The influence of composition on the functionality of hybrid CuO–ZnO–Al2O3/HZSM-5 for the synthesis of DME from CO2 hydrogenation

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A series of CuO–ZnO–Al2O3/HZSM-5 hybrid catalysts with different Cu/Zn ratios and disparate Al2O3 doping were prepared and characterized by XRD, BET, H2-TPR, NH3-TPD and XPS techniques. The optimal Cu/Zn ratio is 7 : 3, and the introduction of a suitable amount of Al2O3 to form hybrid catalysts increased the BET specific area and micropore volume, facilitated the CuO dispersion, decreased the CuO crystallite size, increased the interaction between CuO and ZnO, enhanced the number of weak acid sites, altered the copper chemical state and improved the catalytic performance consequently. The highest CO2 conversion, DME selectivity and DME yield of 27.3%, 67.1% and 18.3%, respectively, were observed over the CZA7H catalyst. The suitable temperature of 260 °C and the appropriate space velocity of 1500 h⁻¹ for one-step synthesis of dimethyl ether (DME) from carbon dioxide (CO2) hydrogenation were also investigated. The 50 h stability of the CZA7H catalyst was also tested.

1. Introduction

CO2 emission is increasing at an unparalleled rate due to fossil fuel combustion in recent years. As a consequence, excessive CO2 release leads to a series of problems such as global warming and environmental pollution. Therefore, CO2 recycling and utilization are very imperative. CO2 hydrogenation to dimethyl ether (DME) is an excellent option.

DME is attracting more and more interest as a green fuel because it produces less CO, NOx, and SO2 particulates when combusted. Therefore, DME is considered as a potential environmentally friendly alternative option to petrol diesel for diesel engines. Meanwhile, DME, as a vital chemical intermediate, can also be used to prepare diversified valuable chemical products especially esters and lower olefins. Furthermore, it can be utilized in several fields, for example, in fuel additives of diesel, home heating and cooking gas, and pro-environmental refrigerants.

The hydrogenation of CO2 to DME over a hybrid catalyst for DME synthesis is principally composed of three independent reactions, methanol synthesis from CO2 hydrogenation (CO2 + 3H2 \rightarrow CH3OH + H2O reaction 1), methanol dehydration to form DME (2CH3OH \rightarrow CH3OCH3 + H2O reaction 2), and a reverse water gas shift reaction (RWGS) (CO2 + H2 \rightarrow CO + H2O reaction 3). DME can be produced via a two-step process including reaction 1 on a copper based catalyst and subsequent reaction 2 over a solid acid catalyst. Furthermore, one-step process (performing the two steps simultaneously over a hybrid catalyst) has a better performance as a thermodynamically favorable course because the equilibrium limitation of reaction 1 can be readily overcome by reaction 2.

Currently, hybrid catalysts of methanol synthesis component and methanol dehydration component are applied to the one-step direct DME synthesis from CO2. The methanol dehydration components are generally solid acid catalyst such as γ-Al2O3, but the active sites of the γ-Al2O3 is Lewis acid sites which are favored for water adsorption, resulting in a significant reduction of the amount of acidic sites and then a decrease of catalytic activity. Another intriguing solid acid catalyst is WO3/ZrO2, but the catalytic activity of WO3/ZrO2 is lower due to its weaker acid strength present.

