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Significantly enhanced dielectric and hydrophobic properties of SiO₂@MgO/PMMA composite films

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In this article, we provide a feasible method to prepare high-dielectric-constant hydrophobic composite films, which show potential application as the insulator layer in electrowetting devices. SiO₂@MgO core-shell nanoparticles were fabricated via a hydrolysis process and embedded into the PMMA matrix. The microstructure of the nanoparticles and the cross-section of the films indicated that a SiO₂ coating has successfully been prepared around the MgO particles with a thickness of about 20–30 nm and the nanofillers were homogeneously dispersed in the polymer. Hydrophobic films (contact angle ~115°) with appropriate glass transition temperature were obtained. The dielectric constant at various frequencies of the functional fillers enhanced with increasing the SiO₂@MgO filler content. The results suggested that SiO₂@MgO is more effective in increasing the dielectric constant of PMMA when compared with MgO sheets. Typically, the dielectric constant of the PMMA composite filled with 40 wt% SiO₂@MgO reaches 19.1 at 40 Hz, in contrast to 9.7 for the composite filled with 40 wt% MgO sheets and 3.8 for pristine PMMA. Also, the composites exhibited low electrical conductivity ($\leq 10^{-7}$) even at high frequency. All the improved performances showed potential application in the dielectric layer of electrowetting devices.

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Introduction

Electrowetting-on-dielectric is a small-scale liquid handling technology that has been significantly used for numerous applications, including electronic displays, optical devices, lab on a chip, liquid transport in microfluidic devices, and surface science.^{1–4} In recent years, the electrowetting display has been widely investigated and plays an important role in the field of display devices, combining the special reflective display characteristics of conventional printed paper with the changeable electronic information.^{2–5} Fig. 1 shows the principle of electrowetting, based on the voltage-controlled transformation of a coloured oil drop contrast to a white substrate.⁹ The applied voltage changed the electrical potential between the ITO electrode and the coloured drop, increasing the charge density in

the interface and resulting in a wetting and flattening variation of the oil droplet. The relationship between the applied voltage and change of contact angle at the solid-liquid interface can be described by the Young-Lippmann equation:^{3,6}

$$\cos \theta_U = \cos \theta_0 + \frac{\epsilon_0 \epsilon}{2d\gamma_{LV}} U^2 \quad (1)$$

where θ_U is the contact angle (CA) at applied voltage U , θ_0 is the CA without voltage bias, γ_{LV} is the interface energy between the liquid drop and ambient air, ϵ and d are the dielectric constant and thickness of the dielectric layer, respectively.

Dielectric layer is one of the vital sections in electrowetting display device, the materials selection and preparation of dielectric layer can directly influence the performance and application of the device. According to the eqn (1), the film should provide some special properties for the electrowetting display devices except for insulation. First, the surface should be hydrophobic to ensure a huge variation in contact angle under electrical field. Second, the film should have a comparatively small threshold voltage because a high actuation voltage may cause electrolysis of the droplet or the breakdown of film. The threshold voltage was related to the dielectric permittivity and thickness of insulating layer. While in most situations, ultra-thin insulators increased the contact angle range at the expense of electrical breakdown and even failed before the contact angle varied large enough.^{7,8} So, a film with high permittivity and hydrophobic properties is essential.

In general, dielectric material can be divided into two categories: polymer and ceramics. Polymers, such as amorphous fluoropolymer,¹³ PDMS,^{9,10} PI,^{11,12} parylene-C,¹¹ parylene-N¹³ and

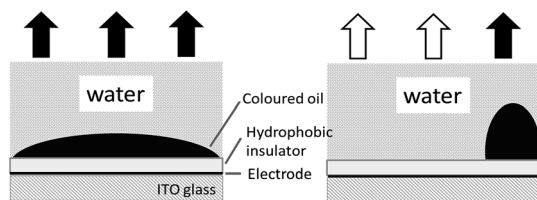


Fig. 1 The principle of electrowetting display.

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parylene-HT,¹⁴ offer the superiorities in hydrophobic properties, economy, low temperature processing and shape and large area preparation. But most of the dielectric constant value of hydrophobic polymer is less than 3, requiring high actuation voltage. For example, Teflon AF1600 (ref. 15 and 16) is a typical fluoropolymer used in electrowetting devices with a high contact angle ($\sim 120^\circ$), while the applied voltage of devices is up to 80 volts, owing to the low dielectric constant ϵ of Teflon AF1600 (1.93). However, common ceramic materials, such as SiO_2 (ref. 17 and 18) ($\epsilon \sim 4$), $(\text{Ba}, \text{Sr})\text{TiO}_3$ (ref. 19) (BST, $\epsilon \sim 180$), Ta_2O_5 (ref. 20–22) ($\epsilon = 20\text{--}25$), Si_3N_4 (ref. 23 and 24) ($\epsilon \sim 8$), and Al_2O_3 (ref. 24–26) ($\epsilon \sim 10$) have relatively high dielectric constant do not provide good hydrophobic property. Also in the preparation section, some special techniques like chemical vapor deposition (CVD), atomic layer deposition (ALD) and sputtering are required to deposit uniform oxide dielectrics, which are always along with high temperature. To reduce the actuation voltage, many researchers covered a thin layer of hydrophobic polymer on the high dielectric film to ensure a high contact angle. Bilayer structures such as Al_2O_3 -Cytop,¹² P (VDF-HFP)-Teflon AF,³² $\text{SiO}_2/\text{Si}_3\text{N}_4$ -Cytop,²⁴ AF1600/ $\text{Si}_3\text{N}_4/\text{TiO}_2$ (ref. 27) and Teflon-AF/CYTOP/ Ta_2O_5 (ref. 33) are used to control the movement of droplet. But this structure design makes the fabrication process complex, which increased the manufacturing cost.

