20 ppb, which was achieved by bubbling ultrapure N<sub>2</sub> gas through the test solution. Subsequently, CO<sub>2</sub> gas was purged for 2 h to saturate the test solution.

### Immersion tests

All immersion tests were conducted in a Hastelloy C276 autoclave in static conditions at 100 °C and varying CO<sub>2</sub> partial pressures (0.15–4 MPa) for 72 h. The mass of the specimens was measured prior to the immersion tests ( $m_0$ ) and after the corrosion products were removed ( $m_1$ ), according to ASTM G1-03.<sup>29</sup> An analytical balance with an accuracy of  $10^{-4}$  g was used for weighing the specimens. The corrosion rate was calculated according to the following equation:

$$CR = \frac{87\,600 \times (m_0 - m_1)}{S \times t \times \rho} \quad (1)$$

where CR is the average corrosion rate in mm y<sup>-1</sup>;  $m_0$  and  $m_1$  are the masses of the specimen before and after the corrosion products were chemically removed, respectively, in g;  $t$  is the exposed time in h;  $\rho$  is the steel density in g cm<sup>-3</sup>, and  $S$  is the exposed surface area in cm<sup>2</sup>.

### Morphology observations and composition analysis

The surface morphology and composition of the corrosion films were investigated by SEM. The composition of the corrosion products and their crystal structure were analyzed by XRD.

**Table 1** Chemical composition of the N80 low alloy steel used herein (wt%)

	C	Si	Mn	P	S	Cr	Mo	Ni	V	Cu
N80	0.26	0.19	1.37	0.009	0.004	0.148	0.028	0.028	0.006	0.019

**Table 2** Main composition of the simulated formation water (g L<sup>-1</sup>)

Composition	NaCl	KCl	CaCl <sub>2</sub>	MgCl <sub>2</sub>	Na <sub>2</sub> SO <sub>4</sub>	NaHCO <sub>3</sub>
Content	28.5	23.2	2.44	4.11	4.78	0.83

### Electrochemical measurements

All electrochemical experiments were performed in a Hastelloy C276 autoclave using a conventional three-electrode system. A schematic diagram of the electrochemical autoclave and the electrode is shown in Fig. 1.

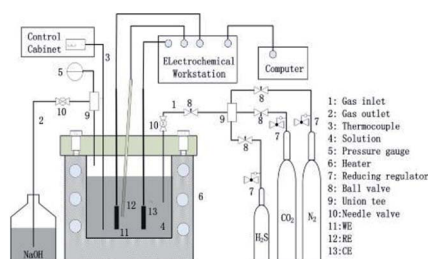
The specimen was used as working electrode, while a platinum sheet and a HTHP Ag/AgCl probe were used as counter and reference electrode, respectively. Electrochemical impedance spectroscopy (EIS) measurements were performed under open-circuit potential (OCP) over a frequency range of 100 kHz to 5 mHz with an alternating current (AC) perturbation potential of  $\pm 5$  mV. ZSimpWin 3.10 was used for fitting the EIS results. Potentiodynamic polarization tests were carried out from  $-250$  (vs. corrosion potential  $E_{\text{corr}}$ ) to 750 mV with a scan rate of  $0.5$  mV s<sup>-1</sup>. All electrochemical measurements were performed at 100 °C under stagnant conditions.

## Results

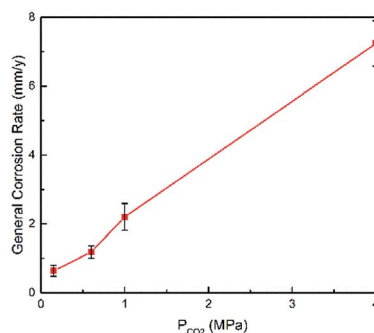
### Immersion tests

Fig. 2 shows the corrosion rate of N80 carbon steel as a function of the CO<sub>2</sub> partial pressure in formation water at 100 °C. We obtained herein the average general corrosion rate, while the ends of the error bars represent the maximum and minimum values, respectively. As shown in Fig. 2, the average corrosion rate increased with the CO<sub>2</sub> partial pressure, corroborating with the observations of Gao<sup>14</sup> and other researchers.<sup>30,31</sup>

Fig. 3 shows the surface morphologies of corrosion scales on N80 steel at various CO<sub>2</sub> partial pressures and 100 °C. The SEM



**Fig. 1** Schematic of the HTHP electrochemical autoclave used for immersion tests and electrochemical characterization (WE-working electrode; RE-reference electrode; CE-counter electrode).



