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# Improvement in the hydrogen storage performance of the as-milled Sm–Mg alloys using MoS<sub>2</sub> nano-particle catalysts

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The effects of the addition of MoS<sub>2</sub> catalyst on the microstructure and hydrogen storage behavior of the as-milled Sm<sub>5</sub>Mg<sub>41</sub> alloys were investigated in this study. The Sm<sub>5</sub>Mg<sub>41</sub> + x wt% MoS<sub>2</sub> (x = 0, 5, and 10) alloys were prepared by milling MoS<sub>2</sub> powders (particle size ≤ 40 nm) and the mechanically ground as-cast Sm<sub>5</sub>Mg<sub>41</sub> alloy powders (particle size ≤ 75 μm) in an argon atmosphere for 5 h. The results demonstrate that the as-milled alloys are composed of Sm<sub>5</sub>Mg<sub>41</sub> and SmMg<sub>3</sub> phases and milling refines the crystal grains. The MgH<sub>2</sub> and Sm<sub>3</sub>H<sub>7</sub> phases appear after hydrogenation, while the Mg and Sm<sub>3</sub>H<sub>7</sub> phases are formed after dehydrogenation. MoS<sub>2</sub> nano-particles are embedded in the alloy surface, which is nanostructured with some crystal defects, such as dislocations, grain boundaries, and twins. These microstructures are advantageous in reducing the total potential barrier that the hydrogen absorption or desorption reaction must overcome, thus improving the hydrogen storage kinetics of the alloys. The dehydrogenation activation energies of the alloys are 122.28, 68.25, and 59.91 kJ mol<sup>-1</sup> H<sub>2</sub> for x = 0, 5, and 10, respectively. The catalyzed alloys begin to release hydrogen at ~241.9 °C, which is 26.4 °C lower than the temperature required for non-catalyzed alloys. The hydrogenation enthalpies of the alloys are -81.72, -78.31, and -78.18 kJ mol<sup>-1</sup> H<sub>2</sub> for x = 0, 5, and 10, respectively. Therefore, the addition of a MoS<sub>2</sub> catalyst significantly improves the hydrogen storage kinetics of Mg-based alloys.

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## Introduction

Hydrogen has extensive applications, including those in aviation, aerospace, metallurgy, and petrochemical industries. It would be successfully applied in commercial vehicles as one of the clean energy resources. The state-of-the-art sustainable H<sub>2</sub> production technologies have developed rapidly and H<sub>2</sub> fuel has widespread applications.<sup>1–9</sup> However, there are some bottlenecks in achieving the practical, efficient, safe, and cheap hydrogen storage systems.

Magnesium-based alloys are one of the most promising hydrogen storage alloys and have been studied extensively because of their high hydrogen storage capacity and low-cost.<sup>10,11</sup> However, they face some disadvantages in terms of their high dehydrogenation temperatures, slow dehydrogenation kinetics, and high reactivity with air and oxygen.<sup>12,13</sup> The key focus of the current research on such materials is on lowering their dehydrogenation temperature, improving their dehydrogenation kinetics, and prolonging their life cycle.

Alloying, nanocrystallization, and catalyst addition are some of the helpful methods for obtaining the low-cost hydrogen storage materials with favorable thermodynamics and kinetics.<sup>14,15</sup>

Most of the current studies on the magnesium-based alloys for hydrogen storage focus on two main mechanisms for the dehydrogenation of MgH<sub>2</sub>. The first mechanism is a “nucleation and growth” model of Mg in bulky particles.<sup>16</sup> Mg nucleates inside MgH<sub>2</sub> (including a spot of residual Mg) and grows with the diffusion of the H atoms. H<sub>2</sub> is synthesized when the H atoms diffuse to the surface of MgH<sub>2</sub>, which indicates the end of the decomposition of MgH<sub>2</sub>. The second model follows a “shrinking core” mechanism,<sup>17</sup> in which Mg nucleates initially on the surfaces of the MgH<sub>2</sub> nano-particles and then grows into the core of the material. Based on the diffusion of the H atoms through the newly formed Mg layer and the formation of the H<sub>2</sub> molecules, the decomposition of MgH<sub>2</sub> is accomplished. In both models, the diffusion rate of the H atoms is the controlling parameter. The diffusion rate of the H atoms in Mg (4 × 10<sup>-13</sup>) is almost three orders of magnitude higher than that in MgH<sub>2</sub> (1.5 × 10<sup>-16</sup>).<sup>18,19</sup> Thus, microstructure nanocrystallization is an effective tool to enhance the kinetics of dehydrogenation. Au *et al.*<sup>20</sup> fabricated MgH<sub>2</sub> nano-particles using carbon aerogels of large surface areas with pore sizes of 6–20 nm and demonstrated hydrogen release at 140 °C. This temperature is much

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lower than that of other Mg-based hydrogen storage alloys. Moreover, this hydrogen storage material reached 80% of the maximum absorption capacity in just 15 min at 300 °C.

Using catalysts/additives to destabilize hydrides of high hydrogen storage density, *e.g.*, MgH<sub>2</sub> with 7.6 wt% H and a desorption temperature as high as 300–400 °C, is one of the most important strategies to improve the thermodynamics and kinetics of the hydrogen storage materials.<sup>21–23</sup> Cui *et al.*<sup>24</sup> pointed out that the Ti-based multivalent catalysts can improve the kinetics of the hydrogen storage materials. During the hydrogenation process, a diatomic Ti ion donates an electron to the hydrogen atom on the Mg surface and converts it into a hydrogen ion, while converting itself into a trivalent Ti ion. The hydrogen ion unites with a Mg atom and forms a weak Mg–H bond, resulting in a reduction in the energy barrier for hydrogenation and dehydrogenation. Lin *et al.*<sup>25</sup> reported a symbiotic CeH<sub>2.73</sub>/CeO<sub>2</sub> catalyst to enhance the hydrogen storage capacity of MgH<sub>2</sub> and demonstrated that a spontaneous hydrogen release effect in the interface region of the symbiotic CeO<sub>2</sub>/CeH<sub>2.73</sub> nano-particle played a role as an efficient “hydrogen pump”. Shahi *et al.*<sup>26</sup> milled an intermetallic hydride, ZrFe<sub>2</sub>H<sub>x</sub>, with MgH<sub>2</sub> to synthesize the MgH<sub>2</sub>–ZrFe<sub>2</sub>H<sub>x</sub> nanocomposites and found that ZrFe<sub>2</sub>H<sub>x</sub> led to a decrease in the dehydrogenation temperature from 410 °C to 290 °C. Furthermore, it significantly improved the hydrogenation kinetics, as observed by the lowered activation energy of ~61 kJ mol<sup>-1</sup> H<sub>2</sub>. El-Eskandarany *et al.*<sup>27</sup> used the reactive ball milling (RBM) method to prepare MgH<sub>2</sub>/5Ni/5Nb<sub>2</sub>O<sub>5</sub> nanocomposite powders, which exhibited an excellent hydriding/dehydriding performance, as evidenced by the short time required to absorb (41 s) and desorb (121 s) 5 wt% H<sub>2</sub> at 250 °C. Although numerous new achievements have been reported, further efforts are urgently necessary to enhance the hydrogen storage performance of the Mg-based alloys.

