Preparation and characterization of a novel positively charged composite hollow fiber nanofiltration membrane based on chitosan lactate†

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A positively charged composite hollow fiber nanofiltration (NF) membrane was prepared via interfacial polymerization (IP) between chitosan lactate (CL) and trimesoyl chloride (TMC) on a polyether sulfone (PES) hollow fiber ultrafiltration (UF) membrane. The chemical structure and the morphologies of the resultant NF membranes were characterized with attenuated total reflectance-infrared spectroscopy (ATR-IR) and scanning electron microscopy (SEM). The rejection of NF membrane for different inorganic salt aqueous solutions followed the order: MgCl2 > ZnCl2 > MgSO4 > NaCl > Na2SO4. It suggested that this novel kind of composite hollow fiber NF membrane is positively charged. The molecular weight cut-off (MWCO) was obtained through the rejection of polyethylene glycol (PEG) solutions with different molecular weights (Mw). The effect of monomer concentrations, the interfacial polymerization time, and the curing temperature, were investigated, respectively. The rejection and the permeate flux of the resultant composite hollow fiber CL membrane fabricated under the optimal conditions towards a MgCl2 solution of 1000 ppm were 95.1% and 10.3 L m⁻² h⁻¹, respectively, at 0.4 MPa and 25 °C. Moreover, the effects of operation conditions on the rejection performance of the composite hollow fiber NF membrane were investigated. It suggested that this novel kind of hollow fiber composite nanofiltration membrane based on CL have excellent stability in rejection performances to salt solutions.

1. Introduction

Currently, nanofiltration (NF) is drawing more and more attention due to its advantages such as lower operation pressure, lower energy consumption, and excellent separation performance of multi-di-valent ions and low-molecular-weight (LWM) organic compounds from 200 to 1000 Da.¹–³ The NF membrane is a kind of pressure-driven membrane, whose mechanisms of rejecting ions and LMW organic compounds are based on a sieving effect and Donnan exclusion.⁴–⁵ NF membranes have been widely used in seawater desalination,⁶ industrial wastewater treatment,⁷ drinking water purification,⁷ biotechnology⁸ and food science.⁹ According to previous studies, positively-charged NF membranes show better performance in some specific fields, such as recovery of high-valence metal ions,¹⁰ separation of positively charged amino acids and proteins,¹¹ and so on. However, most of the current commercial NF membranes on the market are negatively charged.¹²¹³ Thus it is meaningful to develop and industrialize some novel kinds of positively charged NF membranes.

Various methods have been applied to prepare positively charged NF membranes, such as interfacial polymerization, phase inversion method, chemical cross-linking, UV-induced grafting, etc.¹⁵–¹⁸ Wei et al.¹⁹ developed a positively charged NF membrane via interfacial polymerization by using polyethylenimine (PEI) and trimesoyl chloride (TMC). The zeta potentials results indicated that the surface of the resultant PEI composite NF membrane was positively charged as pH is being below 8.2. The resultant NF membrane shows good rejection (R) to metal ions, 92.6, 89.6, 89.2 and 86.3%, to chromium, nickel, zinc and copper ions, respectively. Mahendran, et al.²⁰ prepared a positively charged NF membrane from aminated polysulfone
active and could be modified on chitosan molecular chains, so chitosan is chemically cross-linking. The CS/CA composite membrane had a MWCO of 50 kDa via interfacial polymerization by using chitosan lactate and trimesoyl chloride (TMC) as the aqueous phase solute and the organic phase solute, respectively. Fig. 1(b) shows the molecular structure of TMC. The interfacial polymerization occurred between the residual amine (–NH₂) and the acyl chloride groups (–COCl) on the top of polyether sulfone (PES) hollow fiber ultrafiltration (UF) membrane (Scheme 1). The chemical structure and morphology were characterized with attenuated total reflectance-infrared spectroscopy (ATR-IR) and scanning electron microscopy (SEM). The rejection reached maximum 95.1% for 2000 ppm MgCl₂ solution as the IP time was 120 s. CL/PES composite hollow fiber NF membranes showed good retentions of heavy metal ions, and the rejection of the nanofiltration membrane for inorganic salts followed in an order of: ZnCl₂ > MgCl₂ > MgSO₄ > NaCl > Na₂SO₄, showing the typical rejection characteristic of positively charged NF membrane to different inorganic salts. This work will provide the base for the scale-up and the industrialization of CL composite NF membranes.

