

## PAPER

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# Separation of samarium and europium by solvent extraction with an undiluted quaternary ammonium ionic liquid: towards high-purity medical samarium-153†

 Michiel Van de Voorde,<sup>ab</sup> Karen Van Hecke,<sup>a</sup> Koen Binnemans<sup>b</sup> and Thomas Cardinaels<sup>\*ab</sup>

Long-lived europium-154 impurities are formed during the production of medical samarium-153 in a high-flux nuclear reactor. A method to separate these europium impurities from samarium was investigated using the hydrophobic quaternary ammonium ionic liquid Aliquat 336 nitrate. The separation method consists of the selective reduction of  $\text{Eu}^{3+}$  by zinc metal in an aqueous feed solution containing a high nitrate salt concentration. Subsequent extraction using undiluted Aliquat 336 nitrate leads to an efficient separation of both lanthanides in a relatively short time frame.  $\text{Sm}^{3+}$  was extracted to the neat ionic liquid phase much more efficiently than  $\text{Eu}^{2+}$ . An initial approach using the addition of dicyclohexano-18-crown-6 to capture  $\text{Eu}^{2+}$  in the ionic liquid phase was less efficient.

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## Introduction

The radiolanthanide samarium-153 ( $^{153}\text{Sm}$ ) is applied in nuclear medicine, where it is known under its commercial names Quadramet and Lexidronam.<sup>1,2</sup> In these radiopharmaceuticals, the  $^{153}\text{Sm}$  radioisotope is coordinated to an ethylenediamine tetra(methylene phosphonate) chelating ligand ( $^{153}\text{Sm}$  EDTMP, Fig. 1).<sup>3</sup>  $^{153}\text{Sm}$  serves well in nuclear medicine because of its favorable half-life of 46.284 h and because it decays to the stable  $^{153}\text{Eu}$  nuclide. This causes no severe additional side effects in the human body after treatment.  $^{153}\text{Sm}$  EDTMP is very selective towards the skeleton.<sup>4–7</sup> The  $^{153}\text{Sm}$

radionuclide is commonly produced *via* neutron-irradiation of an enriched  $^{152}\text{Sm}_2\text{O}_3$  target, in a nuclear reactor with a high thermal neutron flux.<sup>8</sup> A product with high yield, high purity and high specific activity is formed. However, since the target is usually irradiated for several days, part of the  $^{153}\text{Sm}$  is already decaying during irradiation and the daughter isotope  $^{153}\text{Eu}$  will be neutron-irradiated as well, leading to the simultaneous production of trace amounts of  $^{154}\text{Eu}$ .<sup>9,10</sup> This radiochemical impurity has a much longer half-life (8.593 year) compared to that of  $^{153}\text{Sm}$ . Relatively large quantities of  $^{154}\text{Eu}$  lead to an unacceptable radiation dose delivered to the patient. The maximum level of impurities is strictly regulated by international and national organizations (*e.g.* WHO, IAEA, FDA). Consequently, Quadramet has a limited shelf life of only a few days after being produced, since expiration is reached at the threshold ratio of 0.093  $\mu\text{Ci}$  ( $=3400$  Bq) of  $^{154}\text{Eu}$  per mCi (37 MBq) of  $^{153}\text{Sm}$ .<sup>9–11</sup> Additionally, long-lived  $^{154}\text{Eu}$  impurities end up in the waste generated in the hospitals. Removal of these  $^{154}\text{Eu}$  impurities would imply a longer product shelf-life for medical use, leading to an increased availability of  $^{153}\text{Sm}$  and a lower background radioactivity of the treated patient. Waste treatment procedures in hospitals can become easier because waste containing short-lived isotopes only can be treated *via* decay storage. Moreover, distribution and transportation deadlines can become more flexible, opening perspectives of feeding a world-wide market. This way, an unexpected outage of a research reactor can be backed-up more easily by another research reactor, ensuring the supply of  $^{153}\text{Sm}$ . Valuable and expensive enriched target material can also be used more efficiently by increasing the irradiation time because the long-lived

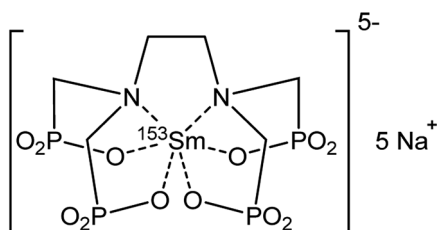


Fig. 1 Chemical structure of  $^{153}\text{Sm}$  EDTMP (commercial names: Quadramet and Lexidronam).

<sup>a</sup>SCK•CEN, Belgian Nuclear Research Centre, Institute for Nuclear Materials Science, Boeretang 200, B-2400 Mol, Belgium. E-mail: thomas.cardinaels@sckcen.be

<sup>b</sup>KU Leuven, Department of Chemistry, Celestijnenlaan 200F, P. O. 2404, B-3001 Heverlee, Belgium

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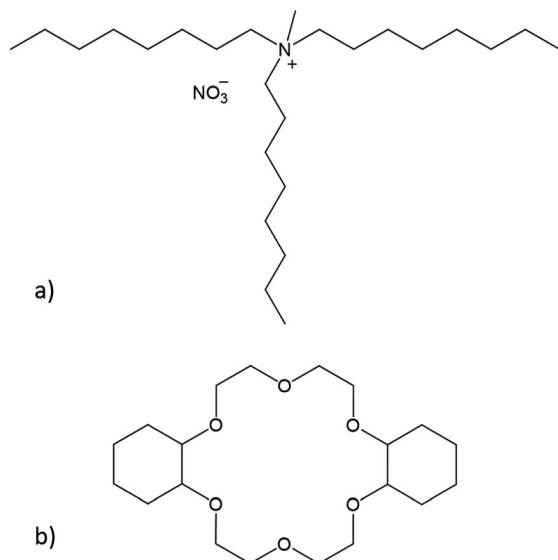


Fig. 2 Chemical structures of (a) the main component of Aliquat 336 nitrate ([A336][NO<sub>3</sub>]) and (b) dicyclohexano-18-crown-6 (DCH18C6).

side-products are removed afterwards. Undeniably, purification of the irradiated target material by separation of <sup>154</sup>Eu from <sup>153</sup>Sm would be beneficial in medical and economical perspective.

Separation of two neighboring lanthanides is very challenging because of their very similar chemical properties. A separation method based on a very small difference in complexation behavior would be too time-consuming to be feasible for the separation of these relatively short-lived radionuclides. Approaches based on the selective reduction of europium from the trivalent to the divalent state, either chemically or electrochemically, changing the chemical properties of europium significantly, have proven to be efficient for the recovery of highly valuable europium from rare-earth ores on an industrial scale.<sup>12–17</sup> In these processes, a phosphorus-containing acidic extractant with high affinity for lanthanides (Ln<sup>3+</sup>) is used most frequently, leaving the Eu<sup>2+</sup> unaffected in the aqueous phase. The use of ion exchange resins is another popular purification method. Taking into account the relatively short half-lives of the medical radionuclides, gravimetric separation methods are too time-consuming to be used. High performance ion chromatography (HPIC) methods to separate radiolanthanides are more suitable, but require more advanced equipment.<sup>18</sup>

In this paper, we conducted a feasibility study to separate samarium and europium *via* two different solvent extraction processes. Prior to the separation process, Eu<sup>3+</sup> was selectively reduced to Eu<sup>2+</sup> by Zn<sup>0</sup>. The water-immiscible phase of the extraction system consisted of the highly hydrophobic ionic liquid (IL) Aliquat 336 nitrate ([A336][NO<sub>3</sub>], Fig. 2a). Ionic liquids are solvents that consist entirely of ions. Moreover, previous studies have shown that the use of undiluted ionic liquids in solvent extraction is a very promising approach for separation of rare-earth elements (REEs).<sup>19–23</sup>

The separation process was performed with and without the addition of a size-selective extractant. The size-selective extractant dicyclohexano-18-crown-6 (DCH18C6, Fig. 2b) was selected because of its capability to efficiently extract Sr<sup>2+</sup>, which has a comparable ionic radius and charge density as Eu<sup>2+</sup>.<sup>24–27</sup> The process including DCH18C6 was aimed at the size-selective extraction of Eu<sup>2+</sup> to the water-immiscible phase, while leaving Sm<sup>3+</sup> in the aqueous phase. The process without addition of DCH18C6 uses the alkaline extraction capacities of the ionic liquid itself to separate samarium and europium.