To design a hydrogen storage material with the fast kinetics and a low desorption temperature, the investigations on the effects of the addition of Mo-containing catalysts to MgH<sub>2</sub> have been initiated.<sup>28,29</sup> It has also been reported that the catalysis of the S ions can improve the hydrogen storage kinetics of MgH<sub>2</sub>.<sup>29</sup> In our previous study, we showed that an activated Sm–Mg alloy,<sup>30,31</sup> containing rare earth (RE) hydride nano-particles and high-density boundaries, can act as a potential Mg-based hydride. The hydrogen storage kinetics of the alloy can be enhanced because the nano-particles exert a catalytic action and the high-density boundaries can provide a number of channels for hydrogen diffusion. Therefore, the effects of adding MoS<sub>2</sub> nano-particle catalysts<sup>32–35</sup> on the microstructure and gaseous hydrogen storage behavior of the as-cast Sm<sub>5</sub>Mg<sub>41</sub> alloys are studied in the current investigation.

## Experimental

The as-cast Sm<sub>5</sub>Mg<sub>41</sub> alloys composed of the major phase Sm<sub>5</sub>Mg<sub>41</sub> (93.367 wt%) and the secondary phase SmMg<sub>3</sub> (6.633 wt%) were manufactured according to the procedure reported in our previous work.<sup>30</sup> The MoS<sub>2</sub>-catalyzed Sm<sub>5</sub>Mg<sub>41</sub> alloys were prepared by milling MoS<sub>2</sub> nano-particles (particle

size ≤ 40 nm, Beijing Dk nano S&T Ltd.) along with the mechanically ground as-cast alloy powders (particle size ≤ 75 μm) at weight fractions of 0%, 5%, and 10% in an argon atmosphere for 5 h. The weight ratio of the powder mixture to Cr–Ni stainless steel balls was 1 : 40 and each tank revolved around its own axis at a constant speed of 350 rpm. In fact, the mass of the precursor was 5.00 g in every tank, but only 4.55 g can be collected as the final product because the material was stuck on the balls and the inner wall of the tank. The elemental compositions of the milled powders were analyzed by inductively coupled plasma atomic emission spectrometry (ICP-AES). The phase compositions and microstructures of the alloys were characterized using an X-ray diffractometer (XRD) and a field emission transmission electron microscope (FETEM, Tecnai G2 F30, operated at 200 kV) equipped with an energy dispersive X-ray spectrometer (EDS) and a selected area electron diffractometer (SAED). The sample (0.5 g) was loaded into a cylindrical reactor for analyzing the pressure–composition isotherms (P–C–I) and the hydrogen absorption/desorption kinetics, which were measured by a PCT Automatic Measuring System (PCT-4SDWIN, Suzuki Shokan Co. Ltd.) in a furnace controlled at an accuracy of ±1 °C. Before measurement, each sample was subjected to five abovementioned hydriding/dehydriding cycles with the hydrogenation reaction occurring at 340 °C and 3 MPa and the dehydrogenation reaction occurring at 340 °C and 1 × 10<sup>-4</sup> MPa. The P–C–I curves were recorded at 320, 340, 360, and 380 °C in a hydrogen pressure range from 0.05 MPa to 3 MPa. The hydrogen absorption analysis was conducted at a pressure of 3 MPa and the temperatures of 270, 300, 360, and 380 °C, while the desorption analysis was conducted at a pressure of 1 × 10<sup>-4</sup> MPa and the temperatures of 300, 320, 340, and 360 °C. The non-isothermal dehydrogenation performance of the alloys was investigated by thermogravimetry (TG, TGA, Q600) at a heating rate of 5 °C min<sup>-1</sup> in an argon atmosphere (99.99% purity, 36 mL min<sup>-1</sup> flow rate).

## Results and discussion

### Composition, structure, and hydriding/dehydriding mechanism

The actual compositions of the Sm<sub>5</sub>Mg<sub>41</sub> + *x* wt% MoS<sub>2</sub> (*x* = 0, 5, and 10) alloys were measured by ICP-AES to be Sm<sub>5</sub>Mg<sub>41</sub> + *x* wt% MoS<sub>2</sub> (*x* = 0, 5, and 10), indicating that there was no contamination by Fe or other impurities; the compositions of the samples are listed in Table 1.

The XRD patterns of the milled Sm<sub>5</sub>Mg<sub>41</sub> + *x* wt% MoS<sub>2</sub> (*x* = 0, 5, and 10) alloys before and after the hydrogen absorption

**Table 1** The actual compositions of the Sm<sub>5</sub>Mg<sub>41</sub> + *x* wt% MoS<sub>2</sub> (*x* = 0, 5, 10) alloys measured by ICP

Sm <sub>5</sub> Mg <sub>41</sub> + <i>x</i> wt% MoS <sub>2</sub>	Sm (wt%)	Mg (wt%)	Mo (wt%)	Fe (wt%)
<i>x</i> = 0	42.99 ± 0.21	57.02 ± 0.29	0.00	0
<i>x</i> = 5	40.84 ± 0.20	54.16 ± 0.27	3.00 ± 0.02	0
<i>x</i> = 10	38.69 ± 0.19	51.31 ± 0.26	5.99 ± 0.03	0



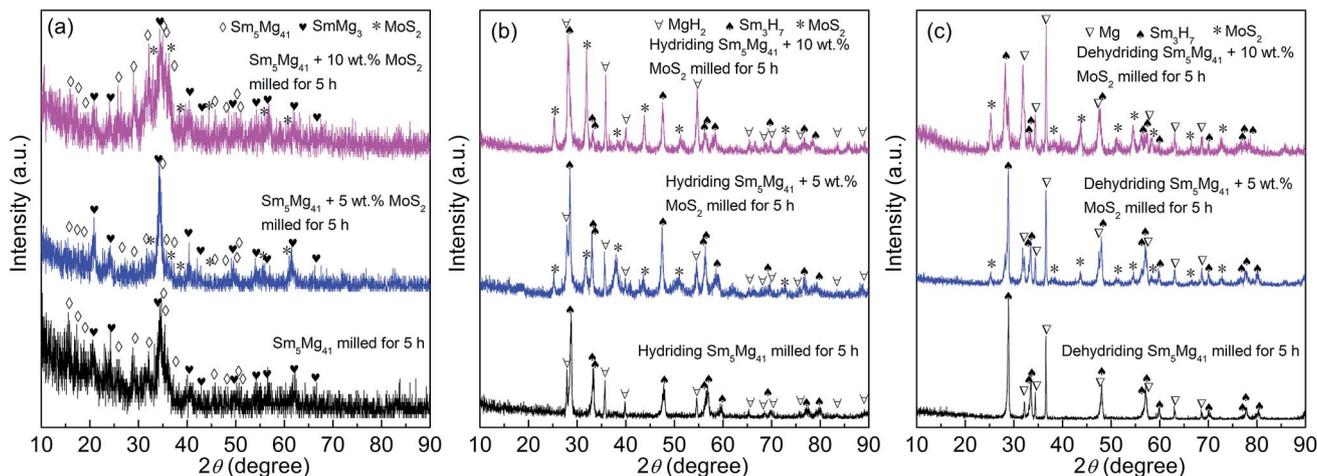


Fig. 1 XRD patterns of the  $\text{Sm}_5\text{Mg}_{41} + x \text{ wt}\% \text{MoS}_2$  ( $x = 0, 5$ , and  $10$ ) alloys milled for 5 h: (a) before hydriding; (b) after hydriding; (c) after dehydriding.