**Fig. 2** Corrosion rate of N80 carbon steel at various CO<sub>2</sub> partial pressures and 100 °C.



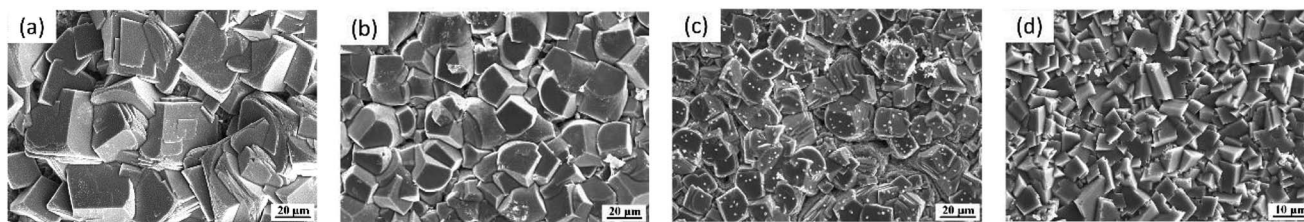


Fig. 3 Surface morphologies of N80 steel under various  $\text{CO}_2$  partial pressures at 100 °C: (a) 0.15 MPa; (b) 0.6 MPa; (c) 1 MPa; and (d) 4 MPa.

micrographs provided in Fig. 3 indicate the difference in crystal density. At 0.15 MPa of  $\text{CO}_2$ , the scale was composed of crystal grains with heterogeneous sizes, as shown in Fig. 3(a). The grains were observed to arrange closely and regularly with crystal size varying from 20 to 40  $\mu\text{m}$  in width. The compactness of the scale increased and the crystal size decreased with the  $\text{CO}_2$  partial pressure. It can be clear seen from Fig. 3(d) that the average size of the crystal reduced to nearly 5–10  $\mu\text{m}$  in width as  $P_{\text{CO}_2}$  increased. In conjunction of these observations, the corrosion rate is obviously increasing. This also indicates that the size and porosity of the crystals in the corrosion product give a contrary indication as to the protectiveness of the layer.

Fig. 4 shows the XRD patterns of the corrosion scale formed on the N80 steel at different  $\text{CO}_2$  partial pressures. The corrosion products were mainly composed of  $\text{FeCO}_3$  and  $\text{Fe}(\text{Ca,Mg})(\text{CO}_3)_2$ . Minor amounts of  $\text{CaCO}_3$  were found on the steel surface. Owing to the isostructuralism of these carbonates,  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  are able to substitute themselves for  $\text{Fe}^{2+}$  in the  $\text{FeCO}_3$  structure and form complex carbonates,<sup>32</sup> which is thermodynamically stable under the test conditions. The intensity of the  $\text{CaCO}_3$  peak decreased with the  $\text{CO}_2$  partial pressure. Which can be explained by the decrease in the solution pH as the  $\text{CO}_2$  partial pressure increased.

### EIS analyses

EIS provides insight into the corrosion processes occurring on the steel surface. The Nyquist plots of the N80 carbon steel at various  $\text{CO}_2$  partial pressures and 100 °C are shown in Fig. 5. The EIS curves showed three responses namely, one high-medium-frequency response and two low-frequency responses. The high-medium-frequency capacitive loop was caused by the corrosion product film, while the low-frequency

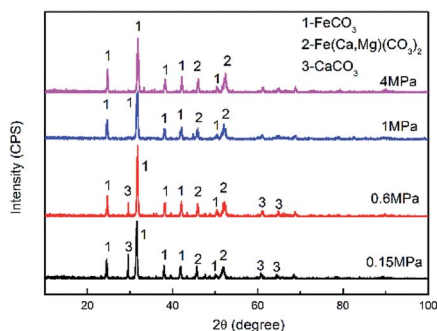


Fig. 4 XRD patterns of the corrosion scale formed on N80 steel at various  $\text{CO}_2$  partial pressures.

capacitive loop was originated by the electric double layer. The electric double-layer capacitance was not constant and changed with frequency and the amplitude because of the dispersion on the electrode surface.<sup>33</sup> The low-frequency inductive loop was caused by the adsorption of the intermediate product  $\text{FeOH}_{\text{ad}}$  on the bare substrate not covered by the corrosion scale. As shown in Fig. 5, the impedance amplitude decreased gradually and the curve shrunk inward with the  $\text{CO}_2$  partial pressure. Moreover, the inductive loop atrophied with the  $\text{CO}_2$  partial pressure.

As shown in Fig. 6, the EIS plots were fitted by the equivalent circuit (EC), where  $Q_{\text{dl}}$  is the constant phase element (CPE) representing the double charge layer capacitance;  $R_s$  and  $R_{\text{ct}}$  are the electrolyte solution resistance and charge transfer resistance, respectively;  $R_{\text{pore}}$  is the pore resistance of the corrosion scale; and  $L$  and  $R_L$  are inductance and inductive resistances, respectively. With regard to the corrosion film not being purely capacitive,  $Q_f$  was selected to fit the film capacitance. The parameters obtained after the fitting are listed in Table 3. As shown in Table 3, the polarization resistance  $R_p$  ( $R_p = R_{\text{pore}} + R_{\text{ct}}$ )

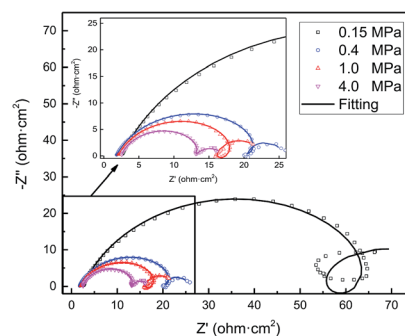


Fig. 5 EIS curves of N80 carbon steel at various  $\text{CO}_2$  partial pressures and 100 °C.

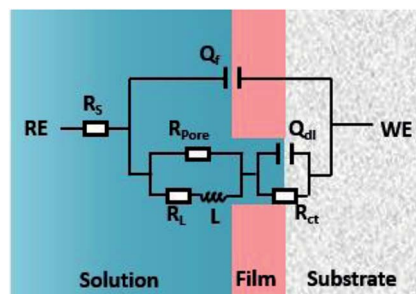


Fig. 6 Electrochemical equivalent circuit used for EIS fittings.



