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Investigation into defect chemistry and relaxation processes in niobium doped and undoped $\text{SrBi}_4\text{Ti}_4\text{O}_{15}$ using impedance spectroscopy†

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The aurivillius family of compounds $\text{SrBi}_4\text{Ti}_4\text{O}_{15}$ (SBTi) and $\text{SrBi}_4\text{Ti}_{3.8}\text{Nb}_{0.2}\text{O}_{15}$ has been prepared using solid state reaction techniques. The niobium doping enhances the value of the dielectric constant, but decreases the phase transition temperature and grain size of SBTi. Grain conductivity evaluated from the impedance data reveals that Nb doping increases the resistance of grains which indicates the decrease in oxygen vacancies. The negative temperature coefficient of resistance shown by the grain boundary conductivity is explained using the Heywang–Jonker model. The variation of ac conductivity with frequency is found to obey Jonscher's universal power law. The frequency exponent (n), pre-exponential factor (A), and bulk dc conductivity (σ_{dc}) are determined from the fitting curves of Jonscher's universal power law. From the frequency exponent (n) versus temperature curve, we conclude that the conduction mechanism of SBTi changes from large-polaron tunneling (300–475 °C) to small-polaron tunneling (475–550 °C), and in that of the niobium doped it is small-polaron tunneling (300–375 °C) to correlated band hopping (375–550 °C). Activation energies have been calculated from different functions such as loss tangent, relaxation time, grain and grain boundary conductivities, and ac and dc conductivity. The activation energies reveal that conductivity in the sample has contributions from migrations of oxygen vacancies, bismuth ion vacancies, electrons ionized from strontium vacancies, strontium ion vacancies and valence fluctuations of $\text{Ti}^{4+}/\text{Ti}^{3+}$ ions.

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1 Introduction

Ferroelectric and piezoelectric ceramics are a special class of materials which have been widely used in actuators, sensors, transducers and other electromechanical devices. Among these, lead zirconate titanate (PZT) based materials have been utilized for device fabrication because of their outstanding ferroelectric and piezoelectric properties. However, the highly toxic lead and its oxide pose serious problems to the environment as well as human health. Due to this fact, the need for lead-free materials which can effectively replace the lead based industry is a serious issue and research challenge. Bismuth layered oxides have been one of the most extensively investigated materials for lead free ferroelectric and piezoelectric applications.

$\text{SrBi}_4\text{Ti}_4\text{O}_{15}$ (SBTi) is a bismuth layer structured ferroelectrics (BLSF) which belongs to the Aurivillius family of compounds. The general formula of the compound is $(\text{Bi}_2\text{O}_2)^{2+}(\text{A}_{m-1}\text{B}_m\text{O}_{3m+1})^{2-}$, where A can be a monovalent, divalent or trivalent metal ion and

B can be a tetravalent, pentavalent or hexavalent metal ion. The m value indicates the number of perovskite layers interleaved with $(\text{Bi}_2\text{O}_2)^{2+}$ layers. The SBTi shows unique properties such as a high Curie temperature (525 °C), high dielectric breakdown strength, fatigue-free nature, low dielectric loss and high anisotropy.¹ These properties make this material a potential candidate for nonvolatile ferroelectric random access memory (NvFRAM) and piezoelectric applications. However, its low remanent polarization, high coercive field, and high processing temperature hinders this material from commercialization.

One of the simplest methods to change the electronic properties of a material without altering the crystal structure is doping. Researchers have extensively investigated the effects of doping in the various sites of SBTi. The loss of Bi_2O_3 during sintering is one of the causes of defects in SBTi. To reduce the bismuth evaporation, researchers have tried partial replacement of bismuth sites with other elements of the lanthanide series such as lanthanum,² praseodymium,³ and erbium.⁴ Reports have shown that this leads to decreases in remanent polarization and transition temperature and has increased the structural distortion and strain in SBTi. Considering the effect of doping in the perovskite layer, reports are available on the replacement of strontium sites with barium⁵ and calcium.⁶ The barium doping increased the dielectric constant and decreased the phase transition temperature. The ferroelectric and

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piezoelectric properties of barium doped SBTi have not been studied until now. It has been reported that the calcium doped SBTi shows an increase in transition temperature but a decrease in dielectric, ferroelectric and piezoelectric properties. When we consider the B-site modification with a same oxidation numbered element, a systematic study of electrical and structural properties has been extensively reported with zirconium⁷ doped SBTi. It has been observed that zirconium doping gently increases the dielectric and piezoelectric properties but decreases the ferroelectric properties. Towards the donor doping on titanium sites, a number of studies have been carried out with niobium,^{1,8,9} vanadium,¹⁰ cobalt,¹¹ tungsten,¹² and molybdenum⁸ doped SBTi. All of the dopants were found to increase the dielectric, ferroelectric and piezoelectric properties of SBTi but among them, a remarkable increase in electrical properties was observed for niobium doped SBTi. It has been reported that the niobium doped SBTi shows a two fold increase in the remanent polarization (2Pr) value compared to SBTi. However, the mechanisms leading to the increase in electrical properties of niobium doped SBTi has not been described in previous studies. In the present work, we investigate different relaxation processes and conduction mechanisms in SBTi and Nb doped SBTi in light of impedance and ac conductivity analyses. This analysis may be helpful for engineering SBTi for technological applications like NvFRAM and piezoelectric sensors.

2 Experimental

The niobium doped and undoped SBTi ceramic samples with the chemical composition of $\text{SrBi}_4\text{Ti}_{4-x}\text{Nb}_x\text{O}_{15}$ ($x = 0, 0.2$) were prepared using a solid state reaction method. Analytical grade metal oxides of Bi_2O_3 (Sigma-Aldrich, 99.9%), TiO_2 (Sigma-Aldrich, 99.0%), SrCO_3 (Sigma-Aldrich, 99.9%) and Nb_2O_5 (Sigma-Aldrich, 99.9%) were used as the starting precursors. The stoichiometric amount of the oxide mixture was weighed and thoroughly mixed in a planetary ball mill (Retsch PM-400, Germany). The powders were mixed in Teflon jars at 250 rpm for 24 h with zirconia balls in an ethanol medium. The slurry obtained after ball milling was dried at 60 °C in a hot air oven. The dried mixture was calcined in air for 3 h at 900 °C in a covered alumina crucible with heating and cooling rates of 10 °C min⁻¹. The powders were again ball milled in Teflon jars at 300 rpm for 72 h in an ethanol medium with a proportion of powder to zirconia balls of 1 : 10. The calcined powders were sieved through a 60 µm sieve and the sieved powders were pressed into circular pellets of 6 mm diameter and 1.5 mm thickness using a uniaxial press at 20 kPa for 30 s, followed by cold isostatic pressing at 200 MPa for 15 min. The pellets were placed in alumina crucibles which were fully surrounded by the powders of the same compositions (to avoid bismuth loss at high temperatures) and were sintered at 1100 °C for 2 h in an air atmosphere with heating and cooling rates of 10 °C min⁻¹. Structural and microstructural characterizations of the samples were carried out using X-ray diffraction (XRD) and scanning electron microscopy (SEM), respectively. The densities of the sintered samples were measured using the Archimedes method

using distilled water as the fluid, and the theoretical densities were calculated using the XRD profiles. Room temperature XRD analysis (Rigaku D/Max-B, CuKα radiation) was conducted on the sintered samples in the diffraction angle (2θ) range of 20–80° with a sampling step of 0.02°. The surface morphology or microstructure of the ceramics was observed on the polished and thermally etched sections using SEM (Hitachi S-4100). The relative densities of all of the sintered samples determined using the Archimedes method were 96–97%. The sintered pellets were polished to a thickness of nearly 1 mm and painted with silver paste on both sides to make electrodes. The dielectric and impedance measurements were carried out as a function of temperature and frequency using a Precision LCR Meter HP4284A, with an operating ac voltage of amplitude 1 V. The temperature and frequency ranges of the measurements were room temperature to 550 °C and 100 Hz to 1 MHz, respectively.