In this work, PMMA³⁴ was chosen as polymer matrix; $\text{SiO}_2@\text{MgO}$ core-shell nanostructure was constructed and embedded into the PMMA for preparing the single-layer dielectric film with high permittivity and hydrophobic properties. In this structure, MgO nanofillers possess a relatively high permittivity ($\epsilon \sim 10$), which are imposed to increase the dielectric constant of PMMA. Furthermore, the permittivity contrast between the inorganic filler and the polymer matrix always lead to inhomogeneous distribution of the electric fields, which may deteriorate the systematic dielectric properties. For this reason, SiO_2 ($\epsilon \sim 4$) wrapped the MgO as interlayer between the fillers and the matrix and also protect MgO powders from hydrolysis and other physicochemical changes. Firstly, the MgO nanosheets were prepared *via* a hydrothermal process with an average thickness of 25 nm. Secondly, the surface-coated MgO nanosheets with a SiO_2 layer were synthesized by a simple hydrolysis process at ambient temperature. Lastly, a single-layer dielectric film is obtained by solution mixture and tape-casting process. A systematic study concerning the influence of nanofillers on dielectric properties, glass transition temperature, conductivity and contact angle of PMMA composites is showed. Commercial MgO-filled composites are also prepared to demonstrate the impact of nanofillers. The obtained $\text{SiO}_2@\text{MgO}/\text{PMMA}$ composites film exhibited high dielectric constant and hydrophobic properties, which has potential value in electrowetting devices.

Results and discussion

Fig. 2(a) shows the XRD patterns of the MgO nanosheets and the $\text{SiO}_2@\text{MgO}$ shell@core nanoparticles. The diffraction peaks of the (1 1 1), (2 0 0), and (2 2 0) planes can be indexed to the cubic ($Fm\bar{3}m$) MgO (JCPDS 45-0946). For $\text{SiO}_2@\text{MgO}$ nanoparticles,

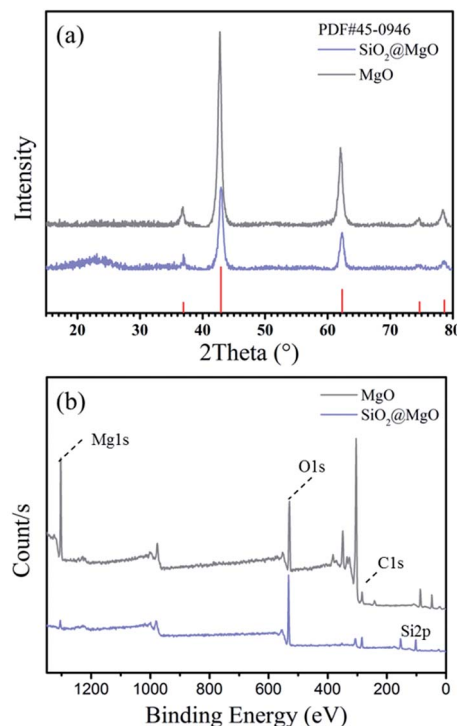


Fig. 2 (a) XRD patterns and (b) XPS of MgO nanosheets and $\text{SiO}_2@\text{MgO}$ powders.

there was no obvious characteristic peak of SiO_2 phase observed in the pattern, indicating that SiO_2 might exist as amorphous phases or has low crystallinity compared with the MgO nanoparticles. And MgO nanosheets show higher intensity of MgO characteristic peaks. To further confirm the composition of the coating, Fig. 2(b) compared the XPS survey spectrum of MgO and $\text{SiO}_2@\text{MgO}$. Both of the two samples contain mainly Mg, O and C elements, and the observed C emission peak may be caused by the transfer process of samples into the UHV chamber.^{28,29} An apparent Si emission peak was observed in the XPS spectrum of $\text{SiO}_2@\text{MgO}$ powders, demonstrating the existence of SiO_2 . The core-shell structure will be confirmed by morphology of samples.