2. Materials and methods

2.1. Materials

Polyether sulfone (PES) hollow fiber ultrafiltration (UF) membranes with MWCO of 50 kDa were self-made in lab. The pure water permeate flux at 0.1 MPa of PES hollow fiber UF membrane is 53 L m⁻² h⁻¹. Chitosan lactate (CL, Mw ~ 30 kDa) with the solubility of 65 g L⁻¹ was purchased from Wuhan
Yuancheng Gongchuang Technology Co. Ltd (Wuhan, China). PEG with different $M_w$ in the range of 200 to 1000 Da and trimesooy chloride (TMC, 98%) was obtained from Shanghai Macklin Biochemical Co. Ltd (Shanghai, China). Inorganic salts, including magnesium chloride (MgCl$_2$, AR), sodium sulfate (Na$_2$SO$_4$, AR), magnesium sulfate (MgSO$_4$, AR), sodium chloride (NaCl, AR), were obtained from Sinopharm Chemical Reagent Co. Ltd (Shanghai, China). All reagents are of analytical grade and there was no further purification.

2.2. Fabrication of PES hollow fiber membrane

The PES hollow fiber membranes were prepared by phase-inversion method. The casting solution contains 16 wt% PES, 10 wt% PVP, 10 wt% PEG400 and 74 wt% DMAc. The casting solution was degassed for 6 h in the pump prior to spinning. Subsequently, the casting solution was spun into a spinneret with the outer diameter of 1.2 mm. After that, the nascent fibers were formed in a coagulation tank after passing through a certain air gap, and then the fibers were collected by a take-up unit. As shown in Fig. S1,† the structure morphology of the hollow fiber membrane was measured by SEM. The parameters of PES hollow fiber membrane were showed in Table S1.†

2.3. Preparation of composite hollow fiber CL/PES NF membranes

After being pre-soaked for 24 h in deionized (DI) water for removing contaminants, the two ends of the hollow fiber membrane were sealed with a sealant to prevent the monomer solution from entering the lumen side of the hollow fiber. The PES UF membranes were immersed in the CL aqueous solution for 5 min and then poured out, and the excess CL aqueous solution was removed at ambient temperature in air by blowing. Next, these membranes were immersed in TMC in n-hexane for 120 s and then poured out. After removing the excess TMC solution by blowing, the membranes were cured for 20 min in an oven at 90 °C. Finally, the resultant composite hollow fiber CL/PES NF membranes were washed extensively, and sealed in a PMMA pipe to obtain the hollow-fiber membrane modules.

2.4. Characterizations of composite hollow fiber NF membranes

The surface and cross-section morphologies of PES UF membranes and as-prepared composite NF membranes were characterized using a scanning electron microscopy (SEM, Phenom ProX, Netherlands). The attenuated total reflectance Fourier transform infrared (ATR-IR) spectra were collected in the range of 600 to 4000 cm$^{-1}$ at a resolution of 4 cm$^{-1}$ with a bench-top spectrometer (Nicolet iS10, Thermo Fisher Scientific, the United States), to characterize the chemical structures of the resultant composite NF membrane surfaces. The hydrophilicities of the membrane surfaces were characterized with the static contact angle measurements (DSA305, Kruss GmbH, Germany) using 0.2 μL droplet of pure water. Surface charge properties of the membranes were studied by measuring streaming potentials at various pH values ranging from 5 to 12 using a SurPASS electrokinetic analyzer (Anton Paar GmbH, Austria). The streaming potential was measured in a 0.001 M KCl solution at 25 °C. Auto titrations with 0.1 M HCl and 0.1 M NaOH were carried out to adjust the pH of the electrolyte solution.

Rejection performance including permeate flux ($F$) and rejection rate ($R$) were measured with a lab-scale cross-flow membrane evaluation apparatus at 25 °C. The tests were carried out with concentration of inorganic salt aqueous solution of 1000 ppm at an operating pressure of 0.4 MPa. The permeation flux ($F$) was calculated using the following equation.

$$F = V/(St)$$

where, $V$ is the volume of permeated aqueous solution during the measurement, $S$ is the effective membrane area, $t$ is the time period for measurement.

The rejection rate was calculated using the following equation:

$$R = 100 \times (1 - (C_p/C_i))$$

where, $C_p$ and $C_i$ (mol L$^{-1}$) are the salt concentration in the permeate and the feed solution. The salt concentrations were obtained by the standard curves of different salts, which show the corresponding relations between the salt concentrations and the electrical conductivities of the aqueous solutions. The electrical conductivities of the salt aqueous solutions were measured by a DDS-11A conductivity meter (Shanghai Leici Instrument Company, China). All experiment results were the average values of 5 measurements.

