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Study on the fouling mechanism and cleaning method in the treatment of polymer flooding produced water with ion exchange membranes†

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The complex interactions between organic and inorganic foulants in polymer flooding produced water (PFPW) play a significant role in membrane fouling characteristics during the treatment processes with ion-exchange membranes (IEMs). In order to ensure the desalination capacity of IEMs during electrodialysis, this work systematically investigated the fouling mechanism and cleaning properties with different synthetic solutions as feed water. The results demonstrated that the desalination rates of the IEMs decreased by 39.73%, 43.05%, 45.81% and 52.72% when fouled by HPAM, HPAM-inorganic (*i.e.*, CaCl_2 and NaHCO_3), oil emulsions and oil-HPAM-inorganic, respectively. The results of membrane resistances and SEM images indicated that organic foulant (*i.e.*, HPAM) and inorganic components have a synergistic effect on the fouling of IEMs. The membrane cleaning method using acid-base-sodium dodecyl benzene sulfonate (SDBS) was proposed here to recover the performance of the IEMs after being fouled by feed solution containing oil-HPAM-inorganic compounds. The desalination rate of the IEMs after membrane cleaning increased from 39.62% to 81.39%. This indicated that the acid-base cleaning alone eliminated the inorganic precipitation and gel layer, and the subsequent SDBS cleaning removed the dominant oil emulsion layer.

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1 Introduction

The oil industry plays an important role in the development of economy and society. In order to ensure continuous oil supply, technologies for enhancing oil recovery have received worldwide attention. At present, Daqing oilfield, the largest one in China, has boosted oil recovery by adopting polymer flooding technology due to its low cost and easy operation. Polymer flooding involves injecting water containing polymer into the oil layer to widen the scope of oil exploitation and increase the oil production.^{1,2} However, this technology has also produced more than 75 million tons of polymer flooding produced water (PFPW) every year.³ PFPW is a complex and multiphase system with solids, liquids, gases, dissolved salts and other types of impurities, and it is harmful to the oil field and the surrounding environment.⁴⁻⁶ Membrane technology, which has gained popularity in water and wastewater treatment, has also been utilized in the treatment of PFPW.⁷⁻¹¹ Some studies have

indicated that the water quality indexes, including concentration of suspended substances, the oil content and the median particle size can meet the standards of water reinjection after a conventional pretreatment followed by an ultrafiltration (UF) process. Nevertheless, the UF effluent still has a high degree of mineralization. The succedent electrodialysis (ED) process has successfully been used to reduce the salinity of PFPW, and wastewater after treatment can meet the requirements for the preparation of a polymer solution aiming for wastewater zero-emission.¹²⁻¹⁴

The ED process utilizes a potential difference as the driving force, in which the anionic and cationic ions migrate from the dilute compartment across the IEMs to the concentrated compartment under a DC electric field.¹⁵⁻¹⁸ ED as an important ion-exchange membrane (IEM) based electrochemical separation process has been extensively in water desalination. Nevertheless, membrane fouling is a main obstruction for the application and development of ED.^{19,20} Foulants in feed solutions may change the physical and chemical properties of the membranes and deteriorate the membrane performance analyzing the fouling mechanism of IEMs is the foundation of exploring measures for membrane fouling control.

Membrane fouling is mainly divided into organic fouling and inorganic fouling. There exist many studies with respect to organic fouling on IEMs.²¹⁻²⁷ Tanaka *et al.*²⁸ investigated the organic fouling mechanism of anion-exchange membranes (AEMs) and found that electrostatic interactions, affinity

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interactions and geometrical factors play important roles in the ED process. Ruiz *et al.*²⁹ studied the influence of a pulsed electric field with a low frequency square-shaped periodic signal during the ED of a casein solution on membrane fouling and indicated that protein fouling might be resulted by the dissociation of water molecules and the heat increase at the anion-exchange membrane (AEM) interface. Some researchers have also focused on the inorganic fouling of IEMs.^{30,31} Bao *et al.*³² indicated that the fouling of inorganic salts on IEMs was reversible, generally in the form of direct surface crystallization and/or precipitation. Meital Asraf-Snir *et al.*³³ investigated the formation of gypsum scale in IEMs under a Donnan exchange regime and found that the scaling in the homogeneous membrane was mainly characterized by surface deposits, while the heterogeneous membrane showed a high degree of internal precipitation. All in all, fouling of the IEMs during ED process is related to the functional groups of the membranes, structure of the membrane polymeric matrix and properties of the foulants. The fouling would increase the membrane electric resistance and decrease the selectivity of the IEMs, resulting in a higher power consumption and a lower water quality.^{34–37} In this regard, effective fouling control techniques are necessary to delay the membrane fouling process, extend the membrane life, and reduce the maintenance cost. At present, regular membrane cleaning is still the most important method for controlling IEM fouling in ED industrial applications.^{38,39} As the wastewater system is complex and stable, interactions might exist between different components, which makes the fouling layer more complicated and causes difficulties in membrane cleaning. As far as we know, previous researches mainly focused on the fouling of a single component in PFPW treatment.^{40,41} The interactions between different foulants in ED process were barely discussed. In addition, there are few studies systematically investigated the cleaning of IEMs fouled by different foulants of PFPW.

In this research, membrane fouling mechanisms during PFPW treatment by ED were fully investigated. Moreover, effects of different cleaning agents were explored and appropriate cleaning methods aimed at different foulants were found out. The fouling properties and cleaning efficiency of the cleaning methods were evaluated by membrane resistance, contact angle, SEM and desalination capacity of the IEMs. In addition,

zeta potentials and ATR-FTIR spectra were measured to verify the fouling mechanism. This work will provide references for controlling membrane fouling and prolonging the life in treating PFPW by ED process.

2 Materials and methods

2.1 Electrodialysis apparatus and membranes

The ED experiments were performed using a six-cell electrodi-lysis apparatus made of plexiglass. As shown in Fig. 1, three anion-exchange membranes (AEMs) and two cation exchange membranes (CEMs) were alternately installed in the ED stack. The effective membrane area of the ED cell was 42 cm². Homogeneous IEMs (Shandong Tianwei Membrane Technology Co., Ltd) made from polyphenylene were applied, and the functional groups of the CEMs and AEMs were sulfonic acid groups and quaternary ammonium groups, respectively. AEMs and CEMs were soaked in deionized water for more than 24 h prior to use.

For the electrode solution, 0.8 L of 0.04 M Na₂SO₄ was used in chamber 1 and 6. Chambers 2 and 5 were filled with 0.5 L of 0.04 M Na₂SO₄. Chambers 3 and 4, which were defined as the concentrated and dilute compartments, respectively, were filled with 0.5 L of the feed solutions (0.05 M NaCl solution or 0.05 M NaCl solution containing a variety of fouling components). The solutions were continuously pumped through the compartments from reservoir vessels using a peristaltic pump BT100-L (Longer Pump, China) with a flow rate of 10 mL min⁻¹.