Fig. 3(a) and (b) show the typical morphology of the 2D petal-like MgO nanosheets with diameters from 0.5 to 1 μm . Detailed observations reveal that surface of MgO was not very flat and nanosheets are estimated by AFM to be around 25 nm in thickness. Fig. 3(c) shows that slightly grooves exist on the surface and induce larger surface area ($131.5 \text{ m}^2 \text{ g}^{-1}$). The microstructure of coating is shown in Fig. 3(d). It can be clearly seen that the core-shell structure and the coverage of the coating is at a high level with fine layered features. The insert picture shows that thickness of the coating layer is about 25–30 nm.

Composite films with different kinds and fractions of fillers were prepared by the solution blending process described in the experimental section. And the thickness of all the films is 40–60 μm measured by the micrometer caliper. Fig. 4 presents the XRD patterns of $\text{SiO}_2@\text{MgO}$ nanoparticles, pure PMMA and $\text{SiO}_2@\text{MgO}$ -PMMA composited with different weight fractions



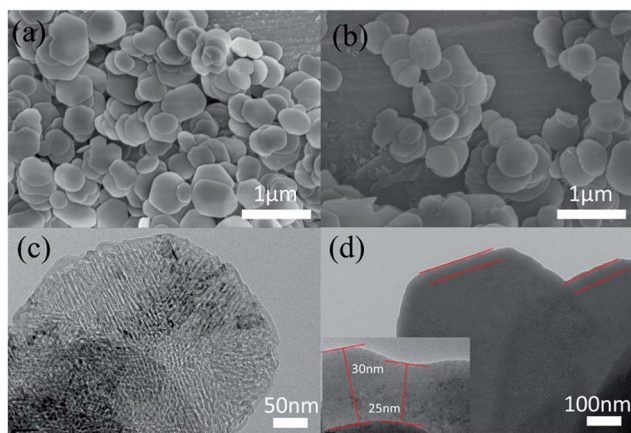


Fig. 3 (a and b) SEM and (c) TEM images of MgO nanosheets; (d) TEM images of core-shell structure of SiO₂@MgO.

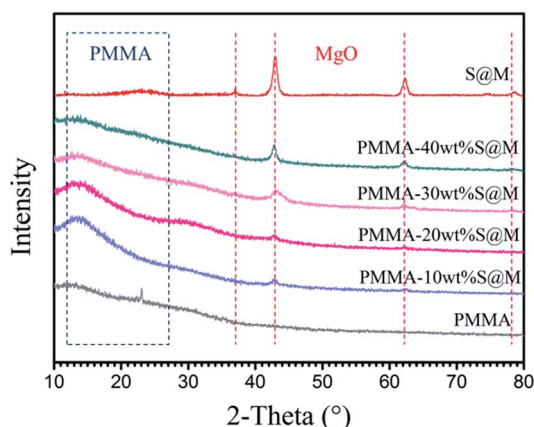


Fig. 4 XRD patterns of SiO₂@MgO particles, pure PMMA and SiO₂@MgO-PMMA composites with different weight fractions of SiO₂@MgO.

of SiO₂@MgO. PMMA is an amorphous polymer and no clearly diffraction peaks can be observed. In the XRD patterns of the composite films, diffraction peaks from MgO and the curve broad from PMMA can be observed. With an increase of MgO content, the X-ray powder diffraction peak curve broad decreases gradually, which means MgO exert a dominant effect on the crystallization behaviour of the nanocomposites.

The SEM images of the freeze-fractured cross-sections of MgO-PMMA and SiO₂@MgO-PMMA composite films at 40 wt% concentration and pure PMMA film are shown in Fig. 5. Due to the surface effect of nanoscale particle, powders prepared by wet process can form aggregation easily during the desiccation period. The aggregation of MgO sheets were obviously observed in Fig. 5(b). After the ultraphonic and stirring process MgO nanopowders can be easily homodispersed in ethanol and a coating of uniform shell can prevent once more aggregation. Compared with MgO-PMMA, SiO₂@MgO powders are homogeneously dispersed in the matrix and few voids could be observed between the particles and the polymer (Fig. 5(a)). The phenomenon suggests that SiO₂ coating layer can protect MgO

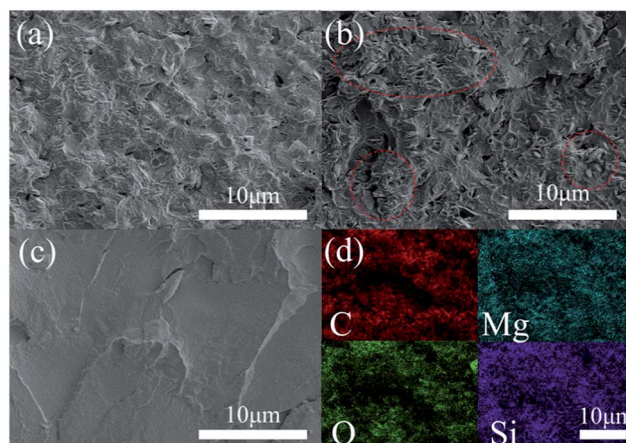


Fig. 5 Freeze-fractured cross-sections of (a) 40 wt% SiO₂@MgO-PMMA, (b) 40 wt% MgO-PMMA and (c) PMMA films. (d) Element distribution of (a).

from agglomeration during the preparation process, which is also beneficial to the dielectric properties of the composites.³⁰ Ke *et al.* also prepared core-shell structured BaTiO₃/SiO₂ to increase the isolation of BaTiO₃ nanoparticles.³¹ Fig. 5(d) shows the element surface distribution in the cross-section of SiO₂@MgO-PMMA composite films by the energy spectrum, which also proves the homogeneously distribution of fillers.

