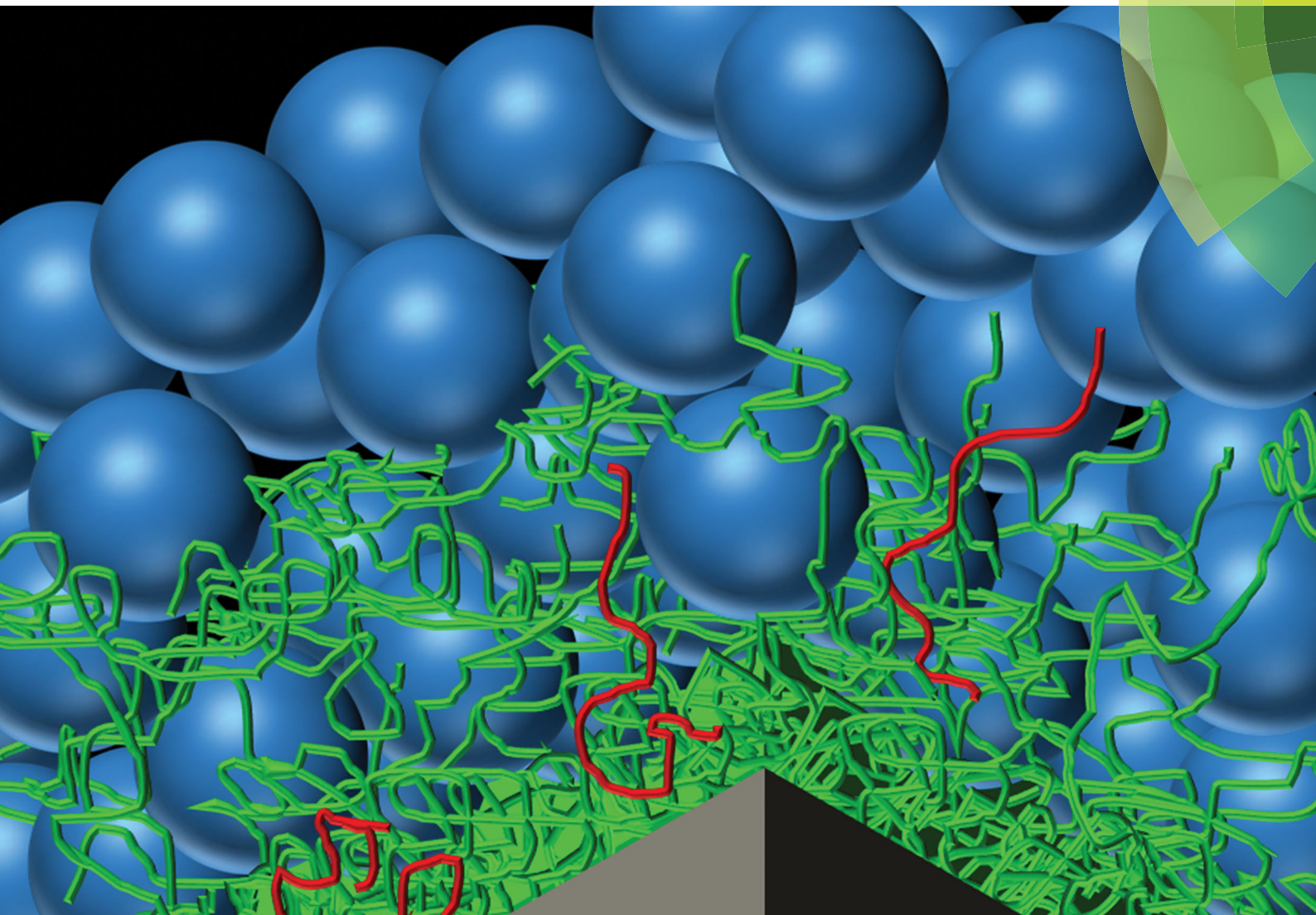


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Zahra Fakhraei, Daeyeon Lee *et al.*

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Effects of polymer–nanoparticle interactions on the viscosity of unentangled polymers under extreme nanoconfinement during capillary rise infiltration†

Jyo Lyn Hor,^a Haonan Wang,^b Zahra Fakhraai^{b*} and Daeyeon Lee^{a*}

We explore the effect of confinement and polymer–nanoparticle interactions on the viscosity of unentangled polymers undergoing capillary rise infiltration (CaRI) in dense packings of nanoparticles. In CaRI, a polymer is thermally induced to wick into the dense packings of nanoparticles, leading to the formation of polymer-infiltrated nanoparticle films, a new class of thin film nanocomposites with extremely high concentrations of nanoparticles. To understand the effect of this extreme nanoconfinement, as well as polymer–nanoparticle interactions on the polymer viscosity in CaRI films, we use two polymers that are known to have very different interactions with SiO₂ nanoparticles. Using *in situ* spectroscopic ellipsometry, we monitor the polymer infiltration process, from which we infer the polymer viscosity based on the Lucas–Washburn model. Our results suggest that physical confinement increases the viscosity by approximately two orders of magnitude. Furthermore, confinement also increases the glass transition temperature of both polymers. Thus, under extreme nanoconfinement, the physical confinement has a more significant impact than the polymer–nanoparticle interactions on the viscosity of unentangled polymers, measured through infiltration dynamics, as well as the glass transition temperature. These findings will provide fundamental frameworks for designing processes to enable the fabrication of CaRI nanocomposite films with a wide range of nanoparticles and polymers.