2.2 Fouling experiments

2.2.1 Preparation of feed solution. All the inorganic salts and the surfactant SDBS were purchased from Sinopharm (Sinopharm Group, China). The crude oil was obtained from the sewage treatment station of the Daqing oilfield. Both crude oil and SDBS (to well disperse hydrophobic oil) were added into water and placed on a high speed magnetic stirrer for 6 h to get the oil emulsion. HPAM was obtained from the Wenxian water purification plant. Its main properties can be found in Table S1.†

2.2.2 Fouling protocol. The fouling experiments were carried out with virgin IEMs under a constant current density of 30 A m⁻². Prior to each ED run, the membranes were soaked in

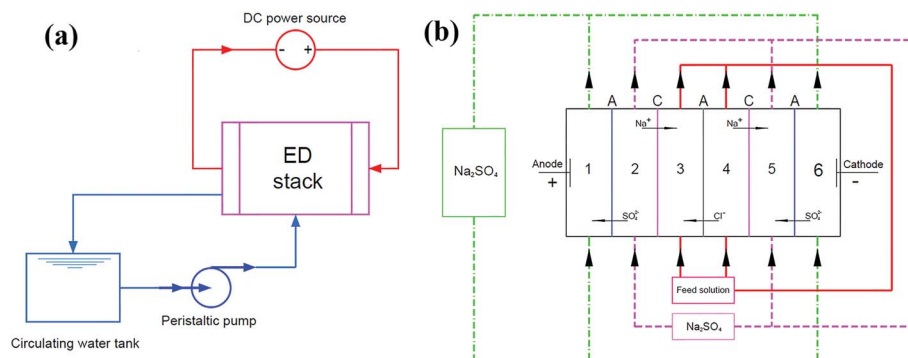


Fig. 1 Schematic diagram of the (a) ED set-up, (b) the six-compartment stack for electrodialysis experiments (C: cation; and A: anion exchange membranes).



0.5 M sodium chloride for 24 h and each of the ED experiments lasted for 24 h at 25 °C. The feed solutions of chamber 3 and 4 in different fouling experiments are listed in Table 1. All fouling experiments were conducted for three times.

2.3 Cleaning experiments

To recover the membrane performance, regular cleaning of the fouled IEMs was necessary after a period time of ED process. *In situ* cleaning experiments were implemented in this study. The solutions in all compartments were switched to the cleaning agent (including 0.1 M HCl, 0.1 M NaOH and 3 wt% SDBS) and all the other conditions of the device unchanged. The cleaning agent, (including 0.1 M HCl, 0.1 M NaOH and/or 3 wt% SDBS), circulated between the ED stack and tank at a maximal flow rate actuated by the peristaltic pump at room temperature (25 ± 1 °C). The cleaned membranes were then stored in a 0.5 M NaCl solution to prepare for subsequent characterization analyses.

Table 2 listed the different cleaning methods adopted according to the membrane fouling type. The cleaning experiments also repeated for three times.

2.4 Analytical methods

2.4.1 Zeta potentials. Zeta potentials of the foulants and membrane surface were measured by Zetasizer Nano ZS90 (Malvern, UK) and SurPASS (Anton Paar, AT), respectively.

2.4.2 Membrane resistance. The membrane resistance was measured by a two-slot device, which was equipped with titanium plates and connected with an AC bridge through a special fixture. The membrane samples were measured in the

apparatus filled with a 0.5 M NaCl solution. The effective area of the membrane was 36 cm^2 . The resistance, R_{m+s} , was measured under a frequency of 1 kHz. Subsequently, the membranes were taken out, and the resistance of the solution was measured. The membrane resistance was calculated using the following equation:

$$R_A = (R_{m+s} - R_s)A \quad (1)$$

where R_A is the membrane resistance, R_{m+s} is the total resistance of the membranes and solution, R_s is the resistance of the solution, and A is the effective area of the membrane.

2.4.3 Contact angle. The contact angle indirectly reflects the hydrophilicity/hydrophobicity of the membrane. In this study, the contact angles of the IEMs were measured by the drop method using an OCA15ES contact angle meter from Data-physics. The IEM samples were dried in a constant temperature oven at 38 °C for at least 24 h before the measurement. The contact angles for different contact times between ultrapure water and the membrane surface were recorded by the SCA software. Each membrane sample was measured more than 5 times at different locations to obtain accurate and reliable results.

2.4.4 Scanning electron microscopy. SEM images were obtained from a Cold Field-emission Scanning Electron Microscope (Japan, Hitachi S-4800). Membrane samples were dried at 38 °C for 24 h before measurement.

2.4.5 Fourier transform infrared spectroscopy. The functional groups of the IEMs were detected using an attenuated total reflectance-Fourier transform infrared (ATR-FTIR)

Table 1 Feed solutions for different fouling processes during the ED process

Experimental number	Components of the feed solution	Fouling type
M1	50 mM NaCl	Virgin IEMs
M2	1 mM CaCl_2 + 50 mM NaHCO_3	Inorganic fouling
M3	200 mg L^{-1} HPAM + 50 mM NaCl	HPAM fouling
M4	200 mg L^{-1} HPAM + 1 mM CaCl_2 + 50 mM NaHCO_3	HPAM-inorganic fouling
M5	100 mg L^{-1} oil emulsion + 50 mM NaCl	Oil emulsion fouling
M6	100 mg L^{-1} oil emulsion + 200 mg L^{-1} HPAM + 1 mM CaCl_2 + 50 mM NaHCO_3	Oil emulsion-HPAM-inorganic fouling

Table 2 Different cleaning methods for the fouled membranes

Methods	Agent	Time
Water cleaning	Distilled water	30 min
Acid cleaning	0.1 M HCl	30 min
Base cleaning	0.1 M NaOH	30 min
SDBS cleaning	0.3 wt% SDBS	30 min
Acid-base cleaning	0.1 M HCl and 0.1 M NaOH	Cleaning in HCl for 30 min and subsequently in NaOH for 30 min
Base-acid cleaning	0.1 M NaOH and 0.1 M HCl	Cleaning in NaOH for 30 min and subsequently in HCl for 30 min
Acid-base-SDBS cleaning	0.1 M NaOH, 0.1 M HCl and 0.3 wt% SDBS	Cleaning in HCl, NaOH and SDBS for 30 min, successively



spectrometer (Nicolet 5700, Thermo Electron Corporation, USA), and all the spectra were collected with OMNIC 8.0 software. The membrane samples were dried in a 38 °C oven for 24 h for complete drying prior to the measurement.

