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# Improvement of structure and electrical conductivity of activated carbon by catalytic graphitization using N<sub>2</sub> plasma pretreatment and iron(III) loading

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In order to improve the amorphous structure of commercially activated carbon (AC) for enhancing its electron transport, nitrogen radio-frequency plasma was firstly used to pretreat AC, followed by impregnation with FeCl<sub>3</sub>·6H<sub>2</sub>O solutions to prepare graphitic carbon under the pyrolysis temperature of 1000 °C. Emphasis was put on investigating the structure and electrical conductivity of post-calcination samples by X-ray diffraction (XRD), Raman spectroscopy, and transmission electron microscopy (TEM) characterization, as well as measuring its powder resistivity. The results show that the structure of annealed composite samples is more ordered as the pretreatment time increased, and the maximum value of electrical conductivity is higher than that of the un-pretreated AC by 20%. Furthermore, by exploring the effect on the reaction of plasma treatment on iron loading by means of X-ray photoelectron spectroscopy (XPS) and energy-dispersive X-ray spectroscopy (EDX), a plausible explanation can be proposed that the content and distribution of iron loaded on the raw AC play a decisive role in the later iron-catalyzed graphitization.

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## 1. Introduction

It is a fact that the amount of fossil resources and energy has been an important constraining factor influencing global development of economy and society. Biomass and bioenergy, as new types of sustainable alternatives, have attracted much attention.<sup>1</sup> Among the many biomass products, activated carbon (AC), which universally has a well-developed pore structure and high surface area, has been widely used in the field of energy storage and environmental protection.<sup>2</sup> On the one hand, as an adsorbent it can effectively remove toxic heavy metal and organic pollutants in wastewater treatment. On the other hand, AC, as a kind of promising electrode material, plays a vital role in current industrial supercapacitors. In recent years, many researchers have paid considerable attention to studying nanostructured carbon, since the detailed morphology of the AC framework will greatly determine its physicochemical properties.<sup>3</sup> Though the manufacturing process of classic AC is mature, the ordered level of AC framework and its electrical conductivity are still not satisfactory.<sup>4</sup> Exceptionally, in contrast with the amorphous AC, graphitic carbon (GC) with highly

ordered region exhibits some advantages, such as high electric conductivity, excellent thermal stability and strong oxidation resistance to acids and bases.<sup>5</sup> Accordingly, the synthetic method of graphitic carbon triggers intense interest from researchers due to its bright application prospect.

Graphitization is a thermodynamically favorable process, which transforms amorphous carbon into well-ordered and three-dimensional graphitic structure.<sup>3,6</sup> In order to prepare GC, two groups of Zhang *et al.* and Ren *et al.* reported that they fabricated GC by pyrolysis at extremely high temperature (>2000 °C) for 12 hours in a vacuum environment.<sup>7,8</sup> However, this process is time-consuming and energy-consuming. Besides, other methods such as chemical vapor deposition and laser ablation are subject to the strict operating condition.<sup>9</sup> By comparison, a technique called catalytic graphitization has been widely adopted *via* introducing certain inorganic or organic additives into carbon sources, and the advantage of this method allows the formation of graphitic structure at a relatively lower temperature (<1000 °C).<sup>6,10</sup> In particular, nonprecious transition metal salts such as ferric(III), cobalt(II), and nickel(II) chlorides are usually functioned as catalyst species.<sup>11</sup> At the same time, the mechanisms of metal-catalyzed graphitization are classified as solid-phase and liquid-phase, which are more dependent on the state of catalyst.<sup>12</sup> Zhou *et al.* revealed that Fe–Ni alloy had a significant catalytic effect to convert PAN-based carbon fibers into crystalline materials at

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moderate temperatures. Moreover, from the results of the graphitization degree of PAN-based carbon fibers coated with Fe–Ni, it can be concluded that the Fe catalyst prevails in the synergic catalytic function.<sup>5</sup> More recently, Hoekstra *et al.* further reported that the iron was the most active catalyst as a consequence of the generation of iron carbides in catalytic graphitization.<sup>9</sup>