The glass transition temperature of PMMA and its nanocomposites with different filler loadings has been showed in Fig. 6. It is apparent that the addition of fillers leads to an increase in the *T_g*. With an increase of SiO₂@MgO loading, *T_g* increases. But the MgO and SiO₂ are ceramic particles, which do not directly contribute to the *T_g* of the matrix. The possible explanation of this phenomenon is the interfacial effect. The interaction of polymer segments surrounding the particles can alter the segment kinetics in the region drastically due to the presence of the interface and the importing of particles enhanced the interface area in the system. In this study, PMMA absorbing or grafting onto the SiO₂ surface decreases molecular mobility, changes the density of packing of polymer segments,

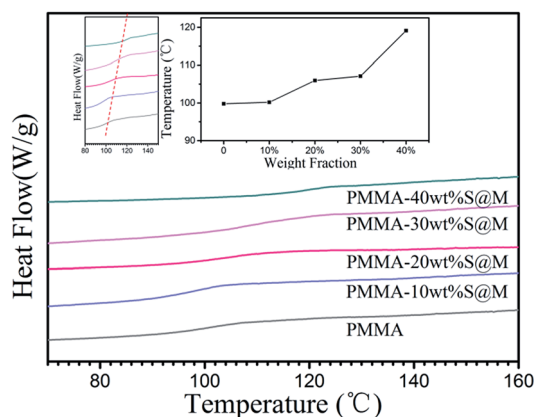


Fig. 6 Glass transition temperature of PMMA and its nano-composites with different filler loadings.



modifies the chain conformation and orientation in the neighbourhood of the surface, and produces a higher glass transition temperature. A similar result of glass transition temperature has also been reported for silica,³² ZnS,³³ aluminum,³⁴ and vapour-grown carbon fiber,³⁵ *etc.* The highest T_g (119.1 °C, 40 wt%) of SiO₂@MgO composites is lower than 120 °C, and can be used as further process as a hydrophobic insulator layer of electrowetting display.

By varying the weight fraction of nanofillers blended with PMMA, we can systematically change the contact angle of the insulator, as shown in Fig. 7. The Young's contact angle increased to about 115°, compared to the pure PMMA ($\theta \sim 78^\circ$). And the Young's contact angle increased as the increasing of the weight fraction of SiO₂@MgO, which is also founded in the BaTiO₃–fluoropolymer nanocomposite.³⁶ The increase of contact angle showed the change of surface energy γ_{SV} , which was caused by the nanofillers. The chain conformation and orientation of polymer around the fillers has changed and even influenced the chain structure near the film surface with increasing fillers. Also, some inevitable surface particles also contributed to the result. A large initial contact angle provides the possibility for a larger range of dynamic contact angle, shown by the Young–Lippmann equation.

Fig. 8(a–c) presents the frequency dependence of room temperature dielectric constant (ϵ), dielectric loss tangent ($\tan \delta$) and electrical conductivity (σ) for the PMMA and its nanocomposites with varied filler weight fractions. For comparison, the properties of composite filled with 40 wt% MgO nanosheets and commercial MgO (c-MgO) are also included. As shown in Fig. 8a, the dielectric constant declines with increasing frequency for all samples in low-frequency region and shows a stronger frequency dependence with increasing SiO₂@MgO content over the whole frequency range. At higher frequencies ($>10^3$), the variation trend of ϵ becomes relatively stable. The dielectric constant increased with increasing SiO₂@MgO content. The frequency variation tendency shows the typical characteristic of interface polarization.³⁷ The dielectric constant of PMMA composite with 40 wt% SiO₂@MgO reaches 19.1 at 40 Hz, in contrasted to 9.7 and 6.8