**Table 3** Parameter values obtained after the fitting of the EIS results of Fig. 5

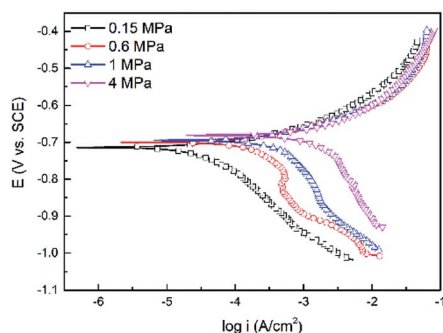
$P_{\text{CO}_2}$ , MPa	$R_s$ , $\Omega \text{ cm}^2$	$Q_f$			$R_{\text{pore}}$ , $\Omega \text{ cm}^2$	$R_L$ , $\Omega \text{ cm}^2$	$L$ , H $\text{cm}^2$	$Q_{\text{dl}}$		
		$Y_0 \times 10^{-3} \Omega \text{ cm}^{-2} \text{ s}^n$	$n$					$Y_0 \Omega \text{ cm}^{-2} \text{ s}^n$	$n$	$R_{\text{ct}}$ , $\Omega \text{ cm}^2$
0.15	2.544	0.955	0.7893	67.72	173.3	119.6		0.20	0.6918	34.38
0.6	1.769	1.312	0.7779	22.93	107.5	9.5		2.62	1	4.86
1	2.095	1.259	0.7911	18.46	59.8	5.3		1.71	0.9403	6.22
4	2.486	0.755	0.827	12.52	77.0	1.6		1.14	0.7937	3.74

of the N80 carbon steel decreased gradually with the  $\text{CO}_2$  partial pressure, indicating the corrosion processes enhanced. The inductance decreased from 119.6 to 1.62 H  $\text{cm}^2$ , in accordance with the EIS curves. It's indicating that the coverage of the corrosion scale increased with the partial pressure of  $\text{CO}_2$ . Note that  $R_{\text{pore}}$  decreased. It revealed that the formation of the corrosion scale on the steel matrix did not restrain the permeation of ions effectively as the partial pressure of  $\text{CO}_2$  increased.

### Polarization experiments

Fig. 7 shows the polarization curves of the N80 carbon steel at different  $\text{CO}_2$  partial pressures and 100 °C. As shown in Fig. 5, the cathodic current increased with the  $\text{CO}_2$  partial pressure. Unlike the cathodic reactions, the increase of  $\text{CO}_2$  partial pressure did not affect the anodic reactions significantly. We can conclude that the corrosion was mainly dominated by cathodic reactions.

Fitted kinetic parameters, corrosion potential ( $E_{\text{corr}}$ ) and corrosion current density ( $i_{\text{corr}}$ ) are listed in Table 4. The corrosion potential shifted towards the less negative values with the  $\text{CO}_2$  partial pressure. The corrosion current density increased from 48 to 2168  $\mu\text{A cm}^{-2}$  as the  $\text{CO}_2$  partial pressure increased from 0.15 to 4 MPa, indicated that the corrosion processes enhanced at higher  $\text{CO}_2$  partial pressure. This trend was in agreement with the immersion results.

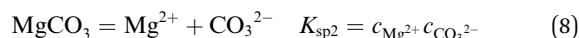
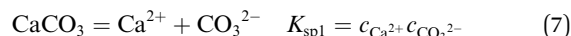
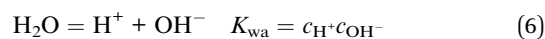
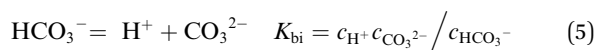
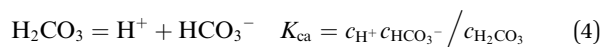
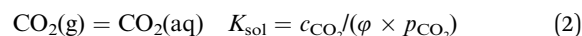
**Fig. 7** Polarization curves of the N80 steel under various  $\text{CO}_2$  partial pressures at 100 °C.**Table 4** Fitting parameters of the polarization curves of N80 steel under different  $\text{CO}_2$  partial pressures at 100 °C

$P_{\text{CO}_2}$ , MPa	0.15	0.6	1	4
$E_{\text{corr}}$ (mV)	-714.7	-699.6	-693.6	-680.9
$i_{\text{corr}}$ ( $\mu\text{A cm}^{-2}$ )	48	162	528	2168

## Discussion

### Corrosion reactions of the steel and formation of the main corrosion products in the $\text{CO}_2$ -containing oilfield formation water system