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Introduction

Incorporating extremely high concentrations (>50 vol%) of nanoparticles (NPs) into nanocomposite films (NCFs) can drastically enhance their properties and functionalities. For example, protective coatings with ultrahigh strength and toughness can be fabricated by emulating the structure of nacre, a natural NCF

with an extremely high loading (>90 vol%) of stiff nanoplatelets.^{1,2} Perovskite solar cells incorporated with a polymer scaffold supporting high concentrations of perovskite crystals show a high energy conversion efficiency, excellent resistance to humidity and self-healing functionalities.³ Separation membranes based on high concentrations of nanoparticles show enhanced permeability and selectivity, overcoming the traditional trade-off between the two separation properties.⁴ In addition, thermal energy storage device exhibits increasing thermal conductivity with nanoparticle loading.⁵ Despite the useful properties and functionalities that can be derived from high concentrations of NPs in NCFs, methods to produce such NCFs require multiple steps and thus tend to be energy-intensive and time-consuming. Solution- or melt-based processes, for example, are challenging to implement for mixtures with high concentrations of NPs because of high viscosity and elasticity, as well as the NPs' tendency to aggregate during processing.^{6,7}

A new class of NCFs that circumvent many of the challenges associated with fabricating highly filled NCFs is polymer-infiltrated nanoparticle films (PINFs). By infiltrating polymers into densely packed NP films, it is possible to create NCFs with extremely high concentrations of NPs.^{8–11} In previous work, we developed a thermally-induced, capillarity-based

^a Department of Chemical and Biomolecular Engineering, University of Pennsylvania, Philadelphia, Pennsylvania 19104, USA. E-mail: daeyeon@seas.upenn.edu

^b Department of Chemistry, University of Pennsylvania, Philadelphia, Pennsylvania 19104, USA. E-mail: fakhraai@sas.upenn.edu

† Electronic supplementary information (ESI) available: Amplitude (Ψ) and phase change (Δ) data and model fit from *in situ* spectroscopic ellipsometry; thickness changes of NPs, composites, and polymer layers during CaRI; linear dependence of h^2 versus t for PS-21k/SiO₂ NP and P2VP/SiO₂ NP annealed at 423 K; sensitivity analysis on the viscosity calculation of the PS-8k/SiO₂ NP based on polymer melt surface tension models and contact angle values; determination of bulk polymer viscosity values from the literature; determination of confined and bulk polymer glass transition temperature (T_g) using spectroscopic ellipsometry; atomic force microscopy (AFM) topography and phase images of the PS-8k/SiO₂ NP bilayer film surface before and after CaRI; glass transition temperature (T_g) measured using spectroscopic ellipsometry and differential scanning calorimetry. See DOI: 10.1039/c7sm02465g

approach – capillary rise infiltration (CaRI), to achieve PINFs with > 50 vol% NP loading.^{8,9} This technique involves first generating a bilayer film of NPs and a polymer, followed by thermally annealing the bilayer above the glass transition temperature (T_g) of the polymer to induce polymer wicking into the voids of the dense NP packing *via* capillarity. PINFs prepared *via* CaRI have very high modulus and hardness as well as scratch and wear resistance owing to their high filler fractions.⁸ We have demonstrated that the CaRI process is robust across systems with different polymer–NP interactions as well as polymer molecular weights and morphologies.^{8,9}

In addition to being a powerful and potentially scalable method of producing PINFs, CaRI provides a unique platform to study the viscosity and glass transition of polymers under extreme nanoconfinement. Despite general acceptance that physical confinement leads to a significant deviation of the polymer behavior from its bulk,^{12,13} a wide range of confinement-induced changes have been reported in the literature, depending on the extent and geometry of confinement, and the polymer–nanoparticle interactions. For instance, some reports have shown that non-attractive nanoparticles significantly slow down the diffusion of polymers in polymer nanocomposites.^{14–17} In contrast, other studies based on molecular dynamics simulations have reported enhanced chain motion under repulsive polymer–nanoparticle interactions.¹⁸ One of the key challenges in deciphering the effect of confinement is that effects of confinement and interfacial effects are often convoluted and thus are difficult to decouple, especially in thin film geometries where free surface effects may play a significant role in glass transition, such that it may mask substrate effects.^{19–24}

In the CaRI system, the characteristic pore size of random close packings of spheres is approximately 20–30% of the NP size.²⁵ It is thus straightforward to confine polymers in extremely small pores (< 10 nm) by using disordered packings of NPs. Polymer chains infiltrating the dense NP packings are very close to the NP surface and could be in contact with multiple nanoparticles, with a negligible effect of the free polymer surface.^{26–28} By analyzing the wicking process of a polymer into a NP packing based on the Lucas–Washburn model, we recently estimated several orders of magnitude increase in the melt viscosity of the unentangled polymer.⁸ This increased viscosity relative to the bulk value suggests that confinement significantly affects the polymer infiltration dynamics in the tight pore network of the NP packing. Therefore, the CaRI of the polymer into NP packing enables us to systematically explore the effect of polymer–NP interactions under extreme nanoconfinement by varying the type of polymer used in CaRI.^{16,17}