3 Results and discussion

3.1 Phase composition and microstructural analysis

Fig. 1 shows the XRD patterns of SBTi and Nb doped SBTi. All of the peaks were indexed based on orthorhombic cells associated with the $A21am$ space group, which is matched with the JCPDS file number 43-0973.⁷ No impurity peaks or additional peaks were observed in SBTi and Nb doped SBTi, which clearly indicates that the crystal structure was not affected by Nb doping. However, it could be observed from the XRD patterns of Nb doped SBTi that the strongest (119) peak has slightly shifted towards lower-angle, indicating an expansion in its lattice constant. The lattice expansion in the case of Nb-doped SBTi can be explained on the basis of the larger ionic radii of Nb^{5+} (0.64 Å) as compared to Ti^{4+} (0.605 Å).¹³ The lattice parameters were calculated within the error limit ± 0.002 Å from the Rietveld refinement (profile refinement, Le Bail method) of diffraction data using Jana 2006 software.¹⁴ Williamson–Hall relation (eqn (1)) was used for calculating the crystallite size and microstrain parameter.¹⁵

$$\beta \cos(\theta) = \frac{\psi\lambda}{l} + 4\eta \sin(\theta) \quad (1)$$

where β is the integral breadth of XRD peaks. This was calculated using Jana 2006 (only Lorentzian components). ψ is the Debye–Scherrer constant (0.94 for spherical crystallites), and λ and θ are the incident X-ray wavelength and the diffraction angle respectively. The values of crystallite size (l) and microstrain parameter (η) were calculated from the y-intercept and the slope of the $\beta \cos(\theta)$ versus $\sin(\theta)$ plot respectively, as shown in Fig. 2. The details of the reliability factors, lattice parameters, crystallite size and microstrain parameters are listed in Table 1. Fig. 3 shows the SEM images of SBTi and Nb doped SBTi. The surface morphology clearly indicates plate-like structures. The SEM images were analyzed using ImageJ software and grain size (G) and aspect ratios (AR) were calculated. Details are given in Table 1. It is clear from the table that the Nb doping decreases the average grain size and aspect ratio. The decreased grain size may increase the number of grains.



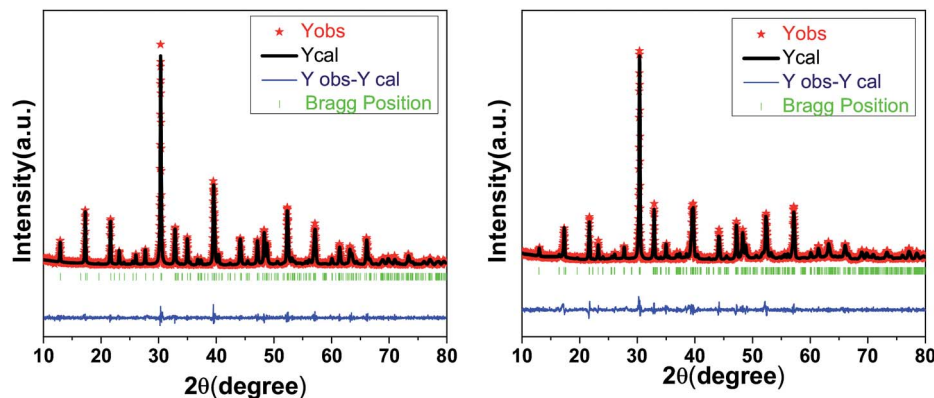


Fig. 1 XRD patterns of SBTi (left) and Nb doped SBTi (right).

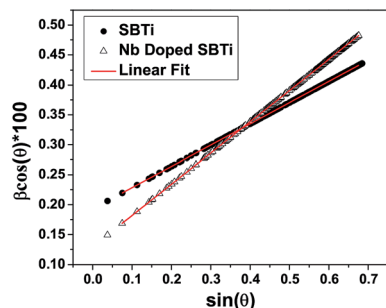


Fig. 2 Linear fit using the Williamson–Hall relation.

3.2 Dielectric studies

Fig. 4 shows the temperature *versus* dielectric constant and dielectric loss plot for SBTi and Nb doped SBTi at 1 MHz. From the plots, it is clear that Nb doping enhance the value of the dielectric constant but reduce the Curie temperature. The reduction of the Curie temperature is due to lattice distortion created by Nb doping. The lattice distortion can be calculated from the tolerance factor (F) defined by¹⁶

$$F = \frac{\Delta_u + \Delta_o}{\sqrt{2}(\Delta_v + \Delta_o)} \quad (2)$$

where Δ_u , Δ_v , and Δ_o are the radii of the A-cation and B-cation and the radius of the anion respectively. For the calculation we used¹³ $\Delta_u = 1.44 \text{ \AA}$ (Sr^{2+}), $\Delta_v = 0.60 \text{ \AA}$ (Ti^{4+}) or $\Delta_v = 0.64 \text{ \AA}$ (Nb^{5+}), and $\Delta_o = 1.40 \text{ \AA}$ (O^{2-}). The calculated values of F are given in Table 1. The tolerance factor was calculated by assuming SrTiO_3 to be undistorted (the effect of Bi_2O_3 layers has not been taken into account). However, the decreased value of the tolerance

factor in the Nb doped case indicated the increase of lattice distortion. The presence of Bi_2O_3 layers in the SBTi crystal structure has displaced Sr^{2+} cations, as well as tilted the TiO_6 octahedra (shown in Fig. 5). The tilting of TiO_6 octahedra is the reason for ferroelectric properties in SBTi.⁷ The doping at titanium sites can change the tilting of TiO_6 octahedra as well as the bond lengths between titanium and oxygen atoms. The Nb doping might be creating more stretching in bond lengths of TiO_6 octahedra that itself may be the reason for the increment of the dielectric constant in the Nb doped system. The replacement of less polarizable Ti^{4+} (electronegativity 1.54) with highly polarizable Nb^{5+} (electronegativity 1.6) may also be responsible for the increase in the dielectric constant of the Nb doped case. In the dielectric loss *versus* temperature plot (see Fig. 4), near the transition temperature a kink was observed for both SBTi and Nb doped SBTi. The kink indicates the movement of ferroelectric domain walls.¹² The Nb doping decrease the dielectric loss of SBTi, is also evident from the plot. The dielectric data was analysed using the Curie–Weiss law which can be described by the relation

$$\frac{1}{\epsilon'_r} = \frac{T - T_0}{\Phi} \quad (3)$$

where ϵ'_r is the real part of the relative permittivity or dielectric constant, T_0 is the Curie–Weiss temperature and Φ is the Curie constant. The plot between $\frac{1}{\epsilon'_r}$ and temperature gives a straight

line with a slope of $\frac{1}{\Phi}$ and the x-axis intercept at T_0 .¹⁷ Fig. 6 shows the Curie–Weiss plot of SBTi and Nb doped SBTi at 1 MHz. The solid red line is the linear fit (adjusted $R^2 > 0.999$) obtained for the Curie–Weiss law. The degree of diffuseness (Γ)