## Experimental

### Materials

Tricaprylammonium chloride (Aliquat® 336, [A336][Cl], 88.2–90.6%), dicyclohexano-18-crown-6 (DCH18C6, ≥98%), LiCl (99%) and HNO<sub>3</sub> (≥65%) were purchased from Sigma-Aldrich (Diegem, Belgium). SmCl<sub>3</sub>·6H<sub>2</sub>O (99.9%) and Eu(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O (99.9%) were purchased from Strem Chemicals, Inc. (Newburyport, USA). Sm(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O (99.9%) and LiNO<sub>3</sub> (anhydrous, 99%) were purchased from Alfa Aesar (Karlsruhe, Germany). EuCl<sub>3</sub>·6H<sub>2</sub>O (99.9%), Sr(NO<sub>3</sub>)<sub>2</sub> (99.9%) and granular zinc (30 mesh, ≥99.7%) were purchased from Acros Organics (Geel, Belgium). SrCl<sub>2</sub>·6H<sub>2</sub>O (≥99%), NH<sub>4</sub>Cl (≥99.8%), Na<sub>2</sub>SO<sub>4</sub> (≥99%) and acetonitrile (≥99.5%) were purchased from Chem-Lab (Zedelgem, Belgium), as well as the Sm, Eu, Zn and Cu standard solutions (≥99.99%, 1000 μg mL<sup>-1</sup>, 2–5% HNO<sub>3</sub>, Plasma HIQU). NH<sub>4</sub>NO<sub>3</sub> (≥99%) was purchased from Merck Millipore (Darmstadt, Germany). All products were used as received, without any further purification steps. Aqueous samples were prepared with Milli-Q water (18.2 MΩ cm at 25 °C).

### Reduction of Eu<sup>3+</sup>

In all experiments, Eu<sup>3+</sup> ( $E^0 = -0.43$  V) was reduced chemically using zinc granules ( $E^0 = -0.76$  V) taking into account the minimal requirements to obtain maximal reduction established by Sayed *et al.*<sup>28</sup> This study proved that a minimal contact time of 1 h and a minimal zinc-to-europium molar ratio of 2.5 are needed to reach maximum reduction of Eu<sup>3+</sup>. Therefore, the aqueous feed solutions, both chloride and nitrate ones, were mixed with a large excess of granular zinc (30 mesh) for 2 h at room temperature. The remarkably high stability of Eu<sup>2+</sup> in aqueous solutions containing high nitrate salt concentrations will be discussed in a dedicated separate publication. The aqueous solutions were purged with nitrogen gas during reduction of Eu<sup>3+</sup> to remove atmospheric and dissolved oxygen. This is necessary to prevent re-oxidation of Eu<sup>2+</sup> by O<sub>2</sub> ( $E^0 = +1.23$  V). The pH of the aqueous feed solution was kept between 4 and 6.5. This way, the pH of the final feed solution remained sufficiently high to avoid re-oxidation of Eu<sup>2+</sup> by H<sup>+</sup> ( $E^0 = 0.00$  V) and sufficiently low to prevent hydrolysis of Sm<sup>3+</sup> or Eu<sup>3+</sup>. Too low pH levels lead to preferential H<sub>2</sub> generation in contact with Zn<sup>0</sup>, *i.e.* Eu<sup>3+</sup> will only be reduced as soon as the H<sup>+</sup> concentration is sufficiently low. Therefore, pH of the aqueous feed solution after reduction will only be slightly acidic. The pH was



measured after  $\text{Eu}^{3+}$  reduction and after extraction by means of a Hamilton Slimtrode pH electrode coupled to a Mettler-Toledo SevenCompact pH meter.

### Preparation of the water-immiscible phase

The water-immiscible phase consisted of neat  $[\text{A336}][\text{NO}_3]$  or  $[\text{A336}][\text{NO}_3]$  containing 0.05 M DCH18C6. Neat  $[\text{A336}][\text{NO}_3]$  was prepared from commercially available  $[\text{A336}][\text{Cl}]$  by a metathesis reaction.  $[\text{A336}][\text{Cl}]$  was dissolved in acetonitrile to decrease the viscosity of the IL and to enhance phase separation. An aqueous solution containing 8 M  $\text{NH}_4\text{NO}_3$  was mixed intensively with the  $[\text{A336}][\text{Cl}]$ -acetonitrile solution. This way, chloride anions were replaced by nitrate anions, a process that is favorable according to the Hofmeister series since nitrate ions are less strongly solvated than chloride ions.<sup>29</sup> After mixing and phase separation, the aqueous phase was removed and tested for remaining chloride by addition of a  $\text{AgNO}_3$  solution. This process was repeated until no chloride traces could be found in the aqueous phase. After achieving full conversion of  $[\text{A336}][\text{Cl}]$  to  $[\text{A336}][\text{NO}_3]$ , acetonitrile was removed by means of a rotary evaporator, followed by treatment at high vacuum using a Schlenk line. Analysis of the final, dry  $[\text{A336}][\text{NO}_3]$  by total reflection X-ray fluorescence (TXRF) showed a remaining chloride concentration of ca. 4 ppm (analysis procedure in ESI†).<sup>30</sup> The ionic liquid was equilibrated with water (Milli-Q) prior to its use in solvent extraction experiments to avoid any significant volume changes during the extraction experiment.

### Extraction experiments

The aqueous feed solutions contained both Sm and Eu. The concentration of each lanthanide was  $1 \text{ g L}^{-1}$  ( $6.6 \times 10^{-3} \text{ M}$ ). Only stable isotopes of samarium and europium were used. The chloride or nitrate concentrations in the aqueous feed solutions were adjusted by the addition of the respective ammonium or lithium salts. Exact concentrations of samarium and europium in the solution after reduction by zinc were determined by ICP-OES. A 1 mL aliquot of the aqueous feed solution was mixed with 1 mL of organic phase, after the reduction of  $\text{Eu}^{3+}$  to  $\text{Eu}^{2+}$ . This organic phase consisted of neat  $[\text{A336}][\text{NO}_3]$  or  $[\text{A336}][\text{NO}_3]$  containing 0.05 M DCH18C6. Both phases were purged intensively with nitrogen gas before extraction to prevent oxidation of  $\text{Eu}^{2+}$  by dissolved oxygen. Both phases were mixed in a 4 mL glass reaction vial at 1700 rpm making use of an Allsheng TMS-200 thermoshaker. Various mixing times (5, 15, 30 and 60 min) and temperatures (25, 40 and 60 °C) were tested in triplicate to find the most suitable separation conditions. After mixing, the reaction vials were centrifuged for 1 min at 5300 rpm using a Thermo Scientific Heraeus 200 Centrifuge to accelerate phase disengagement. Next, the aqueous phase was separated from the ionic liquid phase prior to analysis by ICP-OES. The efficiency of the separation method was evaluated by means of the distribution ratio, the fraction extracted and the separation factor. The distribution ratio ( $D$ ) of a compound is defined as the ratio of the total concentration of this compound in the extract phase to its total concentration in the initial phase:

$$D = \frac{[\text{M}]_{\text{IL,final}}}{[\text{M}]_{\text{Aq,final}}} = \frac{[\text{M}]_{\text{Aq,initial}} - [\text{M}]_{\text{Aq,final}}}{[\text{M}]_{\text{Aq,final}}} \quad (1)$$

