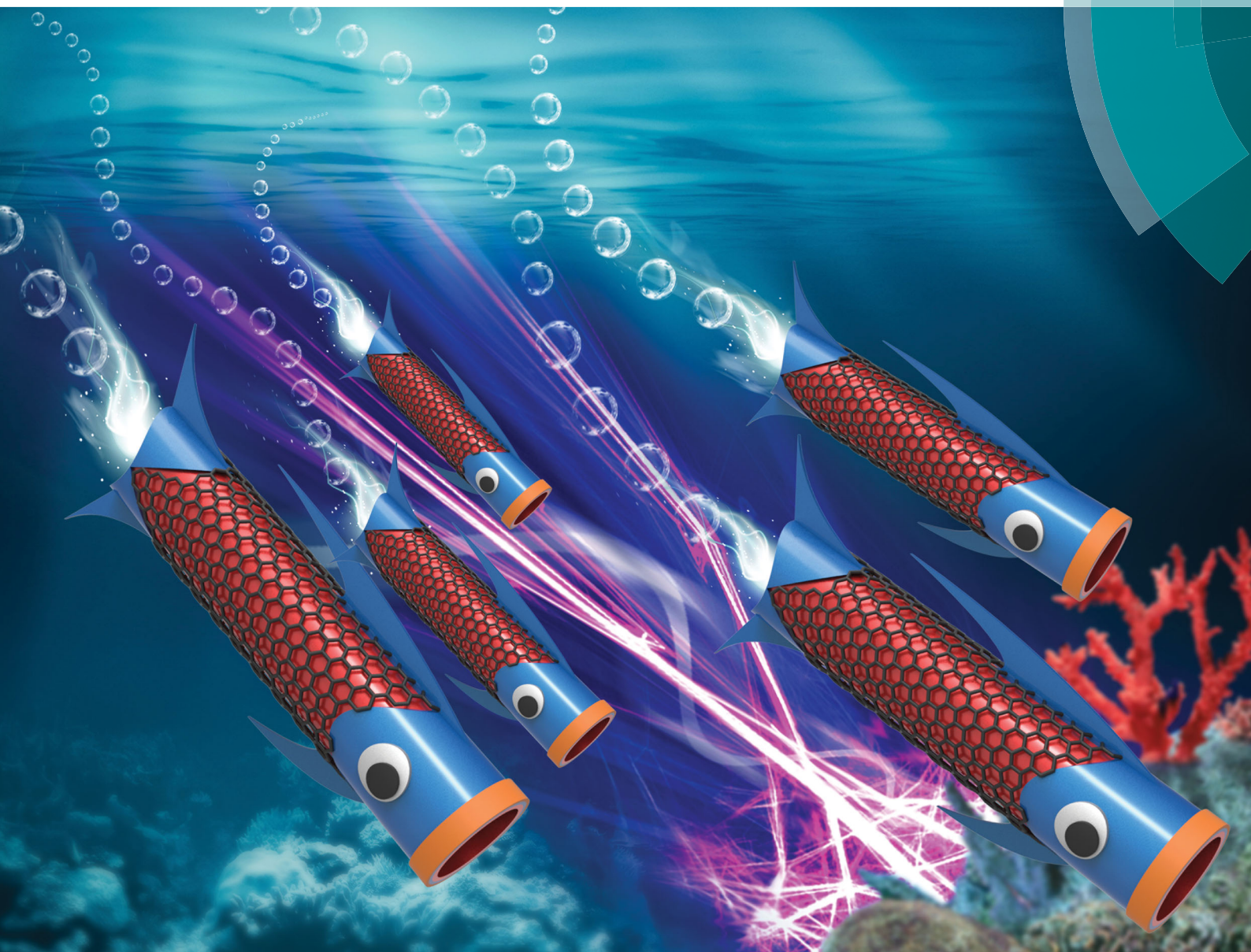


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Pt-Free microengines at extremely low peroxide levels



# Pt-Free microengines at extremely low peroxide levels†

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Herein, we demonstrate that iron oxide modified MnO<sub>2</sub> (FeO<sub>x</sub>-MnO<sub>2</sub>) catalyzed micromotors can be fabricated via electrochemical co-reduction and exhibit exceptional high performance at an extremely low hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) fuel concentration. We observed that graphene/FeO<sub>x</sub>-MnO<sub>2</sub> microtubes could show motion behaviors at fuel concentration as low as 0.03% H<sub>2</sub>O<sub>2</sub>, which is nearly one order of magnitude lower than Pt-based micromotors (normally at above 0.2% H<sub>2</sub>O<sub>2</sub>). Moreover, the micromotors exhibit higher speeds than any other reported catalytic micro/nanomotors (MNM) at low peroxide levels. The FeO<sub>x</sub>-MnO<sub>2</sub> systems are better catalytic MNMs, due to their excellent catalytic activity, easy fabrication, robust structure and movement, as well as low-cost, biocompatible and abundance nature, showing great potential for future applications.