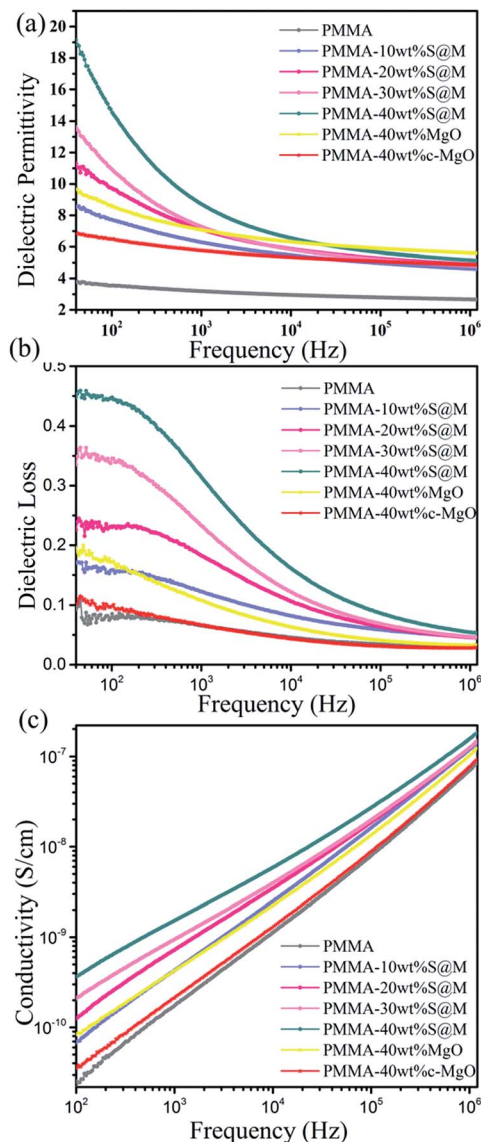


Fig. 8 Frequency dependence of (a) dielectric constant, (b) dielectric loss and (c) conductivity of PMMA, MgO–PMMA and SiO₂@MgO–PMMA composites with different weight ratios.

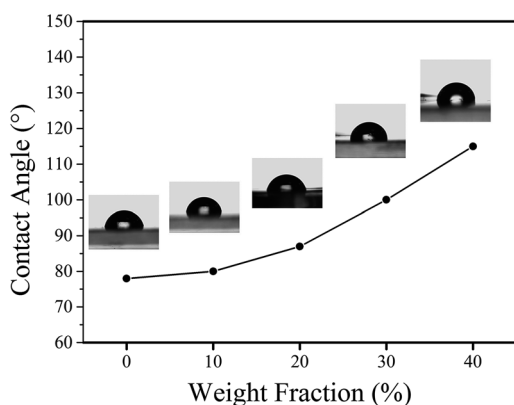


Fig. 7 Contact angles of PMMA and its nanocomposites with different filler loadings.

for the composite with 40 wt% MgO nanosheets and c-MgO, and is nearly 5 times that of pure PMMA (3.8). It should be noted that the dielectric constant of SiO₂ and MgO are 3.9 and 10, respectively, which are lower than 19.1. The results of dielectric constant indicate that SiO₂ coating has a dramatic effect on the dielectric constant of the nanocomposite.³¹ In contrast to the expectation, the ϵ of the core–shell nanocomposite was also higher than the dielectric constant of the nanocomposite with pure MgO. First, the contrast between the MgO and the PMMA may induce the electric field concentration in the polymer³⁸ and SiO₂ acts as a medium layer between matrix and MgO for homogeneous electric field. Pan *et al.* constructed multilayer hierarchical interfaces and used simulation of finite element to demonstrate the effect of core–shell structure.³⁹ Second, the amorphous insulation coating layer could effectively contribute to the mobility of free electrons.³⁹ Third, the coating MgO with



amorphous SiO₂ can reduce the mismatch with amorphous PMMA avoiding agglomeration, air voids and other defects.⁴⁰ The frequency dependence behavior shows the typical characteristic of Maxwell–Wagner–Sillars (MWS) interface polarization, which can make contributions at low-frequency range. The three multiple materials increase interface area and enhance interface polarization.⁴¹ The charge carriers have enough relaxation time to accumulate at the interfaces between two dielectric media, increasing the dielectric loss and dielectric constant of the nanocomposites with a higher amount of nanoparticles and at lower frequencies.

The dielectric loss tangent of all samples also shows strong frequency dependence in Fig. 8(b). Under the frequency for 40 to 10⁶ Hz, the dielectric loss tangent drastically decreases with the increasing frequency and enhances with core-shell nanocomposites content. The trend could be explained by the accumulation of extra sources of space charge carriers induced by inorganic fillers.⁴²

Fig. 8(c) shows the electric conductivity for the nanocomposites increases with the increasing frequency and is only slightly higher than that of pure PMMA over the whole frequency range. The slight increase could be explained by the interface induced by the nanofillers where charge carriers easily accumulated and the same result also existed in other ref. 43 and 44. The electric conductivity of all samples over the frequency from 10² to 10⁶ is lower than 10^{−7} S cm^{−1}, indicating the excellent insulation of the films. The good insulating properties may be attributed to the insulating core-shell nanoparticles and the homogeneous dispersion in the polymer matrix.