Table 1 The details of Rietveld refinements, Williamson–Hall plots, SEM images and the Curie–Weiss law. GOF: goodness of fit, R_{wp} : weighted profile R -factor, a , b , c : lattice parameters, Γ : crystallite size, η : microstrain, F : tolerance factor G : grain size, AR: aspect ratio, T_c : phase transition temperature, T_0 : Curie temperature, Φ : Curie constant, and Γ : degree of diffuseness

| Sample | GOF | R_{wp} | a (Å) | b (Å) | c (Å) | Γ (nm) | η | F | G (μm) | AR | T_c (°C) | T_0 (°C) | Φ | Γ |
|---------|------|----------|---------|---------|---------|---------------|-----------------------|------|----------|------|------------|------------|--------------------|----------|
| SBTi | 1.74 | 14.22 | 5.442 | 5.453 | 41.012 | 64 | 1.54×10^{-3} | 1.00 | 2.65 | 3.80 | 506 | 458 | 0.61×10^5 | 1.11 |
| Nb-SBTi | 2.04 | 17.06 | 5.444 | 5.454 | 41.059 | 43 | 2.27×10^{-3} | 0.98 | 1.34 | 3.27 | 448 | 405 | 0.93×10^5 | 1.13 |



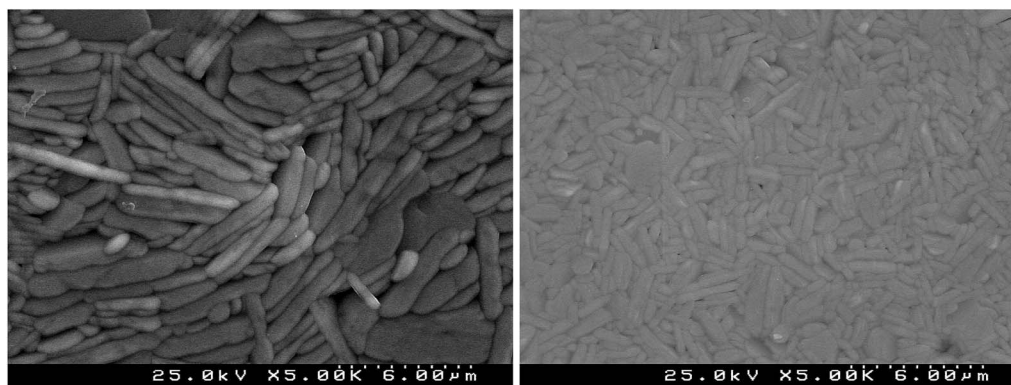


Fig. 3 SEM images of SBTi (left) and Nb doped SBTi (right).

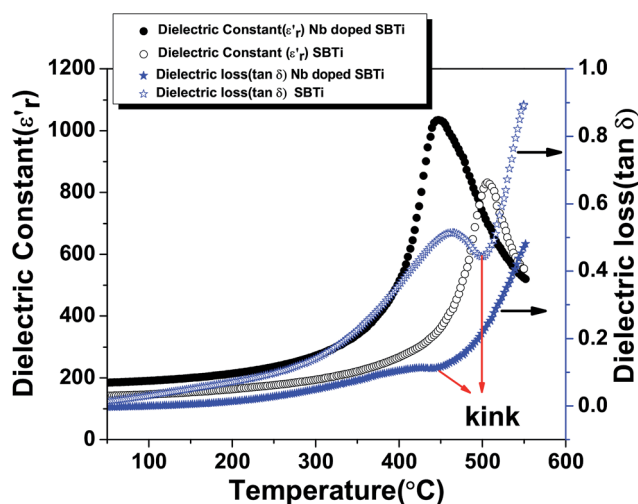


Fig. 4 Temperature dependence of the dielectric constant and dielectric loss at 1 MHz.

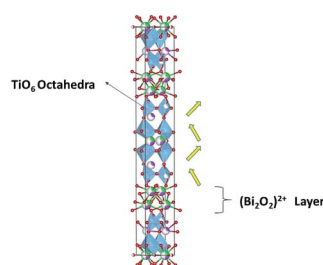


Fig. 5 Crystal structure of $\text{SrBi}_4\text{Ti}_4\text{O}_{15}$, with tilting of TiO_6 octahedra shown.

of the phase transition is obtained from the modified Curie–Weiss law given below,

$$\frac{1}{\epsilon'_r} - \frac{1}{\epsilon'_m} = \frac{(T - T_c)^r}{\Phi'} \quad (4)$$

where r is the degree of diffuseness, Φ' is the Curie-like constant, T_c is the phase transition temperature and ϵ'_m is the maximum value of the dielectric constant at phase transition

temperature T_c . The slope of the $\ln\left(\frac{1}{\epsilon'_r} - \frac{1}{\epsilon'_m}\right)$ versus $\ln(T - T_c)$

plot will give the degree of diffuseness r (Fig. 7).¹⁷ The value of (r) generally lies between 1 and 2. If it is close to one, it is indicative of normal phase transition and if close to two, then of diffused phase transition.¹⁷ All parameters related to the Curie–Weiss and modified Curie–Weiss laws are calculated and listed in Table 1. From the table, it is clear that the phase transitions are normal phase transitions.

3.3 Impedance analysis

By the analysis of impedance data one can easily separate the contributions from grains, grain boundaries and electrode effects from the different time constants associated with each function. Fig. 8 shows the Cole–Cole plots of SBTi and Nb doped SBTi. The plots are composed of two semicircular-arcs caused by the electrically different active regions, namely the grains and grain boundaries. The impedance spectra were fitted using an equivalent circuit consisting of two parallel RC elements connected in series. The fitting was performed using Z-view software. The equivalent circuit is shown in the inset of Fig. 8, where R_1 is the grain resistance, R_2 is the grain boundary resistance, CPE1 is the constant phase element for grains and CPE2 is the constant phase element for grain boundaries. The impedance of constant phase elements can be written as

$$Z = \frac{1}{[Q(j\omega)^v]} \quad (5)$$

where $j = \sqrt{-1}$, ω is the frequency and Q is a constant with dimensions of farad (second) ^{$v-1$} . The value of v represents the magnitude of deviation from the ideal capacitance. It varies from 0 to 1. For an ideal capacitor $v = 1$ and for an ideal resistor it is 0. The value of capacitance associated with grains and grain boundaries is obtained from the following formula

$$C = R\left(\frac{1-v}{v}\right)Q\left(\frac{1}{v}\right) \quad (6)$$

The values of R (R_1 and R_2), Q (for CPE1 and CPE2) and v (for CPE1 and CPE2) were obtained from fitting with the equivalent circuit. The obtained parameters from the fitting data were used



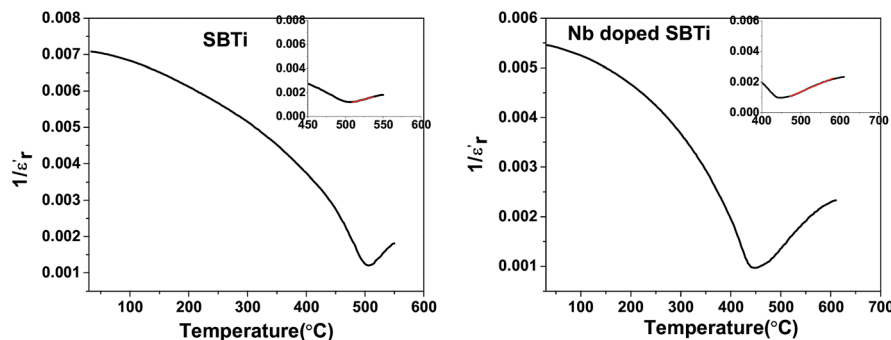


Fig. 6 Curie–Weiss plots at 1 MHz, SBTi (left) and NbSBTi (right).