Micro/nanomotors (MNM) have attracted extensive attention because of their wide potential applications in diverse areas.<sup>1–9</sup> Due to the good catalytic activity in hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) decomposition, precious rare metal platinum (Pt) has always been the most widely used catalytic material to construct MNMs in different geometrical shapes, such as micro/nano-tubular engines,<sup>10–12</sup> Janus particles,<sup>13,14</sup> and bi-segment nanorods.<sup>15</sup> However, the scarcity, high cost and deactivation of Pt limit its further application. Hence, researchers are searching for new catalysts and propelling mechanisms for MNMs.<sup>16</sup> For examples, based on hydrogen bubbles generated by reactive metals with water and acids for propulsion, reactive MNMs have been generated but they exhibit very short lifetimes and the harsh reaction conditions limit their use in real applications.<sup>17</sup> Enzyme-based MNMs were also developed via a new propulsion strategy, because of the good catalytic performance over a wide

range of biocatalytic reactions under mild environmental conditions.<sup>18</sup> Nevertheless, the enzyme based MNMs also suffer from quick deactivation in various media and harsh environments. The sophisticated synthetic procedures and low power output also hinder their future use.

MnO<sub>2</sub>-based MNMs were developed to be an alternative to Pt, due to their low-cost, good propulsion, and robust nature.<sup>16,19</sup> Their polycrystallinity and various synthesis and modification methods provide good opportunities for researchers to design MnO<sub>2</sub> catalyzed MNMs.<sup>20</sup> By geometry design and crystallinity tuning, some MnO<sub>2</sub>-based MNMs have been developed and tested.<sup>21</sup> Although fruitful achievements have been made, the performance of MnO<sub>2</sub> based MNMs still cannot compete with the Pt-based MNMs due to inferior catalytic performance.<sup>22</sup>

Herein we introduce a new catalyst for catalytic MNMs by modifying MnO<sub>2</sub> with mixed valence iron oxide (denoted as FeO<sub>x</sub>-MnO<sub>2</sub>) via cathodic electrochemical co-deposition. We fabricated graphene/FeO<sub>x</sub>-MnO<sub>2</sub> bilayer tubular and rod-shaped micromotors, and evaluated their mobility performance. It is astounding to find that the newly designed micromotors move much faster than any reported MNMs at a low peroxide fuel concentration below 1% H<sub>2</sub>O<sub>2</sub>. What is more, these MnO<sub>2</sub> based MNMs exceed the fuel concentration range limit of the Pt-based MNMs by nearly an order of magnitude, reaching an extremely low value of 0.03% H<sub>2</sub>O<sub>2</sub> with an acceptable speed of 89 ± 59 μm s<sup>-1</sup>. Due to the easiness of fabrication, high catalytic performance, low cost, ecofriendly and biocompatible properties of the newly developed FeO<sub>x</sub>-MnO<sub>2</sub> catalyst, we anticipate that a range of new MNMs based on this groundbreaking new strategy could be developed, and navigated at the very favorably low content of fuels to address diverse issues not limiting to the biomedical and environmental areas.

Scheme S1 (see ESI†) illustrates the fabrication process of the graphene/FeO<sub>x</sub>-MnO<sub>2</sub> micromotors. These bilayer micromotors were constructed via a two-step electrochemical deposition process. Firstly, an outer layer of electrochemically reduced graphene oxide (erGO) was formed by deposition of graphene oxide into the pores of the membrane using a cyclic voltammetry

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(CV) method.<sup>23</sup> Secondly, an inner layer of the  $\text{FeO}_x\text{-MnO}_2$  catalyst was produced *via* cathodic electrochemical co-deposition. The electrochemical reductions of  $\text{MnO}_4^-$  ions and  $\text{Fe}^{3+}$  ions occur simultaneously. The synthetic parameters can be tailored to obtain rod-shaped and tubular micromotors.