The MWCO was known from the permeation test of PEG with different $M_w$ in the range of 200 to 1000 Da. The PEG concentrations in the feed and permeated solution were measured by ultraviolet (UV)-visible (Vis) spectrophotometer (UV-6100, Shanghai Mapada Instruments Co., Ltd., China).

3. Result and discussion

3.1. Chemical structures of membrane surfaces

Fig. 2 shows the ATR-IR spectra of PES substrate and as-prepared CL/PES composite NF membrane. As known from Fig. 2, there is a broad absorbance peak at 3350 cm$^{-1}$, corresponding to the overlap of the amine groups (−N–H) and hydroxyl groups (−O–H) stretching vibrations. A new absorbance peak occurred at 1728 cm$^{-1}$, which was the characteristic peak of the carbonyl group (−C=O) in the lactic acid groups. Absorbance peak at 1650 cm$^{-1}$ attributed to carbonyl group (−C=O) of the amide groups was enhanced significantly, suggesting the occurrence of the interfacial polymerization between the amine groups of CL and the acyl chloride groups of TMC. The peaks around 1578 cm$^{-1}$ and 1486 cm$^{-1}$ are due to the stretching vibration of C=O skeleton in aromatic ring. A new absorbance peak presented at 1083 cm$^{-1}$, which was attributed to the stretching vibration of −C−O of the lactic acid groups.

3.2. Membrane morphologies

The SEM images for the surface and cross-section morphologies of the PES substrate membrane and the CL/PES composite NF
membrane were shown in Fig. 3. It could be observed from Fig. 3(a1) that the surface of PES hollow fiber UF membrane is porous. Fig. 3(a2) shows the cross-section image of PES UF hollow fiber UF membrane, where a typical macrovoid structure of UF membrane could be observed. Fig. 3(b1) shows the surface image of the hollow fiber composite NF membrane, in which no visible pores could be observed on the surface of the resultant CL/PES composite NF membranes. As known from Fig. 3(b2), the dense layer with a thickness of approximate 273 nm could be clearly found out on the top surface of the PES substrate membrane, suggesting that a compact polyamide layer was formed on the PES UF substrate.

3.3. Hydrophilicities of membrane surfaces

The static contact angles of resultant CL/PES composite NF membrane surfaces were shown in Fig. 4. Compared with the PES UF base membrane with a water contact angle of 96.1°, all of the CL/PES composite NF membranes were more hydrophilic because of the formation of the hydrophilic polyamide active layer on the top of PES UF membrane. The static contact angle of the CL/PES composite NF membranes decreased from 65.1 to 26.3° with increasing the CL concentration from 0.8 to 4.8 wt%. The higher the CL concentration in the aqueous phase, the more the hydrophilic groups such as polyamide and hydroxyl groups on the membrane surface, which might be the reason for the increase in the hydrophilicity of resultant CL NF membrane surface.

3.4. Rejection performances

3.4.1. Rejection performances of the CL/PES composite hollow fiber NF membrane to different inorganic salt solutions.

The rejection performances were evaluated with a variety of inorganic salt solutions. The CL/PES composite hollow fiber NF membranes were fabricated under the following conditions: immersion time in 3.2 wt% CL aqueous solution: 5 min, interfacial polymerization (IP) time: 120 s, TMC concentration:
0.25 wt%, and curing temperature: 90 °C. As shown in Fig. 5, the permeate flux ($F$) for a feed solution of ZnCl$_2$, MgCl$_2$, MgSO$_4$, NaCl and Na$_2$SO$_4$ were 10.0, 10.3, 12.7, 14.6, and 14.2 L m$^{-2}$ h$^{-1}$, respectively. The rejections ($R$) decreased in an order of ZnCl$_2$ (95.7%) > MgCl$_2$ (95.1%) > MgSO$_4$ (59.7%) > NaCl (27.6%) > Na$_2$SO$_4$ (22.3%), which could be explained by Donnan exclusion theory. Mg$^{2+}$ has a higher positive valence than Na$^+$, and SO$_4^{2-}$ has a higher negative valence than Cl$^-$. High-valence cations carrying more positive charges lead to a stronger repulsion between the cations and the positively-charged CL/PES composite NF membrane. On the contrary, high-valence anions carrying more negative charges would have a stronger attraction to CL membrane.$^{35}$ The rejection of CL/PES composite NF membrane to ZnCl$_2$ was higher than that to MgCl$_2$. It could be explained by the steric hindrance because the size of Zn$^{2+}$ is larger than that of Mg$^{2+}$. $^{11}$