To the best of our knowledge, in addition to the problem of iron dispersion, the compatibility issue between iron catalysts and AC is also hardly concerned in the previous study. According to theoretical and experimental research, a common conclusion can be summarized that the pores of electrode material are favorable for electrolyte ions transport while lamellar structure like graphite is conducive to the conduction of electrons.<sup>3</sup> Hence, it may be a good choice to load much iron catalysts on the carbon materials surfaces as much as possible, which can be more helpful to iron mobility and prevent porosity channels of carbon materials from being blocked.<sup>9</sup> Based on the above idea, it is imperative to enhance the surfactivity of carbon materials for adsorbing more metal catalyst particles. Hopefully, some literatures have proved that the doping of nitrogen (N) can provide Fe catalyst with active site and support its long-term stability due to a strong interaction existed between Fe and N.<sup>13,14</sup> Compared to the chemical functionalizations or surfactant method, radio-frequency (RF) plasma treatment embodies some competitive advantages in modifying materials surface respect, since it features a fast, efficient, and environmentally friendly technique.<sup>15–17</sup>

On the basis of these prior studies, we present a novel way of coordinating iron and nitrogen, that is, pretreating the raw AC *via* RF nitrogen plasma by varying processing time, and then dip AC into ferric chloride solution for the next heating step. The combination of nitrogen doping and ferric ions loading is beneficial to take full advantage of their own strengths. Nitrogen doping can endow AC with a better affinity on improving surface accessibility.<sup>18</sup> The ferric ions serve as the catalyst, which can facilitate the ordered arrangement of grains during the thermal treatment of precursor.<sup>11,13</sup> The objective of this work was to create a graphite-like material in a reliable and feasible method. To this end, the changes of structural characteristics and electrical properties of catalytic pyrolysis products were discussed.

## 2. Material and methods

### 2.1 Preparation of samples

Firstly, commercial coconut shell-based activated carbon (purchased from Mulinsen Activated Carbon Group, Nanjing, China) was screened into a particle size of less than 100 mesh, followed by drying at 103 °C for 12 h. Subsequently, about 2.5 g AC powder was evenly laid on the glass Petri dish with a diameter of 120 mm and then the dish was placed into a reaction chamber for plasma treatment. The procedure of RF plasma treatment was as following: the chamber was evacuated to about 3 Pa. Afterwards the high-purity nitrogen (N<sub>2</sub>, 99.99%) was fed into the vacuum chamber and maintained volume ventilation for 5 min. For the sake of ensuring the purity of cavity gas, this step would be repeated for 3 times. Finally, the pressure of chamber was required to be controlled at 30 Pa through

adjusting the flow rate of reactive gas.<sup>17</sup> The excitation radio-frequency and power were set at 13.56 MHz and 100 W respectively. The treatment time varied from 2 to 10 min with a time interval of 4 min.

After the completion of modification, a dip adsorption method was used to load iron catalyst on AC. To prepare four bottles of ferric ions solution with a constant concentration of 0.5 wt%, 6.66 g FeCl<sub>3</sub>·6H<sub>2</sub>O (purchased from Nanjing Chemical Reagent Co., Ltd.) were dissolved in 800 mL of distilled water and stirred for 2 h. Then, 800 mL solution was equally divided into four bottles and put 2 g AC with different treatment conditions into each bottle of FeCl<sub>3</sub> solution for shaking 24 h. At last, the impregnated precursors were filtered and dried at 103 °C for 6 h.

The tube furnace was employed for pyrolysis and a temperature-programmed route was set as below. Firstly, the precursors were heated from room temperature to 250 °C with a soak time of 30 min at a rate of 5 °C min<sup>-1</sup> in air atmosphere. Then, the mixtures were continuously heated up to a desired temperature of 1000 °C under 80 mL min<sup>-1</sup> nitrogen gas flow at a ramp rate of 10 °C min<sup>-1</sup> and held at 1000 °C for 2 h. Finally, all annealed composite samples were labeled as PAC-*t*, where the letter “*t*” represented plasma treatment time.