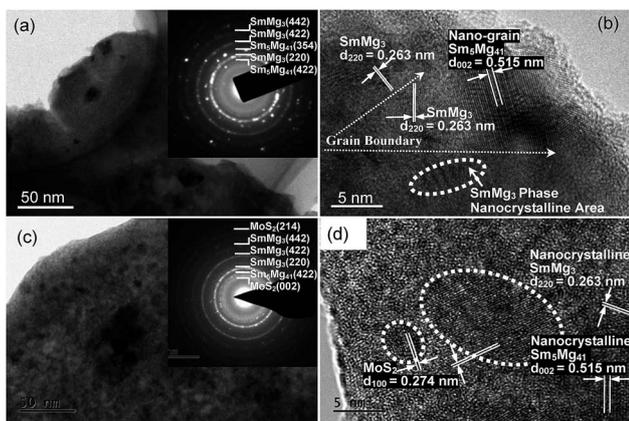


Fig. 2 SAED and TEM micrographs of the non-catalyzed (a and b) and the 5 wt%  $\text{MoS}_2$  catalyzed (c and d)  $\text{Sm}_5\text{Mg}_{41}$  alloys before the hydrogen absorption.

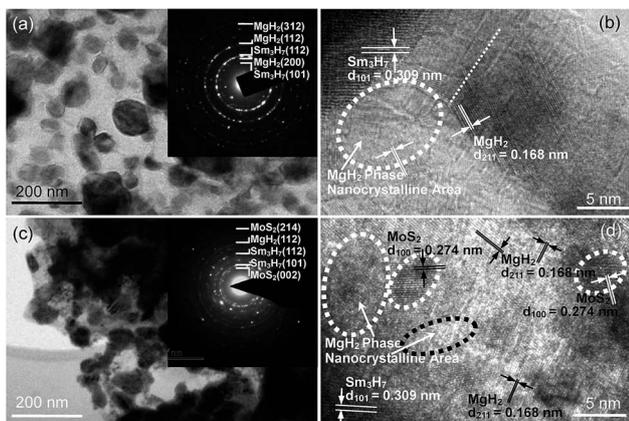


Fig. 3 SAED and TEM micrographs of the non-catalyzed (a and b) and the 5 wt%  $\text{MoS}_2$  catalyzed (c and d)  $\text{Sm}_5\text{Mg}_{41}$  alloys after the hydrogen absorption.

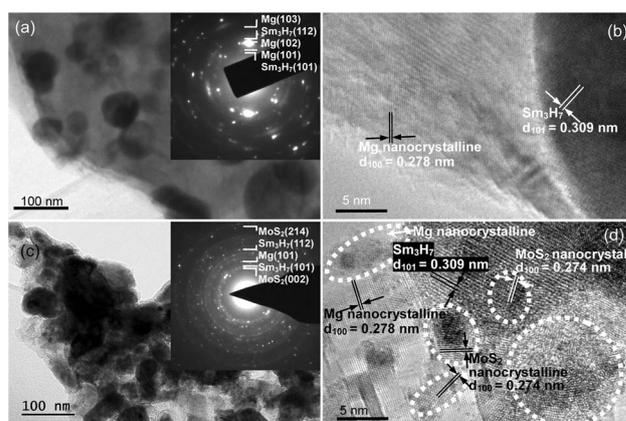


Fig. 4 SAED and TEM micrographs of the non-catalyzed (a and b) and the 5 wt%  $\text{MoS}_2$  catalyzed (c and d)  $\text{Sm}_5\text{Mg}_{41}$  alloys after the hydrogen desorption.

and desorption are depicted in Fig. 1. ICDD identification of the XRD patterns reveals that the milled alloys contain  $\text{Sm}_5\text{Mg}_{41}$  as the major phase and  $\text{SmMg}_3$  as the secondary phase before the hydrogen absorption. It is worth noting that milling causes a significant broadening of the diffraction peaks, implying the grain refining by ball milling. Moreover, this broadening phenomenon is reinforced by the addition of a  $\text{MoS}_2$  catalyst, which always exists in all of the catalyzed alloys due to its higher stability, suggesting that the addition of the  $\text{MoS}_2$  catalyst facilitates the grain refinement and the production of a nanocrystalline microstructure. It can be observed from Fig. 1(b) that three phases,  $\text{MoS}_2$ ,  $\text{Sm}_3\text{H}_7$ , and  $\text{MgH}_2$ , are present in the hydrogenated catalyzed alloys and there are evident crystallization reactions taking place, as reflected by the sharp peaks. The  $\text{MoS}_2$ ,  $\text{Sm}_3\text{H}_7$ , and  $\text{Mg}$  phases can be also found in the dehydrogenated catalyzed alloys (see Fig. 1(c)), suggesting the high thermal stabilities for the  $\text{Sm}_3\text{H}_7$  hydride and the  $\text{MoS}_2$  catalyst phases during the hydriding/dehydriding cycle. Based



on the XRD results, a hydride formation pathway is suggested:  $\text{Sm}_5\text{Mg}_{41} + \text{SmMg}_3 + \text{H}_2 \rightarrow \text{Sm}_3\text{H}_7 + \text{MgH}_2 \leftrightarrow \text{Sm}_3\text{H}_7 + \text{Mg} + \text{H}_2$ .

Fig. 2 shows the bright field TEM images, SAED rings, and HRTEM images of the milled (5 h)  $\text{Sm}_5\text{Mg}_{41} + x$  wt%  $\text{MoS}_2$  ( $x = 0$  and 5) alloys before the hydrogen absorption. Based on the crystallographic electron diffraction calibration results (see the insets in Fig. 2(a) and (c)), it could be confirmed that the alloys contain the  $\text{SmMg}_3$  and  $\text{Sm}_5\text{Mg}_{41}$  phases with an added  $\text{MoS}_2$  phase in the catalyzed alloys. These results are consistent with the XRD observations. A focus zone was randomly chosen to determine the microstructure of the alloys as shown in Fig. 2(b) and (d). As observed in the HRTEM images, the internal microstructure of the alloys contains the  $\text{Sm}_5\text{Mg}_{41}$  nanocrystals with a 0.515 nm interplanar spacing in the (002) direction, the

$\text{SmMg}_3$  nanocrystals with a 0.262 nm interplanar spacing in the (220) direction, and numerous structural defects, including nanocrystallites, lattice dislocations, grain boundaries, and micro-twins. The  $\text{MoS}_2$  nanocrystals with an interplanar spacing of 0.277 nm in the (200) direction were observed to be embedded in the surfaces of the catalyzed alloys.

