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MoS₂ formation induced by amorphous MoS₃ species under lubricated friction

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Amide molybdate has been recently introduced as a friction modifier for tribological applications. Combined with zinc dithiophosphate (ZDDP) and fatty amines, it provides an ultralow friction coefficient. The ultimate product of Mo compound transformations in tribological contact, due to frictional heating and shearing, as well as chemical interactions with oil additives, is molybdenum sulfide (MoS₂). Understanding the decomposition of amide molybdate leading to MoS₂ is of primary importance to the optimization of the design of lubricant formulations. This study focuses on the investigation by Raman spectroscopy of amide molybdate decomposition intermediates. Raman spectra of tribofilms, obtained after friction tests under different temperatures and pressures, revealed the formation of an amorphous MoS₃ intermediate coexisting with MoS₂. However, under severe conditions, the tribofilms are mostly composed of MoS₂.

1. Introduction

Molybdenum disulfide (MoS₂) is a material extensively used in hydrotreating catalysts,^{1,2} photocatalysts,³ electrodes in Li-ion batteries,⁴ or lubricants.⁵ In tribology, MoS₂ is known for its low shearing at sliding interfaces. For example, Martin *et al.*⁶ reported an ultralow friction coefficient in the range of 10⁻³ in an ultra-high vacuum. Such an ultralow friction coefficient is characterized by a friction-induced orientation of the planes parallel to the sliding direction of the MoS₂ nanoparticles.^{6,7} Among molybdenum-based friction modifiers that have been proposed up until now,^{8,9} oil-soluble molybdenum dithiocarbamate (MoDTC) is widely used as a MoS₂ source since it permits the reach of an ultralow friction coefficient in the range 0.05–0.08.^{10–13} Unfortunately, MoDTC friction modifiers suffer from low stability against oxidation, which leads to a loss of efficiency under friction.^{11,14,15} The main additive degradation mechanism is due to a sulfur–oxygen atom substitution, which leads to oxidation and finally to the loss of the efficient MoDTC molecule.¹⁹ An alternative option to limit the oxidation instability involves the use of a sulfur-free organic molybdenum molecule, combined with a molecule acting as a sulfur source. Amide molybdate, where molybdenum is present in the form of an oxygenated Mo(VI) species, is such a candidate.^{16–21} De Barros Bouchet *et al.*²² have recently shown that, once combined with the antiwear zinc

dialkyl dithiophosphate ZDDP (which also brings S into the mixture) and a fatty amine, amide molybdate shows a beneficial effect toward lubrication. In addition to an ultralow friction coefficient of 0.02 under boundary lubrication conditions, this mixture is stable over time. A chemical pathway was proposed to explain MoS₂ formation from amide molybdate. After reacting with the fatty amine, amide molybdate is sulfided into MoS₃ in the presence of ZDDP. Then, under shear, MoS₃ forms MoS₂.

In the case of MoDTC, many attempts have been made to explain the reaction mechanism of MoS₂ formation from MoDTC decomposition upon friction contact. Sakurai *et al.*²³ suggested homolytic fission of the Mo–S bonds between the [MoO₂S₂]²⁻ core and dithiocarbamate ligands. This mechanism was supported by Grossiord *et al.* using XPS spectroscopy.²⁴ Another route for MoDTC decomposition through C–S bond cleavage was also suggested by Coffey *et al.*²⁵ However, few studies have been performed on amide molybdate.^{16–21}

This work focuses on the combination of amide molybdate, ZDDP, and fatty triamine. Our aim is to understand the intermediates involved in MoS₂ formation under friction of this ternary mixture of components. For this purpose, friction tests of the ternary mixtures were conducted at different pressures and temperatures. Then, the tribofilms were spatially characterized by micro-Raman mapping.

2. Experimental

2.1. Lubricant mixtures and solid reference preparation

The lubricants were composed of an amide molybdate friction modifier (Fig. 1), antiwear zinc dialkyldithiophosphate (ZDDP) synthesized from a secondary alcohol (Fig. 1), and a fatty

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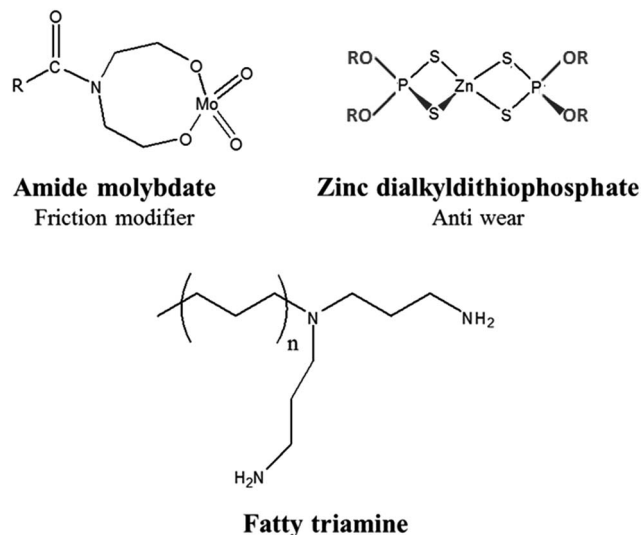


Fig. 1 Lubricant additives: amide molybdate, zinc dialkyldithiophosphate (ZDDP), and fatty triamine.

triamine (Fig. 1). They were respectively purchased from Vanderbilt, Lubrizol, and AkzoNobel.