### 2.2 Characterization methods

X-ray diffractometer (XRD, Bruker D8 FOCUS, Germany) with Cu K $\alpha$  radiation ( $\lambda = 0.154$  nm) and Raman spectrometer (DXR532, America) using an excitation wavelength of 532 nm from an argon ion laser were utilized at room temperature for collecting the structural information of annealed composite samples. The morphology of heated samples was detected by transmission electron microscopy (TEM, JEM-2100F, JEOL Ltd., Tokyo, Japan). The Fe mapping of precursors were recorded by a scanning electron microscopy (SEM, JSM-7600F, Japan) equipped with an energy-dispersive X-ray spectroscope (EDX) analyzer. X-ray photoelectron spectroscopy (XPS, AXIS Ultra DLD, Japan) was used for determining the surface condition of nitrogen on the raw AC with and without RF plasma treatment.<sup>19</sup> The resistivity of samples at room temperature was measured by powder resistivity instrument (ST2722, China) *via* stuffing carbon powders (40- to 60-mesh) into a hollow cylinder with its height of 5 mm and inner diameter of 11.28 mm, and then pressed them in different pressures of 4 and 12 MPa for the further test (Fig. 1).<sup>20</sup>

## 3. Results and discussion

### 3.1 Analysis of structure, phase and morphology

XRD patterns of different precursors heated at 1000 °C with and without RF plasma treatment are illustrated in Fig. 2. The phase identifications of four samples were retrieved by XRD analysis software (Jade 6) and the results were marked on the XRD profiles with special symbols.<sup>21</sup> For all post-calcination materials, it should be noticed that the emergence of typical diffraction of Fe<sub>3</sub>C phase (JCPDS no. 03-0411) at around 66.3°, although the intensity of Fe<sub>3</sub>C reflection is very low. This peak



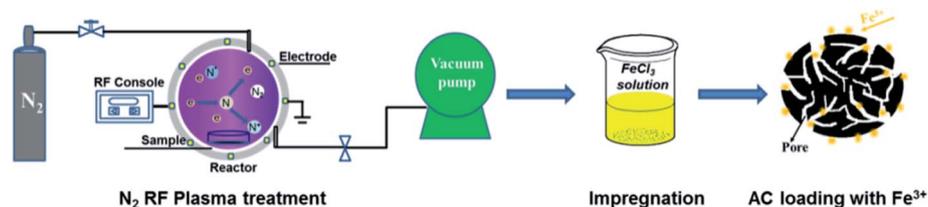


Fig. 1 The schematic diagram of plasma pretreatment and ferric iron ions loading on activated carbon.

can be assigned to the (024) crystalline plane. It is reported that the  $\text{Fe}_3\text{C}$  plays a crucial role as intermediates in catalytic graphitization,<sup>9</sup> since a large quantity of metastable  $\text{Fe}_3\text{C}$  would be resolved into free-C and metallic Fe as thermal treatment temperature rising above 800 °C.<sup>22</sup> To be concrete, the mobility of precipitated Fe would make advancement of graphitization while free-C would make up for defects by entering the skeleton.<sup>23</sup> It is also important to note that the phase of Fe (JCPDS no. 88-2324) is detected for all heated samples, but the intensity of PAC-0 is slightly higher than the remaining three samples, which might be due to the loss of iron mobility and thus making irons stop involving in continuous catalysis. Remarkably, three sharp peaks ascribed to  $\text{Fe}_2\text{P}$  (JCPDS no. 76-0089) can be clearly seen at  $2\theta$  of 40.2°, 44.1°, and 47.1° as well as two identical peaks with relatively low intensity at around  $2\theta = 52.8^\circ$  and  $54^\circ$ , which stand for the peaks of (111), (201), (210), (002), and (300) crystal planes respectively. From the above discussion, a fact can be confirmed here, namely iron phosphide and cementite can coexist in one substrate.<sup>24</sup> Specially, in the case of PAC-0, it is noteworthy to mention that there are two distinctive peaks