Fig. 1 indicates that  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors in microtube and microrod are fabricated successfully. Compared with the smooth tubular microengines, the inner surface of the  $\text{erGO/FeO}_x\text{-MnO}_2$  microengines exhibits a larger surface area of electrochemical active sites for improving the catalytic activity.<sup>24</sup> The co-deposition of iron oxide and  $\text{MnO}_2$  generates a much thinner wall. As shown in Fig. 1A and B, the wall thickness of the tubular micromotors is far less than 1  $\mu\text{m}$ , which demonstrates its good mechanical properties. Without good mechanical strength, these tiny micro structures are very easy to be torn apart or crushed into pieces. This implies that the doping of iron oxide improves the mechanical strength of the micromotors, allowing the formation of the thin wall structured tubular micromotors with good structural integrity. The uniform distribution of carbon, oxygen, manganese, and iron demonstrates that the inner layer of iron oxide doped  $\text{MnO}_2$  was fabricated successfully with good coverage by the outer graphene layer.

As illustrated in Fig. 2, XPS survey further reveals the presence of carbon (C 1s peak), oxygen (O 1s peak), manganese (Mn 2p peaks) and iron (Fe 2p peaks). The results are in good agreement with the SEM and EDX results. The peaks of high-resolution C 1s (Fig. 2B) and O 1s spectra (Fig. S1, ESI†) correspond to the binding energy of various functional groups, such as C-C-H/C=C, C-OH, C=O, and O-C=O, revealing the nature of the covalent bonds of oxygen and carbon atoms.<sup>25</sup>

The quantities of the various functional groups are summarized in Table S1 (ESI†). The ratio of  $\text{sp}^2$  carbons is at 68.33%, which indicates the degree of oxidation of the outer layer of

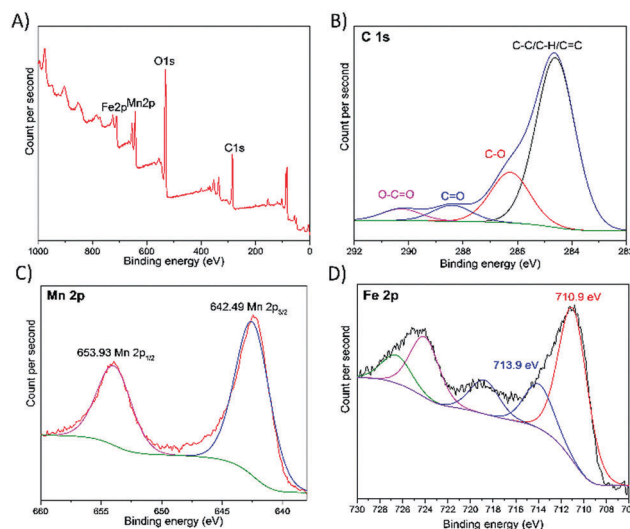


Fig. 2 XPS survey of the  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors. (A) A wide scan showing Mn 2p, O 1s, C 1s and Fe 2p peaks. (B) High-resolution C 1s XPS spectra displaying various functional groups identified on the surface. (C) High-resolution Mn 2p XPS spectra. (D) High-resolution Fe 2p XPS spectra.

the micromotor. Due to a higher cathode current for the reduction of the iron oxide doped  $\text{MnO}_2$  catalyst, the oxidation degree is much lower than our previously designed  $\text{MnO}_2$  based micromotors, which means that more graphene carbon lattices are recovered by the cathode galvanostatic electroreduction.<sup>26</sup> The high-resolution Mn 2p XPS spectra reveal the oxidation state of Mn (Fig. 2C). The peaks observed at the binding energies of 642.49 and 653.93 eV were attributed to the Mn 2p with the spin-orbit splitting of 11.44 eV. The Mn  $2\text{p}_{3/2}$  peak located at 642.49 eV indicates the main oxidation state of  $\text{Mn}^{4+}$ .<sup>26</sup> Fig. 2D shows the high-resolution XPS spectra of Fe 2p for the iron oxide doped  $\text{MnO}_2$  micromotors. The peaks at binding energies of 710.9 and 724.2 eV correspond to Fe  $2\text{p}_{3/2}$  and Fe  $2\text{p}_{1/2}$ , respectively.<sup>27</sup> It can be noted that the Fe atomic distribution is a mixture of  $\text{Fe}^{2+}$  (710.9 eV) and  $\text{Fe}^{3+}$  (713.9 eV) with 77.5% of the iron species as  $\text{Fe}^{2+}$ .<sup>28</sup> Due to the electrochemical reduction process,  $\text{Fe}^{2+}$  ions are generated, but no zero valence iron (the  $\text{Fe}^0$  peak usually exists at around 707.1 eV) was generated. Instead, a small proportion of  $\text{Fe}^{3+}$  was also doped into the  $\text{MnO}_2$  matrix, as shown by the peak around 713.9 eV. Hence, the inner layer catalyst can be denoted as mixed valence iron doped  $\text{MnO}_2$ .