In this equation, the volumes of both phases are equal.  $[\text{M}]_{\text{Aq,initial}}$  represents the initial concentration of the compound in the aqueous feed solution,  $[\text{M}]_{\text{Aq,final}}$  and  $[\text{M}]_{\text{IL,final}}$  represent the concentration of the compound in the aqueous and ionic liquid phase, respectively, after extraction. The fraction extracted (%  $E$ , also percentage extraction) is defined as the ratio of the amount of compound extracted to its total amount in the system. In case both phases are present in equal volume, the fraction extracted can be expressed as:

$$\%E = \frac{[\text{M}]_{\text{IL,final}}}{[\text{M}]_{\text{total}}} \times 100 = \frac{[\text{M}]_{\text{Aq,initial}} - [\text{M}]_{\text{Aq,final}}}{[\text{M}]_{\text{Aq,initial}}} \times 100 \quad (2)$$

In case more elements are present, one can describe the separation factor ( $\alpha$ ), which is the ratio of the distribution ratios of two compounds A and B:

$$\alpha = \frac{D_{\text{A}}}{D_{\text{B}}}, \quad \text{with } D_{\text{A}} \geq D_{\text{B}} \quad (3)$$

Aqueous solutions, *i.e.* the feed solution after reduction by  $\text{Zn}^0$  and the aqueous phase after extraction, were analyzed by using a Perkin Elmer Optima 8300 inductively coupled plasma optical emission spectrometer (ICP-OES) in axial view, with a GemTip CrossFlow II nebulizer, a Scott spray chamber assembly, a sapphire injector and a Hybrid XLT quartz-ceramic torch. Calibration curves were constructed by fitting the results of standard solutions containing 0.01, 0.1, 1 and 10  $\text{mg L}^{-1}$  Sm, Eu, Sr and/or Zn through the origin. Samples of the aqueous solutions to be measured by ICP-OES were diluted 100 times by a 2 wt%  $\text{HNO}_3$  solution.

## Results

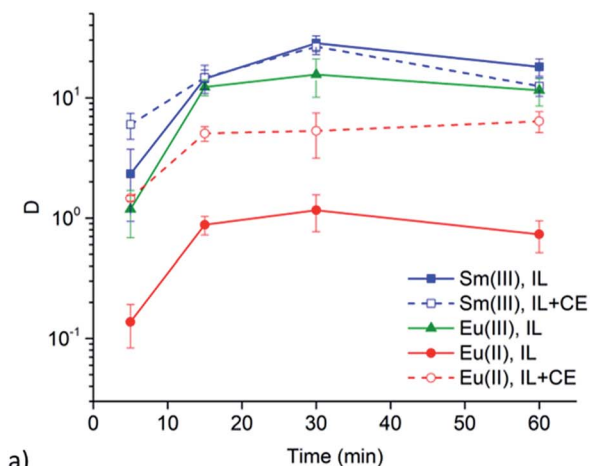
### Selection of anion source and concentration

In a first series of screening experiments, the extraction behavior of  $\text{Sr}^{2+}$  by the crown-ether-containing ionic liquid solution was studied as a simulant for  $\text{Eu}^{2+}$ . Different anion concentrations were used in the aqueous feed solution, *i.e.* 0, 1, 3, 6 and 8 M. Three different sources were used to vary the anion concentration, *i.e.*  $\text{HX}$ ,  $\text{NH}_4\text{X}$  and  $\text{LiX}$  (with  $\text{X} = \text{Cl}^-$  or  $\text{NO}_3^-$ ). Extractions were performed using both  $[\text{A336}][\text{NO}_3]$  (IL) and  $[\text{A336}][\text{NO}_3] + 0.05 \text{ M DCH18C6}$  (IL + CE). Results of these screening experiments are reported in the ESI.† Based on these results, following experiments were conducted with a 6 M lithium salt aqueous feed solution.

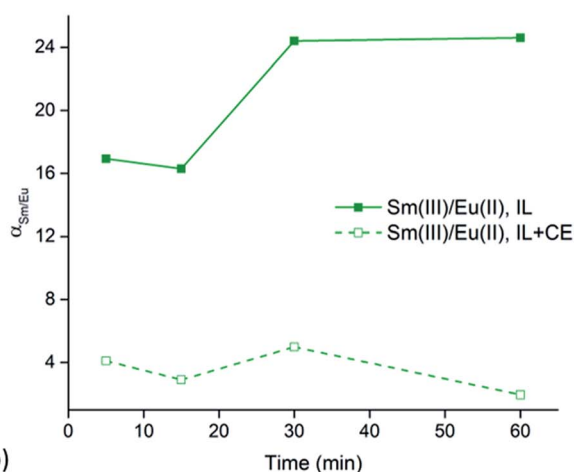
### Time dependence of $\text{Sm}^{3+}/\text{Eu}^{2+}$ separation

Extraction experiments with 6 M  $\text{LiX}$  (with  $\text{X} = \text{Cl}^-$  or  $\text{NO}_3^-$ ) aqueous feed solutions were performed to study the extraction rates of  $\text{Sm}^{3+}$  and  $\text{Eu}^{2+}$ . For comparison and completeness, the extraction of  $\text{Eu}^{3+}$  in the same conditions was studied as well. The feed solutions were mixed with both  $[\text{A336}][\text{NO}_3]$  (IL) and





a)



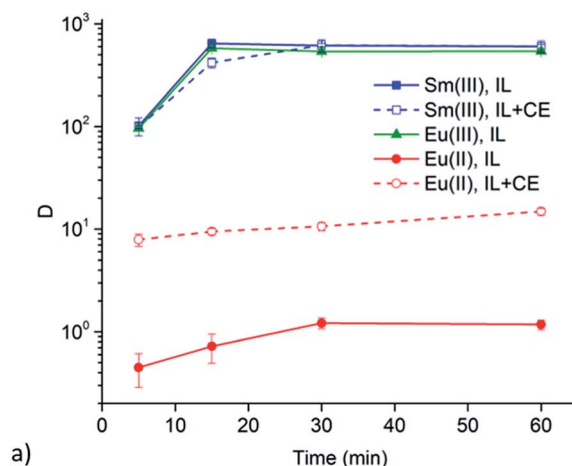
b)

Fig. 3 (a) Distribution ratios (log scale) of  $\text{Sm}^{3+}$  (blue, squares),  $\text{Eu}^{3+}$  (green, triangles) and  $\text{Eu}^{2+}$  (red, circles) and (b) the corresponding separation factor as a function of time (5, 15, 30 and 60 min) using a 6 M  $\text{LiCl}$  aqueous feed solution. The organic phase consisted of neat  $[\text{A336}][\text{NO}_3]$  (IL, solid line, solid symbol) or  $[\text{A336}][\text{NO}_3] + 0.05 \text{ M}$  DCH18C6 (IL + CE, dashed line, open symbol). Extraction parameters:  $\text{O/A} = 1$ ,  $60^\circ\text{C}$  and 1700 rpm.

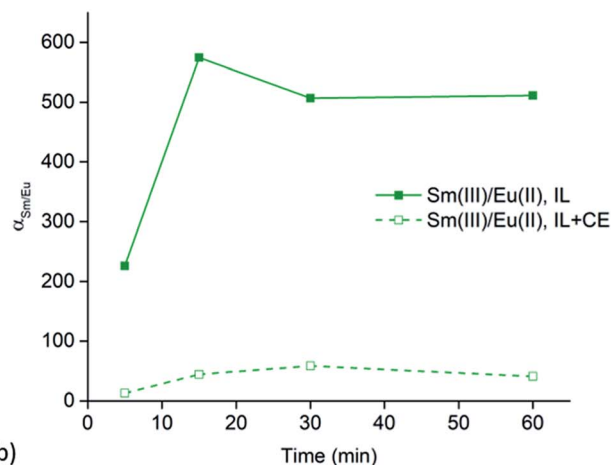
$[\text{A336}][\text{NO}_3] + 0.05 \text{ M}$  DCH18C6 (IL + CE). The distribution ratios of both lanthanides after extraction from a 6 M  $\text{LiCl}$  and a 6 M  $\text{LiNO}_3$  aqueous feed solution are plotted as a function of time in Fig. 3a and 4a. It is immediately clear that high distribution ratios were obtained for the trivalent lanthanides in both systems, especially when using a nitrate aqueous feed solution. As expected, the presence of the crown ether did not influence the extraction behavior of  $\text{Sm}^{3+}$ .  $\text{Eu}^{2+}$  was only reasonably well extracted in presence of the crown ether. Therefore, highest separation factors were reached without the use of a crown ether (Fig. 3b and 4b). It is also clear that separation of the  $\text{Sm}^{3+}$ – $\text{Eu}^{2+}$  couple from a nitrate aqueous feed solution is much more efficient compared to a chloride aqueous feed solution.