located at  $2\theta = 40.9^\circ$ ,  $42.8^\circ$ , which are indicative of the presence of  $\text{Fe}_3\text{P}$  (JCPDS no. 89-2712). However, the composition of  $\text{Fe}_3\text{P}$  disappeared in the rest of heated samples, which were treated by RF nitrogen plasma prior to pyrolysis. The change of surface activity of the raw AC may be responsible for this phenomenon. The detailed surface chemistry would be discussed in Section 3.3. Also, it may further imply that more irons were involved in the catalytic reaction after pretreating the raw AC.<sup>25</sup> Moreover, the formation of iron and phosphorus compounds was due to the phosphorus contamination from the raw AC, which was activated by phosphoric acid. Fortunately, the structural defects of carbon skeleton caused by the initial combination of iron and phosphorus would be improved when the graphitic structure was formed at the final temperature of 1000 °C, at which the iron and phosphorus compounds had synthesized simultaneously.<sup>26</sup>

In particular, the broad diffraction peaks of all samples that appear at  $2\theta$  angles of  $26^\circ$ , which are corresponding to the (002) reflections of graphite.<sup>27</sup> However, these peaks are weak and not prominent, which may result from the background of amorphous phase covering their reflections up.<sup>28</sup> As a matter of fact, there truly exist some graphitized carbons stacking on amorphous carbon matrix. Meanwhile, the shrink of band width between  $20^\circ$  and  $30^\circ$  with different modification conditions indicates the weakening of amorphous state, which probably implies that graphitic regions are progressively expanded for the samples of PAC-2, PAC-6 and PAC-10 through iron-catalyzed graphitization after modification of their corresponding precursors.<sup>29</sup> For precisely confirming the above argument, the interlayer spacing ( $d_{002}$ ) and the average crystallite size ( $L_c$ ) of (002) facet were measured and presented in Table 1, despite there being unavoidable errors in terms of such wide peaks.<sup>27</sup>

It is worth noting that the values of  $d_{002}$  and  $L_c$  for three pretreated samples are decreased as compare to the unpretreated sample, which demonstrates the (002) peak position is gradually close to the typical graphite phase,<sup>30</sup> albeit with turbostratic carbon domination.

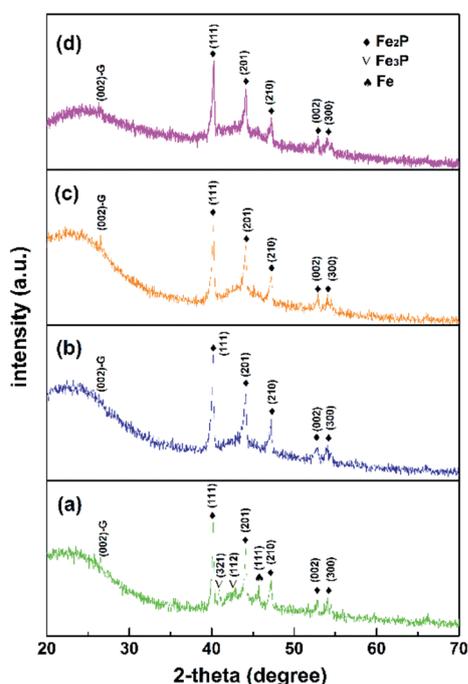


Fig. 2 X-ray diffraction patterns of (a) PAC-0 (b) PAC-2 (c) PAC-6 and (d) PAC-10.