To prepare the lubricant compositions, 400 ppm of Mo amide molybdate, 1% wt of ZDDP, and 0.5% wt of fatty triamine were added to a base oil (PAO4) in a glass vessel and mixed by stirring.

2.2. Reference preparation

The bulk MoS₂ and amorphous MoS₃ references were prepared by thermal decomposition of ammonium tetrathiomolybdate (NH₄)₂MoS₄, at 500 °C under hydrogen and at 200 °C under nitrogen, respectively.

2.3. Tribological experiments

A linear reciprocating friction tribometer with a ball-on-flat configuration was used to generate tribofilms under severe tribological conditions. The selected contact configuration was composed of an AISI 52100 steel ball (6.7 mm radius)/AISI 52100 steel flat. This alloy is a high carbon and chromium-containing bearing steel (0.95–1.10 % C, 0.35 max % Si, 0.20–0.50 % Mn, 0.025 max % P, 0.025 max % S, and 1.30–1.60 % Cr) with a high hardness of about 9 GPa and excellent strength and fatigue

properties. The friction experiments were performed at different temperatures and maximum initial contact pressures (the conditions are summarized in Table 1), and with a maximum sliding speed of about 0.1 m s⁻¹ (center of the track) for a one-hour duration. No run-in period prior to the sliding experiment was performed. Prior to the experiment, both the ball and flat specimens were ultrasonically cleaned in a heptane bath for 30 min in order to remove surface contaminants. The composite roughness of the two surfaces was about 25 nm. An average friction coefficient for each sliding cycle was calculated from one thousand measurements of instantaneous friction coefficients recorded during the cycle.

2.4. Characterization

Confocal Raman spectra were recorded with a LabRam HR Raman spectrometer (Horiba-Jobin Yvon). The exciting laser at 514.5 nm (Ar laser) was focused using a ×50 long working distance objective, leading to spatial resolution of ca. 4 μm. Laser power of 1 mW was used after checking for the absence of laser heating effects. The spectral resolution was lower than

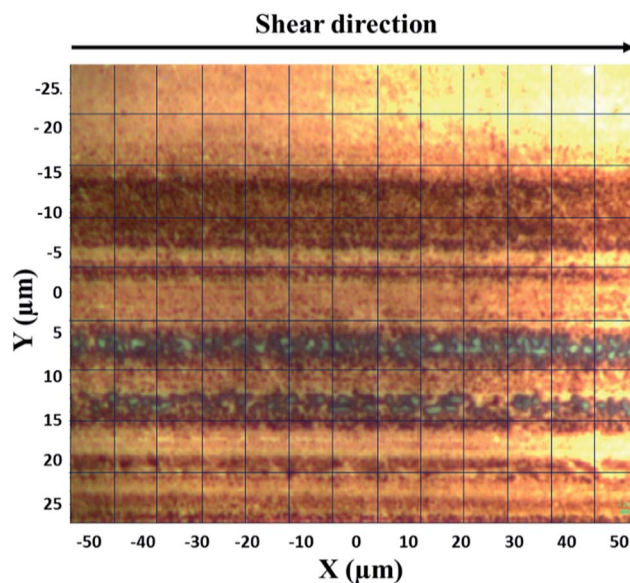


Fig. 2 Example of an optical microscopy picture of an analyzed section (50 per 100 μm). During the mapping, each square of the image was analyzed.

Table 1 Conditions used for the friction tests and obtained FCos

Conditions	Normal force (N)	Maximal contact pressure (MPa)	Temperature (°C)	Mean friction coefficient (μ)
1	3	400	80	0.069
2	7	540	60	0.108
3	7	540	70	0.078
4	7	540	80	0.034
5	7	540	90	0.036
6	7	540	100	0.034
7	7	540	110	0.035
8	15	700	80	0.036



4 cm^{-1} . After the friction tests, the samples were washed for 30 min in a heptane bath under sonication. The Raman mapping analyses were performed on the center of the tribofilms, on a section measuring 50 per 100 μm , with a step of 8 μm , and an autofocus was automatically performed before each analysis. The spectra were first recorded horizontally along a line, before recording vertically to the bottom line (Fig. 2). Each tribofilm was characterized by a mapping sequence containing 117 raw spectra (9×13). Analyses were done under the same conditions of laser power and acquisition time.