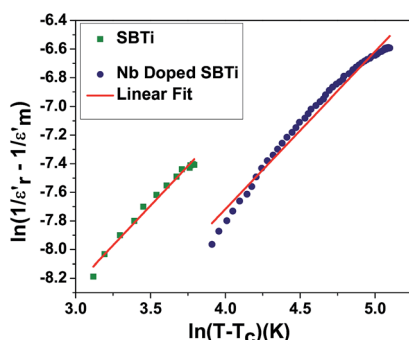


Fig. 7 Modified Curie–Weiss plot at 1 MHz.

to evaluate the relaxation time ($\tau = RC$) associated with grains (τ_g) and grain boundaries (τ_{gb}).¹⁸ The corresponding Arrhenius equation is given below and the Arrhenius plots are shown in Fig. 9.

$$\tau = B \exp - \frac{E_a}{KT} \quad (7)$$

where B is the pre-exponential factor, K is the Boltzmann constant, T is the absolute temperature and E_a is the activation energy. The following relationship has been used for the calculation of grain (σ_g) and grain boundary conductivity (σ_{gb}).¹⁹

$$\sigma = \frac{1}{R} \left(\frac{t}{\rho} \right) \quad (8)$$

where σ is the conductivity, R is the resistance (R_1 or R_2), t is the thickness and ρ is the area of the specimen.¹⁹ Electrical conduction is a thermally activated process and follows the Arrhenius law given below.

$$\sigma = D \exp - \frac{E_a}{KT} \quad (9)$$

where D is the pre-exponential factor. The Arrhenius plots of grain and grain boundary conductivity are shown in Fig. 10. The calculated activation energies from grain and grain boundary relaxation times and grain and grain boundary conductivities are given in Table 2. The reported activation energies based on BaTiO₃ and Bi₂O₃ lattices and their possible reasons are listed in Table 3. Comparison with the table shows that doubly ionized oxygen vacancies, bismuth ion migration and strontium vacancies are present in our samples. A possible representation of the band scheme is given in Fig. 11.

3.4 Grain conductivity

The total bulk grain conductivity (σ_g) can be expressed as a combination of contributions from mobile ions and electronic charge carriers indicated below.¹⁹

$$\sigma_g = fe\mu_e + pe\mu_h + 2e[V_{Sr}']\mu_{Sr} + 4e[V_{Ti}''']\mu_{Ti} + 3e[V_{Bi}''']\mu_{Bi} + 2e[V_0''']\mu_0 \quad (10)$$

where μ_e , μ_h , μ_{Sr} , μ_{Ti} , μ_{Bi} and μ_0 represent the mobilities of electrons, holes, strontium vacancies, titanium vacancies,

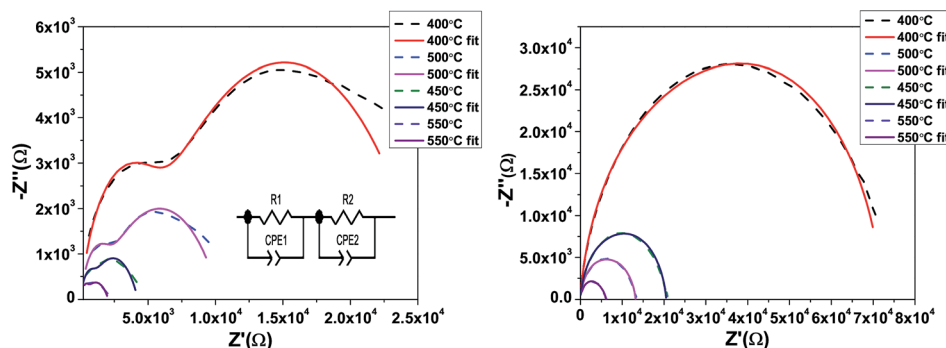


Fig. 8 Cole–Cole plots in the frequency range of 100 Hz to 1 MHz, SBTi (left) and Nb doped SBTi (right).



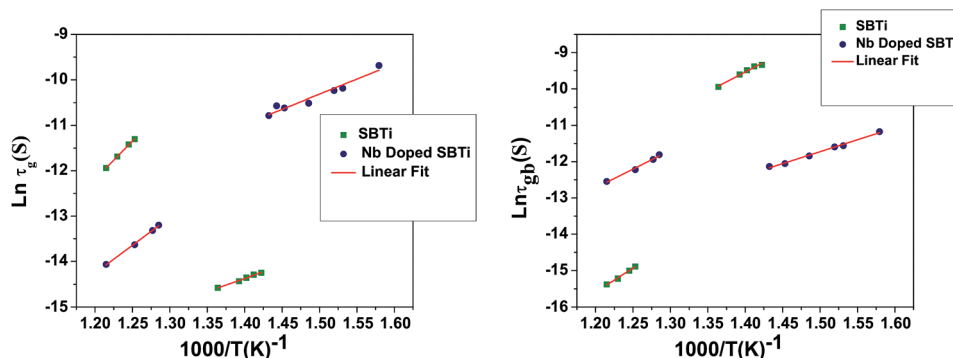
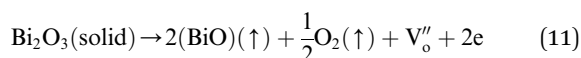


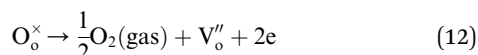
Fig. 9 Arrhenius plot of grain and grain boundary relaxation times.

bismuth vacancies and oxygen vacancies respectively. The quantities f , p , $[V_{\text{Sr}}'']$, $[V_{\text{Ti}}''']$, $[V_{\text{Bi}}''']$ and $[V_{\text{O}}'']$ represent the number of electrons, holes, strontium vacancies, titanium vacancies, bismuth vacancies and oxygen vacancies respectively. The quantity e is the electron charge. Cation vacancies (Sr, Bi, Ti) are relatively immobile because of their heavy mass as well as high activation energy. The mobility of the electronic charge carriers is also less because they move by polaronic hopping in the lattice. So, compared to other contributions to the grain conductivity, the oxygen vacancy motion may contribute much more to grain conductivity.

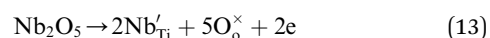
The SBTi ceramics usually contain bismuth vacancies, which is formed during the sintering process. The bismuth vacancy formation is due to its low melting point ($\sim 850^\circ\text{C}$). Along with the bismuth vacancy formation, oxygen vacancies also formed to maintain the charge neutrality. The vacancy formation process can be written as Kröger–Vink notation,⁵



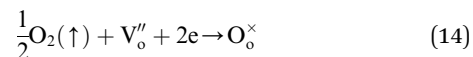
where V_{O}'' is the doubly ionized oxygen vacancies. Apart from oxygen vacancies due to bismuth loss, high temperature sintering can also lead to the neutral oxygen on regular sites ($\text{O}_{\text{O}}^\times$) leaving the lattice, resulting in creating singly or doubly ionized oxygen vacancies. Using the Kröger–Vink notation it can be represented as,¹⁹



In Nb doped SBTi, the introduction of donor type Nb^{5+} ions into Ti^{4+} sites can be written as⁸



where Nb_{Ti}' is the Nb ion with a +1 effective charge at titanium sites. The two electrons coming from the niobium oxide may reduce the oxygen vacancy, as follows⁹



From eqn (14), it is clear that Nb doping decreases the number of oxygen vacancies in the SBTi. This will cause a reduction in the grain conductivity of SBTi. From the Arrhenius plot (Fig. 10) it is clear that Nb doped SBTi shows lower grain conductivity than SBTi. The reduction in the number of oxygen vacancies in Nb doped SBTi is also in line with the activation energy values. The grain conductivity activation energies of SBTi point out the migration of oxygen vacancies (1.04 eV), but for the Nb doped material it is the migration of bismuth ion vacancies (0.57 eV) (refer to Table 2). This means that a reduction in the number of oxygen vacancies happens in Nb doped SBTi.