Table 1 Interlayer spacing ( $d_{002}$ ), crystallite size ( $L_c$ ) of different carbon materials

Sample	$d_{002}$ (Å)	$L_c$ (nm)
PAC-0	3.4577	1.7
PAC-2	3.3801	2.0
PAC-6	3.3756	2.3
PAC-10	3.3570	2.4



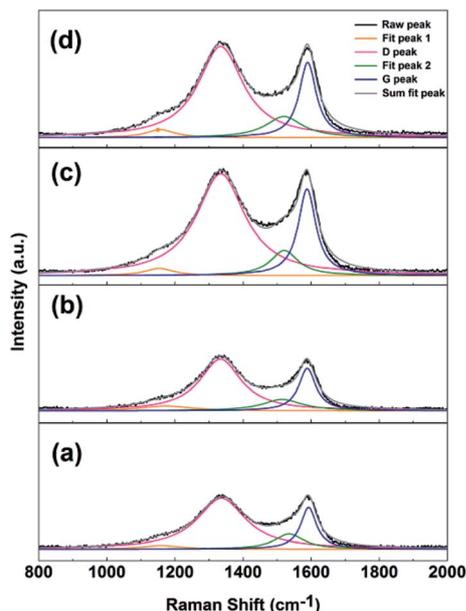


Fig. 3 Raman spectra of (a) PAC-0 (b) PAC-2 (c) PAC-6 and (d) PAC-10.

Raman spectroscopy was employed to further evaluate the ordered degree of structure for all samples. Shown in Fig. 3 is Raman images of PAC-0, PAC-2, PAC-6 and PAC-10 from bottom to top, the deconvolutions of spectras were performed by origin software with Lorentzian curve-fitting procedure. It can be seen that the Raman spectrums of carbon materials are decomposed into four first-order bands and each band represents a form of vibratory mode.<sup>31</sup> There are two well-resolved bands observed in the position of  $1334\text{ cm}^{-1}$  and  $1588\text{ cm}^{-1}$  separately, where two peaks are generally called D band and G band respectively.<sup>32</sup> The D-peak is related to the defective and disordered structure attributed to  $A_{1g}$  mode of  $sp^3$ -hybridized carbon atoms in a cubic lattice, and the G-peak is assigned to  $E_{2g}$  mode of  $sp^2$ -bonded carbon atoms in two-dimensional graphite sheets with the C-C stretching vibrations.<sup>33</sup> However, the G peak of PAC-0 apparently shifts to a position with the higher wavenumber, resulting from small crystallites with little three-dimensional order.<sup>9</sup> In addition, one band at around  $1150\text{ cm}^{-1}$  refers to a region with alicyclics and aliphatic chains of  $\gamma$  (C=C), while the other at  $1516\text{ cm}^{-1}$  is regarded as amorphous carbons with a singly broad and asymmetrical band.<sup>34</sup>

Table 2 Raman spectroscopic parameters obtained by fitting the experimental spectra

Sample	Peak position ( $\text{cm}^{-1}$ )		FWHM ( $\text{cm}^{-1}$ )		$R = A_D/A_G$	$L_a$ (nm)
	D-band	G-band	D-band	G-band		
PAC-0	1336	1592	174	56	3.76	5.11
PAC-2	1334	1587	172	63	3.24	5.93
PAC-6	1334	1588	161	61	3.19	6.03
PAC-10	1334	1589	147	60	2.96	6.49

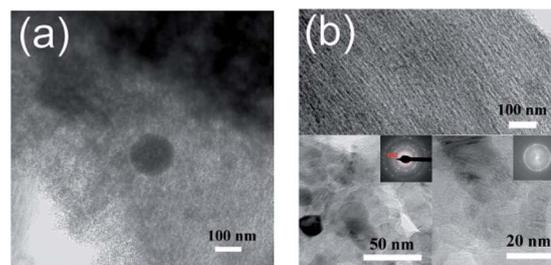


Fig. 4 TEM images of samples (a) PAC-0 and (b) PAC-10.