Besides, SAPO-18 has been used as acid function owing to its uniform microporous structure and a high stability, but SAPO-18 possesses a large number of moderate strength acid sites, which cause catalyst deactivation as well as undesired products by coke deposition. By contrast, HZSM-5 is the most suitable acidic component due to its more hydrophobic character and advantage of Brønsted acidity, which significantly reduces the impact of water on HZSM-5. Furthermore, HZSM-5 possesses weak acid sites which are in favor of methanol dehydration to DME at low temperatures and exhibits high catalytic activity. However, the methanol synthesis components of the hybrid catalysts are various, and the Cu–Zn based catalyst is regarded as the most promising binary catalyst among them. Xia et al. reported the deposition of Zn on the surface of copper can increase surface area and can form a unique site at the Cu–ZnO interface to improve the
adsorption of CO₂ and catalyst activity. To further improve the performance of the Cu–Zn bimetallic compound catalyst, adding an amphoteric metal oxide species as additive to Cu–Zn based catalyst is an efficient method. Al₂O₃ is a prospective co-catalyst of sufficient attraction due to its mechanical and thermal stability, its excellent dispersion feature of copper and zinc. Nevertheless, only a few literatures have reported Al₂O₃ as thermal stability, its excellent dispersion feature of copper and zinc oxide/aluminum catalyst, and found that the combustion processes and physicochemical properties of catalysts depend strongly on the type and amount of fuel. Although CuO was used in the catalytic reduction of NO, the overall selectivity of the product (DME, MeOH, CO) and the selectivity of CO₂, the selectivity of the product (DME, MeOH, CO) and the yield of DME, respectively. Each experimental data was corresponds to an average of three independent measurements, with error of ±2%.

\[
X_{\text{CO}_2} = \frac{\text{CO}_2\text{in} / N_2\text{in} - \text{CO}_2\text{out} / N_2\text{out}}{\text{CO}_2\text{in} / N_2\text{in}} 
\]

\[
S_{\text{P}} = \frac{P_{\text{in}}}{1 - \text{CO}_2\text{out}} 
\]

2. Experimental

2.1 Preparation of CuO–ZnO/HZSM-5 catalysts

A series of CuO–ZnO/HZSM-5 catalysts of diverse Cu/Zn molar ratio were prepared, aiming at confirming optimum composition. Cu(NO₃)₂·3H₂O, Zn(NO₃)₂·6H₂O (Cu/Zn molar ratio ranging from 2:8 to 8:2) were dissolved in ethanol to gain the metal nitrates solution and coprecipitated by oxalate under vigorous stirring at 60 °C in a solution containing the HZSM-5 finely dispersed, with a final CuO–ZnO : HZSM-5 weight ratio of 2 : 1, for convenience of comparison with previous work. The HZSM-5 with a SiO₂/Al₂O₃ ratio of 38 was purchased from Catalyst Plant of Nankai University (China). The slurry was heated to 80 °C and was aged for 2 h under stirring. Subsequently, the slurry was evaporated at the same temperature. Then the obtained product was dried in muffler furnace at 120 °C for 12 h and calcined in air at 400 °C for 4 h. The final product was hybrid catalyst named as CₓZₙ₋ₓH (the x express the molar ratio of CuO : CuO–ZnO) and was pressed, crushed and griddled to get the granules (20–40 mesh).

2.2 Preparation of CuO–ZnO–Al₂O₃/HZSM-5 hybrid catalysts

Thereafter, a series of CuO–ZnO–Al₂O₃/HZSM-5 hybrid catalysts of different Al₂O₃ contents were prepared. Cu(NO₃)₂·3H₂O, Zn(NO₃)₂·6H₂O were weighed according to the optimal Cu/Zn mole ratio which was determined in the preliminary experiments. The mixture was dissolved in ethanol followed by the addition of Al(NO₃)₃·9H₂O. The amount of the Al(NO₃)₃·9H₂O used depended on the required Al₂O₃ contents of 0, 1.0, 3.0, 5.0, 7.0, 10.0 wt% in CuO–ZnO–Al₂O₃. Then, the solution of precursors was added to a vigorously stirred ethanol solution containing the oxalic acid and the powdered HZSM-5 in a constant and slow manner at 60 °C. The weight ratio of the final oxide of CuO–ZnO–Al₂O₃ to HZSM-5 is 2 : 1. The slurry was dealt with the same procedure as the CₓZₙ₋ₓH and the final product was abbreviated as CₓZₓ₋ₓH, where the y represents theoretical Al₂O₃ : CuO–ZnO–Al₂O₃ wt%.