2.4.6 Desalination rate. Desalination experiments were conducted using the ED stack described in section 2.1. The solutions in chamber 1, 2, 5, 6 were 0.04 M Na₂SO₄ and in chamber 3, 4 were 0.05 M NaCl without circulation. The fouled or cleaned membranes were installed in the ED stack and the desalination rate was measured to evaluate the desalination performance of the fouled membranes and the effects of the cleaning methods. The conductivity of the dilute solution was monitored by the conductivity meter in real time for 60 min. The desalination rate (DR) was obtained by the equation:

$$\text{DR (\%)} = (C_0 - C_t)/C_0 \quad (2)$$

where C_0 and C_t were the initial and final (60 min) conductivity of the dilute solution, respectively.

3 Results and discussion

3.1 Organic and inorganic fouling of IEMs

To understand the fouling properties we studied the effects of different foulants in PFPW on the IEMs. A set of fouling experiments (S1–S6, Table 1) were conducted with different feed solutions. Symbol S1–S6 in the figures represented the membranes after different fouling experiments as listed in Table 1. S1 was the virgin membranes without fouling and S2–S6 were inorganic, HPAM, HPAM-inorganic, oil, oil-HPAM-inorganic fouled membranes, respectively.

3.1.1 Desalination performance. Fig. 2 presented the desalination rates (DR) at 60 min of different fouled membranes. M1 and M2 exhibited the largest desalination capabilities with a desalination rate over 90%. The slight difference in the DRs between experiment M1 and M2 indicated that no evident fouling occurred during the inorganic fouling experiment. According to the measurements of zeta potentials of HPAM as presented in Fig. S1,† HPAM is electronegative and

it could foul the AEM due to electrostatic interaction as the fixed functional groups of AEM is positive. As a result, the DR of HPAM-fouled membranes decreased sharply to 52.61%, which was 39.73% lower than that of M1. A lower DR (49.29%) of M4 was observed compared with M3, indicating that membranes were more seriously fouled by HPAM-inorganic components, which could be explained by the “egg-box” model.^{42,43} The calcium ions would bind to the oxygen atoms of carboxylates and bridges were formed between adjacent HPAM molecules, aggravating the fouling effects. Additionally, M6 exhibited the lowest desalination performance with a DR of 39.62%, which was 9.67% lower than that of M4. This meant that the presence of the oil emulsion intensified the HPAM-inorganic fouling on the IEM surface.

3.1.2 Fouling characteristics. The area resistances of all the membranes after experiment M1–M6 were measured and the results were detailed in Fig. 3. As shown in Fig. 3, the membrane resistance of M4 was higher than the membrane resistances of M2 and M3, which further confirmed the synergistic effect of the inorganic components and HPAM on the IEM fouling.

Moreover, the membrane resistances of the AEMs fouled by inorganic solution changed slightly, while the AEMs in the HPAM and HPAM-inorganic system almost doubled the values of the virgin AEM, which was consistent with the analysis of the desalination performance. The results of SEM analysis (see Fig. S4†) also indicated that the membranes were obviously fouled by HPAM and HPAM-inorganic solutions compared with the virgin AEM. The oil-HPAM-inorganic fouling was the most serious as shown in Fig. S4d,† which was in accordance with the measurements of membrane resistance and zeta potentials of membrane surface (see Table S2†). Therefore, the fouling of HPAM-inorganic on the AEM was aggravated by the addition of oil emulsion. The oil emulsion has a strong electrostatic interaction with the AEM owing to its strong electronegativity (see Fig. S2†). In addition, the surfactant SDBS was added in the oil emulsion preparation, which could foul the AEM,⁴⁴ and some of the SDBS molecules would enter the AEM. As a result, the membrane resistance significantly increased. The membrane resistance of oil emulsion-fouled AEM (M5) was larger than that of HPAM-fouled AEM (M3), indicating that the AEMs were more

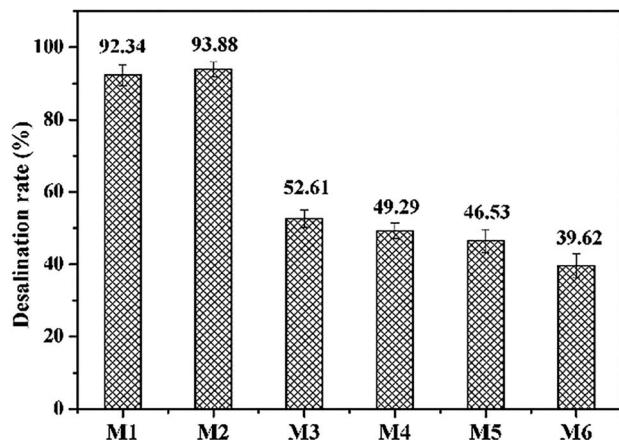


Fig. 2 Effects of different components on the desalination performance of the ED stack.

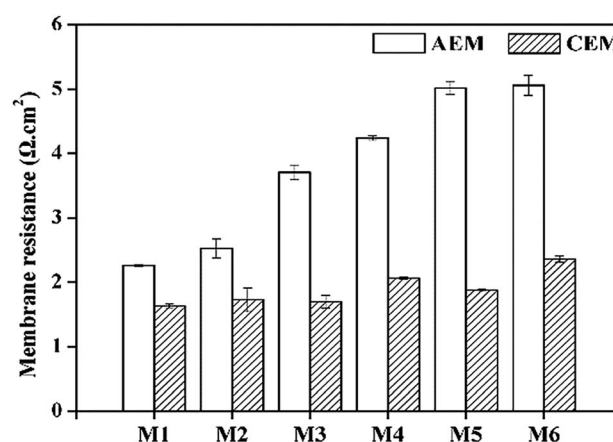


Fig. 3 Effects of different foulants on the membrane resistance.



easily fouled by oil emulsion than HPAM. It can be explained by the results of zeta potentials that oil emulsion was more electronegative than HPAM and the electrostatic attraction was stronger between oil emulsion and the AEMs. Nevertheless, the membrane resistance of the AEM in the oil emulsion–HPAM–inorganic system was almost the same as that in the individual oil emulsion composition, which might be due to the competition between the HPAM and the oil emulsion. We carried the experiments of adsorbing HPAM and oil for further verification. The HPAM molecule and oil emulsion were both electronegative and they would contend for the functional groups on the AEMs. As shown in Fig. S3,[†] the amount of oil emulsion adsorbing on the AEM decreased after the addition of HPAM and the adsorption quantity of HPAM also decreased slightly when mixed with oil.

The membrane resistances of all the CEMs had no remarkable increase compared to that of the AEMs. The membrane resistances of both the separate inorganic and oil emulsion systems increased less than 15% compared to that of the basic virgin CEM, but after combining with HPAM, the values increased somewhat. That is to say, the CEMs were more resistant to the negatively charged foulants, indicating that electrostatic interaction dominated in the fouling process.