In the following, a quantitative discussion based on the full widths at half maximum (FWHM) as well as the integral area of the D-peak and the G-peak were summarized in Table 2. Firstly, the integrated area ratio  $R$  ( $R = A_D/A_G$ ) of the D-peak and the G-peak was determined, the smaller the ratio  $R$ , the higher degree of crystallinity.<sup>30</sup> It can be found that the  $R$  value of PAC-0 is greater than the remaining three specimens, which is consistent with the evolution of the ( $d_{002}$ ) interlayer distance. It seems to suggest that nitrogen functional groups may promote the deposition of ferric iron on the raw AC, thereby making iron can play pivotal catalytic effect. At the same time, by comparing the  $R$  values of PAC-2, PAC-6 and PAC-10, it reflects that the calculated data tends to diminish as processing time increased, which evidences that the crystalline of post-calcination samples is increased overall. Secondly, the FWHM is a useful index,<sup>35</sup> the lattice defects of three pretreated samples are reduced when compared with the FWHM-D of PAC-0. Among the three treated samples, the FWHM-D of PAC-10 narrows from  $172$  to  $147\text{ cm}^{-1}$ , which suggests that the crystallite sizes of the disordered carbon become very small.<sup>9</sup> Moreover, the difference of FWHM-G is not obvious. It might be concluded that the RF nitrogen plasma pretreatment is conducive to a wide distribution for ferric ions loading on the raw AC, and thus leading to an improvement in carbon framework during iron-catalyzed graphitization. Finally, according to the documentation, the in-plane crystallite sizes  $L_a$  can be determined as following eqn (1):<sup>36</sup>

$$L_a = (2.4 \times 10^{-10}) \lambda_1^4 R^{-1} \quad (1)$$

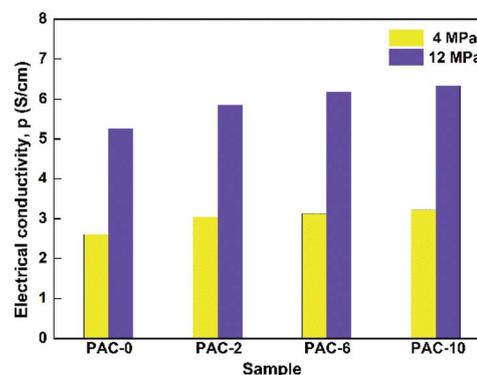


Fig. 5 Electrical conductivity of PAC-0, PAC-2, PAC-6, and PAC-10 under two pressure conditions.



where  $\lambda_1$  is the laser line wavelength ( $\lambda_1 = 532$  nm). Through the calculated  $L_a$ , it can be noticed that even under a same heating temperature of 1000 °C, the size of crystalline growth is different. It may imply that the nitrogen plasma pretreatment can stimulate the fusion of ferric irons and the raw AC, thus further boosting the coalescence of adjacent crystallites along the  $a$ -axis during the final pyrolysis.<sup>37</sup>

According to the XRD and Raman analysis, we applied the TEM technique to directly visualize more detailed structure feature. The PAC-0 and PAC-10 are taken into account and their micrographs are displayed in Fig. 4. For the PAC-0, it basically shows an amorphous orientation state and non-crystalline carbon grains, which are mirrored in the XRD and Raman profiles. In view of the above facts appearing in this sample, it is most likely that the sample lacks adequate intermetallic phase to “etch” into the solid carbon crystallites for inducing their ordered arrangement during the heat treatment.<sup>2</sup> The reason for the absence of iron carbides might be attributed to the content and activity of iron. In the case of PAC-10, with the evolution of carbon crystallite, we investigated its microstructure under three different magnifications. Firstly, as can be seen on the top of Fig. 4b, the pore walls run in parallel arrays, which indicate the presence of lamellar structure.<sup>25</sup> Moreover, for roughly understanding how the iron metal compounds distributing over the material, a selected higher resolution area with an Electron Diffraction (ED) patterns are shown on the bottom left of Fig. 4b, it can be observed that iron-containing compounds disperse uniformly in black while carbon substrates remain in grey. Also, a well-defined diffraction ring corresponding to the (002) plane and the rest crystals were detected by ED patter. This finding strengthens the validity of XRD. Finally, in the enlarged view with a scale of 20 nm, it can be seen in the bulk of this area, the lattice fringes are generated and centered at the metal compounds of  $\text{Fe}_2\text{P}$ , which can be explained by the mechanism of dissolution and re-precipitation of cementite.<sup>38</sup> By comparing the TEM images of PAC-0 and PAC-10, an objective judgement can be made that the pretreated AC precursor is easier to be catalyzed to form graphitic nanostructures.