2.3 Catalyst testing

The hybrid catalyst activity was measured in a continuous-flow fixed-bed reactor made of stainless steel (10 mm inner diameter). 1 mL of the hybrid catalyst was diluted with 0.5 mL of the quartz sand (both in 20–40 mesh). Prior to the test, the catalyst was reduced in situ in a stream of 10% H₂/N₂ at 300 °C for 3 h under atmospheric pressure. After the reduction, the reactor was cooled to room temperature under flowing N₂ and reactant gas flow (H₂/CO₂/N₂ = 3/9/1, molar) was introduced, subsequently raising the pressure to 3.0 MPa and the reaction temperature was raised to 260 °C. Analysis of the products were performed applied a gas chromatograph (SP2100A) equipped with both a TCD (for N₂, CO and CO₂, GDX-101 connected with Porapak T column) and a FID (for CH₄, CH₃OH and DME, Porapak Q column). The CO₂ conversion as well as the selectivity toward CO, CH₃OH and DME are calculated by internal standard method. \( X_{\text{CO}_2}, S_{\text{P}}, \text{and } Y_{\text{DME}} \) represent the conversion of CO₂, the selectivity of the product (DME, MeOH, CO) and the yield of DME, respectively. Each experimental data was corresponds to an average of three independent measurements, with error of ±2%.
where \( P_i \) stands for the concentration of a specific product (DME, MeOH, CO).

\[
Y_{DME} = S_{DME} X_{CO_2}
\] (3)

2.4 Catalyst characterization

X-ray powder diffraction (XRD) patterns of all samples were performed on a Rigaku D/max 2500 PC X-ray diffractometer with Cu-K\( \alpha \) radiation (\( \lambda = 1.54156 \text{ \AA} \)) at a scan rate of 4° min\(^{-1}\) at 50 kV and 250 mA.

The BET surface area of the samples was conducted by N\(_2\) adsorption at \(-196^\circ C\) using a Quantachrome Autosorb 1-C. Before the absorption–desorption measurements, samples were degassed under vacuum at 300 °C for 3 h. The specific BET \( (S_{BET}) \) was estimated from the linear part of the Brunauer–Emmett–Teller (BET) plot.

The X-ray photoelectron spectroscopy (XPS) and X-ray-induced Auger electron spectroscopy were recorded on an ESCALA 250 Xi spectrometer, using a standard Al-K\( \alpha \) X-ray source (1486.6 eV). The binding energy (BE) values were referenced to the adventitious C 1s peak (284.6 eV). Quantification of the surface atomic concentrations was carried out using the sensitivity factors supplied for the XPS instrument.

H\(_2\)-TPR of catalysts were performed on chemisorptions (ChemBET 3000). Before reduction, 0.02 g of sample was pre-heated with flowing He at 400 °C for 60 min, then cooled down room temperature. Subsequently, the temperature was raised in 10% H\(_2\)/Ar (50 mL min\(^{-1}\)) at a ramp rate of 10 °C min to 400 °C. H\(_2\) consumption was detected by TCD.

NH\(_3\)-TPD of the samples were measured on the same apparatus for H\(_2\)-TPR measurements. 0.1 g sample was heated to 400 °C and maintained for 30 min, then the temperature was cooled to 100 °C. After that, a 6 vol% NH\(_3\)/Ar mixture stream was introduced to the sample for 60 min. Then, the examined sample was flushed with helium stream (30 mL min\(^{-1}\)) for 60 min to remove the weak adsorbed NH\(_3\). The temperature was raised from 100 °C to 800 °C at a rate of 10 °C min.

3. Results and discussion

3.1 The effect of the Cu/Zn molar ratio on the catalytic performance of C\(_x\)Z\(_{1-x}\)H catalysts

In order to investigate the optimal Cu/Zn molar ratio of the hybrid catalysts, a series of C\(_x\)Z\(_{10-x}\)H catalysts were prepared. The catalytic performances of catalysts with different Cu/Zn molar ratio were summarized in Table 1. The CO\(_2\) conversion, DME selectivity and the yield of DME increased with the Cu/Zn increased from 2 : 8 to 7 : 3, and decreased if continue raising the Cu/Zn to 8 : 2. The C\(_7\)Z\(_3\)H exhibited the maximum CO\(_2\) conversion, DME selectivity and DME yield values of 19.2%, 47.8% and 9.2%, respectively. The result revealed the Cu/Zn molar ratio can affect the catalytic performance and the optimal Cu/Zn molar ratio of the hybrid catalysts was 7 : 3.