3.5 Grain boundary conductivity

The grain boundary conductivity behaviour has been explained using the basic Heywang–Jonker model.^{22,23} According to the model, the grain boundary consists of back-to-back double

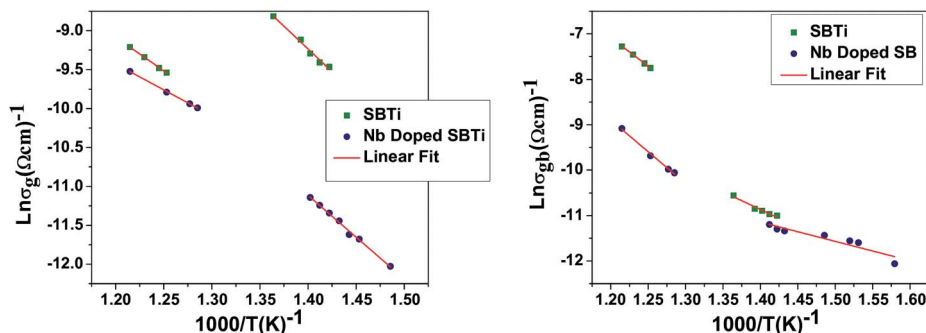


Fig. 10 Arrhenius plot of grain and grain boundary conductivities.



Table 2 Activation energy values (E_a) obtained from Arrhenius plots of grain and grain boundary relaxation times and grain and grain boundary conductivities. τ_g : relaxation time associated with grains. τ_{gb} : relaxation time associated with grain boundaries. σ_g : grain conductivity. σ_{gb} : grain boundary conductivity

| Function | τ_g | τ_g | τ_{gb} | τ_{gb} | σ_g | σ_g | σ_{gb} | σ_{gb} |
|------------------------------|----------|----------|-------------|-------------|------------|------------|---------------|---------------|
| Temperature range (°C) | 550–525 | 470–400 | 550–525 | 470–400 | 550–525 | 450–400 | 550–525 | 450–400 |
| E_a (eV) for SBTi | 1.45 | 0.49 | 1.1 | 0.93 | 0.74 | 1.04 | 1.07 | 0.67 |
| Temperature range (°C) | 550–525 | 470–400 | 550–525 | 470–400 | 550–525 | 450–400 | 550–525 | 450–400 |
| E_a (eV) for Nb doped SBTi | 0.57 | 1.58 | 0.89 | 0.56 | 0.47 | 0.57 | 1.1 | 0.95 |

Schottky barriers. The grain boundary core is made up of cation vacancies. The cation vacancies attract the nearby electrons and become a negatively charged acceptor states, and as a result, the near interface becomes positive. The near interface contains a positive space charge layer on either side of the grain boundary core. These space charge layers are depleted of mobile charge carriers but contain positive effective charge and defects. These depletion layers create a grain boundary barrier with a barrier height (ϕ_0). The schematic diagram is shown in Fig. 12.

In this case the grain boundary core contains bismuth ion vacancies as well as strontium ion vacancies (acceptor states). The presence of bismuth and strontium ion vacancies was also evident from the activation energies (0.67 and 1.58 eV) (refer to Table 2) The positive space charge layer may be composed of oxygen vacancies. The height of the grain boundary barrier (ϕ_0) can be expressed as,²⁴

$$\phi_0 = \frac{e^2 N_s^2}{8\epsilon_0 \epsilon'_{gb} N_d} \quad (15)$$

where e is the electron charge, ϵ_0 is the permittivity of free space and ϵ'_{gb} is the real part of the relative permittivity of the grain boundary region or the dielectric constant of the grain boundary region, N_d is the effective concentration of charged dopants in the bulk and N_s is the concentration of trapped electrons. The relation between the resistivity of the grain boundary (ρ) and the height of the barrier can be written as²⁴

$$\rho = A \exp\left(\frac{\phi_0}{KT}\right) \quad (16)$$

where A is a geometrical factor, K is the Boltzmann constant and T is the absolute temperature. From the Arrhenius plot (Fig. 10), it is clear that the Nb doped samples show lower grain boundary conductivity than SBTi. The negative temperature coefficient of resistance (NTCR) shown by both SBTi and Nb doped SBTi is

also clear from the Arrhenius plot. These observations can be explained using the above model.

From eqn (15), it is clear that the height of the grain boundary barrier (ϕ_0) is inversely proportional to ϵ'_{gb} . Therefore the increase in ϵ'_{gb} will decrease the height of the barrier up to the phase transition temperature (T_c) and thereby a decrease in resistance with temperature is observed up to the phase transition temperature. Above the phase transition temperature, the ϵ'_{gb} starts to decrease and this will increase the height of the grain boundary. Simultaneously, due to the rise in temperature, the energy of the trapped electrons in the grain boundary also increases. When the energy of the electron traps reaches the Fermi level, trapped electrons start to jump to the conduction band, which can depress the increase in the barrier height as well as the resistance. So, the net effect is the increase in conductivity with temperature above the phase transition temperature.

In the case of Nb doped SBTi, it is clear from eqn (13) that the system acquires an extra electron. These extra electrons do not reduce the oxygen vacancies, as in the case of the grains. However they may fall down the grain boundary core, resulting in an increased concentration of trapped electrons (N_s). This means that the Nb doped SBTi has an increased number of trapped electron concentration (N_s) than SBTi. The increase in trapped electron concentration decreases the grain boundary conductivity. This may be the reason behind the decreased grain boundary conductivity of Nb doped SBTi than SBTi. The calculated activation energies for Nb doped SBTi from the grain boundary conductivity show the presence of oxygen vacancies (0.95 eV and 1.1 eV) (refer to Table 2) in the grain boundaries. This experimental observation also indicates the validity of the above-mentioned model.

3.6 ac conductivity analysis

3.6.1 ac conductivity and Jonscher's power law. The response of the ac conductivity with temperature and frequency

Table 3 Summary of conduction processes and their associated range of activation energy values reported in the literature^{19–21}

| Activation energy range (eV) | Conduction process |
|------------------------------|---|
| 0.7–1.21 | Diffusion of doubly ionized oxygen vacancies |
| 1.49–1.51 | Electrons ionized from strontium vacancies |
| 0.1–0.2 | First ionization energy of oxygen vacancies |
| 15 | Titanium vacancy migration |
| 2.8 | Strontium vacancy migration |
| 0.66 | Activation energy of self-diffusion of bismuth ions |
| 0.18–0.48 | Conduction by phonon assisted electron/hole hopping |

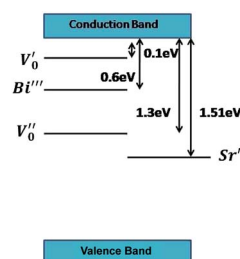


Fig. 11 Schematic diagram of the band scheme.