Elemental analysis of the reference solids was carried out using atomic emission spectroscopy. The mixtures were mineralized at 350/400 $^{\circ}\text{C}$ with a solution made of H_2SO_4 and HNO_3 . The amounts of Mo and S were measured by Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES) using an ACTIVA Horiba Jobin Yvon spectrometer.

3. Results and discussion

3.1. Friction tests

The friction coefficient (FCo) data and FCo time evolution curves during the friction tests are respectively shown in Table 1 and Fig. 3. At a constant contact pressure of 7 N (corresponding to a maximal contact pressure of 540 MPa), the FCo is highly dependent on the temperature. At 60 $^{\circ}\text{C}$, the FCo is 0.108, and it decreases between 60 and 110 $^{\circ}\text{C}$ until it reaches a plateau around 0.035. Then, the temperature was fixed at 80 $^{\circ}\text{C}$ and we varied the contact pressure. At 3 N (corresponding to a maximal contact pressure of 400 MPa), the FCo is 0.069, but it decreases to 0.035 at 7 and 15 N. This decrease in friction under severe conditions has already been observed in the literature.^{10,26,27} The contribution of thermal and mechanical energies is essential to ensure the molecule decomposition and the tribofilm formation. The tribofilms formed during the tests conducted at different temperatures and pressures were then analyzed by Raman spectroscopy.

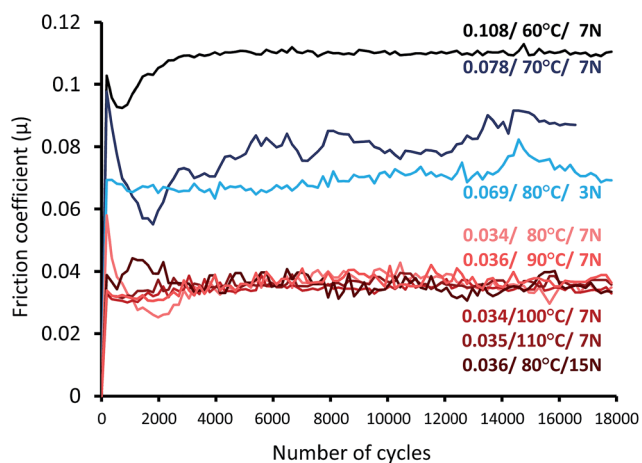


Fig. 3 Evolution of the friction coefficient as a function of the cycle number under different conditions, as indicated in Table 1.

3.2. Characterization by Raman spectroscopy

Confocal Raman spectroscopy mapping is particularly convenient when using flat steel samples and it allows for the spatially resolved characterization of the tribofilms, as well as the identification of the reaction intermediates.

3.2.1. Raman spectra of the reference compounds. Amide molybdate contains molybdenum in a fully oxidized form, while the tribofilm contains MoS_2 . Therefore, the transition of molybdate(vi) to molybdenum(iv) sulfide occurs at some stage involving oxygen to sulfur exchange and the reduction of molybdenum. In a previous paper,²² we proposed a mechanism of MoS_2 formation through $[\text{MoS}_4]^{2-}$ and MoS_3 intermediates, respectively produced by thermal decomposition and under shear. During the chemical change from the oxide to the sulfide forms, the formation of mixed oxo-thiomolybdates is possible. In order to check this hypothesis, we first prepared $(\text{NH}_4)_2\text{MoS}_4$ and $(\text{NH}_4)_2\text{MoO}_2\text{S}_2$ according to the literature.^{28,29} $(\text{NH}_4)_2\text{MoO}_2\text{S}_2$ and $(\text{NH}_4)_2\text{MoS}_4$ (Fig. 4) are characterized by strong and narrow $\nu_s(\text{Mo-S})$ Raman bands, respectively located at 474 and 456 cm^{-1} .³⁰

The Raman spectra of the MoS_3 and MoS_2 references prepared *via* the thermal decomposition of $(\text{NH}_4)_2\text{MoS}_4$ at 200 $^{\circ}\text{C}$ under nitrogen and 500 $^{\circ}\text{C}$ under H_2 , respectively, are presented in Fig. 4.

Crystalline MoS_2 , obtained from the decomposition of $(\text{NH}_4)_2\text{MoS}_4$ at 500 $^{\circ}\text{C}$ under H_2 , has three active Raman bands, E_{1g} , E_{2g}^1 , and A_{1g} , respectively located at 284, 381, and 409 cm^{-1} (Fig. 4), in agreement with the literature.³¹ The amorphous species, prepared by the decomposition of $(\text{NH}_4)_2\text{MoS}_4$ at 200 $^{\circ}\text{C}$ under N_2 , shows several broad bands (Fig. 4). These bands, numbered from 1 to 5 in Fig. 4, are closely located to the ones reported in literature for MoS_3 .³² MoS_3 is characterized by five bands in the ranges 150–160 cm^{-1} , 210–220 cm^{-1} (both