<table>
<thead>
<tr>
<th>Catalyst</th>
<th>Conversion of CO(_2)%</th>
<th>Selectivity/%</th>
<th>Yield/%</th>
<th>DME</th>
</tr>
</thead>
<tbody>
<tr>
<td>C(_2)Z(_7)H</td>
<td>16.06</td>
<td>25.41</td>
<td>5.34</td>
<td>67.35</td>
</tr>
<tr>
<td>C(_2)Z(_6)H</td>
<td>16.44</td>
<td>27.04</td>
<td>8.03</td>
<td>63.14</td>
</tr>
<tr>
<td>C(_2)Z(_5)H</td>
<td>17.71</td>
<td>36.71</td>
<td>5.23</td>
<td>56.16</td>
</tr>
<tr>
<td>C(_2)Z(_4)H</td>
<td>17.46</td>
<td>37.73</td>
<td>5.22</td>
<td>55.22</td>
</tr>
<tr>
<td>C(_2)Z(_3)H</td>
<td>18.06</td>
<td>38.42</td>
<td>6.01</td>
<td>53.70</td>
</tr>
<tr>
<td>C(_2)Z(_2)H</td>
<td>19.20</td>
<td>47.80</td>
<td>1.70</td>
<td>47.80</td>
</tr>
<tr>
<td>C(_2)Z(_1)H</td>
<td>18.36</td>
<td>39.55</td>
<td>5.15</td>
<td>53.49</td>
</tr>
</tbody>
</table>

Table 1  Catalytic performance of the C\(_x\)Z\(_{10-x}\)H Hybrid catalysts

3.2 Catalytic performance of the CZA\(_x\)H catalysts

The catalytic performances of the CZA\(_x\)H catalysts with different Al\(_2\)O\(_3\) contents were listed in Table 2. DME was the major product and the by products included CO and methanol under the reaction temperature of 260 °C, pressure of 3.0 MPa and GHSV of 1500 h\(^{-1}\). Moreover, several hydrocarbons such as CH\(_4\) were also detected. The catalytic performances of the Al\(_2\)O\(_3\)-modified hybrid catalysts were enhanced enormously compared with the Al\(_2\)O\(_3\)-free hybrid catalyst. With the Al\(_2\)O\(_3\) contents increase in the catalysts (range from CZA\(_{10}\)H to CZA\(_{7}\)H), the CO\(_2\) conversion, DME selectivity and the DME yield increased significantly. Further increasing the contents of Al\(_2\)O\(_3\) (CZA\(_{10}\)H) decreased the catalysts activity. The CZA\(_{7}\)H catalyst exhibited the highest catalyst performance and a maximum CO\(_2\) conversion of 27.3% with a DME selectivity of 67.1% and a yield of DME of 18.3%, as shown in Table 2. The DME yield and the DME selectivity of CZA\(_{7}\)H catalyst were appreciably in comparison of nearly 13.5% and 63.4%, respectively, obtained over CuO–ZnO–ZrO\(_2\)/HZSM-5 catalyst reported by Li et al.\(^{24}\) Meanwhile, the DME selectivity of 67.1% for CZA\(_{7}\)H catalyst was significantly higher than 49.2% observed over CuO–ZnO–Al\(_2\)O\(_3\)/HZS-5 catalyst studied by Zhang et al.\(^{31}\) These results indicated suitable Al\(_2\)O\(_3\) additive can improve the catalyst performance significantly.