### Temperature dependence of $\text{Sm}^{3+}/\text{Eu}^{2+}$ separation

Extractions of  $\text{Sm}^{3+}$  and  $\text{Eu}^{2+}$  were executed at 25, 40 and  $60^\circ\text{C}$  to evaluate the influence of the viscosity of the ionic liquid



a)



b)

Fig. 4 (a) Distribution ratios (log scale) of  $\text{Sm}^{3+}$  (blue, squares),  $\text{Eu}^{3+}$  (green, triangles) and  $\text{Eu}^{2+}$  (red, circles) and (b) the corresponding separation factors as a function of time (5, 15, 30 and 60 min) using a 6 M  $\text{LiNO}_3$  aqueous feed solution. The organic phase consisted of neat  $[\text{A336}][\text{NO}_3]$  (IL, solid line, solid symbol) or  $[\text{A336}][\text{NO}_3] + 0.05 \text{ M}$  DCH18C6 (IL + CE, dashed line, open symbol). Extraction parameters:  $\text{O/A} = 1$ ,  $60^\circ\text{C}$  and 1700 rpm.

phase. Results of these extractions from chloride and nitrate aqueous feed solution (6 M of the respective lithium salt) are presented in Fig. 5a and b, respectively. Both graphs show that a change in temperature, and thus a change in viscosity, does not lead to any significant changes in extraction behavior of both  $\text{Sm}^{3+}$  and  $\text{Eu}^{2+}$ .

### Extraction behavior of $\text{Zn}^{2+}$ impurities

$\text{Eu}^{3+}$  can be efficiently and selectively reduced by  $\text{Zn}^0$ , generating  $\text{Zn}^{2+}$  in the feed solution. Therefore, the extraction behavior of  $\text{Zn}^{2+}$  from both chloride and nitrate aqueous feed solutions was studied and compared to the extraction behavior of  $\text{Sm}^{3+}$  and  $\text{Eu}^{2+}$ . From Fig. 6, it is clear that the extraction of  $\text{Zn}^{2+}$  strongly depends on the anions present in the extraction system. The extraction of  $\text{Zn}^{2+}$  proceeded very efficient in case of a high chloride concentration. Therefore, the extraction of  $\text{Zn}^{2+}$  from chloride media led to very high distribution ratios. On the





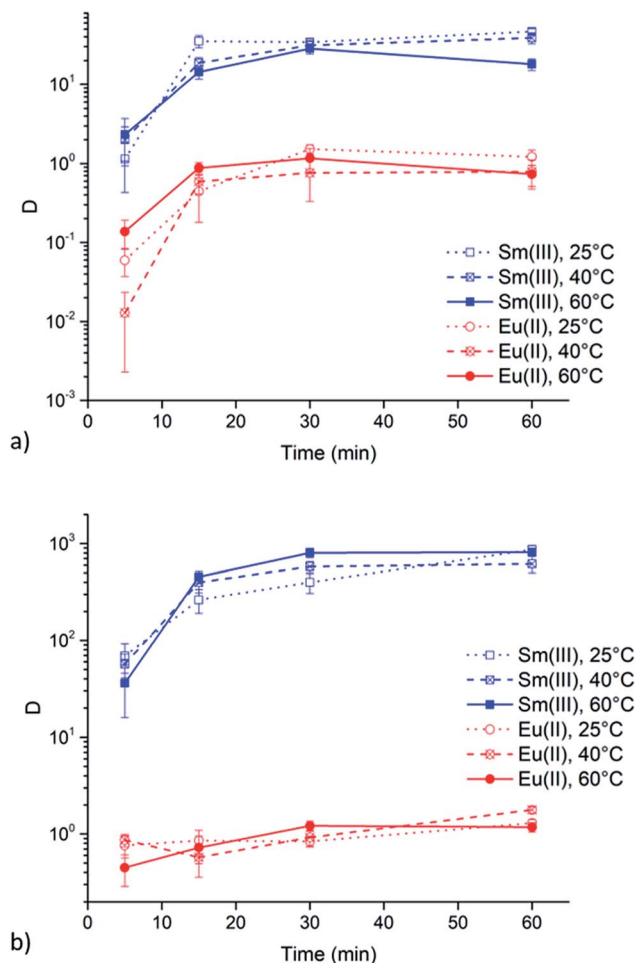


Fig. 5 Distribution ratios (log scale) of  $\text{Sm}^{3+}$  (blue, squares) and  $\text{Eu}^{2+}$  (red, circles) as a function of time (5, 15, 30 and 60 min) using 6 M  $\text{LiNO}_3$  (a) and 6 M  $\text{LiNO}_3$  (b) in the aqueous feed solution at different temperatures (25, 40 and 60 °C). The organic phase consisted of neat  $[\text{A336}][\text{NO}_3]$ . Extraction parameters: O/A = 1 and 1700 rpm.

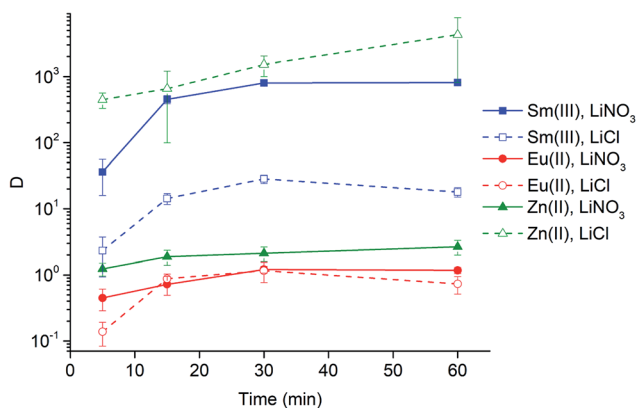


Fig. 6 Distribution ratios (log scale) of  $\text{Sm}^{3+}$  (blue, squares),  $\text{Eu}^{2+}$  (red, circles) and  $\text{Zn}^{2+}$  (green, triangles) as a function of time (5, 15, 30 and 60 min) using 6 M  $\text{LiNO}_3$  (solid line, solid symbol) and LiCl (dashed line, open symbol) in the aqueous feed solution. The organic phase consisted of neat  $[\text{A336}][\text{NO}_3]$ . Extraction parameters: O/A = 1, 60 °C 1700 rpm.

contrary,  $\text{Zn}^{2+}$  was hardly extracted in case only nitrate anions were present in the extraction system. The extraction behavior of  $\text{Zn}^{2+}$  in nitrate media proved to be comparable to the one of  $\text{Eu}^{2+}$ .