In this work, we study the effect of polymer–NP interactions on the viscosity of unentangled polymers in CaRI. We focus our analyses on unentangled polymer chains to exclude the potential contribution of polymer chain (dis)entanglement, which has been attributed to the enhanced mobility of confined polymer chains of high molecular weights.^{29,30} We monitor the infiltration process of unentangled poly(styrene) (PS) and poly(2-vinylpyridine) (P2VP) into densely packed silica NP packings. The P2VP–SiO₂ NP and PS–SiO₂ NP pairs represent strongly and

weakly interacting systems, respectively; the nitrogen atom in P2VP interacts strongly with the hydroxyl groups on the SiO₂ NP surface *via* hydrogen bonding,^{31,32} whereas PS interacts with the SiO₂ NP *via* van der Waals forces. We choose two unentangled polymer molecular weights for each polymer to vary the extent of confinement. This approach enables us to decouple the confinement and interaction effects on the polymer CaRI dynamics. We show that during CaRI, the polymers exhibit higher-than-bulk viscosity, regardless of polymer–NP interactions. We also show that the glass transition temperature (T_g) of these polymers increases significantly in the NP packings, again regardless of polymer–NP interactions. We find that in both systems, the increase in the viscosity is strongly correlated with the increased T_g , and the ratio of viscosity to bulk viscosity does not show a strong dependence on the temperature. These observations suggest that confinement has a more significant impact on the CaRI dynamics than on the extent of polymer–NP interactions.

Experimental

Materials

Poly(styrene) (PS) (PS-8k, M_n = 8000 g mol^{−1}, PDI = 1.10; PS-21k, M_n = 21 000 g mol^{−1}, PDI = 1.04) and poly(2-vinylpyridine) (P2VP) (P2VP-8k, M_n = 7800 g mol^{−1}, PDI = 1.08; P2VP-22k, M_n = 22 000 g mol^{−1}, PDI = 1.06) were purchased from Polymer Source Inc. The silica NP suspension (Ludox TM-50, 25.0 ± 3.5 nm in diameter) was purchased from Sigma Aldrich.

Preparation and characterization of bilayers

Silicon wafers are cut into approximately 1 cm × 1 cm squares. The wafers are rinsed with acetone, isopropanol, and water, and then dried with nitrogen. The wafers are then further cleaned by oxygen plasma treatment for approximately 5 minutes. 5 wt% PS-8k and 6 wt% PS-21k solutions are prepared by dissolving PS in toluene. 8 wt% P2VP-8k and 8 wt% P2VP-22k are prepared by dissolving P2VP in 1-butanol. SiO₂ NP suspension is prepared by diluting the as-purchased suspension in DI water to 10 wt%, and the pH of the suspension is adjusted to ~11 using 1 M potassium hydroxide (KOH) solution. All solutions are bath-sonicated for at least an hour and filtered prior to use. To generate the bilayer films, the polymer layer is first spin-coated onto the silicon substrate using a WS-400BZ-6NPP/Lite spin-coater from Laurell Technologies Corporation. The polymer film is annealed at 393 K under vacuum conditions for 12 h to remove the residual solvent. Then, the polymer film is oxygen plasma-treated for ~2 s to render the film surface hydrophilic, on which the SiO₂ NP layer is spin-coated. This short plasma treatment facilitates the deposition of uniform nanoparticle layers atop polymer films. Our control experiments show that it is possible to create bilayers without plasma treatment by using isopropanol suspensions of silica nanoparticles and that there is little difference in the properties of CaRI composite films made using the two methods. Details will be reported elsewhere. The thickness of the polymer and NP layer is ~200 nm to ensure that there is a sufficient amount of polymer to fill the interstices of

the NP packing, which has an average porosity of ~ 0.35 . To generate a polymer film of ~ 200 nm, 5 wt% PS-8k and 6 wt% PS-21k solutions are spin-coated at 2000 rpm and 5000 rpm, respectively, whereas 8 wt% P2VP-8k and 8 wt% P2VP-22k are spin-coated at 4000 rpm and 5000 rpm, respectively. The 10 wt% SiO₂ NP suspension is spin-coated at 3000 rpm. The bilayer samples are subjected to vacuum for 12 h to remove residual solvents. The vacuum treatment, however, does not significantly change the CaRI behaviour likely indicating that the influence of residual solvent on polymer infiltration dynamics is negligible. Scanning electron microscopy (SEM) images of the bilayer films before and after the polymer infiltration process are taken using a JEOL 7500F HRSEM. Each sample is sputtered with a thin gold/palladium layer using a Cressington Sputter Coater 107 prior to imaging to prevent charging. The samples are imaged at an accelerating voltage of 5 kV, an emission current of 20 μ A, and at a working distance of approximately 8 mm.