Fig. 3 and 4 depict the bright field TEM images, SAED rings, and HRTEM images of the fully hydrogenated  $\text{Sm}_5\text{Mg}_{41} + x$  wt%  $\text{MoS}_2$  ( $x = 0$  and 5) alloys before and after the hydrogen desorption, respectively. The  $\text{Sm}_3\text{H}_7$  nano-particles surrounded by a  $\text{MgH}_2$  matrix-phase can be clearly observed in the hydrogenated alloy. This observation is also supported by the SAED pattern shown in the inset in Fig. 3(a). Moreover, a  $\text{MoS}_2$  phase is present in the catalyzed alloys (see Fig. 3(c)). A  $\text{MgH}_2$

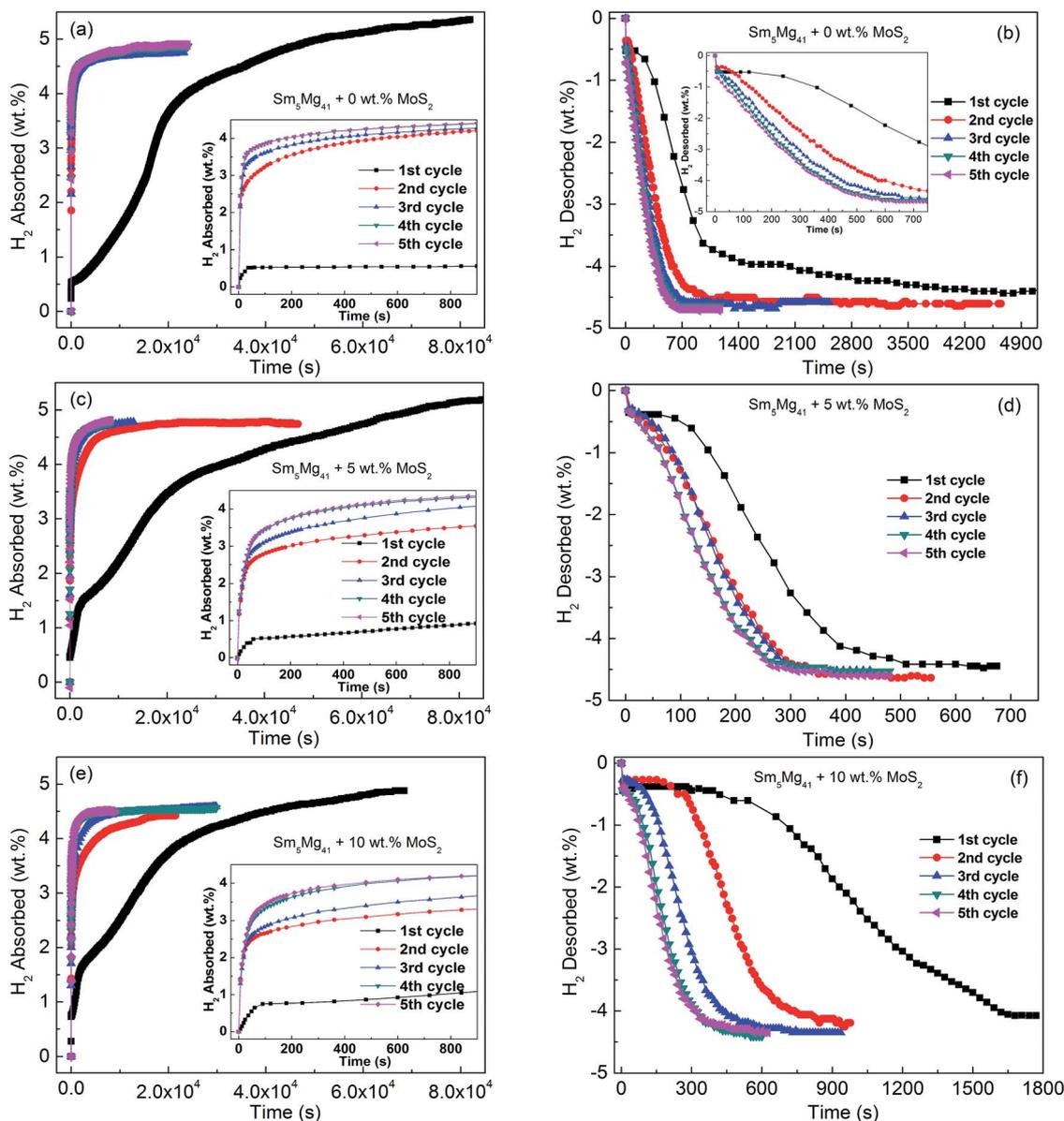


Fig. 5 The isothermal hydrogen absorption and desorption curves of the  $\text{Sm}_5\text{Mg}_{41} + x$  wt%  $\text{MoS}_2$  ( $x = 0, 5$ , and 10) alloys in the cycle activation with the hydrogenation reaction at 340 °C and 3 MPa and the hydrogenation reaction at 340 °C and  $1 \times 10^{-4}$  MPa: (a) and (b)  $x = 0$ ; (c) and (d)  $x = 5$ ; and (e) and (f)  $x = 10$ .



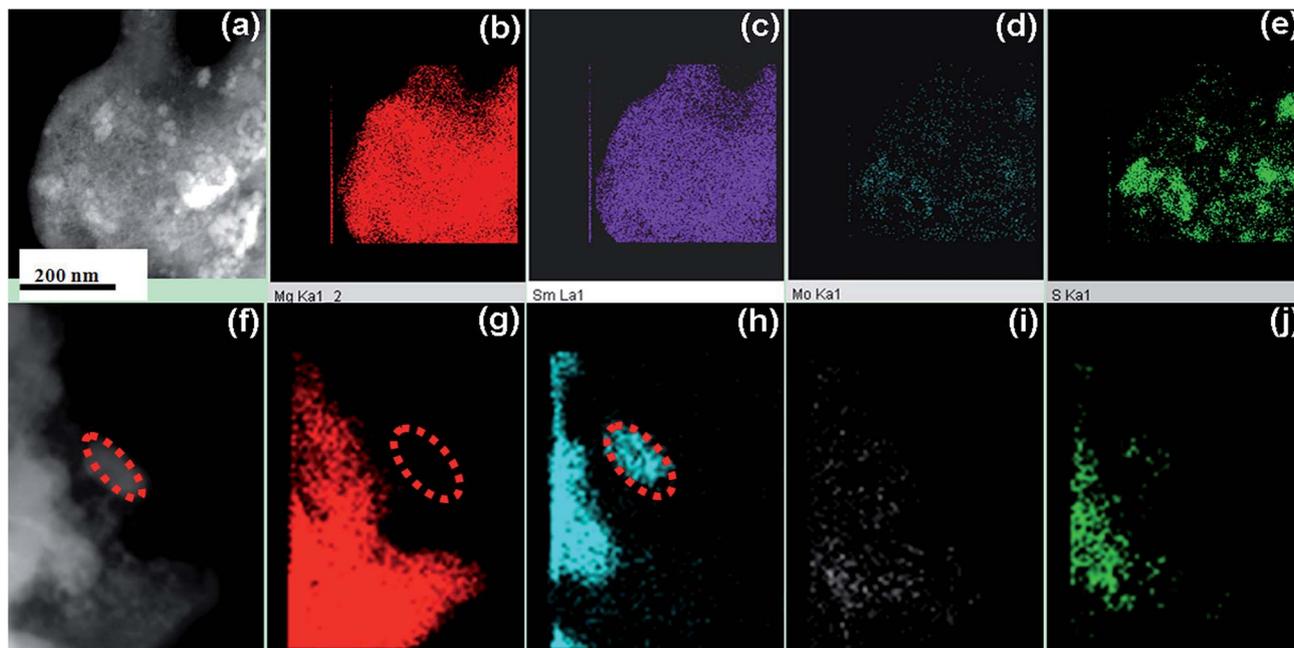


Fig. 6 FETEM micrographs and EDS mapping of the 5 wt% MoS<sub>2</sub> catalyzed Sm<sub>5</sub>Mg<sub>41</sub> alloys before the hydrogen absorption (a–e) and the hydrogenated sample after the hydrogen absorption (f–j).