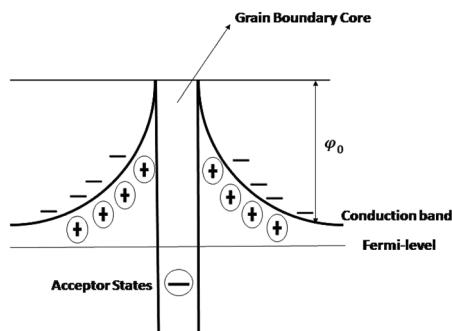


Fig. 12 Schematic diagram of the grain boundary.

provides an insight into the different relaxation mechanisms in the material. The ac conductivities of the samples were calculated using the following relation²⁵

$$\sigma_{ac} = \varepsilon_0 \varepsilon'_r \omega \tan \delta \quad (17)$$

where ε_0 is the permittivity of free space, ω is the frequency, ε'_r is the dielectric constant and $\tan \delta$ is the dielectric loss. The frequency dependence of the ac conductivity shows two regions (see Fig. 13): one is frequency independent and the other is frequency dependent. This behaviour can be explained using Jonscher's universal power law. The ac conductivity plots at different temperatures were fitted using Jonscher's universal power law described below,²⁵

$$\sigma_{ac}(\omega) = \sigma_{dc} + A\omega^n \quad (18)$$

where σ_{dc} , A , and n are the bulk dc conductivity, the pre-exponential factor and the frequency exponent respectively. Fig. 13 shows the ac conductivity *versus* frequency plots at different temperatures along with fitted curves of Jonscher's power law. The mathematical fitting was performed using OriginPro8.5 with a non-linear curve fitting method. The values of σ_{dc} , A and n were obtained from the fitted curves.

The obtained values of the frequency exponent (n) in SBTi and Nb doped SBTi is less than 1, indicating the non-Debye behaviour of the samples. It also shows that the charge carriers undergo a translational motion with sudden hopping.²⁶ The pre-exponential factor A determines the strength of polarizability.²⁷ From Fig. 14, it is clear that compared to SBTi the Nb doped SBTi shows a decrease in A values. This indicates that Nb

doping reduces the polarizability of SBTi. The relation between polarizability (α) and dielectric constant is given by (assuming that the atoms are the same kind)²⁸

$$\alpha = \varepsilon_0 \frac{(\varepsilon'_r - 1)}{z} \quad (19)$$

where ε_0 is the permittivity of free space, ε'_r is the dielectric constant and z is the number of atoms per unit volume. It is clear from the previous section that the Nb doping reduces the number of oxygen vacancies in SBTi. This decrease in the number of oxygen vacancies will increase the value of z in Nb doped SBTi, which in turn causes a decrease in polarizability of Nb doped SBTi. This may be the reason behind the decreased value of A in Nb doped SBTi. However, previous studies by Hao *et al.*¹ show that there is increase in the value of electric polarization of Nb doped SBTi when compared to un-doped SBTi. The polarization (p) of the whole sample can be expressed by the relation,²⁸

$$p = \sum_j \alpha_j z_j E_{\text{local}}(j) \quad (20)$$

This expression is a summing over all atomic positions where α is the polarizability and E_{local} is the local electric field at the atomic site. Even though the polarizability (α) of the Nb doped SBTi decreases, the z and E_{local} values are increasing. This may lead to an increment in the polarization of Nb doped SBTi. The increase in the local electric field (E_{local}) is due to the replacement of less polarizable Ti^{4+} (electronegativity 1.54) with highly polarizable Nb^{5+} (electronegativity 1.6) ions.

3.6.2 Mechanism of ac conduction. The behaviour of n *versus* temperature plots (Fig. 14) tells us about the ac conductivity mechanism. The variation of n with temperature can be directly correlated to the theoretical models of ac conductivity, and Table 4 shows the details. From the table, one can conclude that none of the models completely match with the experimental observations. However, the ac conductivity mechanism can be explained using two models at different temperature regions. In the case of SBTi, large-polaron QMT, and small-polaron QMT models have been used, whereas in the case of Nb doped SBTi, small-polaron QMT and Correlated Barrier Hopping (CBH) models have been used to explain the ac

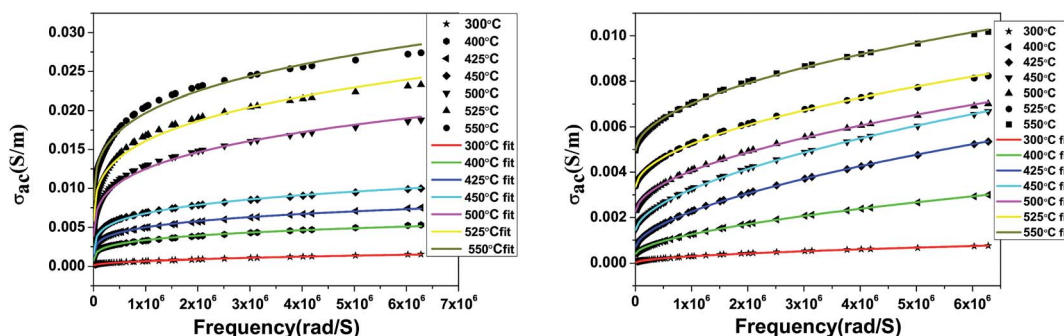


Fig. 13 ac conductivity with frequency along with fitting curves of the power law; SBTi (left) and Nb doped SBTi (right).



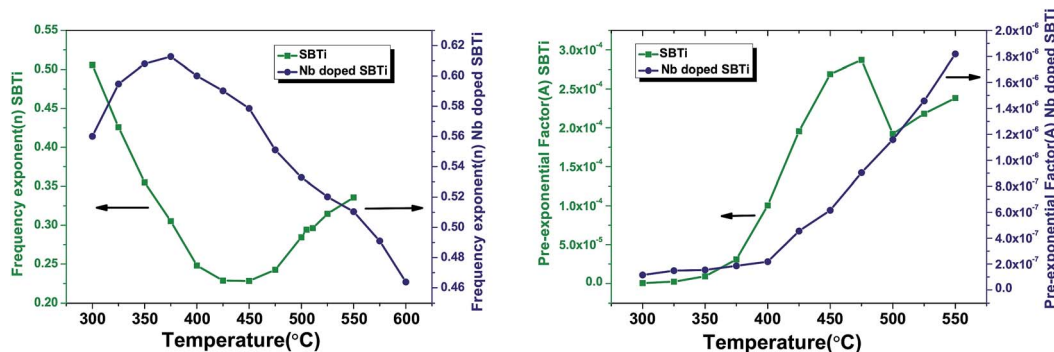


Fig. 14 The plots between the frequency exponent (n) versus temperature (left) and the pre-exponential factor (A) versus temperature (right).

conductivity mechanism. All the mathematical fitting in this section was done using Wolfram Mathematica 10.

According to the large-polaron QMT model, the frequency exponent (n) can be written as,²⁹

$$n = 1 - \frac{1}{L'_\omega} \frac{4 + \frac{6W_{H_0}r'}{KTL_\omega^2}}{\left(1 + \frac{W_{H_0}r'}{KTL_\omega^2}\right)^2} \quad (21)$$

The $L'_\omega = 2\alpha L_\omega$ and $r' = 2\alpha r$ are the reduced quantities where α is the polarizability, L_ω is the tunnelling distance at a frequency ω and r is the polaron radius. K and T are the Boltzmann constant and temperature respectively. The polaron hopping energy (W_H) is given by

$$W_H = W_{H_0} \left(1 - \frac{r}{\chi}\right) \quad (22)$$

where W_{H_0} is a parameter, and χ is the interatomic spacing. Eqn (21) is used to fit with the n versus temperature curve of SBTi, in the temperature range 300 °C to 400 °C (see Fig. 15). The obtained parameters from the fitting curve are $W_{H_0} = -0.1340$ eV and $L'_\omega = 5.7162$. The parameter $r' = 7$ was assumed for the fitting. The higher temperature region was fitted using the small-polaron QMT model.