Characterization of the polymer infiltration process

The polymer infiltration process into the voids of the NP packing is monitored *in situ* using a J.A. Woollam Alpha-SE spectroscopic ellipsometer while the bilayer film sample is annealed above the glass transition temperature (T_g) of the polymer using a Linkam THMS350V heating stage, under constant pressure (ambient conditions). The heating stage has a temperature resolution of ~ 1 K. The stage on which the sample is placed is 22 mm in diameter and is open to ambient air. The Linksys software displays the stage temperature and allows the user to input the desired set-point temperature, heating rate, and hold time for the set-point temperature. The ellipsometry data are collected between $\lambda = 380$ nm and 900 nm at an incident angle of 70° , and is analyzed using the CompleteEASE software package provided by J.A. Woollam. The ψ (Ψ) and δ (Δ) data are fitted using a three-layer (nanoparticle/composite/polymer) Cauchy model on a Si substrate with a native oxide layer.^{8,9} The Cauchy model is expressed as: $n(\lambda) = A + B/\lambda^2 + C/\lambda^4$; $k(\lambda) = 0$, where A , B and C are optical constants, λ is the wavelength, n and k are the real and imaginary components of the index of refraction. The model fitting interprets the raw data into physical parameters describing each layer in the sample, namely the thickness and the refractive index.³³

Glass transition temperature measurements

The glass transition temperatures (T_g) of bulk polymer samples are determined using the TA Instruments Q2000 differential scanning calorimetry (DSC). PS samples are measured in a hermetically sealed pan, whereas P2VP samples are measured in a non-hermetically sealed pan. Each polymer sample (~ 6 mg) is initially cooled to 293 K, before subjecting it to two heating and cooling cycles in the range of 293–423 K at 10 K min^{-1} . T_g is defined as the midpoint of the step transition of the heat flow/capacity and expressed as the average from the two cooling cycle measurements. The T_g values measured using DSC are in good agreement with those reported previously.^{34,35} The T_g values of the confined polymers in the CaRI nanocomposite films are measured using a J.A. Woollam M-2000V

spectroscopic ellipsometer. The PINF is mounted onto a Linkam THMS 600 temperature-controlled stage attached to the ellipsometer. The *in situ* ellipsometry sampling rate is 1 s with high accuracy zone-averaging. Three heating and cooling cycles between 303 K and 423 K under dry nitrogen flow are performed for each sample, with a heating rate of 30 K min^{-1} and a cooling rate of 10 K min^{-1} , respectively. The T_g data are reported upon cooling. The thickness and refractive index of the sample are determined by fitting the cooling ramp raw data to the Cauchy model, as described earlier. T_g of the residual polymer layer and confined polymer for each film is determined *via* the intersection of the linear fits to the supercooled and glassy regimes in the plots of nanocomposite and polymer layer refractive indices *versus* temperature (see ESI,† Fig. S6). The thickness of the composite layer is held constant for the dynamic data fits.

Results and discussion

Polymer infiltration dynamics

To study polymer capillary rise infiltration (CaRI) under confinement, we generate a bilayer composed of a dense disordered packing of 25 nm SiO₂ nanoparticles (NPs) atop a polymer layer. We use poly(styrene) (PS) and poly(2-vinylpyridine) (P2VP) as the weakly and strongly interacting polymers. P2VP is known to interact with SiO₂ NP *via* hydrogen bonding interactions, whereas PS interacts with SiO₂ NPs primarily through van der Waals interactions. We also use PS and P2VP with two different molecular weights: ~ 8000 (8k) and $\sim 21\,000$ (21k) g mol^{-1} . The radii of gyration of 8k and 21k PS and P2VP, calculated based on the Kuhn segment length of each polymer,³⁶ are approximately ~ 2.5 nm and ~ 4 nm, respectively, which are comparable to or slightly larger than the characteristic pore radius of the SiO₂ NP packing (~ 3.5 nm). The bilayer film is annealed above the glass transition temperature (T_g) of the polymer to induce the infiltration of the polymer into the interstices of the NP packing. The changes that take place in the film during the CaRI process are schematically illustrated in Fig. 1.

We perform *in situ* spectroscopic ellipsometry to monitor polymer infiltration into the disordered SiO₂ NP packing. The infiltration of polymers in CaRI has been shown to follow the Lucas–Washburn model, which has been successfully used in prior experimental and computational studies to describe polymer wicking under confinement:^{8,29,37–41}

$$h^2 = \frac{\sigma R \cos \theta}{4\tau^2 \mu} t \quad (1)$$

where h is the height of the NP packing infiltrated by the polymer, σ is the surface tension of the polymer melt, R is the mean pore radius in the NP packing, θ is the contact angle of the polymer melt on the NP surface, τ is the tortuosity of the disordered NP packing, μ is the viscosity of the polymer melt, and t is the annealing time.^{8,39} A three-layer Cauchy model that accounts for the topmost neat SiO₂ NP layer, the middle composite layer, and the bottommost polymer layer, enables us

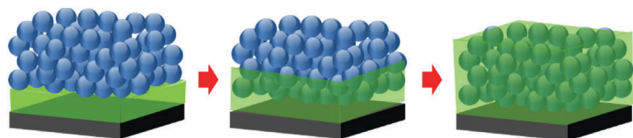


Fig. 1 Schematic illustration of the capillary rise infiltration (CaRI) process of a polymer into voids of a densely packed nanoparticle film. Upon the initiation of the infiltration, the bilayer becomes a three-layer system composed of pure polymer, infiltrated nanoparticles (*i.e.*, composite), and unfilled nanoparticle layers. Upon the completion of CaRI, the system has two layers: the composite (*i.e.*, the nanoparticle layer is completely filled with the polymer) and the pure polymer layers.

to translate the amplitude (Ψ) and phase change (Δ) data from spectroscopic ellipsometry to the index of the refraction of each layer, in order to follow the structural evolution of the bilayer (see the ESI,[†] Fig. S1). To reduce the degrees of freedom and ensure solution uniqueness, we determine and set the refractive indices of the neat SiO_2 NP layer and the neat polymer layer from respective single-component film measurements at ~ 383 K to account for thermal expansion of the polymer layer and the removal of condensed water from the neat SiO_2 NP packing.