polycrystalline phase and some crystal defects such as dislocations, grain boundaries, and twins are clearly observed in the dehydrogenated alloys (see Fig. 3(b) and (d)). It can be seen from Fig. 4(b) and (d) that after dehydrogenation, the Sm<sub>3</sub>H<sub>7</sub> particles exhibit an almost integrated structure with an interplanar spacing of 0.309 nm in the (211) direction, while being surrounded by a Mg phase, in which some crystal defects including lattice dislocations, grain boundaries, and nanocrystals can be clearly observed. Moreover, the MoS<sub>2</sub> nanocrystals embedded in the alloy surface can be clearly observed in the catalyzed alloys both before and after the hydrogen desorption.

Fig. 5 displays the isothermal hydrogenation and dehydrogenation curves of the Sm<sub>5</sub>Mg<sub>41</sub> + *x* wt% MoS<sub>2</sub> (*x* = 0, 5, and 10) alloys activated by five hydriding and dehydriding cycles with the hydrogenation reaction occurring at 340 °C and 3 MPa and the dehydrogenation reaction occurring at 340 °C and 1 × 10<sup>-4</sup> MPa. It can be observed that after more than 5 hydriding/dehydriding cycles, the hydrogen absorption/desorption capacities are about 5.01 wt%, 4.81 wt%, and 4.59 wt% for *x* = 0, 5, and 10, respectively, and the curves remain almost unchanged with a further increase in the number of cycles. Notably, the initial maximum hydrogen capacities are 5.36 wt%, 5.21 wt%, and 4.88 wt% for *x* = 0, 5, and 10, respectively, which are higher than their reversible hydrogen absorption/desorption capacities, indicating that there exist undecomposed hydrides of Sm<sub>3</sub>H<sub>7</sub> in the Sm<sub>5</sub>Mg<sub>41</sub> + *x* wt% MoS<sub>2</sub> (*x* = 0, 5, and 10) alloys during the hydrogen absorption/desorption process. Moreover, the shortest initial hydriding time is exhibited by the *x* = 5 alloy, indicating that the addition of MoS<sub>2</sub> markedly improves the initial hydriding progress of the alloy. However, the improvement is hindered when an excess catalyst is added because the surface of the alloy is covered by the

catalyst. However, the addition of MoS<sub>2</sub> by milling significantly enhances the reversible hydrogen absorption/desorption rate of the alloy after the initial hydriding cycle. Specifically, the time for complete hydrogen desorption of the Sm<sub>5</sub>Mg<sub>41</sub> alloy at 340 °C is reduced from 4900 s to 400 s when MoS<sub>2</sub> is added as a catalyst.

The FETEM analysis was conducted to investigate the changes in the microstructure and the phase distribution of the 5 wt% MoS<sub>2</sub>-catalyzed Sm<sub>5</sub>Mg<sub>41</sub> alloy before and after the hydrogen absorption. Fig. 6 shows the bright field FETEM images and the EDS mapping results, in which the red, purple,

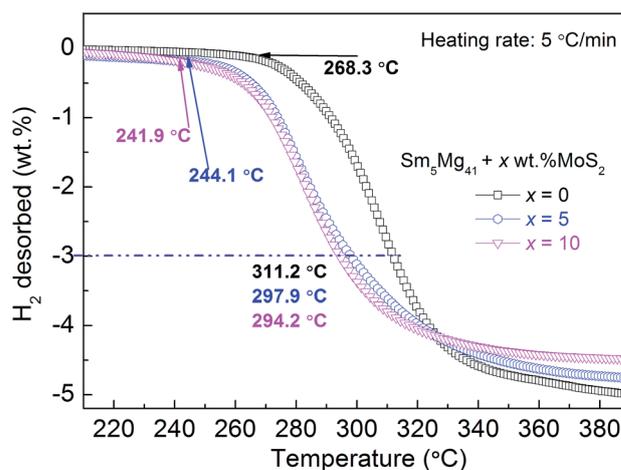


Fig. 7 Temperature programmed desorption curve of the Sm<sub>5</sub>Mg<sub>41</sub> + *x* wt% MoS<sub>2</sub> (*x* = 0, 5, and 10) alloys after the hydrogen absorption at a heating rate of 5 °C min<sup>-1</sup>.



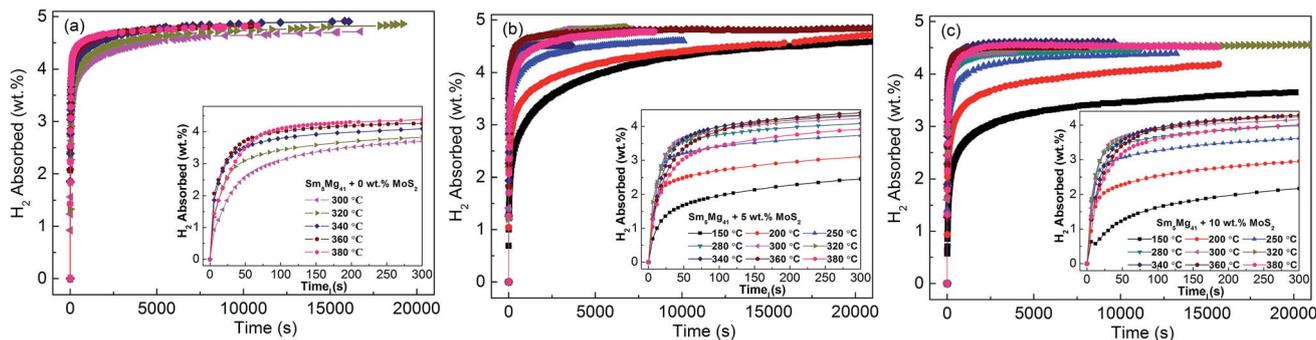


Fig. 8 Isothermal hydrogenation kinetic curves of the  $\text{Sm}_5\text{Mg}_{41} + x \text{ wt}\% \text{ MoS}_2$  ( $x = 0, 5, 10$ ) alloys at different temperatures: (a)  $x = 0$ ; (b)  $x = 5$ ; and (c)  $x = 10$ .

cyan, and green points represent the distributions of Mg, Sm, Mo, and S elements, respectively. As shown in Fig. 6(b) and (c), the Mg and Sm elements have nearly the same distribution in the alloy before the hydrogen absorption. However, the Sm element separates from the Mg element after the hydrogen absorption (see Fig. 6(g) and (h)), indicating the atomic migration of Sm and Mg in the Mg-based  $\text{Sm}_5\text{Mg}_{41}$  alloy during the first hydrogen absorption process. Moreover, Mo and S always exhibit nearly the same distribution in the alloy both before and after the hydrogen absorption. This finding shows that the first hydriding cycle induces an irreversible decomposition of the alloy with the formation of a Mg hydride and the corresponding Sm hydride according to the following mechanism:  $\text{Sm}_5\text{Mg}_{41} + \text{SmMg}_3 + \text{H}_2 \rightarrow \text{Sm}_3\text{H}_7 + \text{MgH}_2$ . The nucleation and growth mechanism of the formed  $\text{Sm}_3\text{H}_7\text{-MgH}_2$  composites can be described as follows. The Mg-based  $\text{Sm}_5\text{Mg}_{41}$  alloy initially transforms into  $\text{Sm}_3\text{H}_7$  and Mg and then into the  $\text{Sm}_3\text{H}_7\text{-MgH}_2$  composites during the hydrogenation process.<sup>30</sup> Moreover, the  $\text{MoS}_2$  phase is stable.