It is known that gaseous  $\text{CO}_2$  is not corrosive. Once  $\text{CO}_2$  dissolved in water, the vapor-liquid equilibrium of  $\text{CO}_2$  is reached, as expressed in Reaction (2). Despite the fact that only a small fraction of  $\text{CO}_2$  dissociates in water to form carbonic acid (Reaction (3)). The as-formed acid is more corrosive to steel than a completely dissociated acid at the same pH.<sup>17,34</sup> It is diprotic and therefore dissociates in two steps (Reactions (4) and (5)). The dissociation of water (Reaction (6)) is also included. The presence of  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  ions in the formation water can result in the precipitation of calcium carbonate ( $\text{CaCO}_3$ ) and magnesium carbonate ( $\text{MgCO}_3$ ) (Reactions (7) and (8), respectively), which may affect the ionic equilibrium. The related equilibrium equations are:



where  $K_{\text{sol}}$  and  $K_{\text{hy}}$  are the solubility and hydrolysis constants of  $\text{CO}_2$ , respectively;  $K_{\text{ca}}$ ,  $K_{\text{bi}}$ , and  $K_{\text{wa}}$  are the dissociation constants of reactions (4)–(6), respectively;  $K_{\text{sp1}}$  and  $K_{\text{sp2}}$  are the solubility product constants of  $\text{CaCO}_3$  and  $\text{MgCO}_3$ , respectively. These constants can be calculated by formulae listed in Table 5, where  $\varphi$  is the fugacity coefficient defined in eqn (9);<sup>35</sup>  $P_{\text{CO}_2}$  is the  $\text{CO}_2$  partial pressure in psi;  $P$  is the total pressure in psi;  $T_k$  is the Kelvin temperature in K; and  $T_f$  is the Fahrenheit temperature in °F.

$$\log \varphi = P \left( 0.0031 - \frac{1.4}{T_k} \right) \quad (9)$$

The ionic strength of a solution is defined as:

$$I = \frac{1}{2} \sum_i m_i z_i^2 \quad (10)$$





**Table 5** Formulae used for the calculation of the reaction equilibrium constants<sup>35,36</sup>

Formula	Reaction
$K_{\text{sol}} = \frac{14.5}{1.00258} \times 10^{-(2.27+5.65 \times 10^{-3} T_f - 8.06 \times 10^{-6} T_f^2 + 0.075 I)}$	(2)
$K_{\text{hy}} = 2.58 \times 10^{-3}$	(3)
$K_{\text{ca}} = 387.6 \times 10^{-(6.41 - 1.594 \times 10^{-3} T_f + 8.52 \times 10^{-6} T_f^2 - 3.07 \times 10^{-5} P - 0.4772 \times I^{1/2} + 0.1180 I)}$	(4)
$K_{\text{bi}} = 10^{-(10.61 - 4.97 \times 10^{-3} T_f + 1.331 \times 10^{-5} T_f^2 - 2.624 \times 10^{-5} P - 1.166 \times I^{1/2} + 0.3466 I)}$	(5)
$K_{\text{wa}} = 10^{-(29.3868 - 0.0737549 T_K + 7.47881 \times 10^{-5} T_K^2)}$	(6)
$K_{\text{sp1}} = 5.288 \times 10^{-10}$	(7)
$K_{\text{sp2}} = 4.781 \times 10^{-8}$	(8)

where  $m_i$  is the concentration of species in the aqueous solution in mol L<sup>-1</sup> and  $z_i$  is the charge of these species.

With regard to the species NaCl, KCl, and Na<sub>2</sub>SO<sub>4</sub> dissociated in the solution completely without affecting the electro-neutrality, and the condition of electronical neutrality provides the following relationship:

$$c_{\text{Na}^+} + 2c_{\text{Ca}^{2+}} + 2c_{\text{Mg}^{2+}} + c_{\text{H}^+} = c_{\text{OH}^-} + c_{\text{HCO}_3^-} + 2c_{\text{CO}_3^{2-}} + c_{\text{Cl}^-} \quad (11)$$

where  $c_{\text{Na}^+}$  is the concentration of Na<sup>+</sup> from dissociated NaHCO<sub>3</sub> ( $9.836 \times 10^{-3}$  mol L<sup>-1</sup>),  $c_{\text{Cl}^-}$  is the Cl<sup>-</sup> concentration from dissociated CaCl<sub>2</sub> and MgCl<sub>2</sub>.  $c_{\text{H}^+}$ ,  $c_{\text{OH}^-}$ ,  $c_{\text{HCO}_3^-}$ ,  $c_{\text{Ca}^{2+}}$ ,  $c_{\text{Mg}^{2+}}$ , and  $c_{\text{CO}_3^{2-}}$  are the equilibrium concentrations of H<sup>+</sup>, OH<sup>-</sup>, HCO<sub>3</sub><sup>-</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup>, and CO<sub>3</sub><sup>2-</sup>, respectively. The concentrations of CO<sub>2</sub> and H<sub>2</sub>CO<sub>3</sub> in solution can be derived by Reactions (2) and (3) and eqn (9) and (10). Combining eqn (4)–(8) with eqn (11), a quartic equation with only one variable,  $c_{\text{H}^+}$ , can be derived:

$$\frac{2 \times (K_{\text{sp1}} + K_{\text{sp2}})}{K_{\text{bi}} \times K_{\text{ca}} \times c_{\text{H}_2\text{CO}_3}} c_{\text{H}^+}^4 + c_{\text{H}^+}^3 + (c_{\text{Na}^+} - c_{\text{Cl}^-}) c_{\text{H}^+}^2 - (K_{\text{wa}} + K_{\text{ca}} \times c_{\text{H}_2\text{CO}_3}) \times c_{\text{H}^+} - 2K_{\text{bi}} \times K_{\text{ca}} \times c_{\text{H}_2\text{CO}_3} = 0 \quad (12)$$

Solving the above equation allows to obtain the concentration of H<sup>+</sup>. All the ionic concentration can be calculated by plugging the concentration of H<sup>+</sup> for the equilibrium eqn (4)–(6), and the results are shown in Table 6. The calculated pH values were in well agreement with the measured values. The pH values and the amount of CO<sub>3</sub><sup>2-</sup> dissociated in the formation water decreased with the CO<sub>2</sub> partial pressure, while the dissolved CO<sub>2</sub>, H<sub>2</sub>CO<sub>3</sub>, and HCO<sub>3</sub><sup>-</sup> increased significantly.