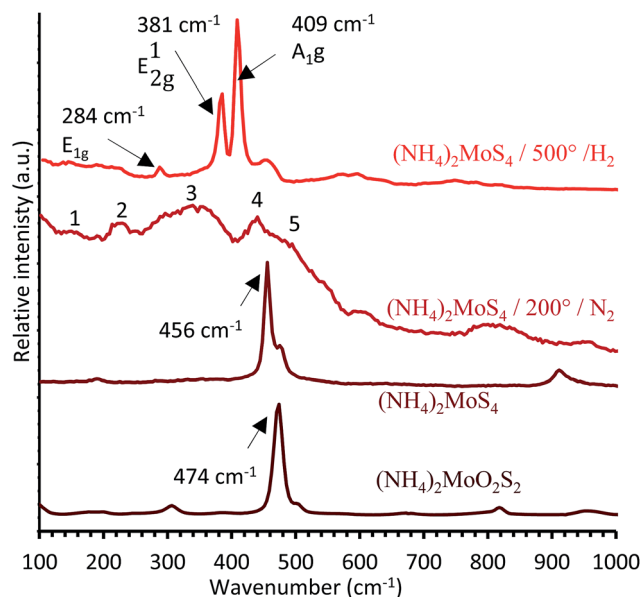


Fig. 4 Reference spectra of $(\text{NH}_4)_2\text{MoO}_2\text{S}_2$, $(\text{NH}_4)_2\text{MoS}_4$, $(\text{NH}_4)_2\text{MoS}_4$ decomposed at 200 $^{\circ}\text{C}$ under N_2 , and $(\text{NH}_4)_2\text{MoS}_4$ decomposed at 500 $^{\circ}\text{C}$ under H_2 .



corresponding to the $\delta(\text{Mo-S})$ angular mode), $300\text{--}360\text{ cm}^{-1}$, $425\text{--}450\text{ cm}^{-1}$ (both corresponding to the $\nu(\text{Mo-S})$ stretching modes), and $520\text{--}550\text{ cm}^{-1}$ (corresponding to the $\nu(\text{S-S})$ stretching modes).^{31,33–35}

3.2.2. Confocal Raman characterization of the tribofilms.

The tribofilms were analyzed by Raman spectroscopy. Mapping of the tribofilm center was carried out for each sample. The mean spectra of the 117 raw spectra recorded for each tribofilm are presented in Fig. 5 and compared to the MoS_2 reference.

There are neither $(\text{NH}_4)_2\text{MoS}_4$ nor $(\text{NH}_4)_2\text{MoO}_2\text{S}_2$ signatures in the Raman spectra. The absence of any significant features both above 600 cm^{-1} and between 800 and 1000 cm^{-1} attests to the fact that no oxide forms of molybdenum (molybdate, MoO_3 , etc.) are present in the tribofilms. However, we observe intense A_{1g} and E_{2g}^1 bands of MoS_2 , evidencing its expected formation in the tribofilms. Moreover, as seen in Fig. 6, the decrease in FCo is accompanied by an increase in the MoS_2 distribution in the tribofilms. In contrast to bulk MoS_2 , which exhibits narrow bands, the tribofilm spectra exhibit broad bands between $280\text{--}400$ and $400\text{--}550\text{ cm}^{-1}$ (Fig. 5). This suggests that MoS_2 is formed together with an amorphous species. Moreover, the band intensity and narrowness increase with temperature (from 70 to $110\text{ }^\circ\text{C}$) and pressure (from 3 N to 15 N). Therefore, the crystallinity of MoS_2 increases under more severe conditions. The broad peak in the $100\text{--}250\text{ cm}^{-1}$ region is attributed to stress-induced disorder in the MoS_2 crystal structure (Fig. 5).^{36,37}

In order to distinguish the different species present in the tribofilms, we focused our study on mapping the test conducted at $90\text{ }^\circ\text{C}$ and 7 N (Fig. 5). As seen in Fig. 7, the intensity of the A_{1g} band is relatively homogeneous across the tribofilm, except for line 6, where the intensity of the A_{1g} band of MoS_2 is the lowest. By analyzing the mean spectrum per line (Fig. 8a), as we move