Fig. 2(a) shows the thickness profile changes of the neat SiO_2 NP layer, the composite layer, and the polymer layer with annealing time for the PS8k/ SiO_2 NP film at 403 K. During CaRI, the polymer wicking into the SiO_2 NP causes a decrease in both the NP and polymer layer thicknesses, while the thickness of the composite layer – the portion of SiO_2 NP layer which has been filled with polymer – increases. This is also evident in Fig. 2(b–e) which shows the polymer filling of the interstices of the SiO_2 NP packing and the decrease in polymer layer thickness after CaRI. The presence of the polymer in the interstices of the NP packing following CaRI is also evident from the atomic force microscopy (AFM) topography and phase images (see ESI,[†] Fig. S7). The interparticle distance between nanoparticles before (25.7 ± 2.9 nm) and after (26.1 ± 2.7 nm) CaRI, estimated from Fig. 2(b and d), shows a negligible change, strongly indicating that the packing density of the nanoparticle layer does not change upon CaRI. Albeit having different infiltration rates, we observe that all polymers follow a similar infiltration behaviour (see the ESI,[†] Fig. S2 and S3). At early times, the formation of the meniscus before the capillary rise and higher initial resistance causes the movement of the polymer melt to be in an unsteady state.⁴² Gradually, the infiltration stabilizes and approaches a steady state, where the slope of the composite growth remains uniform over the course of infiltration. We consider the steady state infiltration process in our analyses to infer the viscosity of the polymer melt based on eqn (1).

From the thickness profiles, we plot the composite layer thickness squared (h_{comp}^2) as a function of time (t) to confirm the Lucas–Washburn model. Fig. 3(a) shows the linear dependencies of h_{comp}^2 versus t for the PS-8k and P2VP-8k systems, consistent with the Lucas–Washburn model. We anneal each polymer–NP system in a range of temperature. For each run,

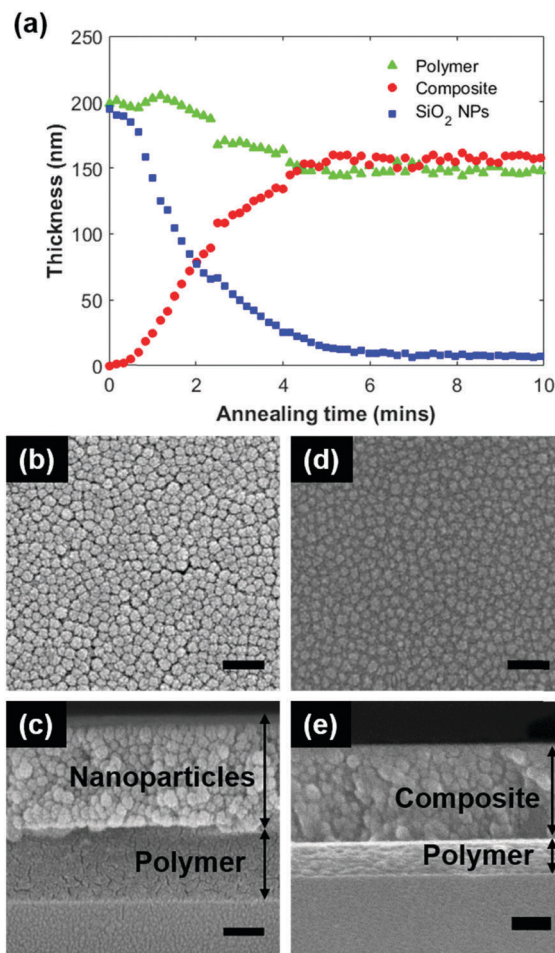


Fig. 2 (a) Thickness profiles of the SiO_2 NP, composite, and neat polymer layers as a function of annealing time, obtained using *in situ* spectroscopic ellipsometry while annealing ~ 200 nm SiO_2 NP/ ~ 200 nm PS-8k bilayer films at 403 K. The SEM images show the (b) top and (c) cross sectional views of the bilayer film before annealing, and the (d) top and (e) cross sectional views of the PINF atop a residual polymer layer after annealing. The scale bars are 100 nm.

we verify the validity of the Lucas–Washburn model as in Fig. 3(a), then extract the slope from each h_{comp}^2 versus t plot, which represents the prefactor in the Lucas–Washburn model $\sigma R \cos \theta / 4\tau^2 \mu$. For each polymer system, the value of the slope, as shown in Fig. 3(b), increases with temperature, indicating a more rapid infiltration process. This observation is consistent with the decreasing polymer melt viscosity as the temperature is increased.