As demonstrated in Fig. 3A, the speed of all the micromotors exhibits an increasing tendency over the entire  $\text{H}_2\text{O}_2$  fuel range with 1% sodium dodecyl sulfate (SDS) as a surfactant. The tubular micromotors demonstrate exceptionally high performance at extremely low peroxide levels. The speed of the  $\text{erGO/FeO}_x\text{-MnO}_2$  tubular micromotors is 4 times faster than that of the  $\text{erGO/Pt}$  micromotors ( $187 \pm 80$  vs.  $37 \pm 10 \mu\text{m s}^{-1}$ ) in 0.1%  $\text{H}_2\text{O}_2$ , which is the minimal fuel requirement for the best reported Pt catalyzed micromotors.<sup>23</sup> What's more, the  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors can easily utilize the even lower fuel concentration of 0.03%  $\text{H}_2\text{O}_2$  with a speed of  $89 \pm 59 \mu\text{m s}^{-1}$ , which is more than two-fold the speed of the  $\text{erGO/Pt}$  micromotors at a much higher fuel concentration of 0.1%  $\text{H}_2\text{O}_2$ .

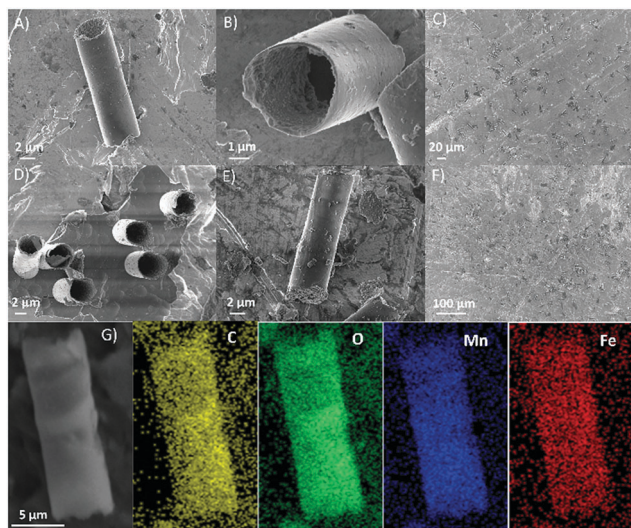


Fig. 1 Scanning electron microscopy (SEM) and energy dispersive X-ray (EDX) mapping analysis of the  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors: (A) a lying microtube, (B) an upright microtube, (C) a number of microtubes, (D) an array of microtubes, (E) a lying microrod, (F) a number of microrods, and (G) EDX mapping analysis of a microtube.



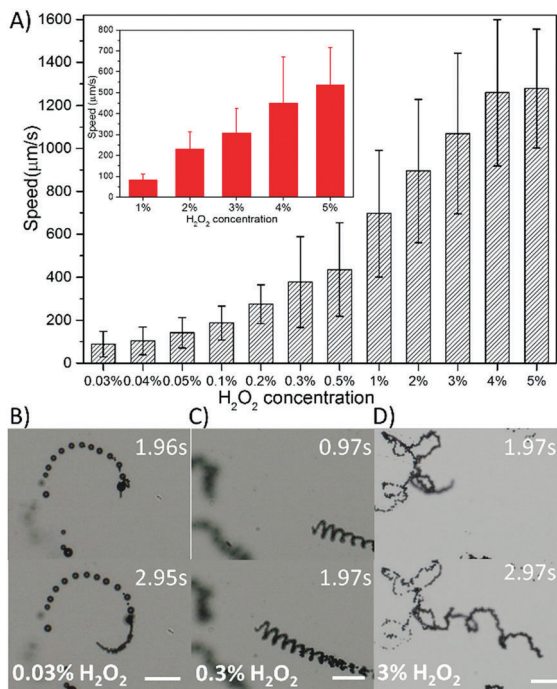


Fig. 3 Speed profile of  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors in 1% SDS ( $n = 50$ ). Average speed of tubular micromotors (inset: rod-shape micromotor) (A); time lapse images of tubular micromotors in 0.03% (B), 0.3% (C), and 3% (D)  $\text{H}_2\text{O}_2$  extracted from the ESI,† Videos S1–S3. (Scale bars: 100  $\mu\text{m}$ .)