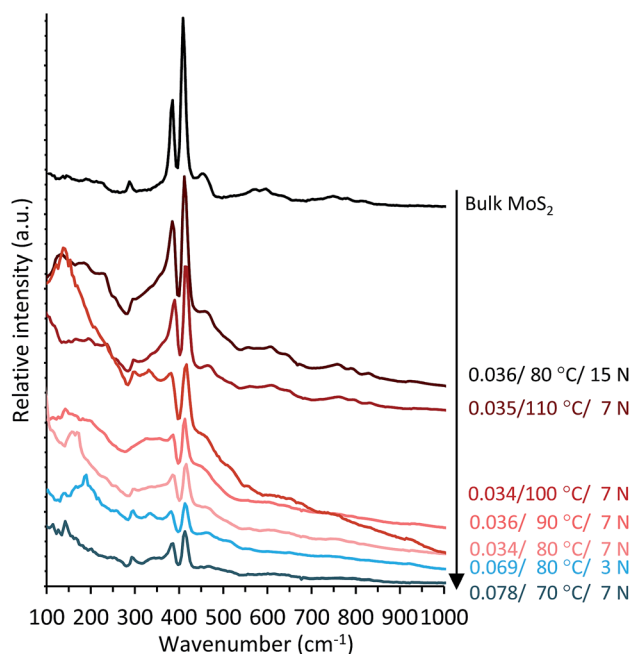


Fig. 5 Raman mean spectra of the tribofilms obtained under different temperature and pressure conditions. The tribofilm spectra are compared to those of the bulk MoS_2 reference.

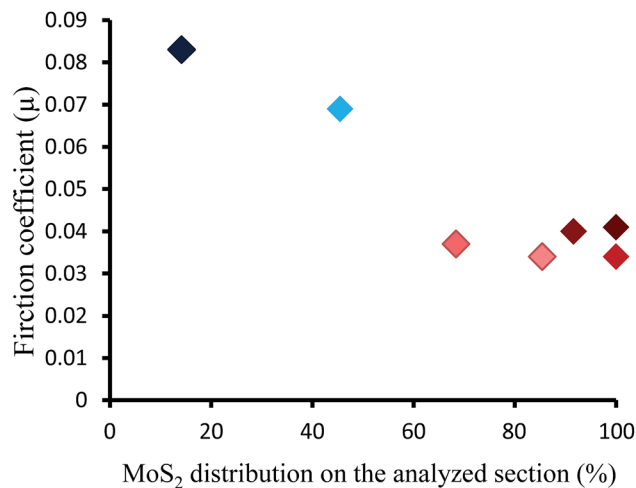


Fig. 6 Evolution of the friction coefficient vs. the proportion of spectra containing MoS_2 in the tribofilms. For this measurement, every spectrum containing MoS_2 was counted, independent of the presence of amorphous species. We fixed a threshold value of 1.1, corresponding to the intensity ratio of the MoS_2 A_{1g} band with respect to the amorphous species band located at $400\text{--}550\text{ cm}^{-1}$, in order to consider the presence of MoS_2 .

across the map from line 0 to 8, *i.e.* from the center of tribofilm to the periphery, it can be seen that the intensity of the A_{1g} and E_{2g}^1 bands decreases, with the amorphous band hiding the E_{2g}^1 band. This amorphous contribution is the most pronounced for line 6. It is even clearer once all the individual spectra of line 6 are compared (Fig. 8b). The A_{1g} band of MoS_2 at 410 cm^{-1} is only seen in the last columns of the raw spectra. Then, we compared these broad bands to the Raman spectrum of the MoS_3 reference (Fig. 9), and they appear rather similar. The blue spectrum of line 6 has broad bands similar to that of the MoS_3 reference (in the ranges $260\text{--}400$ and $410\text{--}580\text{ cm}^{-1}$). Therefore, the amorphous species formed in competition (or as an intermediate) with MoS_2 are of MoS_3 type.

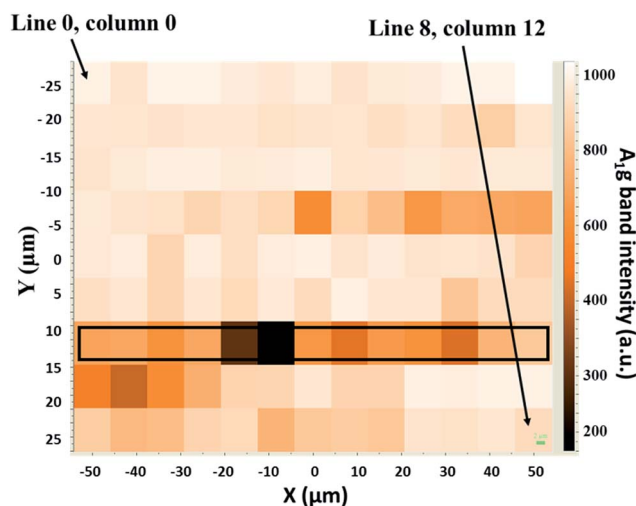


Fig. 7 Intensity of the A_{1g} band according to the location on the tribofilm obtained from the mixture of amide-Mo, ZnDTP, and triamine at $90\text{ }^\circ\text{C}$. The intensity increases from dark (no MoS_2) to bright areas (more MoS_2).