### Hydrogen desorption temperature

To investigate the relationship between the H-desorption temperature and the hydrogen desorption capacity, the temperature programmed desorption curves of the hydrogenated  $\text{Sm}_5\text{Mg}_{41} + x \text{ wt}\% \text{ MoS}_2$  ( $x = 0, 5$ , and  $10$ ) alloys were constructed at a heating rate of  $5 \text{ }^\circ\text{C min}^{-1}$  (Fig. 7). It can be

observed that three non-isothermal dehydrogenation curves are similar in shape, but the initial temperatures of the hydrogen release are different, *i.e.*,  $268.3, 244.1$ , and  $241.9 \text{ }^\circ\text{C}$  for  $x = 0, 5$ , and  $10$ , respectively. There is a visible decrease of  $16.4 \text{ }^\circ\text{C}$  in the initial dehydriding temperature. Moreover, the dehydriding temperatures of the alloys are  $311.2, 297.9$ , and  $294.2 \text{ }^\circ\text{C}$  for  $x = 0, 5$ , and  $10$ , respectively, corresponding to 3 wt% of the hydrogen desorption capacity, while that of pure  $\text{MgH}_2$  is  $428 \text{ }^\circ\text{C}$ .<sup>21</sup> From the above description, it can be inferred that the dehydriding temperature decreased significantly due to the catalytic action of  $\text{MoS}_2$  and  $\text{Sm}_3\text{H}_7$  nano-particles.

### Hydrogen storage kinetics

In order to understand the influence of the addition of  $\text{MoS}_2$  catalyst on the hydrogenation kinetics of the  $\text{Sm}_5\text{Mg}_{41}$  alloys, the isothermal hydrogenation kinetic curves of the alloys were constructed at different temperatures (Fig. 8). It is evident that the catalyst can significantly decrease the temperature of the hydrogen absorption. The absorption temperature of the catalyzed  $\text{Sm}_5\text{Mg}_{41}$  alloys with 5 wt% and 10 wt%  $\text{MoS}_2$  dramatically decreases to  $150 \text{ }^\circ\text{C}$ . Moreover, the hydriding capacities of the experimental samples can reach the values of 3.0 wt% at  $200 \text{ }^\circ\text{C}$  within 300 s. However, the maximum hydrogen absorption capacities are 5.01, 4.87, and 4.60 wt% for the non-catalyzed alloy, 5 wt%-added alloy, and 10 wt%-added alloy, respectively. The reduction in the maximum capacity is attributed to

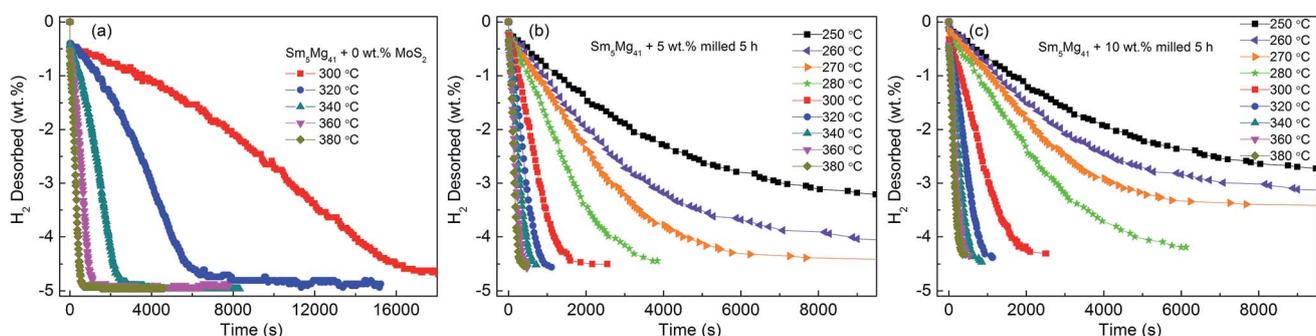


Fig. 9 Isothermal dehydrogenation kinetic curves of the  $\text{Sm}_5\text{Mg}_{41} + x \text{ wt}\% \text{ MoS}_2$  ( $x = 0, 5$ , and  $10$ ) alloys at different temperatures: (a)  $x = 0$ ; (b)  $x = 5$ ; and (c)  $x = 10$ .



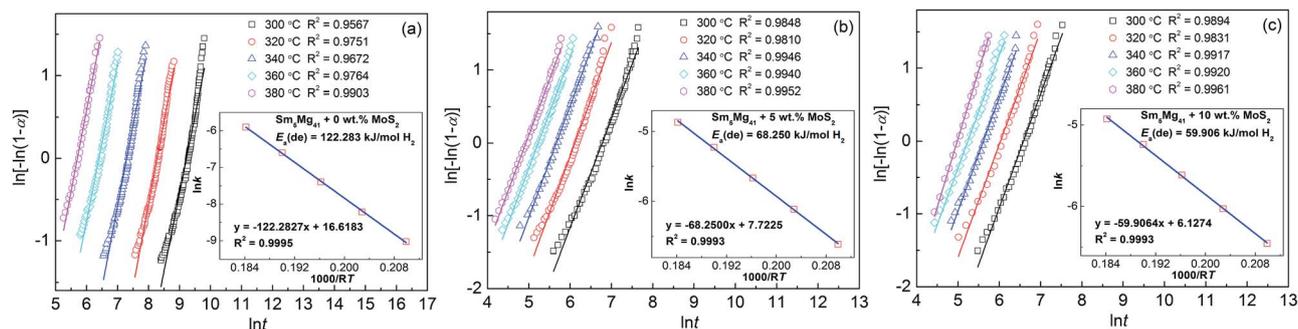


Fig. 10 JMA plots and Arrhenius plots for the dehydrogenation of the  $\text{Sm}_5\text{Mg}_{41} + x \text{ wt}\% \text{ MoS}_2$  ( $x = 0, 5$ , and  $10$ ) alloys: (a)  $x = 0$ ; (b)  $x = 5$ ; and (c)  $x = 10$ .

the inability of the catalyst to react with  $\text{H}_2$  and produce the hydrides. Thus, it can be deduced that the catalyst can markedly enhance the hydriding properties. The catalytic action can be explained as follows. The catalyst enhances the rate of diffusion of  $\text{H}_2$  and decreases the dissociation energy of  $\text{H}_2$  into the H atoms on the surfaces of the alloys.