Fig. 1 shows the effect of reaction temperature on the catalytic performance of CZA\(_{7}\)H catalyst. It can be found that volcanic shape change trends of the CO\(_2\) conversion, DME selectivity and the yield of DME versus the variation of the
temperature. With the temperature rising from 220 °C to 260 °C, the conversion of CO₂, the selectivity of the DME and the DME yield increased obviously 12.7%, 2.7% and 8.9%, respectively, and then reduced sharply when the reaction temperature reached 280 °C. Comparing the catalytic performance data at several reaction temperatures, the optimal catalytic performance for the CZA-H catalyst were obtained at 260 °C. These results can be explained by the hydrogenation of CO₂ for synthesis of DME was a reversible exothermic reaction, the reverse reaction favored with an excessive temperature. Meanwhile, the main side reaction RWGS was an endothermic reaction thus the CO selectivity increased and the selectivity and yield of DME decreased with the reaction temperature higher than 260 °C. In addition, the CZA-H catalyst activity may also decrease due to the Cu sintered and crystallized gradually with the conversion of CO₂, the selectivity of the DME and the DME yield increased obviously 12.7%, 2.7% and 8.9%, respectively, as the space velocity increased from 1500 to 3000 h⁻¹. With the space velocity increasing, the contact time between reactants and the catalyst becomes short, consequently both the CO₂ hydrogenation to methanol and methanol dehydration to DME reactions could not proceed sufficiently. Therefore, the conversion of CO₂ and the selectivity of the DME reduced distinctly indicating the efficient effect the space velocity on the catalytic performance.

3.3 Stability of the CZA₇H catalyst

The stability of CZA₇H catalyst was studied for the reaction of DME synthesis via CO₂ hydrogenation at 260 °C and 3.0 MPa with GHSV = 1500 h⁻¹. The stability results were recorded every 2 h, as shown in Fig. 3. It can be found that the CO₂ conversion of and the DME selectivity decrease slightly from 27.3% and 67.1% to 25.3% and 62.1% during the continuous 50 h reaction process, respectively. The result indicated that the CZA-H catalyst possessed better catalytic performance and stability.

3.4 The structure of the catalysts

Fig. 4 illustrates the XRD patterns of a series of CZA₇H catalysts with different Al₂O₃ contents before H₂ reduction. For all catalysts, the diffraction peaks at 2θ = 35.5°, 38.7°, 48.7°, 53.4°, 58.2°, 61.5°, 66.2°, 72.3° and 74.9° can be ascribed to CuO phase (JCPDS no. 48-1548), the peaks at 2θ = 31.7°, 34.3°, 36.1°, 47.4°, 56.5°, 62.8° and 67.8° can be attributed to ZnO phase (JCPDS no. 65-3411), and the peaks appear in the 2θ range of 21–25° can be matched to HZSM-5 (JCPDS no. 44-0003). The peaks corresponding to Al₂O₃ phase cannot be observed, indicating that the presence of Al₂O₃ were amorphous phase or highly dispersed in the catalyst body phase. Compared with the peaks of catalyst CZA₇H, the peaks of catalysts with Al₂O₃ become weaker, indicating the CuO–ZnO oxides possess less intensive crystallinity. The diffraction peaks of CuO and ZnO weakened and broadened gradually with the increasing of Al₂O₃ contents, even some diffraction peaks of CuO and ZnO phase disappeared, suggesting the decrease of grain size. The grain sizes of CuO (dCuO) and ZnO (dZnO) for CZA₇H catalysts calculated by Scherrer’s equation are listed in Table 3. These results indicated obviously that the additive of Al₂O₃ can improve the CuO dispersion and
can decrease the grain size of CuO. For all catalysts, the grain size of ZnO phase is greater than that of CuO phase, indicating ZnO phase closely relates to CuO phase. Shimokawabe et al. considered the grain size of ZnO is larger than CuO due to CuO can be well dissolved on the ZnO particles. As a consequence, the active interface increased with the improving the dispersion of CuO. Fig. 5 shows the XRD patterns of the reduced CZA0H and CZA7H catalysts. For these two catalysts, the diffraction peaks at $2\theta = 43.3^\circ, 50.4^\circ$ and $74.1^\circ$ can be ascribed to metallic copper phase (JCPDS no. 04-0836). No diffraction peaks of CuO can be detected, indicating all CuO in the catalysts reduced to Cu. The intensity of diffraction peaks of Cu for reduced CZA7H catalyst decrease significantly, compared to the corresponding peaks for CZA0H catalyst. Furthermore, the grain size of Cu decreased significantly for CZA7H catalyst. As shown in Table 3, and the grain sizes of Cu ($d_{\text{CuO}}$) which calculated by Scherrer’s equation for reduced CZA0H and CZA7H are 21.4 nm and 9.7 nm, respectively. These results suggest that the addition of Al2O3 can effectively inhibit the Cu crystals growth.