### 3.2 Analysis of electrical conductivity

The intrinsic electrical conductivity of carbon powders themselves is an essential parameter when it comes to the selection and application of electrode material. Also, the nature of electron transport is proportional to the degree of crystalline order in carbon material.<sup>39</sup> As is shown in Fig. 5, the values of electrical conductivity exhibit certain regularity with respect to precursors whether being treated or not. With the prolongation of pretreatment time, the obtained value tends to rise step by step. This indirectly verifies that the crystalline volume fraction has been enlarged through pretreating the raw AC prior to pyrolysis. Especially, in the case of PAC-10, when setting test pressure at 12 MPa, it was determined as  $6.23 \text{ S cm}^{-1}$ , which was superior to the  $\text{Fe}_3\text{O}_4$ /carbon composite nanofibers and Fe-N-doped carbon capsules.<sup>13,40</sup> when compared with the blank sample, the electrical conductivity of PAC-10 raised by 23.8%

and 20.3% at test pressures of 4 MPa and 12 MPa separately. At the same time, the reason why the electrical conductivity of same sample varied with the given pressure is linked with their compaction degree. Notably, the results of conductivity are in good accordance with the above structure characterizations of XRD, Raman and TEM.

### 3.3 Analysis of reactions during plasma treatment and iron(III) loading

Based on the above comprehensive analysis, it had been demonstrated by XRD, Raman, TEM and electrical conductivity that the raw AC with and without pretreatment would have some impact on their subsequent graphitization during the heat treatment. Herein, in order to elucidate the reason why there exists difference on the structure and electrical conductivity for four post-annealed samples, two types of characterization techniques were applied to investigate the blank and the pretreated raw AC. Firstly, XPS measurements were employed to examine the chemical state of N 1s on the surface of raw AC. As is shown in Fig. 6a, the untreated raw AC is dominated by a single peak, which is associated with the amides. By contrast, the N 1s of pretreated raw AC was divided into three peaks by deconvolution and Gaussian curve fitting. These peaks belong to the pyridinic-N, amides and quaternary-N, respectively,<sup>41</sup> which suggest that nitrogen is indeed introduced on the raw AC surface by nitrogen plasma treatment. Furthermore, a quantitative study of nitrogen species based on the fraction of each integrated peak area was carried out and summarized in the Table 3. According to the concrete data, it can be evidently found that the added nitrogen is mainly present in the form of pyridinic-N and quaternary-N, which are the leading functional species on the surface. Their emergence might be owing to the nitrogenous radicals generated from nitrogen RF plasma etching the carbon fragments, such as substituting oxygen-containing species or incorporating into the aromatic rings to form pyridinic-N and quaternary-N, thus making the surface functional.<sup>18,42</sup>

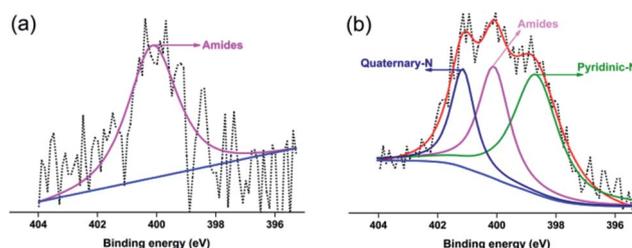


Fig. 6 N 1s XPS spectra for the raw AC of (a) PAC-0 and (b) PAC-10.