According to corrosion thermodynamics, the Nernst-equation can be used to illustrate the acceleration effect of

the CO<sub>2</sub> partial pressure on the cathodic reactions. The possible cathodic reactions<sup>35,37,38</sup> taking place on N80 steel in CO<sub>2</sub>-saturated formation water are eqn (13)–(16):

$$2\text{H}^+ + 2\text{e} = \text{H}_2 \quad E_1 = E_1^0 + \frac{RT}{nF} \ln c_{\text{H}^+} \quad (13)$$

$$\text{H}_2\text{CO}_3 + \text{e} = \text{HCO}_3^- + \text{H} \quad E_2 = E_2^0 + \frac{RT}{nF} \ln \frac{c_{\text{H}_2\text{CO}_3}}{c_{\text{HCO}_3^-}} \quad (14)$$

$$\text{HCO}_3^- + \text{e} = \text{CO}_3^{2-} + \text{H} \quad E_3 = E_3^0 + \frac{RT}{nF} \ln \frac{c_{\text{HCO}_3^-}}{c_{\text{CO}_3^{2-}}} \quad (15)$$

$$\text{H}_2\text{O} + \text{e} = \text{OH}^- + \text{H} \quad E_4 = E_4^0 + \frac{RT}{nF} \ln \frac{1}{c_{\text{OH}^-}} \quad (16)$$

where  $E^0$  is the potential in standard conditions in V;  $R$  is the gas constant ( $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ );  $T$  is temperature in K;  $n$  is the number of electrons flowing through the corrosion cell; and  $F$  is the Faraday constant and equals to 96 500 C.

During the steel corrosion processes, iron dissolved forming corrosion products on the surface of the electrode according to the following reactions:<sup>8,38–40</sup>

$$\text{Fe} = \text{Fe}^{2+} + 2\text{e} \quad E_5 = E_5^0 + \frac{RT}{nF} \ln c_{\text{Fe}^{2+}} \quad (17)$$

$$\text{Fe} + \text{H}_2\text{CO}_3 = \text{FeCO}_3 + 2\text{H}^+ + 2\text{e} \quad E_6 = E_6^0 + \frac{RT}{nF} \ln \frac{c_{\text{H}^+}^2}{c_{\text{H}_2\text{CO}_3}} \quad (18)$$

$$\text{Fe} + \text{HCO}_3^- = \text{FeCO}_3 + \text{H}^+ + 2\text{e} \quad E_7 = E_7^0 + \frac{RT}{nF} \ln \frac{c_{\text{H}^+}}{c_{\text{HCO}_3^-}} \quad (19)$$

$$\text{Fe} + \text{CO}_3^{2-} = \text{FeCO}_3 + 2\text{e} \quad E_8 = E_8^0 + \frac{RT}{nF} \ln \frac{1}{c_{\text{CO}_3^{2-}}} \quad (20)$$

**Table 6** Ionic concentrations in the formation water (mol L<sup>-1</sup>) and pH values under various CO<sub>2</sub> partial pressures at 100 °C

$P_{\text{CO}_2}$ MPa	$c_{\text{CO}_2}$	$c_{\text{H}_2\text{CO}_3}$	$c_{\text{HCO}_3^-}$	$c_{\text{CO}_3^{2-}}$	$c_{\text{H}^+}$	$c_{\text{OH}^-}$	pH <sub>calculated</sub>	pH <sub>measured</sub>
0.15	$1.31 \times 10^{-2}$	$3.38 \times 10^{-5}$	$4.06 \times 10^{-3}$	$7.76 \times 10^{-7}$	$2.80 \times 10^{-6}$	$1.88 \times 10^{-7}$	5.55	5.47
0.6	$4.75 \times 10^{-2}$	$12.26 \times 10^{-5}$	$7.63 \times 10^{-3}$	$7.55 \times 10^{-7}$	$5.43 \times 10^{-6}$	$9.69 \times 10^{-7}$	5.27	5.31
1	$7.26 \times 10^{-2}$	$18.73 \times 10^{-5}$	$9.37 \times 10^{-3}$	$7.45 \times 10^{-7}$	$6.79 \times 10^{-6}$	$7.76 \times 10^{-8}$	5.17	5.06
4	$15.11 \times 10^{-2}$	$38.99 \times 10^{-5}$	$1.33 \times 10^{-2}$	$7.22 \times 10^{-7}$	$1.02 \times 10^{-5}$	$5.15 \times 10^{-8}$	4.99	4.88