Based on each slope, we infer the viscosity μ of the confined polymer by estimating the remaining parameters in the Lucas–Washburn prefactor, $\sigma R \cos \theta / 4\tau^2 \mu$, from literature values.^{42–44} Table 1 summarizes the parameters that are used to determine the viscosity μ . The pore radius R and tortuosity τ values are intrinsic to the SiO_2 NP packing and are estimated based on the size of the NP and the porosity of the packing.^{25,45} The surface tension of PS and P2VP are estimated based on the molecular weight and the temperature of the melt.^{46,47} There are varying reports of PS contact angles on silicon oxide surfaces ranging

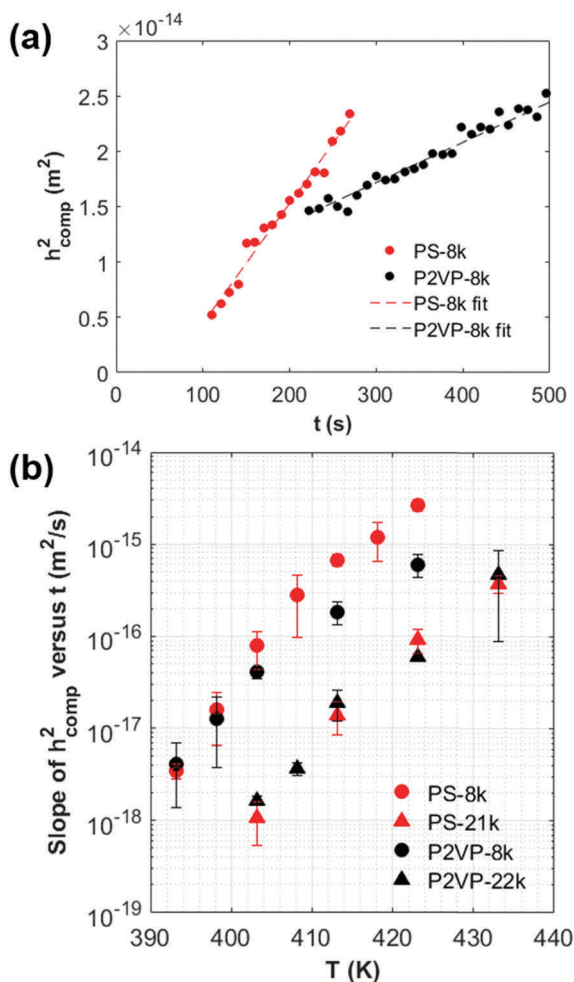


Fig. 3 (a) The composite layer thickness squared, h_{comp}^2 of PS-8k and P2VP-8k composite versus annealing time, t , when the bilayer films are annealed at 403 K, shows a linear fit and agrees well with the Lucas–Washburn model. (b) The slope of h_{comp}^2 versus t as a function of annealing temperature, T for PS-8k, P2VP-8k, PS-21k, and P2VP-22k.

from 7° – 23° ,^{29,48} we choose $\theta = 20^\circ$ for this purpose, but the temperature-dependence of viscosity is independent of this choice. P2VP is reported to form a strongly bound layer on the SiO₂ NP surface due to favourable hydrogen bonding,^{31,49–51} thus we estimate $\theta \sim 0^\circ$ in the case of P2VP. We perform a sensitivity analysis by testing a range of contact angle values θ and considering other empirical relations in calculating the polymer surface tension, $\sigma(T)$ (see the ESI,† Fig. S4). This analysis confirms that the magnitude of the estimated viscosity of the confined polymer is robust across a range of estimated θ

and $\sigma(T)$ parameters. To assess the effect of confinement and polymer–NP interactions, we compare the measured confined polymer viscosity with bulk values which are obtained from literature values.^{52,53}

Role of confinement and polymer–NP interactions

To assess the role of confinement and polymer–NP interactions, we compare the confined and bulk polymer viscosity as a function of temperature, as shown in Fig. 4. For both polymers, we note a significant increase in the viscosity of the confined polymer relative to the bulk values reported in the literature,^{52,53} regardless of the polymer–NP interaction strength. The two graphs show remarkable similarities in the absolute values of viscosities for the confined PS and P2VP, and the extents of viscosity increases are also very similar.

The relative increase in the viscosity due to confinement ($\mu_{\text{confined}}/\mu_{\text{bulk}}$) also does not strongly depend on temperature, as shown in Fig. 5. This is the opposite of what one would expect if the polymer–NP interactions significantly slowed the chain motion. In particular, the strength of hydrogen bonding is known to be strongly temperature dependent;⁵⁴ thus one may have expected a strong temperature dependence of the normalized viscosity in the case of P2VP, which we do not observe. Furthermore, for a given polymer, there is no significant difference in $\mu_{\text{confined}}/\mu_{\text{bulk}}$ for the two molecular weights (Fig. 5). These observations imply that the increase in viscosity is not strongly influenced by the polymer–NP interactions.

The significant increase in the polymer viscosity is reminiscent of an abrupt increase reported for the viscosity of simple liquids such as siloxane confined in a very narrow slit, although the phenomenon was attributed to a liquid-to-solid-like (*i.e.*, first-order-like) transition in packing of the molecule.⁵⁵ More relevant to our observation is the slowdown of chain diffusion observed in polymer nanocomposites, which was attributed to entropic barriers that are associated with chains passing through small constrictions between NPs. These studies showed that stronger interactions between NPs and polymers do not necessarily lead to more significant reduction in diffusivity,^{17,54} consistent with our observations. Other measures of polymer dynamics have also described slowing down of chain relaxation^{14,56} and diffusion^{16,57} near strongly and weakly interacting solid surfaces. Another mechanism that could lead to the observed slowdown is the tortuous path and the high curvature in the NP packings which can increase the interchain packing proximity.⁵⁸ Such a change could in turn significantly strengthen polymer–NP interactions even in the case of the weak polymer–NP interacting system and lead to increased viscosity.