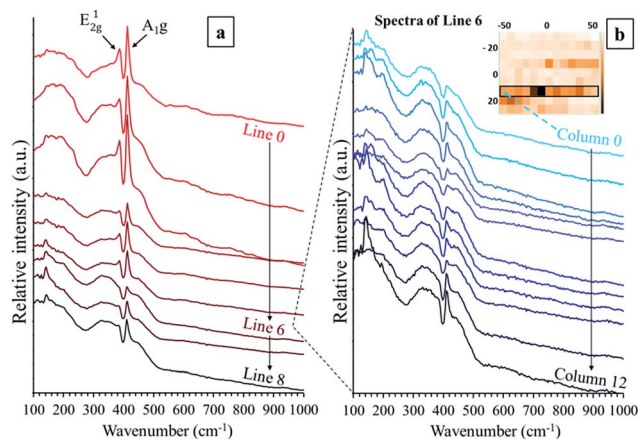


Fig. 8 Raman spectra of the tribofilm from the mixture of amide-Mo, ZnDTP, and triamine at 90 °C: (a) mean spectrum for each line (from 0 to 8), and (b) individual spectra of line 6.

The sulfur-rich sulfide, MoS_3 , known for its catalytic³⁸ and electrochemical properties,^{34,39,40} can only be prepared as an amorphous substance. MoS_3 can be prepared by acidic precipitation of $(\text{NH}_4)_2\text{MoS}_4$,⁴¹ by reacting molybdenum halides with hexamethyldisilathiane,³⁴ or as in the present work, by gentle thermal decomposition of $(\text{NH}_4)_2\text{MoS}_4$. Its structure is not exactly clear and different models have been proposed, including chain-like and trimeric structures,^{42–45} which cannot mutually be excluded because the chemical connectivity in an amorphous solid might strongly depend on the preparation technique used to obtain it. This type of species has already been observed in materials derived from tribological experiments. Khaemba *et al.*,^{13,46,47} reported its formation as a sulfur-rich MoS_x species, an intermediate in the decomposition of MoDTC to MoS_2 under soft friction conditions. Moreover, whereas no more species other than MoS_3 and MoS_2 were observed in that study, the authors reported the simultaneous formation of MoS_x ($x \sim 3$), MoS_2 , and FeMoO_4 species.⁴⁶

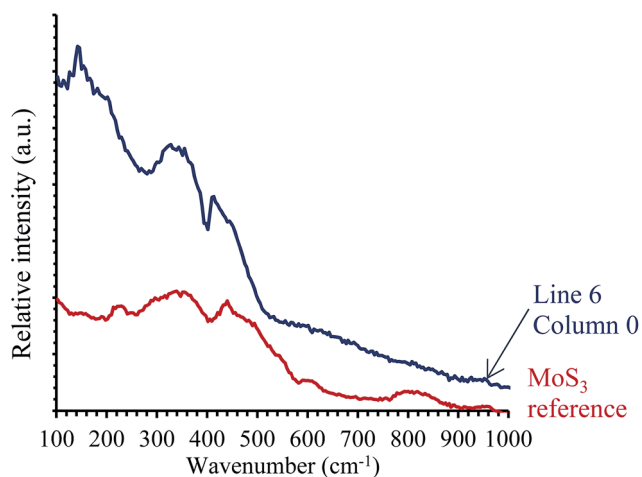


Fig. 9 Raman spectrum of the amorphous species from line 6, in comparison with that of the MoS_3 amorphous species made via the decomposition of $(\text{NH}_4)_2\text{MoS}_4$ at 200 °C.

For molybdenum-containing lubricants, it is widely accepted that friction reduction is achieved due to the formation of MoS_2 single sheets in the contact zone.^{24,48,49} The widely used MoDTC molecule already contains three sulfur atoms per molybdenum atom, sufficient to stoichiometrically form MoS_3 and then MoS_2 , due to an intramolecular decomposition process induced by applied stress and temperature. As amide molybdate is an oxidic precursor, molybdenum sulfide species are formed in a complex process involving interaction with the sulfur-containing ZDDP molecule. Therefore, pathways involving different possible intermediates may occur. Herein, we clearly demonstrate that the only intermediate present in the tribofilms, in a tangible amount, is an amorphous MoS_3 -like sulfide. Remarkably, no oxygenated Mo species are detected in the tribofilm.

Raman mapping strongly suggests that MoS_3 is an intermediate and not an extraneous compound formed alongside MoS_2 . Indeed, as the mapping point moves from the center of the zone towards the periphery, the relative amount of MoS_3 increases and that of MoS_2 decreases. This evolution obviously occurs in relation to the local temperature and pressure created in the contact zone by the ball friction. Indeed, according to TGA measurements under nitrogen, the $[\text{MoS}_4]^{2-}$ species first decomposes to MoS_3 between 120 to 260 °C and then MoS_3 decomposes to MoS_2 above 300 °C, *i.e.* at higher temperatures than the ones used during the tribotest.⁵⁰