3.4.2. Effects of preparation conditions on the rejection performances of CL/PES composite hollow-fiber NF membranes. Using the CL aqueous solutions with different concentration ranging from 0.1 to 0.3 wt%, the CL/PES composite hollow fiber NF membranes were fabricated under the following conditions: immersion time in the CL aqueous solution: 5 min, interfacial polymerization (IP) time: 120 s, TMC concentration: 0.25 wt%, and curing temperature: 90 °C. The rejection performances of the resultant CL/PES composite NF membranes were investigated, and the results were shown in Fig. 6. As seen from Fig. 6, with increasing CL concentration, the rejection ($R$) to MgCl$_2$ solution increased gradually from 77.6 to 95.1%, and the permeate flux ($F$) decreased from 15.2 to 9.1 L m$^{-2}$ h$^{-1}$. This might be due to the formation of a more compact and thicker polyamide layer on top of the PES UF membrane with the increase in CL concentration.$^{35}$

The influence of TMC concentration on rejection performance was investigated as well, as shown in Fig. 7. As TMC concentration ranged from 0.1 to 0.35 wt%, the other preparation parameters were as the following: immersion time in 3.2 wt% CL aqueous solution: 5 min, IP time: 120 s, and curing temperature: 90 °C. It could be seen from Fig. 7 that the rejection ($R$) to MgCl$_2$ solution increase from 69.5 to 95.1% with increasing TMC concentration from 0.1 to 0.25 wt%. The rejection ($R$) began to decrease as TMC concentration was higher than 0.25 wt%. This could be attributed to carboxylate radical ($\text{–COO}^-$) produced from the hydrolyzation of the excess acyl chloride groups, weakening the positive chargeability of the CL/PES composite NF membrane.$^{36}$ As shown in Fig. 8, the isoelectric point (IEP) of the hollow fiber NF membrane prepared at TMC concentration of 0.25 wt% was at a pH value of approximately 9.2. It indicated that the fabricated composite hollow fiber NF membrane is positively charged. And the NF membranes prepared at TMC concentration of 0.30 wt% and 0.35 wt% showed the lower IEPs of approximately 8.7 and 8.3. The permeate flux ($F$) decreased slightly as TMC concentration increased from 0.1 to 0.35 wt%. The reason might be that the
more TMC monomer would accelerate the formation rate of the polyamide layer on top of the PES UF membrane.

The interfacial polymerization (IP) time is an important preparation condition affecting the rejection performance of the resultant CL/PES composite hollow fiber NF membrane. Fig. 9 shows the effects of IP time in the range of 30 to 180 s on the rejection performances under the condition of immersion time in 3.2 wt% CL aqueous solution for 5 min, TMC concentration of 0.25 wt% and heat treatment for 20 min under 90 °C. The permeate flux \( (F) \) decreased sharply with increasing the IP time from 30 to 120 s. As the IP time was prolonged further, there was no significant change in permeate flux \( (F) \). It could be explained that the further IP time tend to form a denser active layer, and the IP almost finished in 120 s. The rejection \( (R) \) to MgCl\(_2\) solution increased firstly, and then decreased with increasing the IP time. The rejection \( (R) \) reached the maximum of 95.1% for MgCl\(_2\) solution as the IP time was 120 s. It was due to the unreacted acyl chloride groups as well, which is the same as the effect of excess TMC concentration.

Post-heat treatment is another important way to increase the rejection of the resultant NF membrane. It plays a role in promoting the removal of excess organic solvent from polyamide thin film and facilitating the cross-linking of amine and acyl chloride. Hence the effects of different post-heat curing temperature from 30 to 150 °C were investigated under the condition of immersion time in 3.2 wt% CL aqueous solution for 5 min, TMC concentration of 0.25 wt%, the reaction time for 4 min and heat treatment time for 20 min. As shown in Fig. 10, the permeate flux \( (F) \) of the resultant NF membrane decreased as the curing temperature increased simultaneously. The rejection \( (R) \) to MgCl\(_2\) solution increased with the increase in the curing temperature, and then decreased as the curing temperature was higher than 90 °C. Since the higher curing temperature would increase the cross-linking degree and accelerate the movements of polymer molecular chains, and the

![Fig. 7 Influence of TMC concentrations on rejection performance of the CL/PES composite hollow fiber NF membrane.](image1)

![Fig. 8 Zeta potential of the NF hollow fiber membranes (TMC concentration: 0.25 wt%, 0.30 wt% and 0.35 wt%).](image2)