## Discussion

### Defining two separation approaches

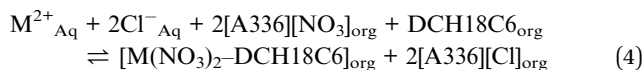
In this study, the separation of samarium and europium was investigated with and without the use of a size selective extractant. Many studies report on the efficient extraction of  $\text{Sr}^{2+}$  by a 18-crown-6 (18C6) derivative as extractant.<sup>31–34</sup> These 18C6-based crown ethers are able to capture a metal ion with a specific ion size in their cavity (2.6–3.2 Å). The six oxygen atoms of the crown ether serve as donor atoms to coordinate the metal ion.<sup>35</sup> Therefore, they are considered to be highly size-selective.<sup>36</sup> Ions that are either too large or too small do not interact properly with the crown ether. This also accounts for the trivalent lanthanides ( $\text{Ln}^{3+}$ ), which have an ionic radius varying from 0.977 Å for  $\text{Lu}^{3+}$  to 1.16 Å for  $\text{La}^{3+}$  (values given for coordination number 8). Moreover, the considerable hydration energy of trivalent lanthanide ions prevents efficient coordination by the crown ether. Lowering of the oxidation state, *i.e.* the addition of an electron, leads to an increased ionic radius, a decreased charge density and a decreased hydration enthalpy. Thus,  $\text{Ln}^{2+}$  ions are more favorable to properly interact with 18C6-based extractants.<sup>37</sup> In the lanthanide series, only europium has a relatively stable divalent state in aqueous solutions because of its half-filled 4f subshell. Therefore, the use of a size-selective extractant to selectively trap the  $\text{Eu}^{2+}$  impurities in the 18C6-cavity in the organic phase was studied as a first approach to separate the Sm/Eu couple, leaving  $\text{Sm}^{3+}$  behind in the aqueous phase. In this study, dicyclohexano-18-crown-6 (DCH18C6) was used because of its high hydrophobicity and because DCH18C6 already served well in extracting  $\text{Sr}^{2+}$  in numerous studies. The ionic radius of  $\text{Eu}^{2+}$  (1.25 Å) is similar to the one of  $\text{Sr}^{2+}$  (1.26 Å). Moreover, DCH18C6 already proved to be significantly radiation-resistant.<sup>38–42</sup>

The alkaline extraction capacities of the ionic liquid itself were used in a second approach, without the addition of any extractants. Trivalent lanthanide ions have the advantage of being able to form anionic complexes with bidentate nitrate ligands, whereas divalent metal ions are unable to form these species.<sup>23,43</sup>  $\text{Sm}^{3+}$  will thus be extracted to the water-immiscible ionic liquid phase, while  $\text{Eu}^{2+}$  remains in the aqueous phase. Vander Hoogerstraete *et al.* showed the efficiency of this strategy to recycle rare-earth elements from permanent magnets and nickel metal hydride batteries.<sup>23</sup> Both approaches were studied in parallel throughout the experiments.

In both approaches, the water-immiscible phase consisted of the highly hydrophobic ionic liquid Aliquat 336 nitrate ( $[\text{A336}][\text{NO}_3]$ ). Indeed, the use of this type undiluted ionic liquids proved to be selective for separation of rare earth elements (REEs) in previous solvent extraction studies.<sup>19–23,43</sup> The rationale behind the use of  $[\text{A336}][\text{NO}_3]$  is fourfold. (1) The use of  $[\text{A336}][\text{NO}_3]$  ensures a system complying completely with the CHON principle, making use of compounds containing only

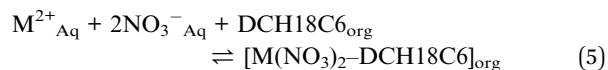


carbon (C), hydrogen (H), oxygen (O) and nitrogen (N).<sup>44,45</sup> This is highly important for the final disposal and waste treatment of the ionic liquid, which becomes radioactively contaminated when applied for separation of radiolanthanides, an aspect that is frequently overlooked in nuclear applications on ionic liquids. (2) Ionic liquids have promising properties compared to conventional molecular solvents, leading to processes with increased safety, chemical stability and radiation-resistivity.<sup>46–48</sup> (3) [A336][NO<sub>3</sub>] possesses a highly hydrophobic cation whereas the inorganic anion is well soluble in both the aqueous and ionic liquid phase. This ensures a minimal amount of organic compounds ending up in the aqueous phase after extraction. This is opposite to the [C<sub>n</sub>mim][Tf<sub>2</sub>N] ionic liquids that are frequently used in combination with 18C6-based crown ethers.<sup>31,34,49</sup> These ionic liquids operate *via* a cation extraction mechanism in case a short alkyl chain (C<sub>n</sub>) is used, losing ionic liquid cations to the aqueous phase. This, however, is unfavorable because these contaminations are not compatible with any pharmaceutical application. Additionally, radiolysis of the fluorinated anion can generate harmful and hazardous compounds. (4) [A336][NO<sub>3</sub>] is a source of nitrate ions for improved extraction efficiency in a split-anion extraction mechanism in case the feed solution contains chloride ions.<sup>50</sup> Nitrate ions are more efficient in coordinating the metal ions in crown ether complexes compared to chloride ions. The small bite angle of nitrate ions allows them to coordinate the metal ions bidentately, *i.e.* taking up little space in the coordination sphere, whereas chloride can only coordinate monodentately. The formation of two M–O bonds is energetically more favorable than the formation of one M–Cl bond, outweighing the considerable M–OH<sub>2</sub> bond energy. This way, the neutral [Sr(NO<sub>3</sub>)<sub>2</sub>–DCH18C6] and [Eu(NO<sub>3</sub>)<sub>2</sub>–DCH18C6] complexes are formed preferentially. Extraction to the ionic liquid phase occurs *via* neutral complex partitioning, indicated by the increase in extraction efficiency (reflected in the rising distribution ratio) with increasing anion concentration (Fig. S2, ESI†).<sup>34</sup> This is similar to the extraction of alkaline earth metals by crown ethers in molecular diluents, like 1-octanol.<sup>49</sup> Ion exchange mechanisms, like observed by Garvey *et al.* for [C<sub>n</sub>mim][Tf<sub>2</sub>N], are unlikely to happen. In the proposed extraction mechanism, anions have to be co-extracted to maintain charge-neutrality. When extracting from chloride aqueous media, chloride anions replace the nitrate anions of the ionic liquid (eqn (4)), similar to the so-called split-anion extraction by Larsson and Binnemans.<sup>50</sup>



This reaction, however, might be hampered because of the considerable hydration energy of the chloride ions.<sup>33,34,50</sup> Dehydration, extraction and solvation by the ionic liquid might thus be unfavorable. The use of high salt concentrations in the aqueous feed increases the ionic strength significantly, resulting in less hydrated ions. This way, the ions are more prone to form extractable species. Extraction from nitrate aqueous solutions can proceed more efficiently because of

their lower hydration energy (eqn (5)). Moreover, the ionic liquid phase is composed of nitrate ions, resulting in a more favorable transfer according to the Hofmeister series.<sup>29</sup>



### Selection of anion source and concentration

In a first series of screening experiments, the extraction behavior of Sr<sup>2+</sup> as Eu<sup>2+</sup> simulant was studied to find the optimal extraction parameters. Different anion concentrations and anion sources were used in the aqueous feed solution. Most efficient extraction of Sr<sup>2+</sup> by [A336][NO<sub>3</sub>]-DCH18C6 was obtained using an aqueous phase with high lithium salt concentration (Fig. S1, ESI†). The use of other anion sources, *i.e.* HX and NH<sub>4</sub>X (with X = Cl<sup>−</sup> or NO<sub>3</sub><sup>−</sup>), proved to be much less efficient, resulting in much lower distribution ratios. The lower efficiency by using HX and NH<sub>4</sub>X was most probably due to the occupation of the crown ether cavity by H<sub>3</sub>O<sup>+</sup> and NH<sub>4</sub><sup>+</sup>. Previous studies already proved that these ions could properly fit in this cavity because of their ion size.<sup>51,52</sup> Li<sup>+</sup> has a smaller ionic radius and therefore interacts less efficiently with the crown ether, resulting in better extraction results. Thus, the selection of a non-interfering source of additional anions is of high importance in these crown-ether-based extraction systems.

After irradiation, the target material, *i.e.* Sm<sub>2</sub>O<sub>3</sub>, has to be dissolved. Most frequently, this is done by means of concentrated mineral acids, like HCl or HNO<sub>3</sub>. However, high acid concentrations are disadvantageous for two reasons. First of all, Eu<sup>2+</sup> is extracted less efficiently by the crown ether from highly acidic media because the H<sub>3</sub>O<sup>+</sup> ions occupy the cavity of the crown ether. Secondly, Eu<sup>2+</sup> is unable to be stabilized in a high H<sup>+</sup> concentration. Additionally, significant volumes of hydrogen gas would be generated during the reduction step, leading to unsafe situations. Therefore, the mixture should be adjusted to the most ideal extraction conditions after dissolution, meaning an increase in pH and anion concentration by the addition of non-interfering compounds. Evaporation to almost dryness followed by dissolution in other aqueous media is another possibility.