Moreover, the minimal fuel content is two orders of magnitude lower than the 3% value of the graphene/ $\text{MnO}_2$  micromotors.<sup>26</sup> At a slightly higher fuel concentration of 3%, the  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors can easily exceed  $1 \text{ mm s}^{-1}$ , which is also remarkably high compared with polymeric/Pt micromotors, PANI/Pt, PPy/Pt, and PEDOT/Pt, which cannot exceed  $1 \text{ mm s}^{-1}$  in 3%  $\text{H}_2\text{O}_2$ .<sup>24</sup> The  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors also exceed the speed of all the Pt based rolled-up multi-layer tubular micromotors and Janus motors at a relatively higher fuel content.<sup>10,29</sup> As shown in Fig. 3B, the tubular micromotors show circular motion behaviors at 0.03%  $\text{H}_2\text{O}_2$ . Ultra fast helical and irregular motion behaviors were also observed (Fig. 3C and D). As far as we know, Pt based micromotors require at least 0.1%  $\text{H}_2\text{O}_2$  for propulsion, and  $\text{MnO}_2$  based micromotors demand an even higher fuel concentration, while we demonstrate here that the Pt-free mixed valence iron oxide doped  $\text{MnO}_2$  catalyzed micromotors could extend the fuel concentration to a very low threshold value of 0.03% with an acceptable velocity. The ground-breaking new catalyst along with the simple and low-cost fabrication method provides a new strategy to fabricate MNMs and will greatly boost motion in the tiny world.

As the surfactant is indispensable for the motion of bubble propelled tubular MNMs, the effect of the surfactant on the motion of  $\text{FeO}_x\text{-MnO}_2$  micromotors could provide an insight for us to manipulate the motion behaviors.<sup>30,31</sup> Hence we investigated the mobility of the micromotors in 1%, 0.5%, and 0.05%  $\text{H}_2\text{O}_2$  with different SDS concentrations, as shown in Fig. 4A–C, respectively.

At an extremely low content of the surfactant, the micromotors could not move, while at a very high content of the surfactant,

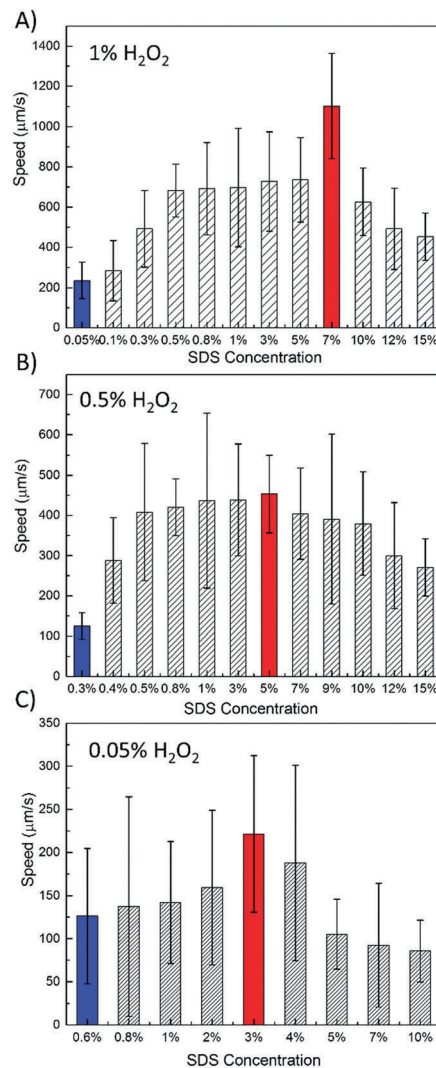


Fig. 4 Dependence of average speed of  $\text{erGO/FeO}_x\text{-MnO}_2$  micromotors with varying SDS contents in 1%  $\text{H}_2\text{O}_2$  (A), 0.5%  $\text{H}_2\text{O}_2$  (B), and 0.05%  $\text{H}_2\text{O}_2$  (C) ( $n = 50$ ).