The BET Surface areas ($S_{\text{BET}}$) and the calculated average pore diameter of the catalysts are also listed in Table 3. The $S_{\text{BET}}$ of the catalysts approximately increases from 131.7 m$^2$ g$^{-1}$ to 161.2 m$^2$ g$^{-1}$ with the increasing of Al2O3 contents (from CZA0H to CZA7H), then sharply decreases to 143.5 m$^2$ g$^{-1}$ when the Al2O3 contents continuing increasing (CZA10H). The variation trend of the micropore volumes is the same as the $S_{\text{BET}}$ while the trend of average pore diameter of the catalysts is contrary to the $S_{\text{BET}}$ generally. These results illustrate that the pore structure of the hybrid catalysts can be changed by the introduction of Al2O3. Meanwhile, a maximum $S_{\text{BET}}$ of 161.2 m$^2$ g$^{-1}$ and a minimum average pore diameter of 6.8 nm are detected for the CZA7H catalyst which possesses the smallest grain sizes of Cu ($d_{\text{Cu}}$), as determined from XRD. The result revealed that why the catalyst of CZA7H exhibited the maximum of the CO2 conversion, the DME selectivity and the DME yield simultaneously.

### 3.5 The reducibility of the catalysts

TPR measurements were carried out in order to evaluate the reduction behavior of all the catalysts. Fig. 6 shows the H2-TPR profiles of the CZAxH catalysts with different Al2O3 contents. It can be found only a single reduction peak with any satellite peaks for all the catalysts. The result illustrate the opinion the copper oxides on the CZAxH catalysts are easy to be reduced. Since ZnO and Al2O3 cannot be reduced under the experimental condition, the single high temperature reduction peak can be ascribed to the reduction of CuO species with strongly interaction with ZnO and Al2O3. With Al2O3 content increasing, the reduction peak maximum firstly shifted towards higher temperature from CZA0H to CZA7H catalysts, and then shifted towards lower temperature for CZA10H, as shown in Fig. 6. The CZA7H catalyst possessed the highest reduction temperature at 373 °C, which indicated the strongest interaction between the catalysts.

<table>
<thead>
<tr>
<th>Catalyst</th>
<th>$S_{\text{BET}}$(m$^2$ g$^{-1}$)</th>
<th>$V_1$ (Micropore volume)/(cm$^3$ g$^{-1}$)</th>
<th>$D$ (Average pore diameter)/nm</th>
<th>$d_{\text{CuO}}$/nm</th>
<th>$d_{\text{Cu}}$/nm</th>
<th>$d_{\text{ZnO}}$/nm</th>
</tr>
</thead>
<tbody>
<tr>
<td>CZA0H</td>
<td>131.7</td>
<td>0.032</td>
<td>8.0</td>
<td>20.4</td>
<td>21.4</td>
<td>29.1</td>
</tr>
<tr>
<td>CZA1H</td>
<td>132.1</td>
<td>0.024</td>
<td>8.7</td>
<td>15.4</td>
<td>—</td>
<td>17.6</td>
</tr>
<tr>
<td>CZA3H</td>
<td>133.4</td>
<td>0.028</td>
<td>7.7</td>
<td>14.4</td>
<td>—</td>
<td>16.5</td>
</tr>
<tr>
<td>CZA5H</td>
<td>134.1</td>
<td>0.031</td>
<td>7.6</td>
<td>11.4</td>
<td>—</td>
<td>14.1</td>
</tr>
<tr>
<td>CZA7H</td>
<td>161.2</td>
<td>0.037</td>
<td>6.8</td>
<td>10.9</td>
<td>9.7</td>
<td>13.4</td>
</tr>
<tr>
<td>CZA10H</td>
<td>143.5</td>
<td>0.030</td>
<td>7.6</td>
<td>10.6</td>
<td>—</td>
<td>12.3</td>
</tr>
</tbody>
</table>