Table 1 Parameters used for estimation of viscosity using the Lucas–Washburn model^{25,29,31,45–49,51}

Polymer/nanoparticle	Average pore radius, R (nm)	Tortuosity, τ	Surface tension as function of temperature, $\sigma(T [^\circ\text{C}])$ (mN m ^{−1})	Polymer contact angle on SiO ₂ NP, θ
PS-8k/SiO ₂ NP	3.5	1.95	$40.5 - 0.068T$	20°
PS-21k/SiO ₂ NP	3.5	1.95	$42.1 - 0.068T$	20°
P2VP-8k/SiO ₂ NP	3.5	1.95	$46.7 - 0.063T$	0°
P2VP-22k/SiO ₂ NP	3.5	1.95	$46.7 - 0.063T$	0°

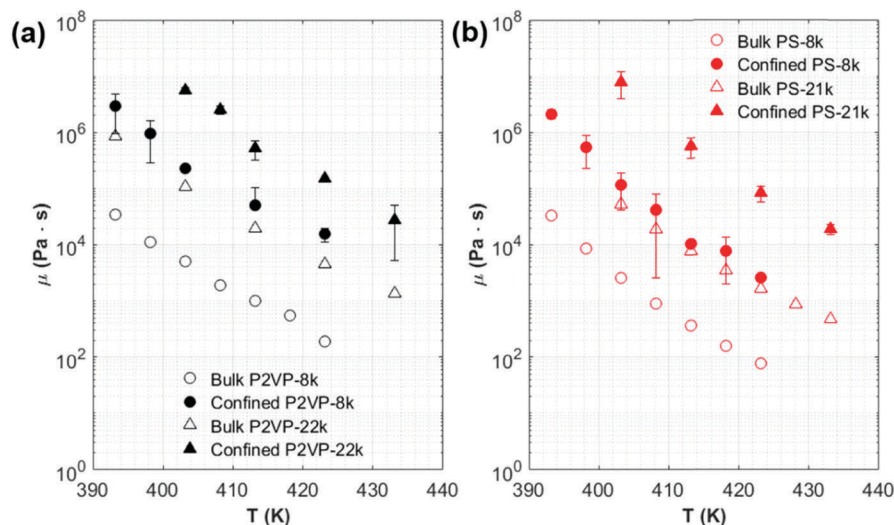


Fig. 4 Bulk and confined polymer viscosity of (a) P2VP-8k and P2VP-22k, and (b) PS-8k and PS-21k as a function of temperature. Each data point for the confined polymer viscosities is an average of at least 2 runs, and the error bar represents 1 standard deviation. The bulk viscosity values are obtained from the literature (see the ESI†).

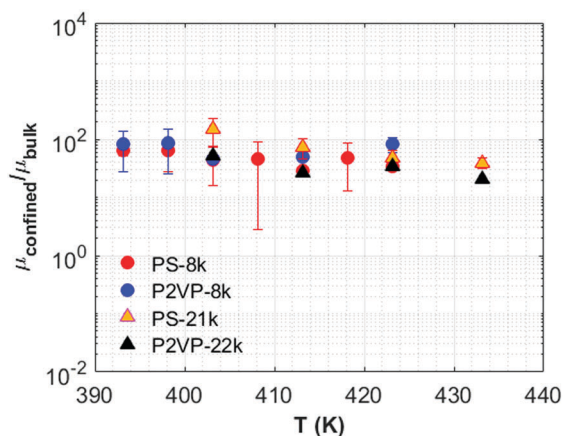


Fig. 5 The confined polymer viscosity normalized by the bulk viscosity ($\mu_{\text{confined}}/\mu_{\text{bulk}}$) for all polymer systems, as a function of temperature.

Interestingly, reports on the viscosity of polymers in thin films provide some conflicting trends. The viscosity of polymers in thin films decrease for a weakly interacting polymer-substrate system, which has been attributed to the enhanced free surface dynamics.⁵⁸ The polymer viscosity in thin films has been reported to increase for a strongly interacting polymer-substrate system above a threshold temperature.⁵⁹ Increases in the viscosity of unentangled polymers during CaRI in dense nanoparticle packings (Fig. 4 and 5) are in stark contrast to the enhanced mobility observed in the capillary rise of highly entangled polymers in cylindrical pores of anodized aluminium oxide (AAO) membranes.²⁹ We attribute this discrepancy to the difference in confinement geometry and disentanglement effects. When infiltrating a dense nanoparticle packing, polymer chains transport through tortuous pathways with variable pore sizes (narrow necks and wide gaps), instead of straight, uniform, cylindrical nanochannels in AAO membranes. The narrow regions

may act as entropic barriers, where polymer chains have to sample multiple conformations to squeeze through the narrow pores for infiltration to occur. The enhanced mobility of high molecular weight polymers under confinement was attributed to a disentanglement effect,^{29,30} whereby increased confinement leads to decreased entanglement density. In our case, we do not expect such a phenomenon to play a role as both molecular weights studied here are below the entanglement limit.