From the small-polaron QMT model, the relation between the frequency exponent (n) and the temperature (T) can be written as,²⁹

$$n = 1 - \frac{4}{\ln\left(\frac{1}{\omega\tau_0}\right) - \frac{W}{KT}} \quad (23)$$

where ω is the frequency, τ_0 is the relaxation time, K is the Boltzmann constant and W is the polaron hopping energy. The n versus temperature curve of SBTi in the temperature range 450 °C to 550 °C was fitted with eqn (23) (see Fig. 15). The obtained value of the polaron hopping energy (W) from the fitted curve is 0.702 eV. The values of $\omega = 10^5$ Hz and $\tau_0 = 10^{-12}$ s were assumed for the fitting.

The variation of the frequency exponent (n) with temperature for Nb doped SBTi is also fitted with eqn (23), in the temperature range 300 °C to 375 °C (see Fig. 16). The values of $\omega = 10^5$ Hz and $\tau_0 = 10^{-14}$ s were assumed for the fitting and the obtained value of the polaron hopping energy (W) is 0.570 eV. The higher temperature range was fitted with the CBH model (see Fig. 16). The relation between n and the temperature from the CBH model is given below,²⁹

$$n = 1 - \frac{6KT}{W_m - KT \ln\left(\frac{1}{\omega\tau_0}\right)} \quad (24)$$

where ω is the frequency, τ_0 is the relaxation time, K is the Boltzmann constant and W_m is the barrier height. The obtained values of W_m and τ_0 from the fitted curve are 0.951 eV and 2.710×10^{-6} s respectively. The value of $\omega = 10^5$ Hz was assumed for the fitting.

Table 4 Summary of co-relations between ac conductivity models and the functional dependence of the frequency exponent (n) with temperature²⁹

| Model name | Variation of frequency exponent (n) with temperature |
|------------------------------------|--|
| Quantum Mechanical Tunneling (QMT) | $n = 0.81$, independent of temperature |
| Small-polaron QMT | Increasing n with increasing temperature |
| Large-polaron QMT | (1) High value of the polaron radius: n exhibits a minimum at a certain temperature and subsequently increases in a fashion similar to small-polaron QMT (2) Low value of the polaron radius: decreasing n with increasing temperature, but much steeper than CBH |
| Hopping Over a Barrier (HOB) | $n = 1$, independent of temperature |
| Correlated Barrier Hopping (CBH) | Decreasing n with increasing temperature |



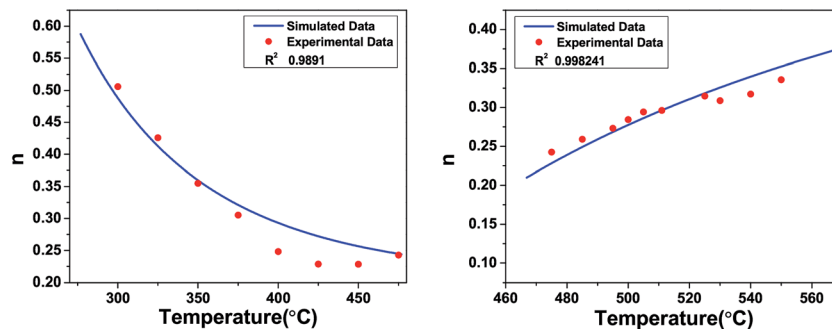


Fig. 15 Frequency exponent versus temperature for SBTi, fitted with the large-polaron QMT model (left) and the small-polaron QMT model (right).

The parameters and the activation energies from the fitting are physically possible values and this proves the validity of the models. Note that the changes in conduction mechanism which occur in both samples are in the vicinity of the Curie–Weiss temperature (458 °C and 405 °C). The Curie–Weiss temperature is that at which the change in crystal structure occurs. It is important to note that in the ferroelectric region, the conduction mechanism in SBTi is large-polaron but is small-polaron for Nb doped SBTi. The main difference between the large-polaron and small-polaron models is related to the spreading of lattice distortion. If the lattice distortions spread over many lattice sites, then it is called large-polaron. If the distortions are limited to the nearest neighbouring ions, then it is small-polaron.³⁰ Therefore, the change in the conduction mechanism indicates the reduction of lattice distortions in Nb doped SBTi. This again leads to the conclusion that the number of oxygen vacancies has been reduced by niobium doping.

3.6.3 ac conductivity in terms of hopping frequency. For further understanding of the relaxation process, we analyzed the ac conductivity response with temperature using the Arrhenius law given below

$$\sigma_{ac} = M \exp - \frac{E_{ac}}{KT} \quad (25)$$

where M is the ac conductivity pre-exponential factor, K is the Boltzmann constant and E_{ac} is the ac conductivity activation energy. Fig. 17 shows the Arrhenius plot and the activation energies are given in Table 5. The activation energy obtained can be correlated with the possible conduction processes given in Table 3. The activation energy in the low temperature (180–

35 °C) region of SBTi indicates the presence of singly ionized oxygen vacancies, and it can be represented as⁷



At high temperatures the singly ionized oxygen may become doubly ionized oxygen vacancies (eqn (27)). The presence of doubly ionized oxygen vacancies at high temperature is evident from the activation energies obtained from various functions (Tables 5 and 2). Apart from the bismuth vacancy migration (0.51 eV), the phonon-assisted electron or hole hopping also happens in our samples (0.34 eV and 0.37 eV) (Table 5). The possible mechanism for the phonon-assisted electron or hole hopping might be the valency fluctuations of Ti^{4+}/Ti^{3+} ions. In the Nb doped SBTi, 5% of Ti^{4+} ions were replaced with Nb^{5+} ions. This will effectively decrease the ac conductivity contributed from valency fluctuations of Ti^{4+}/Ti^{3+} ions. This leads to a decrease in ac conductivity of Nb doped SBTi as seen in Fig. 13. The power law expressed in hopping frequency (ω_p) is³¹

$$\sigma_{ac}(\omega) = \sigma_{dc} \left[1 + \frac{A\omega^n}{\sigma_{dc}} \right] = \sigma_{dc} \left[1 + \left(\frac{\omega}{\omega_p} \right)^n \right] \quad (28)$$

$$\text{where, } \omega_p = \left(\frac{\sigma_{dc}}{A} \right)^{\frac{1}{n}} \quad (29)$$

The hopping frequency is the frequency at which the conductivity relaxation begins to appear. In general, σ_{dc} (bulk dc

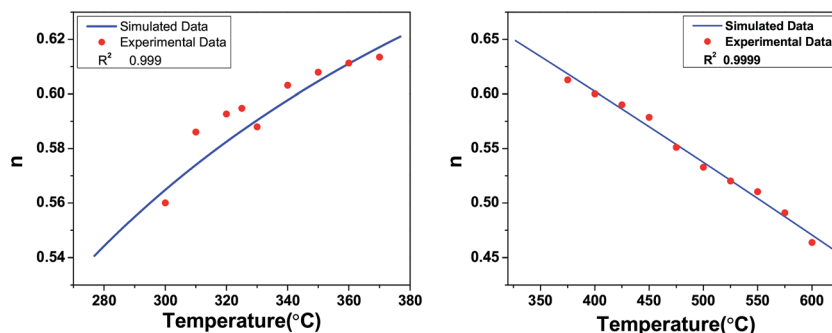


Fig. 16 Frequency exponent versus temperature for Nb doped SBTi, fitted with the small-polaron QMT model (left) and the CBH model (right).