Fig. 4 showed the contact angles of different sides of the fouled membranes. The dilute side of the membrane refers to the side facing the dilute compartments (chamber 4). Similarly, the concentrated side refers to the side facing the concentrated compartment (chamber 3). As seen in Fig. 4a, the contact angle of the dilute side of the AEM decreased after HPAM fouling compared with that of the virgin and inorganic component-fouled AEMs. As the HPAM is electronegative, it would move towards the dilute side of the AEMs under the extra electric field. In addition, the HPAM molecule was larger than the membrane pore. Therefore, the HPAM accumulated and formed a gel layer on the dilute side of the AEM. Moreover, the HPAM molecules were rich in hydrophilic groups, such as carboxyl groups, with smaller contact angles than that of the AEMs, which led to the hydrophilization of the HPAM-fouled AEMs.⁴⁵

Similarly, negatively charged emulsified oil droplets formed a dense fouling layer on the dilute side of the AEM, but the contact angle of this side increased after the fouling because the

oil emulsion was hydrophobic. The contact angle on the dilute side of the AEMs in the oil emulsion–HPAM–inorganic solution significantly increased compared to that on the virgin AEM, but it decreased in the HPAM–inorganic solution, demonstrating that the oil emulsion fouled the dilute side of the AEM. As shown in Fig. 4b, the oil emulsion–HPAM–inorganic composite was basically consistent with the HPAM–inorganic composite in terms of the contact angles on the dilute side of the CEMs. However, the contact angle of the former was much higher than that on the concentrated side of the CEM, which indicated that the dilute side was mainly fouled by inorganic component and oil emulsion dominated in fouling the concentrate sides of the CEM.

3.2 The effect of different cleaning methods

The polymer flooding wastewater has complex components and the fouling on IEMs is complicated. A set of cleaning experiments were firstly carried out to find out the suitable cleaning method aimed at the appointed foulant. Then the most efficient cleaning protocol was explored for oil–HPAM–inorganic fouled membranes. The desalination rate, area resistance and contact angle of the cleaned were measured to assess the cleaning effects.

3.2.1 Cleaning of HPAM, oil and HPAM–inorganic foulants.

Fig. 5 showed the effects of acid cleaning and base cleaning on the recovery of desalination performance and membrane resistance of HPAM-fouled membranes. The desalination rate only increased 3% after water cleaning, but the rate significantly recovered to 78.42% after acid cleaning and 83.86% after base cleanings. The membrane resistances decreased to some extent after chemical cleaning and NaOH solution exhibited better cleaning effect. The SEM images in Fig. S5[†] showed that base cleaning can effectively remove the HPAM foulant.

The cleaning effect of SDBS on the oil emulsion fouled membranes was shown in Fig. 6. The SDBS cleaning displayed excellent cleaning performances on the oil emulsion fouled IEMs with an increase of desalination rate of 33.63%. The membrane resistance of the fouled AEM decreased obviously after cleaning and the resistance of CEM restored to the original value, which was in accordance with the result of desalination performance that the SDBS could efficiently clean the oil fouled membranes.

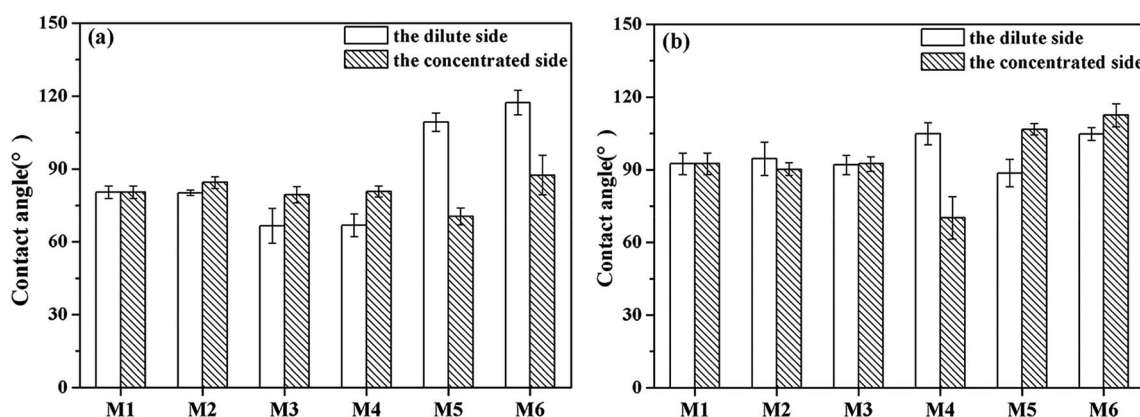


Fig. 4 Effect of the membrane fouling on the contact angles of the IEMs: (a) AEM and (b) CEM.



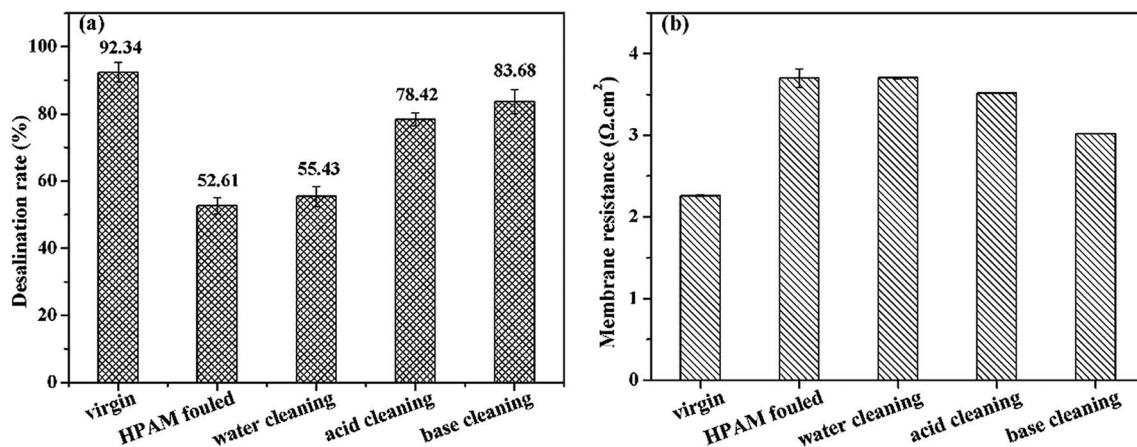


Fig. 5 Recovery of (a) desalination performance of ED stack and (b) membrane resistances of the cleaned AEMs fouled by HPAM.