Because of their similar charge density and ionic radius, comparable extraction trends for Eu<sup>2+</sup> and Sr<sup>2+</sup> were to be expected. It was observed that Eu<sup>2+</sup> follows indeed a similar trend as Sr<sup>2+</sup> when extracted by DCH18C6 from chloride and nitrate aqueous media (Fig. S2, ESI†). Reasonably high distribution ratios were obtained using high salt concentrations, *i.e.* ≥ 6 M LiX. Again, the use of nitrate aqueous media yielded in much higher extraction efficiency compared to the use of chloride aqueous media, leading to distribution ratios well above (1).

It was noted that a significant amount of Eu<sup>2+</sup>, was also extracted towards the DCH18C6-free ionic liquid phase when using high salt concentrations. Significant extraction of Eu<sup>2+</sup> in a DCH18C6-free system was not expected since it deviates from the behavior of Sr<sup>2+</sup>, where no extraction was observed at all. Therefore, it is believed that a partial re-oxidation of Eu<sup>2+</sup> to

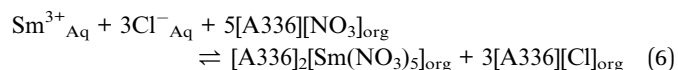


$\text{Eu}^{3+}$  have occurred during these experiments, whereby  $\text{Eu}^{3+}$  is extracted towards the organic phase without the interaction of a crown ether. Therefore, it is important to keep the extraction time as low as possible.

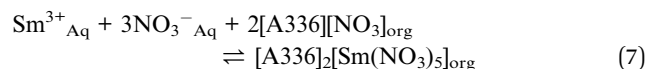
### Time dependence of $\text{Sm}^{3+}/\text{Eu}^{2+}$ separation

The significant extractability of  $\text{Eu}^{2+}$  by  $[\text{A336}][\text{NO}_3] + 0.05 \text{ M DCH18C6}$  and the low extractability of  $\text{Eu}^{2+}$  by  $[\text{A336}][\text{NO}_3]$  seem to support both separation approaches so far. To arrive at a separation system, it is important to study the extraction behavior of  $\text{Sm}^{3+}$  as well. A fast separation is advantageous taking into account the decay of  $^{153}\text{Sm}$  and possible re-oxidation of  $\text{Eu}^{2+}$ . Therefore, the distribution ratios of samarium and europium were studied as a function of time. For comparison and completeness, the distribution ratio of  $\text{Eu}^{3+}$  in the same conditions was studied in parallel.

From the extraction results in Fig. 3a and 4a, from chloride and nitrate media, respectively, it was immediately clear that much higher distribution ratios were obtained for  $\text{Sm}^{3+}$  compared to  $\text{Eu}^{2+}$ , with and without the use of DCH18C6. As expected, the presence of DCH18C6 in the ionic liquid did not influence the extraction behavior of  $\text{Sm}^{3+}$  because of its smaller ionic radius and higher hydration energy. The high difference in distribution ratio allows an efficient Sm/Eu separation. The DCH18C6-free system is favored because of the much lower  $\text{Eu}^{2+}$  extraction. Separation factors of 24 were reached using chloride media (Fig. 3b), whereas separation factors well above 600 were reached using nitrate media (Fig. 4b).  $\text{Sm}^{3+}$  was extracted to the ionic liquid phase *via* the split-anion extraction mechanism, as was described by Larsson and Binnemans (eqn (6)).<sup>50</sup> This extraction mechanism makes use of the strong affinity of nitrate ions for the IL phase, while the chloride ions have a higher affinity for the aqueous phase.



According to this extraction mechanism, the ionic liquid phase serves as a source of complexing anions. This way, no additional extractants are needed. However, chloride ions have to be transferred to the ionic liquid phase as well to ensure charge neutrality. The extraction of chloride ions is hampered because of their considerable hydration energy, as was also the case for the extraction of  $\text{M}^{2+}$  by DCH18C6 from chloride media. The much higher extraction efficiency for  $\text{Sm}^{3+}$  from nitrate aqueous media can be attributed to the lower hydration energy and higher hydrophobicity of nitrate ions.<sup>29,34</sup> The high nitrate concentrations are needed to form extractable species. Trivalent lanthanide ions show the advantage of being able to form anionic complexes with bidentate nitrate ligands, whereas other elements cannot.<sup>23</sup> Vander Hoogerstraete *et al.* already showed that the trivalent lanthanides ( $\text{Ln}^{3+}$ ) are extracted as pentanitrate complexes  $[\text{Ln}(\text{NO}_3)_5]^{2-}$  (eqn (7)). Speciation studies using extended X-ray absorption fine structure (EXAFS) support this extraction behavior (ESI).



Larsson and Binnemans already pointed out that all trivalent lanthanides ( $\text{Ln}^{3+}$ ) show a similar extraction behavior with quaternary ammonium ionic liquids, with a decreasing trend in extraction efficiency across the lanthanide series.<sup>50</sup> Thus, the slightly lower extraction efficiency of  $\text{Eu}^{3+}$  compared to  $\text{Sm}^{3+}$  is in full agreement with these findings (Fig. 3b and 4b). The slightly lower extractability of  $\text{Eu}^{3+}$  can probably be attributed to its slightly higher hydration energy because of its smaller ionic radius.<sup>53,54</sup> Nevertheless, it is obvious that no efficient separation can be achieved without reduction of europium.

The high distribution ratios of  $\text{Sm}^{3+}$  are favorable for the second separation approach, *i.e.* the extraction of  $\text{Sm}^{3+}$  to the ionic liquid phase, while  $\text{Eu}^{2+}$  remains in the aqueous phase. Therefore, it can be concluded that the first separation approach, making use of a size-selective extractant to extract  $\text{Eu}^{2+}$ , becomes superfluous. This also implies that different chloride or nitrate salts can be used to increase the salt concentration in the aqueous feed solution, *i.e.* the origin of the salt is less of importance regarding the separation method. Therefore, a salt causing less problems regarding the intended medical application can be chosen. Of course, the salt has to be highly soluble in the aqueous feed to reach the required concentration for optimal separation.

Efficient stripping of  $\text{Sm}^{3+}$  from the loaded IL phase can be achieved by decreasing the salt concentration in the aqueous phase, *i.e.*  $\text{Sm}^{3+}$  can be stripped by water.<sup>43</sup> Reduction of the salt concentration in the system leads to a lower ionic strength.  $\text{Sm}^{3+}$  can thus be hydrated more easily, *i.e.*  $\text{Sm}^{3+}$  gains higher affinity for the aqueous phase. Therefore, no harsh conditions, like highly acidic media, are needed.  $\text{Sm}^{3+}$  was quantitatively (>98%) back-extracted to the aqueous phase by water in a single step. The strip solution can be slightly acidified to prevent any hydrolysis of  $\text{Sm}^{3+}$ .

### Temperature dependence of $\text{Sm}^{3+}/\text{Eu}^{2+}$ separation

Undiluted ionic liquids are highly viscous at room temperature. This is also the case for quaternary ammonium ionic liquids containing long carbon chains, like  $[\text{A336}][\text{NO}_3]$ . This high viscosity implies a more difficult mass transfer, leading to reduced extraction speed. However, the viscosity drastically decreases with increasing temperature. Therefore, the above mentioned results were all obtained at 60 °C, a temperature at which  $[\text{A336}][\text{NO}_3]$  has a significant lower viscosity but at which experiments are still easy to handle. The viscosity of water-saturated  $[\text{A336}][\text{NO}_3]$  decreases from 204 mPa s at 25 °C to 95 mPa s at 40 °C and 42 mPa s at 60 °C. Extractions of  $\text{Sm}^{3+}$  and  $\text{Eu}^{2+}$  were executed at these temperatures to evaluate the influence of a changing viscosity of the ionic liquid phase. The results in Fig. 5 show that a change in temperature, and thus a change in viscosity, does not lead to significant changes in the extraction behavior of both  $\text{Sm}^{3+}$  and  $\text{Eu}^{2+}$ . Therefore, mass transfer might not be the rate-determining step.