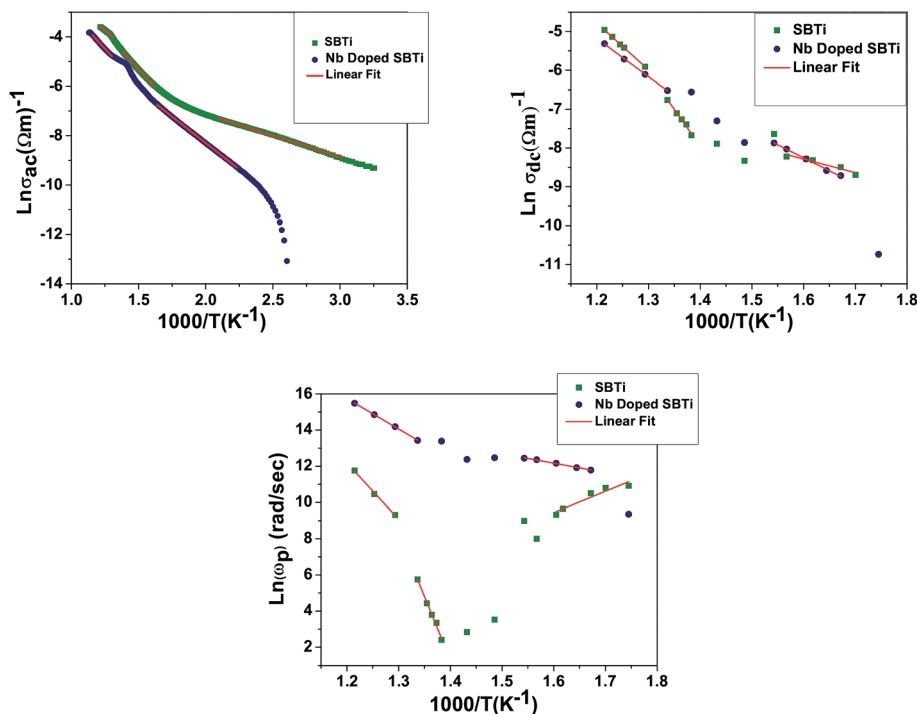


Fig. 17 Arrhenius plots of ac conductivity, dc conductivity and hopping frequency at 1 MHz.

Table 5 Activation energy values obtained from the Arrhenius plots of ac conductivity, bulk dc conductivity and hopping frequency. E_{ac} : ac conductivity activation energy, E_{dc} : dc conductivity activation energy, and E_p : activation energy for hopping frequency

| Activation energy (eV) | E_{ac} | E_{ac} | E_{ac} | E_{dc} | E_{dc} | E_{dc} | E_p | E_p | E_p |
|------------------------|----------|----------|----------|----------|----------|----------|---------|---------|---------|
| Temperature range (°C) | 550–525 | 490–350 | 180–35 | 550–525 | 475–450 | 375–300 | 550–525 | 475–450 | 375–300 |
| For SBTi | 0.34 | 0.51 | 0.15 | 1.05 | 1.63 | 0.43 | 2.68 | 6.04 | 1.15 |
| Activation energy (eV) | E_{ac} | E_{ac} | E_{ac} | E_{dc} | E_{dc} | E_{dc} | E_p | E_p | E_p |
| Temperature range (°C) | 550–525 | 490–350 | 550–475 | 375–325 | 550–475 | 375–325 | 550–475 | 375–325 | 375–325 |
| For Nb doped SBTi | 0.51 | 0.37 | 0.85 | 0.57 | 1.45 | 0.44 | | | |

conductivity) and ω_p are thermally activated parameters and follow the Arrhenius laws given below,³¹

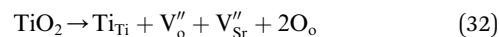
$$\sigma_{dc} = H \exp - \frac{E_{dc}}{KT} \quad (30)$$

$$\omega_p = I \exp - \frac{E_p}{KT} \quad (31)$$

where H is the dc conductivity pre-exponential factor, K is the Boltzmann constant, E_{dc} is the dc conductivity activation energy, I is the pre-exponential of hopping frequency and E_p is the activation energy for hopping frequency. The corresponding activation energies are obtained from the Arrhenius plots (Fig. 17). The calculated activation energies are listed in Table 5. The activation energy obtained (Table 5) can be correlated with the possible conduction process (Table 3).

The activation energy values E_{dc} and E_p are not the same, and this shows that the charge carriers has to overcome different energy barriers while conducting and relaxing. The reason for the activation energy of 6 eV (475–450 °C in SBTi) is a confusing matter, even though the reported activation energies from titanium based half-Heusler compounds show that 5–6 eV is

due to self-diffusion of titanium ions.³² But, it is worth to note that the reported activation energy for titanium vacancy migration in BaTiO₃ is 15 eV.¹⁹ The activation energy from various functions also points to the strontium vacancy formation and migration of strontium vacancies in SBTi and Nb doped SBTi. In SBTi, there is a possibility of excess accommodation of titanium ions in the lattice, which can lead to the formation of doubly ionized strontium vacancies. This can be represented as,²¹



In the Nb doped SBTi, the excess charge of Nb⁵⁺ is compensated in two ways, one is through the formation of conduction electrons (which will reduce oxygen vacancies) and the second is by strontium vacancies.

4 Conclusions

The SBTi and Nb doped SBTi ceramics have been successfully synthesized using solid state reactions. The XRD pattern shows



that the Nb substitution does not change the crystal structure of SBTi. The observed phase transitions are normal. The Nb substitution decreases the transition temperature of SBTi (506 °C to 448 °C) but increases the dielectric constant. The relaxation times and grain and grain boundary conductivities have been obtained from fitted parameters of the Cole–Cole plots. The grain boundary conductivity was analyzed in the light of the Heywang–Jonker model. The Heywang–Jonker model was successful in the case of BaTiO₃ ceramics and we extended it to bismuth layered oxides. The frequency dependent ac conductivity at different temperatures has been analyzed using Jonscher's power law. Many authors have explained the ac conductivity in view of Jonscher's power law but in the current article we correlated the frequency exponent (n) with ac conductivity models. Taking into consideration the models, we concluded that the conduction mechanism of SBTi from 300 °C to 475 °C is large-polaron tunneling and from 475 °C to 550 °C is small-polaron tunneling. For the Nb doped case, the conduction mechanism from 300 °C to 375 °C is small-polaron tunneling and from 375 °C to 550 °C is correlated band hopping. Furthermore, Jonscher's power law has been used for calculating the hopping frequency and activation energies associated with it. The activation energies evaluated from different functions indicate that the conductivity in the SBTi sample has contributions from the migration of singly and doubly ionized oxygen vacancies, bismuth ion vacancies, electrons ejected from strontium ions, strontium ion vacancies and valance fluctuations of Ti⁴⁺/Ti³⁺ ions. From the analysis of activation energies, ac conductivity models, and Jonscher's power law, we concluded that donor ion Nb⁵⁺ doping in SBTi reduces the defects originating from oxygen vacancies. The reduction in oxygen vacancies might be the reason for the improved electrical properties of Nb doped SBTi.

Conflicts of interest

There are no conflicts to declare.

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