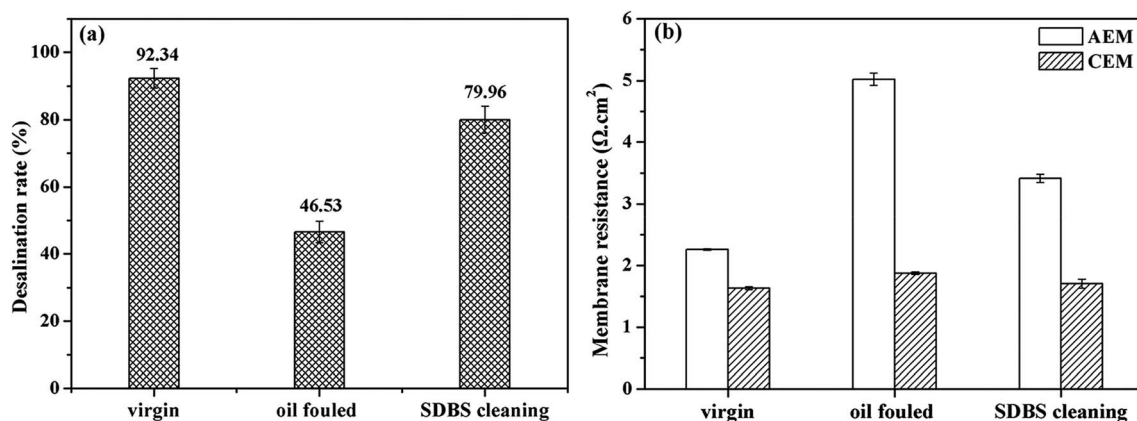


Fig. 6 Recovery of (a) desalination performance of ED stack and (b) membrane resistances of the cleaned IEMs fouled by oil emulsion.

Fig. 7 presented the results of cleaning of HPAM-inorganic fouled IEMs. We have known that both acid and base cleaning presented effects on restoring the performance of the HPAM fouled IEMs. In addition, acid solution can remove the inorganic scale. As for the HPAM-inorganic fouled membranes, the

inorganic scale and some HPAM could be cleaned firstly by HCl, and the followed base cleaning removed the remained HPAM. Therefore, the acid–base cleaned membranes showed the best recovery of desalination performance and membrane resistance (see Fig. S5e†).

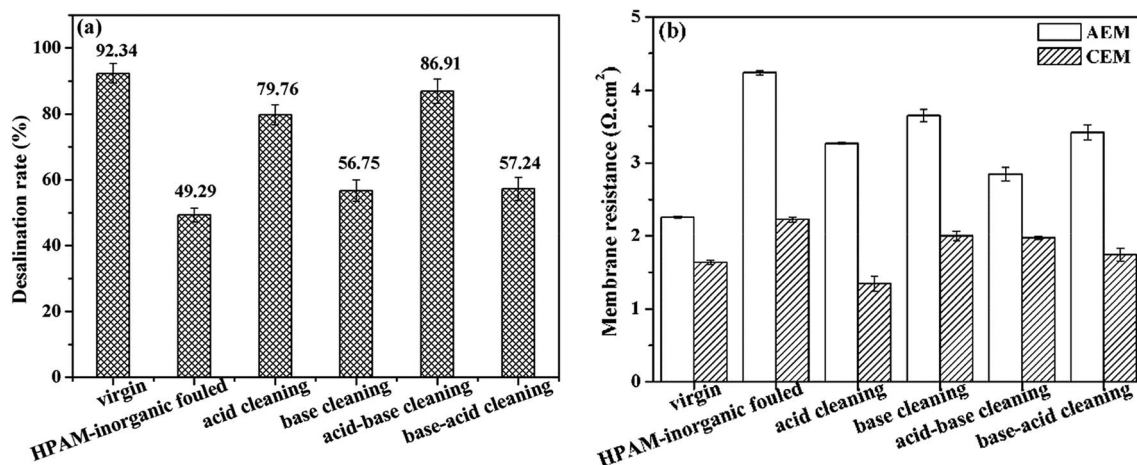


Fig. 7 (a) Desalination performances and (b) membrane resistances of the cleaned IEMs fouled by HPAM-inorganic components.



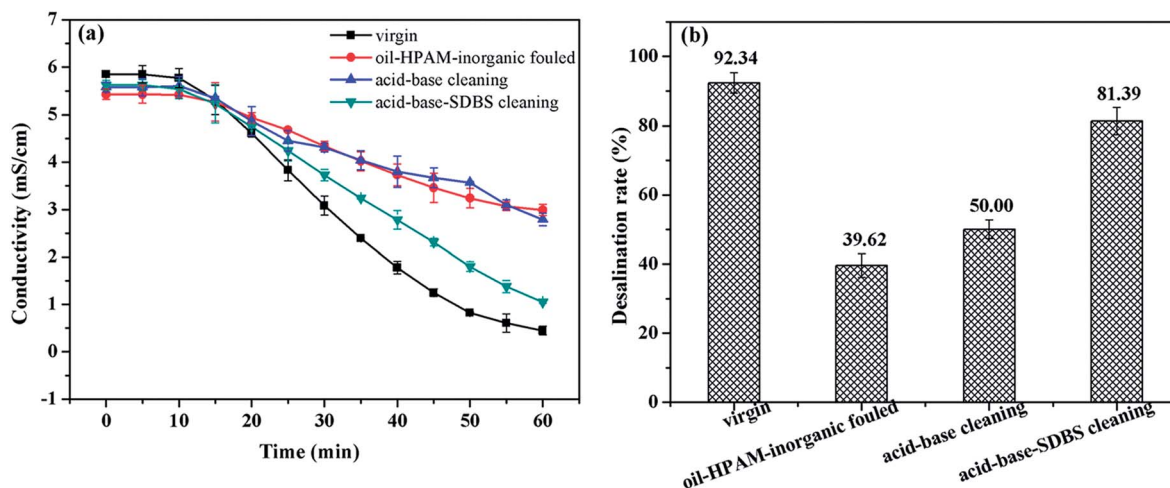


Fig. 8 Recovery of the desalination performance of ED after cleaning the oil emulsion-HPAM-inorganic fouling: (a) time dependence of the conductivity in dilute solutions; (b) desalination rate of ED.

3.2.2 Cleaning of membranes fouled by oil-HPAM-inorganic component. According to the studies mentioned above, the SDBS cleaning and HCl combined with NaOH cleaning displayed excellent cleaning performances on the oil emulsion and HPAM-inorganic-fouled IEMs, respectively. Hence, chemical cleaning methods, including acid-base cleaning and acid-base-SDBS cleaning, were utilized to thoroughly investigate their cleaning effects on the oil-HPAM-inorganic fouling.

The decrease in conductivity of the dilute solutions and the desalination rates at 60 min for the cleaned IEMs were presented in Fig. 8.

As we can see in Fig. 8, the virgin IEMs exhibited the highest desalination capacity with the lowest dilute solution conductivity and highest desalination rate. The oil-HPAM-inorganic-fouled IEMs exhibited the worst desalination performance. The desalination performance recovered to 81.39% from 39.62% in the fouled IEMs after the acid-base-SDBS cleaning (see Fig. S5†). However, the acid-base cleaning method only had a slight effect on the recovery of the desalination performance with a poor desalination rate of 50.00%.