the high viscosity of the fluid would have an adverse effect on the motion to decrease the speed of micromotors. Hence, the minimal and optimal SDS surfactant contents for the micromotors at certain  $\text{H}_2\text{O}_2$  fuel contents are important. As shown in Fig. 4, the blue bar corresponds to the minimal SDS concentration, while the red bar corresponds to the optimal surfactant content. It is interesting to note that as the fuel concentration drops from 1% to 0.05%, the minimal SDS concentration increases from 0.05% at 1%  $\text{H}_2\text{O}_2$  to 0.3% at 0.5%  $\text{H}_2\text{O}_2$  and finally reaches 0.6% at 0.05%  $\text{H}_2\text{O}_2$ . Meanwhile, the optimal SDS concentrations are 7%, 5%, and 3%, respectively. Under the optimized conditions, the speed of the  $\text{erGO/FeO}_x\text{-MnO}_2$  tubular micromotors are  $1102 \pm 262 \mu\text{m s}^{-1}$ ,  $453 \pm 97 \mu\text{m s}^{-1}$ , and  $222 \pm 91 \mu\text{m s}^{-1}$  in 1%, 0.5%, and 0.05%  $\text{H}_2\text{O}_2$ , respectively. The higher performance is usually obtained at moderate surfactant concentrations. This phenomenon can be used in sensing, detection, and motion based analysis. To the best of our knowledge, the unveiled high speed mobility properties at this low



content of fuels far exceed other reported MNMs under the same fuel conditions (Table S2, ESI†). As the toxicity of high concentration of  $\text{H}_2\text{O}_2$  fuels is the major obstacle for biomedical applications, the iron modified manganese oxide MNMs will show a good prospect in biomedical and environmental applications due to the lower toxicity of the MNMs. The new types of MNMs provide a route to minimize the use of toxic fuel and surfactants and thus pave the way for biomedical applications, such as drug delivery. This new strategy could also minimize the environmental impact as lower contents of fuel and surfactants are needed for efficient motion.

For such fascinating mobility performance of this new-type of microengine, several effects take place. First and most importantly, the mixed valence iron doped  $\text{MnO}_2$  catalyst exhibits a much high catalytic activity for  $\text{H}_2\text{O}_2$  decomposition to produce oxygen, which gives faster generation and ejection of microbubbles. The rough inner catalytic layer also contributes to the improved catalytic performance. Secondly, the improved mechanical strength of the  $\text{FeO}_x\text{-MnO}_2$  catalyst allows for the formation of a thin-walled tubular structure, thus significantly reducing the weight of the micromotors. Thirdly, the big difference in density between the iron oxide modified  $\text{MnO}_2$  (usually the density is  $\approx 5 \text{ g cm}^{-3}$ ) and Pt (the density is  $\approx 20 \text{ g cm}^{-3}$ ) makes  $\text{MnO}_2$  based MNMs much lighter than Pt-based tubular microengines. Fourthly, the ultra-thin wall of the graphene/ $\text{FeO}_x\text{-MnO}_2$  tubular microengines would facilitate the fluid flow in the microtubes and minimize the effect of fluid resistance. Therefore, the structure design of the thin wall and the improved catalytic performance of the tubular microengines resulted in the exceptional high mobility at extremely low peroxide levels.

In conclusion, we demonstrate the first example of tubular microengines that propel efficiently by the thrust of oxygen bubbles in an extremely low  $\text{H}_2\text{O}_2$  level (0.03%), which is nearly an order of magnitude lower than the previously reported values at above 0.2%. At below 1% of  $\text{H}_2\text{O}_2$  fuel, the graphene/ $\text{FeO}_x\text{-MnO}_2$  micromotors can move at far higher speeds than any reported MNMs. Such high-performance, low-cost micromotors could greatly expand the research and applications of micro/nano-scale motion tools and devices, and could thus lead to new biomedical and environmental applications for drug delivery or biological entity manipulation and environmental cleaning. In addition, the doping fabrication strategy provides a new approach for the designing of new types of MNMs.

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## Conflicts of interest

There are no conflicts to declare.

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