4. Conclusions

This work focused on the decomposition mechanism of amide molybdate as a friction modifier additive. Combined with ZDDP and fatty amine, it provides an ultralow friction coefficient under severe lubricating conditions. In order to investigate the decomposition mechanism of amide molybdate, two series of experimental friction tests were performed, varying the temperature and pressure. The results show that the friction decreases as the severity of the conditions increases. The tribofilm compositions were analyzed using confocal Raman spectroscopy. Under softer conditions, amorphous species are mainly formed, coexisting with MoS_2 . However, under severe conditions, MoS_2 is mostly formed. The amorphous species are attributed to a MoS_3 -type compound, which is an intermediate during the formation of MoS_2 . However, if ultralow friction is not achieved, MoS_3 is found in the final tribofilm, coexisting with MoS_2 . It is possible to modulate the test conditions in order to ensure MoS_2 formation and to limit MoS_3 formation. However, given the fact that engine conditions differ from one part to another, it would be interesting to design another Mo-containing friction modifier that could produce MoS_2 across a larger range of friction conditions.

Conflicts of interest

There are no conflicts to declare.

References

- 1 H. Topsøe, *Appl. Catal., A*, 2007, **322**, 3–8.



- 2 L. Van Haandel, G. M. Bremmer, E. J. M. Hensen and T. Weber, *J. Catal.*, 2017, **351**, 95–106.
- 3 Z. Lei, W. You, M. Liu, G. Zhou, T. Takata and M. Hara, *Chem. Commun.*, 2003, 2142–2143.
- 4 L. Ye, C. Wu, W. Guo and Y. Xie, *Chem. Commun.*, 2006, **2**, 4738.
- 5 M. Chhowala and G. A. J. Amaratinga, *Nature*, 2000, **407**, 164–167.
- 6 J. M. Martin, C. Donnet, T. Le Mogne and T. Epicier, *Phys. Rev. B: Condens. Matter Mater. Phys.*, 1993, **48**, 10583–10586.
- 7 J. M. Martin, H. Pascal, C. Donnet, T. Le Mogne, J. L. Loubet and T. Epicier, *Surf. Coat. Technol.*, 1994, **69**, 427–432.
- 8 P. C. H. Mitchell, *Wear*, 1984, **100**, 281–300.
- 9 H. Spikes, *Tribol. Lett.*, 2015, **60**, 1–26.
- 10 J. Graham and S. Korcek, *Tribol. Trans.*, 2001, **44**, 626–636.
- 11 M. De Feo, C. Minfray, M. I. De Barros-Bouchet, B. Thiebaut, T. Le Mogne, B. Vacher and J. M. Martin, *Tribol. Int.*, 2015, **92**, 126–135.
- 12 A. Morina, A. Neville, J. H. Green and M. Priest, in *Tribology and Interface Engineering Series*, ed. D. Dowson, M. Priest, G. Dalmaz and A. A. Lubrecht, Elsevier Masson SAS, 2005, vol. 48, pp. 757–767.
- 13 D. N. Khaemba, F. Jarnias, B. Thiebaut, A. Neville and M. J. Ardian, *J. Phys. D: Appl. Phys.*, 2017, **50**, 085302–085310.
- 14 M. De Feo, C. Minfray, M. I. De Barros-Bouchet, B. Thiebaut and J. M. Martin, *RSC Adv.*, 2015, **5**, 93786–93796.
- 15 M. De Feo, M. I. De Barros-Bouchet, C. Minfray, T. Le Mogne, F. Meunier, L. Yang, B. Thiebaut and J. M. Martin, *Wear*, 2016, **348**, 116–125.
- 16 O. Gorbachev, M. I. De Barros Bouchet, J. M. Martin, D. Léonard, T. Le-Mogne, R. Iovine, B. Thiebaut and C. Héau, *Tribol. Int.*, 2016, **99**, 278–288.
- 17 M. Debord, C. Charrin and J. Guerin, Composition lubrifiante à fuel éco longue durée, FR3039165A1, 2015.
- 18 Y. F. Suen and J. H. McLain, Multifunctional molybdenum containing compounds, method of making and using, and lubricating oil compositions containing same, US20160369199A1, 2016.
- 19 K. Fletcher, W. Y. Lam, K. Yang and J. Styer, Lubricating with molybdenum and their use for improving low speed pre-ignition, US20170015929A1, 2017.