Fig. 9 shows the hydrogen desorption curves of the as-milled  $\text{Sm}_5\text{Mg}_{41}$  alloys with different  $\text{MoS}_2$  loadings at different temperatures. The dehydrogenation capacities of the alloys decrease with an increase in the  $\text{MoS}_2$  weight fraction because of its dead-weight. In other words, the maximum dehydrogenation capacities of the  $\text{Sm}_5\text{Mg}_{41} + x \text{ wt}\% \text{ MoS}_2$  ( $x = 0, 5$ , and  $10$ ) alloys at  $360^\circ\text{C}$  are  $4.88 \text{ wt}\%$ ,  $4.57 \text{ wt}\%$ , and  $4.35 \text{ wt}\%$ , respectively, for  $x = 0, 5$ , and  $10$ . These values are lower than their hydrogenation capacity values because the stored hydrogen cannot be desorbed fully in a closed test system. The times to desorb  $3.5 \text{ wt}\%$  hydrogen at  $300, 320, 340, 360$ , and  $380^\circ\text{C}$  are  $12\,180, 4530, 1704, 702$ , and  $352 \text{ s}$ , respectively, in the case of the non-catalyzed  $\text{Sm}_5\text{Mg}_{41}$  alloy,  $970, 552, 362, 244$ , and  $184 \text{ s}$ , respectively, in the case of the  $5 \text{ wt}\% \text{ MoS}_2$  added  $\text{Sm}_5\text{Mg}_{41}$  alloy, and  $1272, 621, 386, 261$ , and  $199 \text{ s}$  in the case of the  $10 \text{ wt}\% \text{ MoS}_2$  added  $\text{Sm}_5\text{Mg}_{41}$  alloy. It can be observed from the comparison that the dehydriding rates decrease with a decrease in the temperature. Adding  $5 \text{ wt}\% \text{ MoS}_2$  markedly improves the dehydrogenation kinetics of the  $\text{Sm}_5\text{Mg}_{41}$  alloy, but the improvement is hindered when an excess catalyst is added because of its dead-weight.

Hydrogen desorption activation energy is an important factor in describing the dehydrogenation kinetics of an alloy.<sup>36</sup> In this study, we chose the Arrhenius method to describe the effect of the  $\text{MoS}_2$  addition on the dehydrogenation process. The dehydrogenation kinetics is primarily determined by the energy barrier, which needs to be overcome before  $\text{MgH}_2$  can release  $\text{H}_2$ . The activation energy is defined as the total energy overcome during the dehydrogenation process. In the current study, the dehydrogenation process of  $\text{Sm}_5\text{Mg}_{41}$  follows a nucleation and growth process. The Johnson–Mehl–Avrami (JMA) model is used to simulate this process as follows:

$$\ln[-\ln(1 - \alpha)] = \eta \ln k + \eta \ln t \quad (1)$$

where  $\alpha$  is the phase fraction transformed at time  $t$ , which can be identified using a normalized hydrogen wt% (range from 0 to 1),  $\eta$  is the Avrami exponent, and  $k$  is an effective kinetic parameter. Using the logarithmic form of eqn (1), the JMA plots of  $\ln[-\ln(1 - \alpha)]$  vs.  $\ln t$  can be drawn at the temperatures of  $300, 320, 340, 360$ , and  $380^\circ\text{C}$  at different  $\text{MoS}_2$  contents, as shown in Fig. 10. The fitting lines of the JMA plots are almost linear, which indicates that the dehydrogenation reaction exhibits an instantaneous nucleation followed by an interface-controlled three-dimensional growth process. The slope and intercept of the JMA plots represent the values of  $\eta$  and  $\eta \ln k$ , respectively, from which the value of the rate constant  $k$  could be deduced. Using the Arrhenius method, the dehydrogenation activation energy  $E_a(\text{de})$  can be calculated as follows:

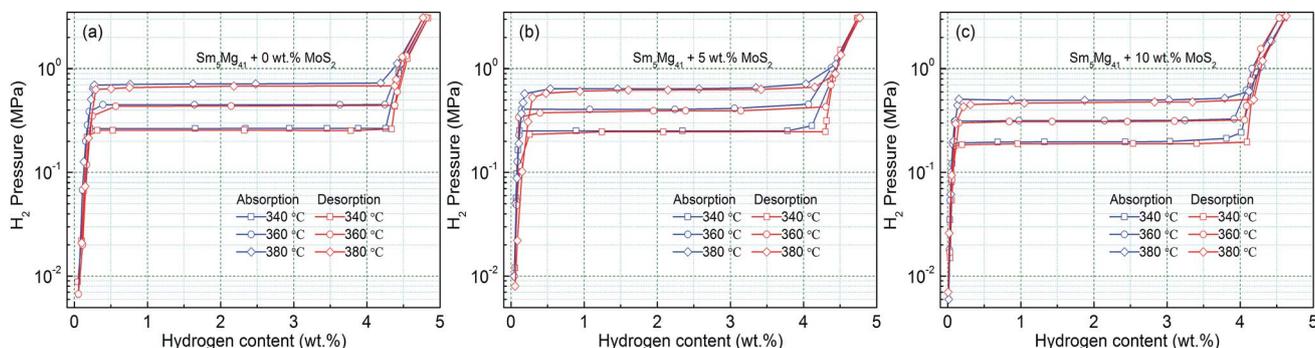
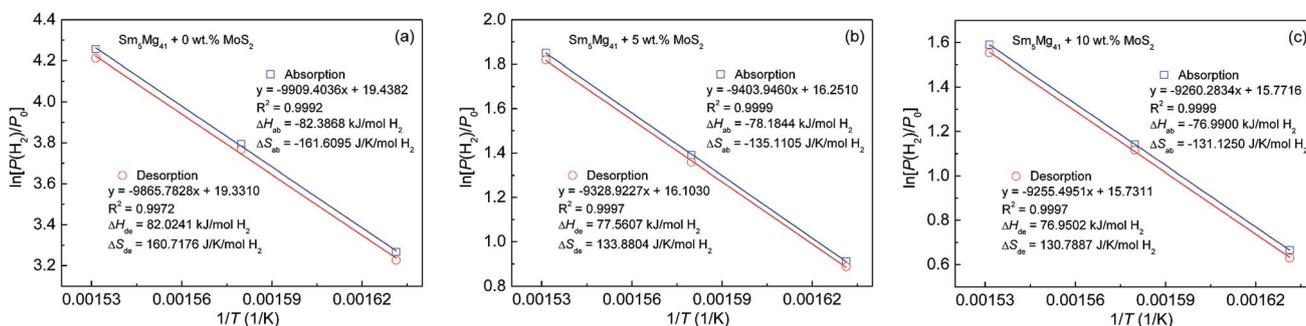


Fig. 11 P–C–I curves of the  $\text{Sm}_5\text{Mg}_{41} + x \text{ wt}\% \text{ MoS}_2$  ( $x = 0, 5$ , and  $10$ ) alloys measured at different temperatures: (a)  $x = 0$ ; (b)  $x = 5$ ; and (c)  $x = 10$ .