### Extraction behavior of $\text{Zn}^{2+}$ impurities

$\text{Eu}^{3+}$  can be efficiently and selectively reduced using chemical or electrochemical reduction methods. The chemical method makes use of  $\text{Zn}^0$  grains, which are oxidized to  $\text{Zn}^{2+}$ . Hence, the introduction of extra impurities in the feed solution must be taken into account when using this chemical reduction method. Therefore, the extraction behavior of  $\text{Zn}^{2+}$  from both chloride and nitrate aqueous feed solution was studied and compared to the extraction behavior of  $\text{Sm}^{3+}$ . The results in Fig. 6 clearly show that the extraction of  $\text{Zn}^{2+}$  is highly dependent on the anions present in the extraction system, *i.e.*  $\text{Zn}^{2+}$  is hardly extracted in case only nitrate anions are present in the extraction system, whereas the extraction of  $\text{Zn}^{2+}$  is very high in case of high chloride concentrations. This observation was expected because it is well known that the extraction of transition metals to quaternary ammonium and phosphonium chloride ionic liquids proceeds efficiently.<sup>19,55</sup> Therefore, the extraction of  $\text{Zn}^{2+}$  from chloride media gives very high distribution ratios. Hence,  $\text{Sm}^{3+}$  can be efficiently separated from  $\text{Zn}^{2+}$  *via* selective stripping of the loaded  $[\text{A336}][\text{NO}_3]$  phase.  $\text{Sm}^{3+}$  is transferred back to the aqueous phase upon reduction of the salt concentration in the system, while  $\text{Zn}^{2+}$  remains in the organic phase because of its high affinity for the ionic liquid. However, another approach is needed in case of an extraction from nitrate media, considering the low extractability of  $\text{Zn}^{2+}$  from nitrate media. In fact, the extraction behavior of  $\text{Zn}^{2+}$  is comparable to that of  $\text{Eu}^{2+}$ . Therefore, reasonably good separation from samarium

can already be achieved in the forward extraction step. Considering these results,  $\text{Zn}^{2+}$  impurities originating from the chemical reduction method can be efficiently removed.

### Outlook: separation scheme for the purification of samarium-153

Based on this feasibility study, following full separation process concept to produce high purity samarium-153 can be proposed (Fig. 7): (1) dissolution of the target material by  $\text{HNO}_3$  and adjustment of the pH (4–6.5) and anion concentration (6 M  $\text{NO}_3^-$ ) by the addition of a non-interfering nitrate salt (*e.g.*  $\text{NH}_4\text{NO}_3$  or  $\text{LiNO}_3$ ). The total europium concentration must be adjusted by the addition of stable isotopes to facilitate the separation procedure. (2) The selective reduction of europium to its divalent state by zinc metal. (3) The forward extraction of  $\text{Sm}^{3+}$  to the ionic liquid phase, consisting of undiluted  $[\text{A336}][\text{NO}_3]$ .  $\text{Eu}^{2+}$  and  $\text{Zn}^{2+}$  remain in the aqueous phase. (4) Separation of both phases. (5) Stripping (=back-extraction) of  $\text{Sm}^{3+}$  from the loaded ionic liquid phase can be easily performed by the addition of water, lowering the total salt concentration.

## Conclusion

A feasibility study to develop an efficient method to separate samarium and europium was conducted in scope of the purification process to produce high-purity  $^{153}\text{Sm}$  for medical applications. The separation method consists of the selective reduction of  $\text{Eu}^{3+}$  by zinc metal in an aqueous feed solution containing a high chloride or nitrate salt concentration (6 M). Subsequent extraction using the quaternary ammonium ionic liquid  $[\text{A336}][\text{NO}_3]$  leads to a good separation of both lanthanides in a relatively short time frame.  $\text{Sm}^{3+}$  proved to be extracted to the neat  $[\text{A336}][\text{NO}_3]$  phase much more efficiently compared to  $\text{Eu}^{2+}$ . A first approach using the addition of DCH18C6 to capture  $\text{Eu}^{2+}$  in the ionic liquid phase proved to be less efficient. Therefore, the separation process using neat  $[\text{A336}][\text{NO}_3]$  is the preferred approach, extracting  $\text{Sm}^{3+}$  to the ionic liquid phase while  $\text{Eu}^{2+}$  remains in the aqueous phase. Moreover, it was shown that the use of a nitrate aqueous feed solution leads to a more efficient separation method compared to the use of a chloride aqueous feed solution.  $\text{Zn}^{2+}$  ions originating from the chemical reduction method showed a very low extractability in nitrate media. This way, simultaneous removal of  $\text{Eu}^{2+}$  and  $\text{Zn}^{2+}$  from  $\text{Sm}^{3+}$  can be achieved in the forward extraction step. Therefore, this separation method can be used to arrive at a purified product with extended shelf-life. This leads to an increased availability of  $^{153}\text{Sm}$  radioisotopes and a decreased background radiation of  $^{154}\text{Eu}$  in the patient after treatment. The separation method can also be applied for efficient removal of  $\text{Eu}^{2+}$  from any other  $\text{Ln}^{3+}$  because all trivalent lanthanide ions tend to have a similar extraction behavior as  $\text{Sm}^{3+}$ .

## Conflicts of interest

There are no conflicts to declare.

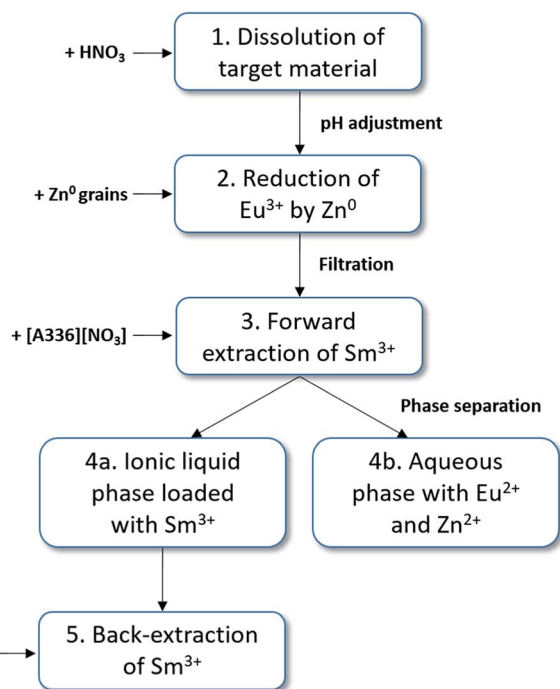


Fig. 7 Separation concept scheme for the purification of  $^{153}\text{Sm}$ . (1) Dissolution of the target material in  $\text{HNO}_3$  and adjustment of the pH and salt concentration, (2) reduction of  $\text{Eu}^{3+}$  by  $\text{Zn}^0$ , (3) forward extraction of  $\text{Sm}^{3+}$  to  $[\text{A336}][\text{NO}_3]$ , leaving  $\text{Eu}^{2+}$  and  $\text{Zn}^{2+}$  in the aqueous phase, (4) separation of both phases, (5) back-extraction of  $\text{Sm}^{3+}$  by addition of water.