Monitoring the infiltration dynamics in CaRI provides insights into the effects of confinement on translational (*i.e.*, centre-of-mass) mobility of the polymers, whereas the determination of glass transition temperature of the polymers provides indirect information regarding their segmental relaxation under extreme confinement, as T_g is typically attributed to the arresting of segmental modes of motion in bulk polymers.^{60–62} We determine the T_g values of the fully annealed films, consisting of a composite layer atop a residual polymer layer, *via* spectroscopic ellipsometry, which is a well-established method for the accurate determination of T_g values of polymers under confined geometries.^{22,23,63–66} We use a 2-layer composite/polymer model to fit the spectroscopic ellipsometry data (see the ESI† Fig. S6). We also measure the T_g values of the bulk polymer samples independently *via* differential scanning calorimetry (DSC) to validate our spectroscopic ellipsometry T_g measurements (see the ESI† Table T1).

Fig. 6 shows the confined and bulk T_g values for each polymer-NP system. In all systems, we observe increased T_g in the confined systems relative to the bulk, which is highly correlated with the increased viscosity we observe, even in the case of the weakly interacting system (PS-SiO₂). Previous studies have shown that while strong interfacial interactions between SiO₂ and P2VP do not necessarily lead to increased T_g in nanocomposites, confinement has shown to increase T_g .^{22,67} Although most studies involving PS films on SiO₂ show decrease in T_g due to the free surface effect,^{63,65} one study

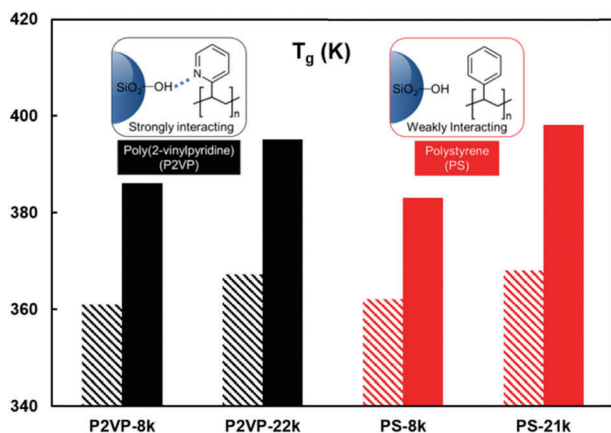


Fig. 6 The glass transition temperature T_g of P2VP (black) and PS (red) in the bulk (striped bar) and the confined state (filled bar).

has shown that the T_g value of PS confined in AAO membranes with 55 nm pores, in the absence of free surface, increases, consistent with our results.⁵⁸

Surprisingly, in our current study, the increase in T_g for the two polymers of similar molecular weights are approximately the same. Also, a similar increase in ΔT_g values is observed for the two polymers when the molecular weight of the polymers is increased. These observations point to the fact that physical confinement has a stronger impact on the glass transition of polymers than polymer-NP interactions under these extreme nanoconfinement conditions. This is in contrast to measurements in thin films where free surface (polymer-air interface) effects always dominate, resulting in a decrease in average T_g for PS as opposed to increased T_g in P2VP.^{22,23} Overall, observed increases in T_g values are consistent with the increased viscosity for PS and P2VP, suggesting that the increased viscosity in CaRI under extreme nanoconfinement is likely correlated with the impact of confinement on segmental motion of the chains as deduced from their T_g values.

Conclusions

In this work, we perform capillary rise infiltration (CaRI) of unentangled polymers into a disordered, dense nanoparticle packing of SiO_2 to study the viscosity and glass transition of the polymers with different polymer-nanoparticle interactions under extreme nanoconfinement, where the polymer chain size is comparable or smaller than the average pore size. Using the Lucas-Washburn model, we measure the viscosity of the polymer during infiltration in disordered nanoparticle packings, and observe increased viscosity of unentangled polymers under such extreme nanoconfinement conditions relative to their respective bulk values, significantly different from the results obtained based on highly entangled polymers undergoing capillary rise in well-defined cylindrical pores. Surprisingly and somewhat unexpectedly, the extent of the viscosity increase is not strongly dependent upon the polymer-NP interactions. We also observe a comparable increase in T_g for both the

strongly and the weakly interacting polymer-NP systems, which is different from prior studies on T_g changes observed in supported polymer thin films.

Overall, our results demonstrate that confinement, rather than polymer-NP interactions, has a more significant impact on the viscosity and glass transition of polymers in CaRI systems. The increases in T_g are strongly correlated with the viscosity changes observed for the two polymers, suggesting that extreme nanoconfinement affects the transport phenomena of polymers by influencing the segmental motion. Our results provide fundamental frameworks for the optimization of process parameters such as temperature and annealing time to enable scalable manufacturing of polymer-infiltrated NP films using CaRI.

There are several outstanding questions that warrant future investigation. Our ongoing work, for instance, focuses on the infiltration dynamics of highly entangled polymers to test the validity of the Lucas-Washburn model. The effect of molecular weight and polymer-nanoparticle interactions of polymers on the mechanical properties of CaRI composites is potentially of significant importance as high molecular weight polymers can lead to bridging of multiple NPs and in turn a significant enhancement of the toughness of the composite.

Conflicts of interest

There are no conflicts to declare.

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