Dielectric breakdown strength (BDS) is also an important property of the nanocomposites determining the applied electric field away from breakdown. The characteristic BDS is a statistic value and analyzed by a two-parameter Weibull distribution function, described as:^{45,46}

$$P = 1 - \exp \left[- \left(\frac{E_b}{E_0} \right)^\beta \right]$$

where P is the cumulative probability of electric failure, E_b is the measured breakdown, E_0 is the scale parameter describing the strength for which there is a 63% probability for the sample to breakdown, and shape parameter β presents the scatter of the data and is positive. The experimental data with a discrete data will have a small value of β .^{47,48} The figure of BDS Weibull distribution is compared in Fig. 9 and the characteristic breakdown strength and shape parameter of MgO–PMMA and SiO₂@MgO–PMMA composites are showed in the Table 1. Each sample had been measured more than 10 tests and the BDS of them are over 100 MV m^{−1}. The characteristic breakdown strength of the composites decreased with increasing nanofillers, which was due to the uneven distribution contour of electric field. SiO₂ layer reduced the defect but it still remained. It worth mentioning that the SiO₂@MgO/PMMA composite with 40 wt% filler shows a similar characteristic BDS value to that of c-MgO–PMMA composite and shows a slightly lower value to that of MgO–PMMA composite with the same weight fraction. The phenomenon is similar to those reported before for other

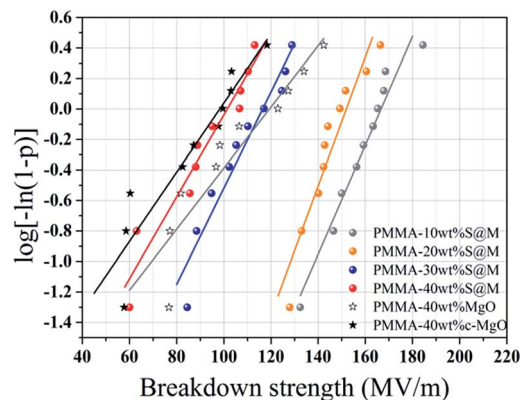


Fig. 9 Weibull plots of the breakdown strength for MgO–PMMA and SiO₂@MgO–PMMA composites.

Table 1 Characteristic breakdown strength and shape parameter of composites

Sample	SiO ₂ @MgO				MgO	c-MgO
	10 wt%	20 wt%	30 wt%	40 wt%	40 wt%	40 wt%
E_b	167	152	116	101	119	98
β	14.46	7.77	12.96	5.16	4.90	4.23

inorganic/polymer composites.⁴⁷ The SiO₂@MgO–PMMA one show much higher dielectric constants than another two composites as mentioned above. Therefore, the 40 wt% SiO₂@MgO–PMMA composite exhibits greater potential in fabricating electrowetting devices. A similar β value trend to that of characteristic BDS ranged from 4.2 to 14.5, and a higher β value suggests the dielectric reliability of the nanocomposites.

Conclusions

In summary, core-shell structure SiO₂@MgO particles have been successfully fabricated by a hydrolysis process as functional fillers and MgO nanosheets have been prepared *via* a facile hydrothermal process. Microstructure analyses indicated that SiO₂@MgO particles homogeneously dispersed in PMMA matrix. Hydrophobic film (contact angle $\sim 115^\circ$) with appropriate glass transition temperature was obtained. Compared with commercial MgO-filled composites, the frequency dependent dielectric properties of the functional fillers showed much greater increase (about 300%), while presented similar breakdown strength (over 100 MV m^{−1}). Especially, all the composites exhibited low electric conductivity ($\leq 10^{-7}$) even at high frequency. Our work could provide a feasible method to prepare high-dielectric-constant insulator layer with hydrophobic properties in electrowetting devices.

Experimental

Materials

Magnesium chloride hexahydrate (MgCl₂·6H₂O), polyvinyl pyrrolidone (PVP, K30), *N,N*-dimethylformamide (DMF) and



magnesium oxide (MgO, <50 nm, 99.9% metal basis) were purchased from Aladdin Industrial Corporation. Tetraethyl orthosilicate (TEOS), ethanol and ammonia solution (30 wt%) were supplied by Sinopharm Chemical Reagent Co. Ltd., China. The poly(methyl methacrylate) (PMMA) was provided by Sigma-Aldrich with average molecular weight about 120 000 by GPC. All chemicals were used as received without any further treatment.

Synthesis of MgO nanosheets

The MgO nanosheets were prepared by a single step hydrothermal approach. In a typical procedure, 20 mmol $\text{MgCl}_2 \cdot 6\text{H}_2\text{O}$ and 1 g PVP was added into 65 mL deionized water containing 3 mL ammonia. After stirring for 30 min at room temperature, the solution was transferred into a 100 mL Teflon-lined stainless steel autoclave and heated to 180 °C and maintained for 3 hours. Then the precipitates were washed with ethanol and deionized water for several times and dried at 60 °C for 12 h. Finally, the as-synthesized white powders were calcined in air at 500 °C for 3 h and harvested for subsequent preparation.

Synthesis of SiO_2 @MgO core-shell nanoparticles

SiO_2 @MgO powders were prepared by a hydrolysis method, 1 g as-prepared MgO nanosheets were added to 70 mL ethanol. After ultrasonic dispersion for 20 min, 1.5 mL ammonia solution in 4 mL deionized water and 0.8 mL TEOS in 20 mL ethanol were consecutively added. And the mixture was continuously stirred for 6 hours at the room temperature. The products were separated out and washed only by ethanol for several times, and then dried at 60 °C under vacuum condition.