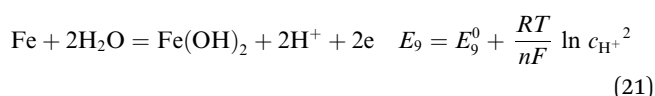


**Table 7** Standard Gibbs free energy of the species in the formation water<sup>34</sup>

Species	$\Delta G_f^0$ (kJ mol <sup>-1</sup> )	Species	$\Delta G_f^0$ (kJ mol <sup>-1</sup> )
H <sup>+</sup>	0	Fe	0
H <sub>2</sub> O (l)	-237.129	Fe <sup>2+</sup> (aq)	-78.90
H <sub>2</sub> CO <sub>3</sub> (aq)	-623.08	FeCO <sub>3</sub> (s)	-666.67
HCO <sub>3</sub> <sup>-</sup> (aq)	-586.77	Fe(OH) <sub>2</sub>	-486.5
CO <sub>3</sub> <sup>2-</sup> (aq)	-527.81	OH <sup>-</sup> (aq)	-157.244

**Table 8** Standard electrode potential of all the possible reactions (V)

$E_1^0$	$E_2^0$	$E_3^0$	$E_4^0$	$E_5^0$	$E_6^0$	$E_7^0$	$E_8^0$	$E_9^0$
0	-0.34	-0.61	-0.83	-0.44	-0.23	-0.41	-0.72	-0.06



As shown in Table 8, the standard electrode potential of all the reactions ( $E_0$ ) can be calculated by eqn (22) and (23) that combines the standard Gibbs free energy of the reactants ( $\Delta G_{f,\text{products}}^0$ ) or products ( $\Delta G_{f,\text{reactions}}^0$ ) listed in Table 7. Then, we substitute the calculated standard electrode potential into eqn (13)–(21) to obtain the equilibrium electrode potentials of the possible reactions at different CO<sub>2</sub> partial pressures, which Table 9. It should be pointed out that Reaction (17) was not included in the equilibrium potential calculation because the concentration of ferrous ions at the initial stage of corrosion is low and unknown, which can be considered negligible.

$$\Delta G = \sum v \Delta G_{f,\text{products}}^0 - \sum v \Delta G_{f,\text{reactions}}^0 \quad (22)$$

$$E_0 = -\frac{\Delta G}{nF} \quad (23)$$

Fig. 8 compares the measured corrosion potential from Fig. 7,  $E_{\text{corr}}$ , and the calculated equilibrium potential of each possible reaction as a function of the CO<sub>2</sub> partial pressure. According to the mixed potential theory, only anodic reactions with potentials more negative than  $E_{\text{corr}}$  and cathodic reactions with potentials more positive than  $E_{\text{corr}}$  can occur. According to this theory, all the cathodic reactions which is shown in Fig. 8(a) can take place with the exception of Reaction (14), the reduction

of H<sub>2</sub>CO<sub>3</sub> to generate bicarbonate ions, because the equilibrium potential of Reaction (14) is more negative than the corrosion potential. Therefore, the cathodic reactions of N80 steel in the CO<sub>2</sub><sup>-</sup>-containing formation water included the reduction of H<sup>+</sup>, HCO<sub>3</sub><sup>-</sup>, and H<sub>2</sub>O. However, the reduction of water shows much slower reaction kinetics, resulting in minimal contribution to the total cathodic reaction.<sup>9</sup> As shown in Fig. 8(b), all the anodic reactions can take place. It should be pointed out that Reaction (21) can occur only at CO<sub>2</sub> partial pressures lower than 1 MPa. Therefore, the anodic reactions taking place on N80 in the CO<sub>2</sub>-containing formation water included the direct dissolution of iron (Reaction (17)), the formation of FeCO<sub>3</sub> scale (Reactions (18)–(20)), and the hydrolysis of iron (Reaction 21) at CO<sub>2</sub> partial pressures lower than 1 MPa. However, although the equilibrium potential of Reaction (20) is more negative than  $E_{\text{corr}}$ , this reaction is ignorable because of its low reaction kinetics as a result of the extremely low concentration of CO<sub>3</sub><sup>2-</sup> ions.<sup>35</sup>

### Corrosion mechanism of the steel in the CO<sub>2</sub>-containing oilfield formation water system

At low CO<sub>2</sub> partial pressures, the amount of dissociated HCO<sub>3</sub><sup>-</sup> and CO<sub>3</sub><sup>2-</sup> is limited. The reduction of H<sup>+</sup> ions became the dominant cathodic reaction and the cathodic polarization curves were under charge transfer control. The concentration of HCO<sub>3</sub><sup>-</sup> (Table 6) increased with the CO<sub>2</sub> partial pressure and more HCO<sub>3</sub><sup>-</sup> ions transferred from the solution to the matrix surface, accelerating the cathodic reactions to generate CO<sub>3</sub><sup>2-</sup> in solution. Therefore, higher CO<sub>2</sub> partial pressures resulted in higher corrosion rates not only as a result of the lower pH value but also by increasing the rate of the bicarbonate reduction process.<sup>10</sup> Then the supersaturation and precipitation rates of FeCO<sub>3</sub> were also accelerated correspondingly. The coverage of the corrosion scale increased. Burkle<sup>41</sup> was also discussed the morphology and development of the FeCO<sub>3</sub> crystals over time. Burkle stated that the steel surface was almost entirely covered by FeCO<sub>3</sub> crystals after several hours of exposure. According to the Faraday admittance reported by Cao<sup>42</sup> and Zhu,<sup>25</sup> as the coverage rate ( $\theta$ ) of the corrosion scale increases, the inductance loop becomes smaller, which is pretty much in line with the herein obtained Nyquist plots.