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## References

- 1 P. Anderson and R. Nunez, *Expert Rev. Anticancer Ther.*, 2007, **7**, 1517–1527.
- 2 P. J. Blower, *Dalton Trans.*, 2015, **44**, 4819–4844.
- 3 A. J. Amoroso, I. A. Fallis and S. J. A. Pope, *Coord. Chem. Rev.*, 2017, **340**, 198–219.
- 4 M. Castro and A. Portilla, Sm-153 EDTMP - a new palliative therapy agent against pain in cases of bone metastases, in *Modern trends in radiopharmaceuticals for diagnosis and therapy*, IAEA-TECDOC-1029, IAEA, Vienna, 1998.
- 5 C. L. Maini, S. Bergomi, L. Romano and R. Sciuto, *Eur. J. Nucl. Med. Mol. Imaging*, 2004, **31**, S171–S178.
- 6 T. F. Sandeman, R. S. Budd and J. J. Martin, *Clinical Oncology*, 1992, **4**, 160–164.
- 7 S. Bhattacharyya and M. Dixit, *Dalton Trans.*, 2011, **40**, 6112–6128.
- 8 B. Ponsard, *J. Labelled Compd. Radiopharm.*, 2007, **50**, 333–337.
- 9 T. Loebe, B. Hettwig and H. W. Fischer, *Appl. Radiat. Isot.*, 2014, **94**, 40–43.
- 10 L. Moro, D. Fantinato, F. Frigerio, G. Shamhan and G. Angelovski, *J. Phys.: Conf. Ser.*, 2006, **41**, 535–537.
- 11 J. A. Kalef-Ezra, S. T. Valakis and S. Pallada, *Phys. Med.*, 2015, **31**, 104–107.
- 12 J. S. Preston and A. C. du Preez, *Miner. Process. Extr. Metall. Rev.*, 1998, **18**, 175–200.
- 13 J. S. Preston and A. C. du Preez, *J. Chem. Technol. Biotechnol.*, 1996, **65**, 93–101.
- 14 J. Garcia and M. J. Allen, *Eur. J. Inorg. Chem.*, 2012, 4550–4563.
- 15 T. Hirai and I. Komasa, *J. Chem. Eng. Jpn.*, 1992, **25**, 644–648.
- 16 T. Hirai and I. Komasa, *Miner. Process. Extr. Metall. Rev.*, 1997, **17**, 81–107.
- 17 S. Nishihama, T. Hirai and I. Komasa, *J. Solid State Chem.*, 2003, **171**, 101–108.
- 18 K. Van Hoecke, J. Bussé, M. Gysemans, L. Adriaensen, A. Dobney and T. Cardinaels, *J. Radioanal. Nucl. Chem.*, 2017, **314**, 1727–1739.
- 19 C. Deferm, M. Van de Voorde, J. Luyten, H. Oosterhof, J. Franssaer and K. Binnemans, *Green Chem.*, 2016, **18**, 4116–4127.
- 20 D. Dupont and K. Binnemans, *Green Chem.*, 2015, **17**, 856–868.
- 21 B. Onghena and K. Binnemans, *Ind. Eng. Chem. Res.*, 2015, **54**, 1887–1898.
- 22 A. Rout and K. Binnemans, *Dalton Trans.*, 2014, **43**, 1862–1872.
- 23 T. Vander Hoogerstraete and K. Binnemans, *Green Chem.*, 2014, **16**, 1594–1606.
- 24 G. Ye, F. Bai, J. Wei, J. Wang and J. Chen, *J. Hazard. Mater.*, 2012, **225–226**, 8–14.
- 25 H. Y. Zhou, T. L. Yu, Y. Y. Ao, J. Peng and M. L. Zhai, *Acta Phys.-Chim. Sin.*, 2014, **30**, 1581–1586.
- 26 G. Moreau, L. Helm, J. Purans and A. E. Merbach, *J. Phys. Chem. A*, 2002, **106**, 3034–3043.
- 27 G. Moreau, R. Scopelliti, L. Helm, J. Purans and A. E. Merbach, *J. Phys. Chem. A*, 2002, **106**, 9612–9622.
- 28 S. A. Sayed, K. A. Rabie and I. E. Salama, *Sep. Purif. Technol.*, 2005, **46**, 145–154.
- 29 D. Dupont, D. Depuydt and K. Binnemans, *J. Phys. Chem. B*, 2015, **119**, 6747–6757.
- 30 T. Vander Hoogerstraete, S. Jamar, S. Wellens and K. Binnemans, *Anal. Chem.*, 2014, **86**, 3931–3938.
- 31 S. Dai, Y. H. Ju and C. E. Barnes, *Dalton Trans.*, 1999, 1201–1202.
- 32 D. I. Djigailo, S. V. Smirnova, I. I. Torocheshnikova, A. G. Vendilo, K. I. Popov and I. V. Pletnev, *Moscow Univ. Chem. Bull.*, 2009, **64**, 130–133.
- 33 E. P. Horwitz, M. L. Dietz and D. E. Fisher, *Solvent Extr. Ion Exch.*, 1990, **8**, 199–208.
- 34 S. L. Garvey, C. A. Hawkins and M. L. Dietz, *Talanta*, 2012, **95**, 25–30.
- 35 C. J. Pedersen, *Science*, 1988, **241**, 536–540.
- 36 A. H. Bond, M. L. Dietz and R. Chiarizia, *Ind. Eng. Chem. Res.*, 2000, **39**, 3442–3464.
- 37 J. Christoffers and P. Starynowicz, *Polyhedron*, 2008, **27**, 2688–2692.
- 38 V. M. Abashkin, D. W. Wester, J. A. Campbell and K. E. Grant, *Radiat. Phys. Chem.*, 1996, **48**, 463–472.
- 39 Y. Ao, W. Yuan, T. Yu, J. Peng, J. Li, M. Zhai and L. Zhao, *Phys. Chem. Chem. Phys.*, 2015, **17**, 3457–3462.
- 40 M. Draye, A. Favre-Réguillon, R. Faure and M. Lemaire, *Radiat. Phys. Chem.*, 2008, **77**, 581–584.
- 41 E. I. Grigorev, O. V. Mikhailitsyna, S. V. Nesterov and L. I. Trakhtenberg, *High Energy Chem.*, 1997, **31**, 16–19.
- 42 S. V. Nesterov, *Russ. Chem. Rev.*, 2000, **69**, 769–782.
- 43 K. Larsson and K. Binnemans, *J. Sustain. Metall.*, 2017, **3**, 73–78.
- 44 H. H. Dam, D. N. Reinhoudt and W. Verboom, *Chem. Soc. Rev.*, 2007, **36**, 367–377.
- 45 J. Rydberg, M. Cox, C. Musikas and G. R. Choppin, *Solvent Extraction Principles and Practice*, Marcel Dekker Inc., USA, 2nd edn, 2004.
- 46 J. N. Chubb, P. Lagos and J. Lienlaf, *J. Electroanal. Chem.*, 2005, **63**, 119–127.
- 47 G. L. Hearn, *J. Loss Prev. Process Ind.*, 2002, **15**, 105–109.
- 48 D. Allen, G. Baston, A. E. Bradley, T. Gorman, A. Haile, I. Hamblett, J. E. Hatter, M. J. F. Healey, B. Hodgson, R. Lewin, K. V. Lovell, B. Newton, W. R. Pitner, D. W. Rooney, D. Sanders, K. R. Seddon, H. E. Sims and R. C. Thied, *Green Chem.*, 2002, **4**, 152–158.



- 49 M. L. Dietz and J. A. Dzielawa, *Chem. Commun.*, 2001, 2124–2125.
- 50 K. Larsson and K. Binnemans, *Hydrometallurgy*, 2015, **156**, 206–214.
- 51 E. Makrlík, P. Toman and P. Vaňura, *Acta Chim. Slov.*, 2013, **60**, 193–197.
- 52 P. Vaňura and E. Makrlík, *J. Radioanal. Nucl. Chem.*, 2001, **250**, 369–371.
- 53 S. Andersson, K. Eberhardt, C. Ekberg, J.-O. Liljenzin, M. Nilsson and G. Skarnemark, *Radiochim. Acta*, 2006, **94**, 469–474.
- 54 M. R. Antonio, D. R. McAlister and E. P. Horwitz, *Dalton Trans.*, 2015, **44**, 515–521.
- 55 K. Larsson and K. Binnemans, *Green Chem.*, 2014, **16**, 4595–4603.