Table 3 Comparison of the surface groups' content of different N species for the blank and the pretreated sample

Sample	Total N (at%)	Pyridinic-N	Amides	Quaternary-N
PAC-0	0.39	—	0.39	—
PAC-10	1.07	0.51	0.35	0.21



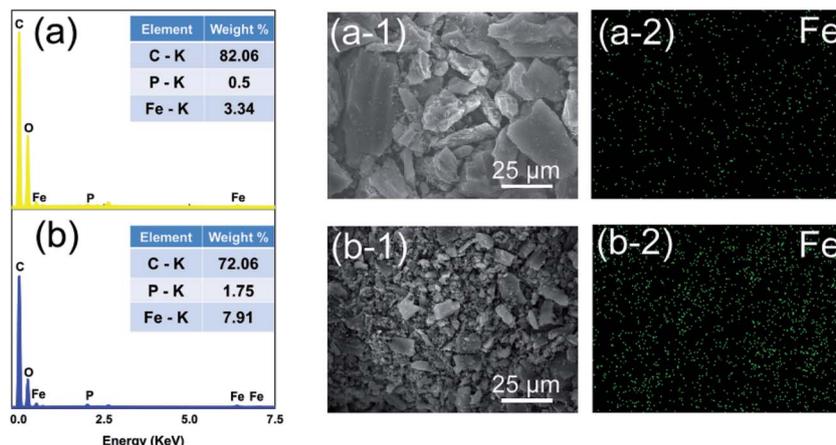


Fig. 7 EDX and Fe elements maps corresponding to the SEM images for the precursors of PAC-0 with (a), (a-1), (a-2) and PAC-10 with (b), (b-1), (b-2).

Most importantly, it is reported that nitrogen-containing groups generally have a stronger ability to adsorb metal ions as a function of coordination mechanism,<sup>43,44</sup> which can be explained that the pyridinic nitrogen provides richly active sites for holding ferric ions, while the existence of quaternary nitrogen raises the surface hydrophilicity and wettability of the raw AC.<sup>45</sup> Consequently, with the surface accessibility of pretreated AC being improved, it could be speculated that the binding sites between the ferric ions and carbon matrix was extremely increased when soaking the pretreated AC in  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  solution. Furthermore, for the sake of supporting the discussion of XPS section, EDX with Fe elemental mapping was performed to distinguish the difference regarding the adsorption capacity and dispersion of iron between pure AC and pretreated one. On one hand, by visually comparing Fig. 7(a-2) and (b-2), it can be observed that irons loading on the pretreated AC are more abundant and homogeneous than the blank sample. On the other hand, the EDX data supplies a definite proof to above phenomenon simultaneously.

To sum up, it can be conjectured that the content and distribution of iron on the raw AC affect the following catalytic graphitization, thus bringing about the structural difference for heated samples. Finally, these distinctions are embodied in the form of electrical conductivity.

## 4. Conclusions

In conclusion, the raw AC with and without pretreatment and then loading ferric ions were heated up to 1000 °C for fabricating distinguished carbon. Their structures and electronic conductivities were compared and the main results were as following. Firstly, all the pretreated samples were superior to the untreated in terms of the order degree of structure, with evidence of iron catalyst exhibiting a better bonding property on the raw AC surface after pretreating the carriers. Among all activated carbons being catalyzed, the PAC-10 presented a distinct lamellar structure, which was referred to quasi-graphitization, but the degree of graphitization was still low as a whole. Secondly, from the point

view of electrical conductivity, the electron transport rates had positive correlation with the pretreatment time of the raw AC. This implied that the crystalline arrangement tended to be well-ordered. Finally, we deduced that the content and the distribution of iron had effect on the catalytic graphitization of raw AC. It is therefore concluded that the nitrogen RF plasma treatment can be beneficial to enhancing the surface activity of AC, and thus has a positive effect on loading ferric ions, subsequently the degree of graphitization being affected in high temperature environment.

## Conflicts of interest

There are no conflicts to declare.

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