The precipitation of FeCO<sub>3</sub> crystal involves two steps namely, nucleation and particle growth. Supersaturation levels exceeding 1 initiated the nucleation of FeCO<sub>3</sub>. Nesic<sup>43</sup> pointed out that higher  $P_{\text{CO}_2}$  leads to a higher supersaturation which accelerates FeCO<sub>3</sub> precipitation and scale growth. Once stable nuclei were formed, crystal growth is then dominant process.<sup>9</sup> Therefore, high nucleation rate led to crystalline films with

**Table 9** Equilibrium electrode potential of the possible reactions (13)–(21) in the CO<sub>2</sub>-saturated formation water at 100 °C (V)

$P_{\text{CO}_2}$ , MPa	$E_1$	$E_2$	$E_3$	$E_4$	$E_6$	$E_7$	$E_8$	$E_9$
0.15	-0.6520	-0.7719	-0.5767	-0.5721	-0.7116	-0.7720	-0.7339	-0.7154
0.6	-0.6307	-0.7508	-0.5556	-0.5508	-0.7110	-0.7715	-0.7334	-0.6941
1	-0.6236	-0.7438	-0.5585	-0.5437	-0.7106	-0.7712	-0.7332	-0.6870
4	-0.6104	-0.7316	-0.5362	-0.5305	-0.7092	-0.7703	-0.7327	-0.6738



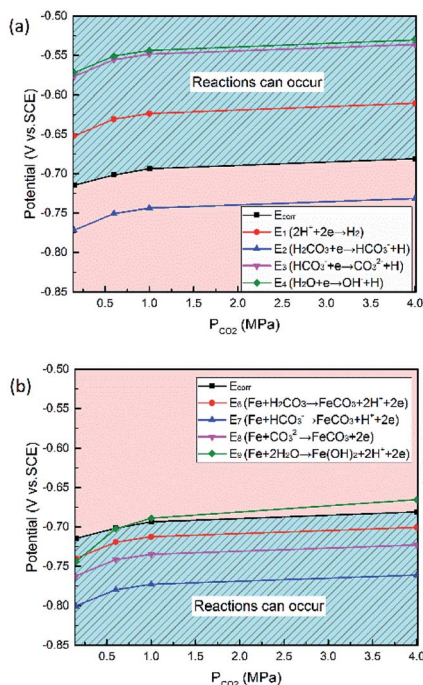


Fig. 8 Comparison of the measured corrosion potential ( $E_{\text{corr}}$ ) and the calculated equilibrium potential of anodic (a) and cathodic (b) reactions as a function of the  $\text{CO}_2$  partial pressure.

small and fine grains at high  $\text{CO}_2$  partial pressures. In contrast, a rather rough scale with large grains was formed at low  $\text{CO}_2$  partial pressures because of the low original nucleation rates resulted in relatively large spaces between the  $\text{FeCO}_3$  grains.

However, the corrosion scales became denser but the corrosion rate at high  $\text{CO}_2$  partial pressures increased, which implied that this dense scale did not protect the steel matrix effectively. The decrease of pore resistance verified this point and the observations from Gao, *et al.*<sup>14</sup> suggest similar effects that thicker and denser scale formed on pipeline carbon steel have poor protectiveness.

## Conclusions

In this study, the effect of high  $\text{CO}_2$  partial pressures on the corrosion behaviour of carbon steel in the formation water system at 100 °C was investigated by various electrochemical measurements and surface analysis, combined with thermodynamic calculations of the potential anodic/cathodic reactions. Based on the electrochemical and theoretical results, the following conclusions can be drawn:

(1) The corrosion potentials were calculated for each possible anodic/cathodic reaction. The anodic reactions of the steel included the direct dissolution of Fe, the formation of  $\text{FeCO}_3$  scale, and the hydrolysis of Fe up to 1 MPa of  $\text{CO}_2$ . The cathodic reactions included the reduction of  $\text{H}^+$ ,  $\text{HCO}_3^-$ , and  $\text{H}_2\text{O}$ .

(2) The anodic reactions were not affected by the  $\text{CO}_2$  partial pressure significantly, while the cathodic reactions were strongly enhanced *via* reduction of the pH and increase of the rate of bicarbonate reduction.

(3) The concentration of  $\text{HCO}_3^-$  increased with the  $\text{CO}_2$  partial pressure, and the precipitation rate of  $\text{FeCO}_3$  were also accelerated. Small and fine  $\text{FeCO}_3$  scale grains were formed on the steel surface at high  $\text{CO}_2$  partial pressure. This scale showed poor protectiveness and the  $\text{CO}_2$  corrosion processes was enhanced as a result.

## Conflicts of interest

There are no conflicts to declare.