As shown in Fig. 9, the membrane resistances of the AEMs sharply increased by 124.57% because of the oil-HPAM-inorganic fouling. In addition, after the acid-base-SDBS cleaning, the value decreased to $3.82 \Omega \text{ cm}^2$, which was only 64.65% higher than that of the virgin AEMs. However, the value only decreased $0.37 \Omega \text{ cm}^2$ after the acid-base cleaning compared with that of the fouled AEMs and was still 108.62% higher than that of the virgin ones. The results were consistent with the desalination performances and indicated that the acid-base cleaning could only eliminate the HPAM and inorganic fouling layers. The subsequent SDBS cleaning played an important role in removing the dominant oil emulsion layer and recovering the membrane properties.

However, for the CEMs, the membrane resistances of the fouled membranes were only 43.29% higher than that of the virgin ones. This indicated that the CEMs were not seriously fouled by the oil-HPAM-inorganic complex. Moreover, the

membrane resistance almost recovered to that of the virgin level after the acid-base and acid-base-SDBS cleaning. Therefore, it was concluded that the oil-HPAM-inorganic complex had little effect on the CEMs.

The results of the contact angle measurements were presented in Fig. 10. For the AEMs, the contact angles of the dilute side increased nearly 40° , while those of the concentrate side increased by 10° compared to that of the virgin AEMs (see Fig. 8a and b). In addition, after the chemical cleaning, the contact angles of the concentrated side almost returned to that of the virgin level. However, only the acid-base-SDBS cleaning resulted in the same recovery effect, and the acid-base cleaning had limited effects for the recovery of the contact angle.

We previously knew that the oil-HPAM-inorganic complex would severely foul the dilute side of the AEMs and that the oil emulsion dominated the fouling procedure. As a result, the contact angle of the dilute side obviously recovered after the acid-base-SDBS cleaning, but limited improvement was observed after the acid-base cleaning. In contrast, the concentrated side was not badly fouled by the oil emulsion, and the contact angle was basically recovered after the acid-base cleaning.

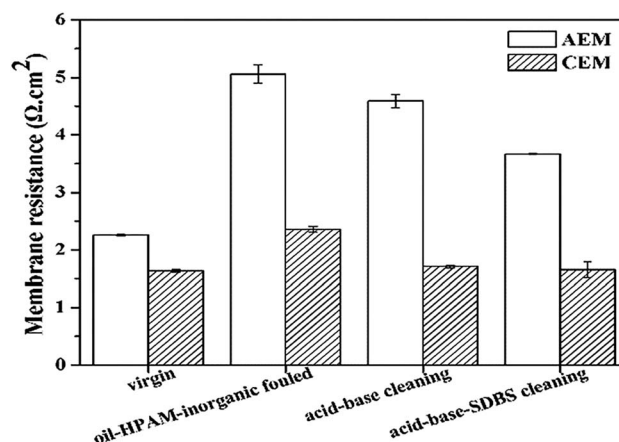


Fig. 9 Recovery of the membrane resistances of the IEMs after cleaning the oil emulsion-HPAM-inorganic fouling.



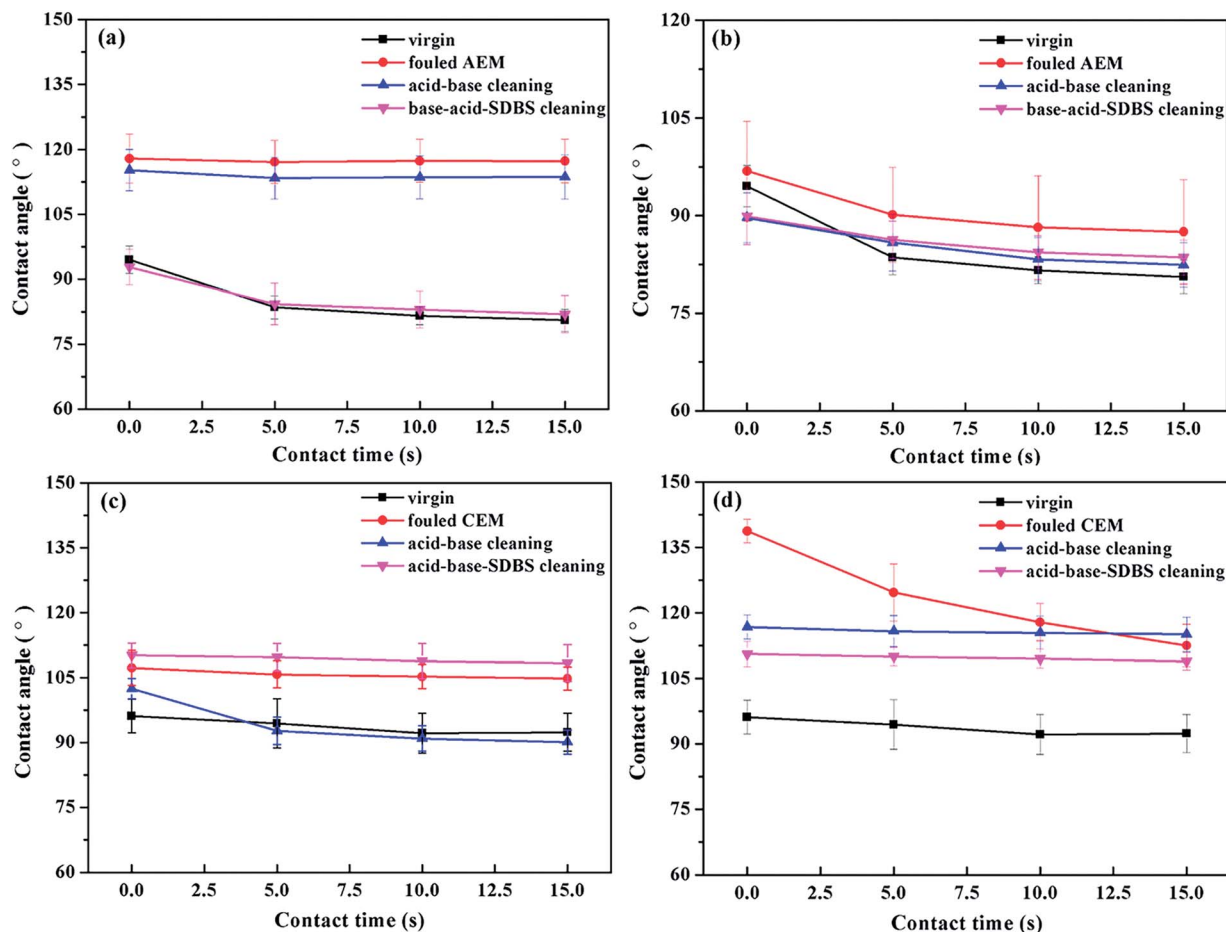


Fig. 10 Contact angles of the oil emulsion-HPAM-inorganic-fouled and cleaned IEMs: (a) AEMs, dilute side, (b) AEMs, concentrated side, (c) CEMs, dilute side and (d) CEMs, concentrated side.