- 20 M. K. Patel and V. J. Gatto, Additive for lubricant compositions comprising a sulfur-free organomolybdenum compound, and triazole or a derivated triazole, US20170044456A1, 2017.
- 21 R. Iovine and C. Charrin, Lubricant composition based on neutralized amines and molybdenum, WO2017149119A1, 2017.
- 22 M. I. De Barros Bouchet, J. M. Martin, C. Oumahi, O. Gorbachev, P. Afanasiev, C. Geantet, R. Iovine, B. Thiebaut and C. Heau, *Tribol. Int.*, 2018, **119**, 600–607.
- 23 T. Sakurai, H. Okabe and H. Isoyama, *Bull. Jpn. Pet. Inst.*, 1971, **13**, 243–249.
- 24 C. Grossiord, K. Varlot, J. M. Martin, T. Le Mogne, C. Esnouf and K. Inoue, *Tribol. Int.*, 1998, **31**, 737–743.
- 25 A. Coffey, G. D. Forster and G. J. Hogarth, *J. Chem. Soc., Dalton Trans.*, 1996, **2**, 183–193.
- 26 J. Graham, H. Spikes and R. Jensen, *Tribol. Trans.*, 2001, **4**, 37–41.
- 27 Y. Tamai, T. Inazumi and K.-I. J. Manabe, *J. Mater. Process. Technol.*, 2016, **227**, 161–168.
- 28 T. Decamp, Etude de l'évolution des propriétés adsorbantes et catalytiques des sulfures de métaux de transition en fonction du rapport soufre sur métal, Thèse de doctorat en Sciences, Catalyse, Lyon 1, 1992.
- 29 J. W. McDonald, G. D. Friesen, L. D. Rosenhein and W. E. Newton, *Inorg. Chim. Acta*, 1983, **72**, 205–210.
- 30 A. Muller, W. Jaegermann and W. J. Hellmann, *J. Mol. Struct.*, 1983, **100**, 559–570.
- 31 C. H. Chang and S. S. Chan, *J. Catal.*, 1981, **72**, 139–148.
- 32 M. Olga Guerrero-Perez, E. Rojas, A. Gutierrez-Alejandre, J. Ramirez, F. Sacher-Minero, C. Fernandez-Vargas and M. A. Banãres, *Phys. Chem. Chem. Phys.*, 2011, **13**, 9260–9267.
- 33 R. N. Bhattacharya, C. Y. Lee and F. H. J. Pollak, *J. Non-Cryst. Solids*, 1987, **91**, 235–242.
- 34 C. Sourisseau, O. Gorochov and D. M. Schleich, *J. Mater. Sci. Eng. B*, 1989, **3**, 113–117.
- 35 T. Weber, J. C. Muijsers and J. W. J. Niemantsverdriet, *J. Phys. Chem.*, 1995, **99**, 9194–9200.
- 36 N. T. McDevitt, J. S. Zabinski, M. S. Donley and J. E. Bultman, *Appl. Spectrosc.*, 1994, **48**, 733–736.
- 37 N. T. McDevitt, J. E. Bultman and J. S. Zabinski, *Appl. Spectrosc.*, 1998, **52**, 2–6.
- 38 B. Liu, Z. Jin, L. Bai, J. Liang, Q. Zhang, N. Wang, C. Liu, C. Wei, Y. Zhao and X. Zhang, *J. Mater. Chem. A.*, 2016, **4**, 14204–14212.
- 39 H. Shin, H. J. Doerr, C. Deshpandey, P. Fuqua, B. Dunn and R. F. Bunshah, *Surf. Coat. Technol.*, 1988, **36**, 859–865.
- 40 Y. Deng, L. R. L. Ting, P. H. L. Neo, Y. J. Zhang, A. A. Peterson and B. S. Yeo, *ACS Catal.*, 2016, **6**, 7790–7798.
- 41 J. C. Wildervanck and F. Jellinek, *Z. Anorg. Allg. Chem.*, 1964, **328**, 309–318.
- 42 S. J. Hibble, D. A. Rice, D. M. Pickup and M. P. Beer, *Inorg. Chem.*, 1995, **34**, 5109–5113.
- 43 S. J. Hibble, R. I. Walton, D. M. Pickup and A. C. J. Hannon, *J. Non-Cryst. Solids*, 1998, **232–234**, 434–439.
- 44 K. S. Liang, J. P. DeNeufville, A. J. Jacobson and R. R. J. Chianelli, *J. Non-Cryst. Solids*, 1980, **36**, 1249–1254.
- 45 F. Z. Chien, S. C. Moss, K. S. Liang and R. R. Chianelli, *Phys. Rev. B: Condens. Matter Mater. Phys.*, 1984, **29**, 4606–4615.
- 46 D. N. Khaemba, A. Neville and A. Morina, *RSC Adv.*, 2016, **6**, 38637–38646.
- 47 D. N. Khaemba, A. Neville and A. Morina, *Tribol. Lett. Lett.*, 2015, **59**, 1–17.
- 48 J. M. Martin, C. Grossiord, T. Le Mogne and J. Igarashi, *Wear*, 2000, **245**, 107–115.
- 49 M. I. De Barros Bouchet, J. M. Martin, T. Le Mogne, P. Bilas, B. Vacher and Y. Yamada, *Wear*, 2005, **258**, 1643–1650.
- 50 J. L. Brito, M. Ilija and P. Hernández, *Thermochim. Acta*, 1995, **256**, 325–338.