**Table 2** Plateau pressures from the P–C–I curves at different temperatures and the calculated enthalpy and entropy for the hydrogen absorption and desorption process of the MoS<sub>2</sub> catalyzed Sm<sub>5</sub>Mg<sub>41</sub> alloys

		Plateau pressure (MPa)			Thermodynamic parameters	
		340 °C	360 °C	380 °C	$\Delta H$ (kJ mol <sup>-1</sup> )	$\Delta S$ (J K <sup>-1</sup> mol <sup>-1</sup> )
As-milled 5 h Sm <sub>5</sub> Mg <sub>41</sub> alloys	Absorption	0.266	0.451	0.716	-82.3868	-161.6095
	Desorption	0.255	0.438	0.684	82.0241	160.7176
Added 5 wt% MoS <sub>2</sub>	Absorption	0.252	0.407	0.645	-78.1844	-135.1105
	Desorption	0.246	0.394	0.625	77.5607	133.8804
Added 10 wt% MoS <sub>2</sub>	Absorption	0.197	0.317	0.497	-76.9900	-131.1250
	Desorption	0.190	0.309	0.479	76.9502	130.7887



**Fig. 12** Van't Hoff plots of the Sm<sub>5</sub>Mg<sub>41</sub> + x wt% MoS<sub>2</sub> (x = 0, 5, and 10) alloys measured at different temperatures: (a) x = 0; (b) x = 5; and (c) x = 10.

$$k = A \exp[-E_a(\text{de})/RT] \quad (2)$$

where  $k$  is an effective kinetic parameter, as defined previously,  $A$  is a temperature independent coefficient,  $R$  is the universal gas constant (8.3145 J mol<sup>-1</sup> K<sup>-1</sup>), and  $T$  is the absolute temperature. Using the logarithmic transform of eqn (2), the Arrhenius plots of  $\ln k$  vs.  $1/T$  can be drawn as shown in the inset in Fig. 10. The fitting lines of all of the Arrhenius plots are almost linear. From the slopes of the fitting lines, the activation energies of the Sm<sub>5</sub>Mg<sub>41</sub> alloys are calculated to be 122.28, 68.25, and 59.91 kJ mol<sup>-1</sup> H<sub>2</sub> for  $x = 0, 5,$  and  $10,$  respectively, which indicates that the activation energies of the Sm<sub>5</sub>Mg<sub>41</sub> alloys decreased with an increase in the MoS<sub>2</sub> content. The nano-MoS<sub>2</sub> used as the catalysts markedly reduces the energy barrier and lowers the driving forces required for nucleation during the dehydrogenation reaction. In addition, the  $E_a(\text{de})$  value of the as-milled Sm<sub>5</sub>Mg<sub>41</sub> alloy is much lower than that of pure milled MgH<sub>2</sub> (158.5 kJ mol<sup>-1</sup> H<sub>2</sub>),<sup>37</sup> suggesting that Sm<sub>3</sub>H<sub>7</sub> can catalyze the desorption reaction of MgH<sub>2</sub>, and the similar results have been demonstrated in the Sm<sub>5</sub>Mg<sub>41</sub> alloys.<sup>30</sup>

### Hydrogen storage thermodynamics

In order to analyze the influence of the catalyst on the hydrogen storage thermodynamics of the Sm<sub>5</sub>Mg<sub>41</sub> + x wt% MoS<sub>2</sub> ( $x = 0, 5,$  and  $10$ ) alloys, the P–C–I curves were constructed at different temperatures. Fig. 11 shows that each curve has only one flat hydrogen equilibrium plateau. The thermodynamic data obtained from the P–C–I measurements are listed in Table 2. It can

be found that the absorption/desorption pressure plateaus reduce with an increase in the MoS<sub>2</sub> content, which attributes to Mo that can facilitate the dissociation of hydrogen.<sup>38</sup>

According to the absorption/desorption pressure plateaus, the thermodynamic parameters, *viz.*, enthalpy change ( $\Delta H$ ) and entropy change ( $\Delta S$ ), can be estimated from the Van't Hoff equation<sup>30</sup> as shown below:

$$\ln[P(\text{H}_2)/P_0] = \Delta H/(RT) - \Delta S/R \quad (3)$$

where  $P_0 = 1$  atm, and  $R$  and  $P(\text{H}_2)$  refer to the gas constant and the equilibrium plateau pressure, respectively. The Van't Hoff curves ( $\ln[P(\text{H}_2)/P_0]$  vs.  $1/T$ ) are illustrated in Fig. 12. According to the slopes and intercepts of the fitting lines obtained from the experimental data, the thermodynamic parameters can be calculated (Table 2). The changes in the hydrogenation enthalpies ( $\Delta H_{\text{ab}}$ ) are 82.39, 78.18, and 76.99 kJ mol<sup>-1</sup> H<sub>2</sub> for  $x = 0, 5,$  and  $10,$  respectively, while the corresponding changes in the dehydrogenation enthalpies ( $\Delta H_{\text{de}}$ ) are -82.02, -77.56, and -76.95 kJ mol<sup>-1</sup> H<sub>2</sub>. However, the  $\Delta H_{\text{de}}$  value of the experimental alloys is very close to that of pure Mg, namely, -76 to -78 kJ mol<sup>-1</sup>,<sup>39,40</sup> which suggests that the addition of a MoS<sub>2</sub> catalyst could not change the thermodynamic properties in terms of the hydrogen storage in the Mg-based alloys.

## Conclusions

(1) The alloys are composed of the nanocrystal phases of Sm<sub>5</sub>Mg<sub>41</sub>, SmMg<sub>3</sub>, and MoS<sub>2</sub>. Mechanical milling and catalyst



doping lead to a reduction in the particle sizes. These particles can store a strain energy, which contributes to an improvement in the hydrogen storage kinetics. The MoS<sub>2</sub> phase is stable during the absorption/desorption cycling process. The MgH<sub>2</sub> and Sm<sub>3</sub>H<sub>7</sub> phases are formed after the hydrogen absorption, while the Mg and Sm<sub>3</sub>H<sub>7</sub> phases are generated after the hydrogen desorption. The hydriding/dehydriding reaction mechanism is as follows: Sm<sub>5</sub>Mg<sub>41</sub> + SmMg<sub>3</sub> + H<sub>2</sub> → Sm<sub>3</sub>H<sub>7</sub> + MgH<sub>2</sub> ↔ Sm<sub>3</sub>H<sub>7</sub> + Mg + H<sub>2</sub>.

(2) The activation energies of dehydrogenation are estimated to be 122.283, 68.250, and 59.906 kJ mol<sup>-1</sup> H<sub>2</sub> at the MoS<sub>2</sub> catalyst contents of 0, 5, and 10 wt%, respectively, which suggests that the nano-MoS<sub>2</sub> reduces the energy barrier and lowers the driving forces required for nucleation during the dehydrogenation reaction.

(3) The catalyzed alloys begin to release hydrogen at ~241.9 °C, which is ~26.4 °C lower than that of the non-catalyzed alloy. The hydrogenation enthalpy of the 10 wt% MoS<sub>2</sub>-catalyzed alloy is determined to be ~76.99 kJ mol<sup>-1</sup> H<sub>2</sub>, which is very close to that of pure Mg, indicating that catalyst addition could not alter the thermodynamic properties in terms of the hydrogen storage in the Mg-based alloys.

## Conflicts of interest

There are no conflicts to declare.

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