For the CEMs, the contact angles on both sides of the fouled CEMs increased significantly, as shown in Fig. 10c and d. As shown in Fig. 4b, the dilute sides of the CEMs were mostly fouled by the HPAM-inorganic ingredient, so the acid-base cleaning could effectively eliminate the gel layer and the inorganic layer. Hence, the contact angle almost recovered to that of the virgin level after the acid-base cleaning. However, with the subsequent SDBS cleaning, the sulfonic groups of the SDBS molecules and the immobilization groups of the CEM formed an affinity effect, and the long chains of the alkyl groups of the SDBS resulted in a larger contact angle on the dilute side.

Similarly, as shown in Fig. 4b, the oil emulsion component was dominant during the fouling process of the CEMs on the concentrated side. Meanwhile, because of the electrostatic repulsion between the oil droplets and the CEM, the oil emulsion fouling layer was relatively loose and randomly distributed, which led to unstable contact angles on the concentrated side. In addition, the values in Fig. 10d also showed that the fouling layer was effectively removed by the acid-base-SDBS cleaning. However, the contact angle was still larger than that of virgin CEM because of the affinity between the sulfonic acid groups of SDBS and the CEM.

3.2.3 FTIR spectra. The functional groups of the IEMs were further detected using an attenuated total reflectance-Fourier transform infrared (ATR-FTIR) spectrometer, and the FTIR spectra of both sides of the oil emulsion-HPAM-inorganic-fouled IEMs before and after the chemical cleaning are presented in Fig. 11.

As shown in Fig. 11a, all the spectral lines had absorption peaks at 1608 cm^{-1} , 1465 cm^{-1} , 1306 cm^{-1} and 1190 cm^{-1} , corresponding to the C-C stretching vibration of the aromatic ring, the asymmetric bending vibration of the C-H bond in CH_2 , the out-of-plane deformation swing of the C-H bond in CH_2 and C-O-C stretching vibration of the ethers, respectively, which were from the matrix of the polyphenylene ether IEMs.

Compared to that of the virgin membranes, new group frequency absorption peaks appeared at multiple positions for both the dilute and concentrated sides of the fouled membranes. Characteristic peaks for alkanes from crude oil, such as the C-H asymmetric stretching vibration at 2923 cm^{-1} and symmetrical stretching vibration at 2855 cm^{-1} , were observed. The asymmetric stretching vibration at 1120 cm^{-1} of the S=O bond in the sulfonic acid group and the stretching vibration at 1660 cm^{-1} of the C=O bond in the amide group indicated the existence of SDBS and HPAM molecules. The



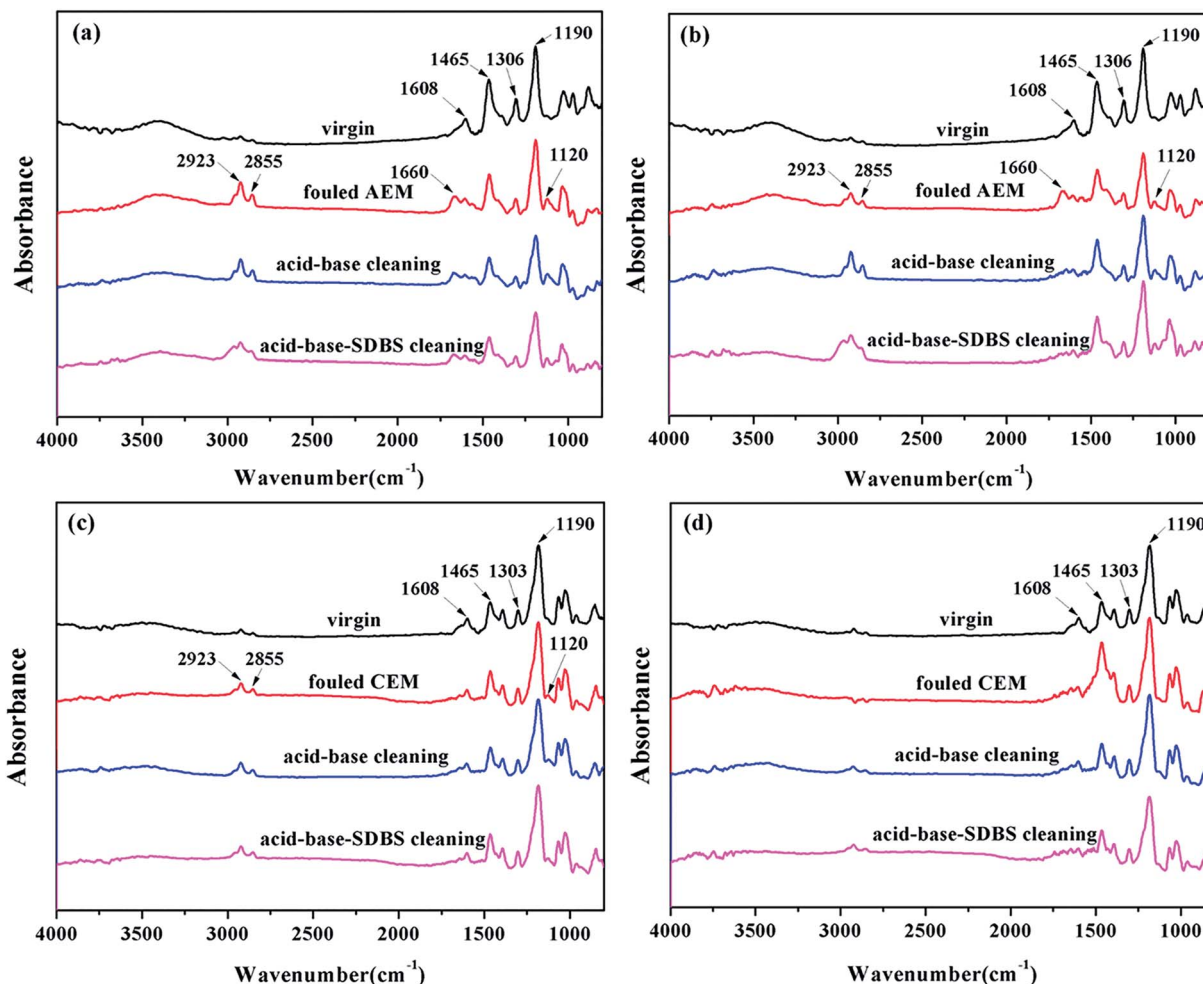


Fig. 11 IR spectra of the IEMs after cleaning the oil emulsion-HPAM-inorganic fouling: (a) AEMs, dilute side, (b) AEMs, concentrated side, (c) CEMs, dilute side and (d) CEMs, concentrated side.

results demonstrated that both sides of the AEM were subjected to oil emulsion and HPAM fouling. The difference was the absorption peak at 1660 cm^{-1} on the concentrated side disappeared after the chemical cleaning, and the corresponding peak still remained on the dilute side, which illustrated that the dilute side was more severely fouled by the organic component and more difficult to clean by chemical cleaning.