* Determined by Scherrer’s equation.
heterogeneous CuO particles with metal oxides. The CZA-H catalyst exhibited the best catalytic performance which might be explained that strongly interaction between CuO and oxides was beneficial to CO₂ hydrogenation to DME.⁴³ Meanwhile, the CZA-H catalyst possessed the largest area among the reducing peaks, which revealed that the hydrogen consumption of the catalyst was enhanced significantly, as shown in Table 4. The result implied the largest amount of easily reducible well-dispersed copper oxide existed, which might also be ascribed to the improving dispersion of the CuO particles.⁴⁴ This may be one reason why when increase Al₂O₃ contents in the catalysts from CZA₁H to CZA₇H, the conversion and selectivity significantly increased and a further increase in Al₂O₃ contents adversely influenced conversion and selectivity simultaneously.

### 3.6 Surface acidity of the CuO-ZnO-Al₂O₃/HZSM-5 catalysts

Fig. 7 shows NH₃-TPD profiles of the CZA-H catalysts with different Al₂O₃ contents. It can be found three NH₃ desorption peaks which located in the range of 50–200 °C (denoted as peak α), 200–350 °C (denoted as peak β), and 350–600 °C (denoted as peak γ), respectively. The α, β and γ peaks were attributed to weak, medium and strong acid sites, respectively, indicating the presence of three strength acid sites on the hybrid catalysts.⁴⁵ The intensity of the low-temperature peak α of weak acid sites firstly increased with increasing Al₂O₃ contents (from CZA₀H to CZA₇H) and then declined with further increasing Al₂O₃ additive, which was agreement with the trend of S_{NET} and H₂-TPR. The CZA-H catalyst of the highest peak intensity possessed the largest amount of weak acid sites which were beneficial for methanol dehydration to DME at low temperatures.⁴⁶ This might be ascribed to the fact Al₂O₃ owned weak acidic characters. In addition, the intensity and the position of the peaks β exhibited unconspicuous changes with doping different Al₂O₃ contents, implying that the strength and amount of medium acid sites cannot be influenced by Al₂O₃ additive substantially. The position of peaks γ shifted towards higher temperature gradually, indicating the intensity of strong acid sites increased with increasing Al₂O₃ doping, leading to the increase of hydrocarbons in the products. This might be attributed to the fact that the HZSM-5 with possessed strong acid sites could be modified by more oxalic acid with the addition of the more Al₂O₃ contents, during the preparation of hybrid catalysts by the co-precipitation method.⁴⁷,⁴⁸ From the above, the amount of weak acid sites enhanced with optimal Al₂O₃ modified, which was in favor of obtaining the highest catalytic performance for one-step DME synthesis reaction.⁴⁹