Preparation of PMMA composites

PMMA particles were first dissolved in DMF, and stirred for 4 hours to get a homogeneous solution. Then a certain amount of prepared SiO_2 @MgO particles were added into the solution and sonicated in an ultrasonic washer for 1 h. After vigorously stirring at room temperature for 24 h, the homogeneous mixture was put into vacuum container for 1 h to discharge bubbles. The mixture was poured onto a clean glass plate and shaped by casting equipment (MSK-AFA-III, HEFEI Ke Jing Materials Technology Co., Ltd.). The film was dried in a vacuum oven at 60 °C for 12 h to remove the residual DMF. Pure PMMA and MgO-PMMA films were also prepared with same method as comparison.

Characterization

The X-ray diffraction patterns of the products were evaluated with Cu K α radiation (XRD, EMPYREAN, PANalytical Co., The Netherlands). The chemical composition of the products was identified by the ESCALAB 250XI X-ray photoelectron spectrometer (XPS, Thermo Fisher Scientific, USA). The morphology of products were observed by a field emission scanning electron microscopy (FESEM, S-4800, Hitachi Ltd, Japan) and a transmission electron microscopy (TEM, Tecnai G2 F20, FEI Co.,

Netherlands) with an accelerating voltage of 200 kV. The surface area of MgO sheets were measured by AUTOSORB-IQ2-MP (Quantachrome Co., America). The thickness of MgO nanosheets was measured by atomic force microscope (AFM). Glass-transition temperature (T_g) was determined by differential scanning calorimetry (DSC, Perkin-Elmer DSC-7 analyzer) with a heating rate of 10 °C min⁻¹ from 80 to 200 °C under a nitrogen flow. Static contact angle (CA) was obtained by OCA20 (Data-physics, Germany). The dielectric properties of the films were obtained with 100 nm copper electrodes on the both side of them.

Conflicts of interest

There are no conflicts to declare.

Acknowledgements

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Notes and references

- 1 J. R. Choudhuri, D. Vanzo, P. A. Madden, M. Salanne, D. Bratko and A. Luzar, *ACS Nano*, 2016, **10**, 8536–8544.
- 2 Y.-P. Zhao and Y. Wang, *Rev. Adhes. Adhes.*, 2013, **1**, 114–174.
- 3 F. Mugele and J. Baret, *J. Phys.: Condens. Matter*, 2005, **17**.
- 4 P. T. C. Lee, C. Chiu, T. Lee, T. Chang, M. Wu, W. Cheng, S. Kuo and J. Lin, *ACS Appl. Mater. Interfaces*, 2013, **5**, 5914–5920.
- 5 B. Shapira, P. Shoval, N. Tractinsky and J. Meyer, *J. Assoc. Inf. Sci. Technol.*, 2009, **60**, 2333–2346.
- 6 R. Shama, D. Andelman, B. Berge and R. Hayes, *Soft Matter*, 2008, **4**, 38–45.
- 7 A. Schultz, S. Chevalliot, S. Kuiper and J. Heikenfeld, *Thin Solid Films*, 2013, **534**, 348–355.
- 8 M. Mibus, X. Hu, C. R. Knospe, M. L. Reed and G. Zangari, *ACS Appl. Mater. Interfaces*, 2016, **8**, 15767–15777.
- 9 C. Li and H. Jiang, *Appl. Phys. Lett.*, 2012, **100**, 231105–2311054.
- 10 W. Dai and Y. Zhao, *Int. J. Nonlinear Sci. Numer. Simul.*, 2007, **8**, 519–526.
- 11 J. B. Chae, J. O. Kwon, J. S. Yang, D. Kim, K. Rhee and S. K. Chung, *Sens. Actuators, A*, 2014, **215**, 8–16.
- 12 P. Mach, T. Krupenkin, S. Yang and J. A. Rogers, *Appl. Phys. Lett.*, 2002, **81**, 202–204.
- 13 H. Verheijen and M. M. Prins, *Langmuir*, 1999, **15**, 6616–6620.
- 14 Y. Y. Lin, R. D. Evans, E. Welch, B. N. Hsu, A. C. Madison and R. B. Fair, *Sens. Actuators, B*, 2010, **150**, 465–470.
- 15 E. Seyrat and R. A. Hayes, *J. Appl. Phys.*, 2001, **90**, 1383–1386.
- 16 S. Millefiorini, A. H. Tkaczyk, R. Sedev, J. Efthimiadis and J. Ralston, *J. Am. Chem. Soc.*, 2006, **128**, 3098–3101.
- 17 S. Berry, J. Kedzierski and B. Abedian, *Langmuir*, 2007, **23**, 12429–12435.