Similarly, as shown in Fig. 11c, a new peak did not appear on the dilute side of the oil-HPAM-inorganic-fouled CEMs, and no apparent changes were observed after the chemical cleaning. However, as shown in Fig. 11d, absorption peaks at 2923 cm^{-1} and 2855 cm^{-1} , corresponding to the C-H stretching vibrations from crude oil, and 1120 cm^{-1} , corresponding to the S=O asymmetric stretching vibration, indicated that oil emulsion fouled the concentrated side of the CEMs. Meanwhile, after the chemical cleaning, the oil emulsion fouling was not completely removed because the new absorption peaks were still present.

No obvious difference was observed in the IEMs after the acid-base-SDBS cleaning compared to those after the acid-base cleaning. This was probably because the oil emulsion fouling was not completely removed.

3.3 Fouling route and cleaning theory

According to all the experimental results, scheme of the fouling route and cleaning mechanism was presented in Fig. 12. The AEMs were mainly fouled by HPAM and oil on the dilute side due to electrostatic attraction. Meanwhile, the inorganic component could synergize the fouling of HPAM because Ca^{2+} can form coordination bond by means of complexation reaction with the HPAM molecules. The CEMs were more susceptible to inorganic scales. Oil emulsion also fouled the CEMs on the concentrated side. HCl can expedite the protonation of HPAM molecules, *i.e.*, changing more carboxylates into carboxyl groups and reducing the electronegativity of HPAM, which abates the electrostatic interactions between HPAM and the IEMs. Consequently, a portion of the contaminated layer would be eliminated by the acid cleaning. On the other hand, sodium hydroxide can effectively disintegrate the gel layer by reacting with the carboxyl and amide groups of HPAM. Simultaneously, an increase in the electronegativity under alkaline conditions aggravated the intermolecular repulsion between the HPAM molecules, which caused the loose fouling layer to detach from the membrane surface. As a consequence, the acid-base



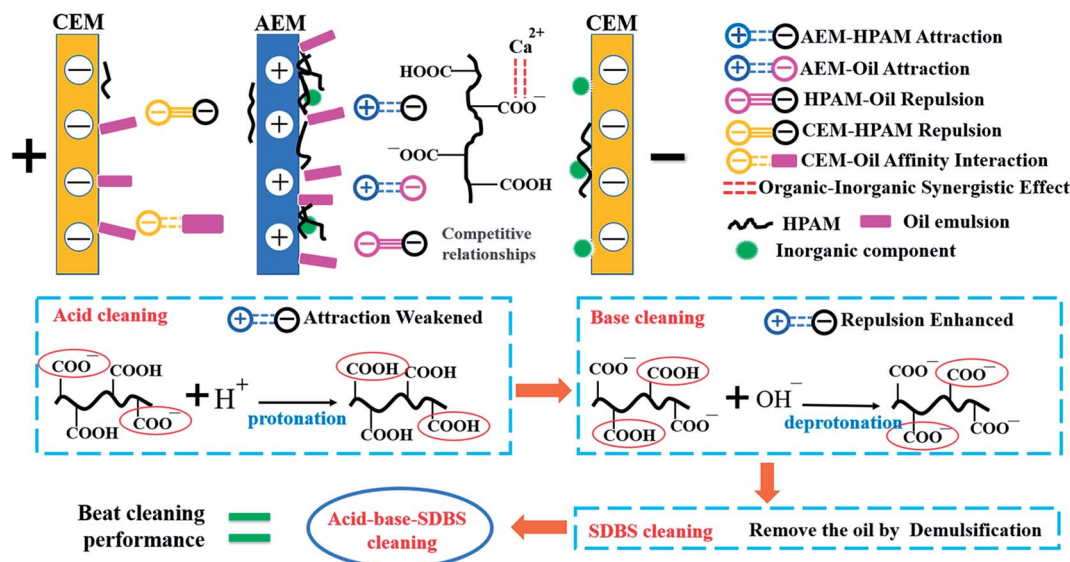


Fig. 12 Schematic diagram of the fouling route and cleaning theory.

cleaning can eliminate the gel layer and the inorganic fouling layer. However, it had little effect on the oil emulsion layer, which led to the poor recovery of the desalination rate.

As shown in Fig. 2, the oil emulsion-fouled IEMs exhibited the lowest desalination compared with that of the inorganic-fouled, HPAM-fouled and HPAM-inorganic-fouled IEMs. The oil emulsion layer was dominant in the oil-HPAM-inorganic-fouled IEMs, which agreed with the poor cleaning effect of the acid-base cleaning. SDBS, an anionic surfactant with excellent demulsification abilities, which can effectively remove the oil emulsion layer, was subsequently adopted to recover the oil-HPAM-inorganic-fouled IEMs after the acid-base cleaning. As a result, the desalination performance of the fouled IEMs significantly recovered.

4 Conclusions

In this study, the fouling of IEMs in flooding wastewater treatments and the effects of different chemical cleaning methods were investigated. The desalination rate, membrane resistance, contact angles and ATR-FTIR were used for the characterization of the fouled and cleaned IEMs.

Fouling experiments indicated that inorganic components could combine with HPAM to foul the IEMs, which was demonstrated by lower desalination rates and higher membrane resistances compared with that of the IEMs with inorganic fouling and HPAM fouling. Moreover, the oil emulsion intensified the HPAM-inorganic fouling as the IEMs fouled by the oil emulsion-HPAM-inorganic components showed the lowest desalination performance and the oil emulsion prevailed in fouling the dilute side of the AEM. The inorganic component dominated in fouling the dilute side of the CEM while the concentrated side mostly suffered oil fouling.

Cleaning experiments were conducted to restore the fouled membranes. The desalination rate and other indicators of HPAM fouled IEMs were significantly recovered after acid

cleaning and base cleaning. Membranes fouled by the HPAM-inorganic component and oil emulsions were effectively cleaned by the acid-base and SDBS cleaning, respectively. The acid-base-SDBS cleaning method achieved an excellent cleaning effect on the oil-HPAM-inorganic-fouled IEMs with an increase of 36.45% in the desalination performance. The results of ATR-FTIR spectra indicated that the dilute side of the AEM was more severely fouled by the organic component (oil emulsion and/or HPAM) than the concentrated side and difficult to cleaning by chemical cleaning.

Conflicts of interest

There are no conflicts to declare.

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