3.7 XPS analysis

The XPS spectra of reduced catalysts are shown in Fig. 8. Both of the spectra contained two peaks at about 1022 and 1045 eV (Fig. 8a), which were assigned to Zn 2p_{1/2} and Zn 2p_{1/2} peaks of ZnO, respectively, with a spin energy separation of 23 eV.⁴⁵ This illustrates that the Zn atoms are in a completely oxidized state and were not reduced.⁴⁴ It can be observed a single peak centered at near 74.2 eV in Fig. 8b, which was attributed to Al 2p_{3/2} of Al₂O₃, therefore, the form of Al was Al₂O₃. Fig. 8c showed the XPS spectra of the Cu 2p for the reduced CZA₀H and CZA₇H catalysts. Two reduced catalysts displayed Cu 2p_{3/2} and Cu 2p_{1/2} main characteristics peaks with binding energy (BE) values of approximately 932.6 eV and 952.6 eV, respectively, with a Cu 2p core level split spin–orbit components (ΔCu 2p) of 20.0 eV. The shake-up satellite peaks between 940 eV and 945 eV were not detected, which illustrates the absence of Cu⁷⁺ species in both CZA₀H and CZA₇H catalysts can be reduced to Cu⁺ and/or Cu⁰ species completely.⁴⁵,⁴⁴ Meanwhile, the binding energy (BE) of Cu 2p_{3/2} and Cu 2p_{1/2} for reduced CZA-H can be observed slightly shifted towards lower BE values, which revealed an enhancement on the interaction between Cu and ZnO with the increasing Al₂O₃ contents.⁴⁵ The result indicated an influence on Cu chemical combination state due to the increase of the outer-shell electron density of Cu as a consequence of the introduction of additive Al₂O₃. Liu et al. thought that the
The chemical state of Cu was tightly related to the catalysts performance for CO₂ hydrogenation to DME. This point might be one reason answerable for doping Al₂O₃ affect the activity of the hybrid catalysts. To distinguish Cu⁺ and Cu⁰ species, the kinetic energies (KE) of the Cu LMM X-ray auger electron spectroscopy (XAES) spectrum are measured. As shown in Fig. 8d, a broad and asymmetric peak was divided into two peaks, which centered at near 916.5 and 918.7 eV for both reduced CZA₀H and CZA₇H catalysts. The two symmetrical peaks are corresponding to the Cu⁺ and Cu⁰ species, respectively. The line position in the Cu LMM Auger electron spectrum of the two reduced catalysts illustrated that the Cu⁰ was the predominant copper species on the CZA₀H and CZA₇H catalysts surface. Furthermore, the Cu⁰/Cu⁺ area ratios of the two reduced catalysts were calculated based on the corresponding Cu LMM peaks. The area ratio of the reduced CZA₇H catalyst is a bit higher than that of the CZA₀H catalyst, which indicated that Cu⁰ species but not Cu⁺ species might in charge of the activity of these catalysts. The result might be another reason responsible for the improvement in catalytic performance for the Al₂O₃-modified hybrid catalysts.

4. Conclusions

The work discussed the effect of the amount of Al₂O₃ additive of the CuO–ZnO–Al₂O₃/HZSM-5 catalysts on the physicochemical properties and catalytic performance of the hybrid catalysts based on the optimizing Cu/Zn ratio. The hybrid catalysts for the reaction of CO₂ directly hydrogenation to DME improved the CuO dispersion, reduced the CuO crystallite size, decreased the grain size of the Cu, enhanced the BET surface areas, increased the interaction between the CuO and ZnO, enhanced the amount of weak acid sites, changed the copper chemical state on the catalysts surface and enhanced the catalytic activity and stability with the introduction of the Al₂O₃ contents. In addition, the influence of the reaction temperature and the space velocity on the catalytic performance of the catalysts modified by Al₂O₃ was also investigated. The optimal Al₂O₃ contents [Al₂O₃ : CuO–ZnO–Al₂O₃ wt%] of the CuO–ZnO–Al₂O₃/HZSM-5 catalysts was 7.0 wt% under the proper Cu/Zn ratio of 7 : 3. The CZA₇H catalyst for CO₂ hydrogenation to DME showed the maximum CO₂ conversion, DME selectivity and DME yield of 27.3%, 67.1% and 18.3%, respectively, under the reaction conditions of the optimal reaction temperature 260 °C, the appropriate space velocity of GHSV 1500 h⁻¹ and the conventional pressure of 3.0 MPa.

Conflicts of interest

There are no conflicts to declare.
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