![Fig. 9 Effect of IP time on the rejection performances of the resultant CL/PES composite hollow fiber NF membrane.](image3)

![Fig. 10 Effects of the post-heat curing temperature on the rejection performances of the resultant CL/PES composite hollow fiber NF membrane.](image4)
post-heat curing would lead to the shrinkage as well, and then a tighter polyamide active layer was formed. As shown in Fig. S2, the MWCO of the NF membrane prepared under 30 °C was approximate 893 Da, and the NF membrane prepared under 60 °C shows the MWCO of 726 Da. Moreover, as the curing temperature was higher than 90 °C, the base membrane shrunk further and stripped from the polyamide active layer during the curing period, causing the defects on the membrane surface, and resulting in a decrease in the rejection ($R$). The morphology of the NF membrane prepared under the curing temperature of 150 °C was characterized with SEM. It could be observed in Fig. S3, the active layer stripped from the base membrane obviously.

### 3.4.3. Effects of the operating conditions on the rejection performances

The effects of the operating conditions including the operating pressure and the concentration of the feed solution were investigated. Fig. 11 shows the influences of the operating pressure. It could be seen that the permeate flux ($F$) increased linearly from 5.0 to 25.1 L m⁻² h⁻¹ with the increase of the operating pressure from 0.2 to 1.0 MPa. Meanwhile, there was nearly no change in the rejections ($R$) to MgCl₂ solution.

Fig. 12 shows the effects of the feed concentration on the rejection performances at 0.4 MPa and ambient temperature. As the concentration of MgCl₂ increased from 0.5 to 2.5 g L⁻¹, both of the permeate flux ($F$) and the rejection ($R$) to MgCl₂ solution decreased gradually. It could be explained by Donnan equilibrium theory. With the increase in the feed concentration, the electrostatic shielding effect of Cl⁻ ions towards the positively charged membrane increased, resulting in the decrease of membrane charge density. On the other hand, the increase in the feed concentration would lead to a higher osmotic pressure, which decreased the driving force for the permeation and caused the decrease in the permeate flux ($F$).

### 3.4.4. MWCO of the CL/PES composite hollow fiber NF membrane

Under the following preparation condition: the CL/PES composite hollow fiber NF membranes were fabricated under the following conditions: immersion time in 3.2 wt% CL aqueous solution: 5 min, interfacial polymerization (IP) time: 120 s, TMC concentration: 0.25 wt%, and curing temperature: 90 °C. The MWCO was determined via the permeation tests using PEG model solutes. The MWCO was determined with the $M_w$ of the PEG when the rejection ($R$) to the PEG solution is equal to 90%. The rejection ($R$) to PEG with the $M_w$ ranging from 200 to 1000 Da were shown in Fig. 13. It could be seen that the MWCO of the CL/PES composite hollow fiber NF membrane was approximate 506 Da.

### 4. Conclusions

Chitosan lactate (CL) was used as the monomer of the aqueous phase for the interfacial polymerization (IP) on the PES hollow fiber UF membrane for the first time. CL also has the merit of low cost, nontoxicity, and environment friendliness. Compared with the previous researches on chitosan-based NF membranes,
the aqueous monomer in this work has excellent water solubility and positively charge. In addition, interfacial polymerization has the advantages over coating and cross-linking, such as high reaction rate, short preparation time, and easy operation, which make the industrialization of this work possible in the near future.

The as-prepared CL/PES composite hollow fiber NF membranes were positively charged and following the rejection order to different inorganic salt solutions: ZnCl$_2$ (95.7%) > MgCl$_2$ (95.1%) > MgSO$_4$ (59.7%) > NaCl (27.6%) > Na$_2$SO$_4$ (22.3%). The rejection ($R$) to MgCl$_2$ solution was 95.1% while the permeate flux ($F$) was 10.3 L m$^{-2}$ h$^{-1}$ at 0.4 MPa and ambient temperature. It could be known from the cross-section SEM image that the thickness of the polyamide active layer was about 273 nm. The operating pressure and the feed solution could influence the rejection performances of the CL/PES composite hollow fiber NF membranes. This work will provide the base for the positively charged composite hollow fiber NF membranes using the chitosan derivatives as the aqueous monomers for the interfacial polymerizations. There should be the high potentiality for the industrialization of this kind of novel composite NF membrane materials due to the short IP time, the abundance, and the environment friendliness of the aqueous monomers.

**Conflicts of interest**

There are no conflicts to declare.

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