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## References

- 1 A. Kahyarian, M. Achour and S. Nesic, in *Trends in Oil and Gas Corrosion Research and Technologies*, 2017, pp. 149–190.
- 2 P. Sui, J. Sun, Y. Hua, H. Liu, M. Zhou, Y. Zhang, J. Liu and Y. Wang, *Int. J. Greenhouse Gas Control*, 2018, **73**, 60–69.
- 3 S. Nesic, *Corros. Sci.*, 2007, **49**, 4308–4338.
- 4 M. H. Sk, A. M. Abdullah, M. Ko, B. Ingham, N. Laycock, R. Arul and D. E. Williams, *Corros. Sci.*, 2017, **126**, 26–36.
- 5 J. Han, J. Zhang and J. W. Carey, *Int. J. Greenhouse Gas Control*, 2011, **5**, 1680–1683.
- 6 D. Dwivedi, K. Lepkova and T. Becker, *RSC Adv.*, 2017, **7**, 4580–4610.
- 7 M. B. Kermani and A. Morshed, *Corrosion*, 2003, **59**, 659–683.
- 8 B. R. Linter and G. T. Burstein, *Corros. Sci.*, 1999, **41**, 117–139.
- 9 R. Barker, D. Burkle, T. Charpentier, H. Thompson and A. Neville, *Corros. Sci.*, 2018, **142**, 312–341.
- 10 G. Schmitt and M. Horstemeier, in *Corrosion 2006*, NACE International, 2006.
- 11 G. Schmitt, in *Corrosion 2015*, NACE International, 2015.
- 12 A. Dugstad, in *Corrosion 2006*, NACE international, 2006.
- 13 R. Barker, Y. Hua and A. Neville, *Int. Mater. Rev.*, 2017, **62**, 1–31.
- 14 K. Gao, F. Yu, X. Pang, G. Zhang, L. Qiao, W. Chu and M. Lu, *Corros. Sci.*, 2008, **50**, 2796–2803.
- 15 M. Gao, X. Pang and K. Gao, *Corros. Sci.*, 2011, **53**, 557–568.
- 16 S. Nesic, J. Postlethwaite and S. Olsen, *Corrosion*, 1996, **52**, 280–294.
- 17 J. M. Bockris and D. Drazic, *Electrochim. Acta*, 1962, **7**, 293–313.
- 18 S. Nesic, N. Thevenot, J. L. Crolet and D. Drazic, in *Corrosion 1996*, NACE International, 1996.
- 19 T. D. C. Almeida, M. C. E. Bandeira, R. M. Moreira and O. R. Mattos, *Corros. Sci.*, 2017, **120**, 239–250.
- 20 H. Liu, T. Gu, G. Zhang, G. Liu and Y. Cheng, *Corros. Sci.*, 2018, **136**, 47–59.
- 21 H. M. Ezuber, *Mater. Des.*, 2009, **30**, 3420–3427.
- 22 G. Schmitt, in *Corrosion 1985*, NACE International, 1985.



- 23 R. Nyborg and A. Dugstad, in *Corrosion 1998*, NACE International, 1998.
- 24 M. B. Tomson and M. L. Johnson, in *SPE 1991*, SPE International, 1991.
- 25 S. Zhu, A. Fu, J. Miao, Z. Yin, G. Zhou and J. Wei, *Corros. Sci.*, 2011, **53**, 3156–3165.
- 26 Z. Qiu, C. Qiong, Z. Chang, Z. Zhao, C. Zhao and Z. Ye, *Petroleum Exploration and Development*, 2012, **39**, 256–260.
- 27 K. Videm and A. Dugstad, in *Corrosion 1988*, NACE International, 1988.
- 28 A. B. Gavanluei, B. Mishra and D. L. Olson, in *Corrosion 2013*, NACE International, 2013.
- 29 ASTM G1-03, in *Standard*, ASTM International, 2017.
- 30 S. Arumugam, N. Tajallipour and P. J. Teevens, in *Corrosion 2014*, NACE International, 2014.
- 31 Y. Sun and S. Nesic, in *Corrosion 2004*, NACE International, 2004.
- 32 Y. Hua, A. Shamsa, R. Backer and A. Neville, *Appl. Surf. Sci.*, 2018, **455**, 667–682.
- 33 W. Wang, W. Yan, L. Zhu, P. Hu, Y. Shan and K. Yang, *Mater. Des.*, 2009, **30**, 3436–3443.
- 34 S. Nesic, M. Nordsveen, R. Nyborg and A. Stangeland, in *Corrosion 2001*, NACE International, 2001.
- 35 G. Zhang and Y. Cheng, *Corros. Sci.*, 2009, **51**, 87–94.
- 36 P. Atkin and J. D. Paula, *Physical Chemistry*, Oxford university press, Oxford, 8th edn, 2006.
- 37 B. Wang, L. Xu, G. Liu and M. Lu, *Corros. Sci.*, 2018, **136**, 210–220.
- 38 L. Wei, X. Pang and K. Gao, *Corros. Sci.*, 2016, **111**, 637–648.
- 39 D. H. Davies and G. T. Burstein, *Corrosion*, 1980, **36**, 416–422.
- 40 G. Zhang, Y. Zeng, X. Guo, F. Jiang, D. Shi and Z. Chen, *Corros. Sci.*, 2012, **65**, 37–47.
- 41 D. Burkle, R. D. Motte, W. Taleb, A. Kleppe, T. Comyn, S. M. Vargas, A. Neville and R. Barker, *Electrochim. Acta*, 2017, **255**, 127–144.
- 42 C. Cao, *Electrochim. Acta*, 1990, **35**, 837–844.
- 43 S. Nesic and K. L. J. Lee, *Corrosion*, 2003, **59**, 616–628.