- 18 S. K. Cho, H. Moon and C. Kim, *J. Microelectromech. Syst.*, 2003, **12**, 70–80.
- 19 H. Moon, S. K. Cho, R. L. Garrell and C. C. Kim, *J. Appl. Phys.*, 2002, **92**, 4080–4087.
- 20 Y. Li, W. Parkes, L. I. Haworth, A. J. Ross, J. T. M. Stevenson and A. J. Walton, *J. Microelectromech. Syst.*, 2008, **17**, 1481–1488.
- 21 N. Novkovski, A. Paskaleva and E. Atanassova, *Semicond. Sci. Technol.*, 2005, **20**, 233–238.
- 22 L. Huang, B. Koo and C. C. J. Kim, *J. Microelectromech. Syst.*, 2013, **22**, 253–255.
- 23 J. K. Lee, K. Park, H. Kim and S. H. Kong, *Sens. Actuators, B*, 2011, **160**, 1593–1598.
- 24 B. Raj, N. R. Smith, L. Christy, M. Dhindsa and J. Heikenfeld, *IEEE Xplore Conference: University/Government/Industry Micro/Nano Symposium*, 2008, pp. 187–190, DOI: 10.1109/ugim.2008.55.
- 25 J. H. Chang, D. Y. Choi, S. Han and J. J. Pak, *Microfluid. Nanofluid.*, 2010, **8**, 269–273.
- 26 M. Esposto, S. Krishnamoorthy, D. N. Nath, S. Bajaj, T. Hung and S. Rajan, *Appl. Phys. Lett.*, 2011, **99**, 133503.
- 27 Y. B. Sawane, S. Ogale and A. Banpurkar, *ACS Appl. Mater. Interfaces*, 2016, **8**, 24049–24056.
- 28 G. Liu, W. Jaegermann, J. He, V. Sundstrom and L. Sun, *J. Phys. Chem. B*, 2002, **106**, 5814–5819.
- 29 X. Xiao, H. Yang, N. Xu, L. Hu and Q. Zhang, *RSC Adv.*, 2015, **5**, 79342–79347.
- 30 U. C. Chung, C. Elissalde, S. Mornet, M. Maglione and C. Estournès, *Appl. Phys. Lett.*, 2009, **94**, 072903.
- 31 K. Yu, Y. Niu, Y. Bai, Y. Zhou and H. Wang, *Appl. Phys. Lett.*, 2013, **102**, 102903.
- 32 J. L. H. Chau, C. Hsieh, Y. Lin and A. Li, *Prog. Org. Coat.*, 2008, **62**, 436–439.
- 33 S. Agrawal, D. Patidar and N. S. Saxena, *Phase Transitions*, 2011, **84**, 888–900.
- 34 B. J. Ash, R. W. Siegel and L. S. Schadler, *J. Polym. Sci., Part B: Polym. Phys.*, 2004, **42**, 4371–4383.
- 35 J. Zeng, B. Saltysiak, W. S. Johnson, D. A. Schiraldi and S. Kumar, *Composites, Part B*, 2004, **35**, 173–178.
- 36 M. K. Kilaru, J. Heikenfeld, G. Lin and J. E. Mark, *Appl. Phys. Lett.*, 2007, **90**, 212906.
- 37 D. Yu, N. Xu, L. Hu, Q. Zhang and H. Yang, *J. Mater. Chem. C*, 2015, **3**, 4016–4022.
- 38 X. Zhang, Y. Shen, Q. Zhang, L. Gu, Y. Hu, J. Du, Y. Lin and C. W. Nan, *Adv. Mater.*, 2015, **27**, 819–824.
- 39 Z. Pan, J. Zhai and B. Shen, *J. Mater. Chem. A*, 2017, **5**, 15217–15226.
- 40 Y. Deng, D. Qi, C. Deng, X. Zhang and D. Zhao, *J. Am. Chem. Soc.*, 2008, **130**, 28–29.
- 41 T. Tanaka, M. Kozako, N. Fuse and Y. Ohki, *IEEE Trans. Dielectr. Electr. Insul.*, 2005, **12**, 669–681.
- 42 G. Wang, Y. Wu, X. Zhang, Y. Li, L. Guo and M. Cao, *J. Mater. Chem.*, 2014, **2**, 8644–8651.
- 43 N. Xu, L. Hu, Q. Zhang, X. Xiao, H. Yang and E. Yu, *ACS Appl. Mater. Interfaces*, 2015, **7**, 27373–27381.
- 44 E. Yu, Q. Zhang, N. Xu and H. Yang, *RSC Adv.*, 2017, **7**, 3949–3957.
- 45 X. Huang, L. Xie, Z. Hu and P. Jiang, *IEEE Trans. Dielectr. Electr. Insul.*, 2011, **18**, 375–383.
- 46 Z.-M. Dang, J.-K. Yuan, J.-W. Zha, T. Zhou, S.-T. Li and G.-H. Hu, *Prog. Mater. Sci.*, 2012, **57**, 660–723.
- 47 Q. Li, G. Zhang, F. Liu, K. Han, M. R. Gadinski, C. Xiong and Q. Wang, *Energy Environ. Sci.*, 2015, **8**, 922–931.
- 48 Q. Li, K. Han, M. R. Gadinski, G. Zhang and Q. Wang, *Adv. Mater.*, 2014, **26**, 6244–6249.

