Formation of large-area stretchable 3D graphene–nickel particle foams and their sensor applications

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Stretchable sensors are essential and important for the new-type stretchable intelligent electronic devices. Three-dimensional (3D) graphene foams are attractive to increase the sensitivity and stretchability, benefiting from a high specific surface area and mechanical strength. Herein, 3D graphene/nickel particles (Gr–NiP) peaseed foams, which were fabricated using CVD and stamp-transfer processes, are proposed and used for stretchable sensor applications. The existing nickel particles, covered by graphene layers, are useful for the formation of 3D nanostructures and separated from each other for stretchable applications. A stretchability (ε) of such Gr–NiP foams of up to 80% can be achieved. A low limit of detection (<1%) and excellent linearity (R² = 0.997) are also present. Sunken ravines between the Ni particles provide favorable sites to grow Ag nanoflowers (AgNFs), which can enhance the electromagnetic coupling for SERS application. Such stretchable substrates can be used as ultrasensitive biosensors to detect the molecules on the surfaces of any shape.

1. Introduction

As new equipment, stretchable devices show good properties under larger and long-time mechanical stress conditions, which can be useful for use in human implantation devices, flexible portable devices, and wearable and wireless sensing devices. Stretchable sensors are essential components of the new-type stretchable intelligent electronic devices, such as the wearable health-monitoring patch, robotic sensory skin, and tele-surgery electronic glove. Stretchability and sensitivity are the primary elements of the stretchable sensors. Existing stretchable sensors based on bulky technologies involving metal and semiconductors are cheap but have a very limited stretchability. High stretchability (ε > 50%) is of compelling interest for emerging applications, such as human-friendly interactive electronics. For example, the movements of human joints can generate strains as high as 55% upon stretching and contracting.

Recently, nanoscale materials have been studied to fabricate stretchable devices. Carbonaceous materials, including carbon nanotubes (CNTs) and graphene, have drawn tremendous attention due to their advantages of flexibility, fast response, and high sensitivity. Compared with CNTs, graphene-based materials offer a better solution for preparing highly sensitive and stretchable sensors, benefiting from their plane periodic lattice structure, which can be used as an ideal surface support. Piezoresistive monolayer and few-layer graphene have been used for strain detection with a limited stretchability (<6%). Flexible and foldable graphene can also be wrinkled or rippled to produce 3D graphene films to prepare large-area stretchable graphene.

In order to further increase the sensitivity and conductivity of graphene-based sensors, 3D sponge-like graphene foam, which has a rich porous structure with a higher conductivity, specific surface area, and mechanical strength, has been reported. 3D graphene foams have been fabricated by growing graphene on copper or nickel foam substrate and then etching away the metal template. Such 3D graphene foam, which could be stretched to >100%, is attractive for stretchable devices and consequently has been studied by several researchers.

The porous nature of this 3D graphene foam, with a large specific surface area (up to 850 m² g⁻¹), is also suitable to make functional composites by filling the pores with nanoparticles, polymers, or other functional materials. In this study, 3D Gr–NiP nanostructures, composed of graphene and Ni particles, were proposed to fabricate stretchable sensors with a stretchability of 80%. The existing nickel particles, separated from each other and covered by graphene layers, are useful for the creation of 3D nanostructures by preventing a collapse of all the graphene foam onto the stretchable elastomer. A simple stamp-transfer process can be used to transfer such floating Gr–NiP foams.

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Sunken ravines between the Ni particles are also can be formed due to the etching processes and the presence of the Ni particles. This gives the possibility of both high stretchability and the favorable sites for the formation of 3D AgNFs by the use of in situ growth methods without any acute conditions (detailed in the methods section). This innovative method puts forward a new idea for the synthesis of 3D nanostructures. Such 3D metal nanostructures (nanospheres,24 nanostars,25 and nanoflowers26), which contain a special fine structure, large specific surface area, and larger size, can avoid the aggregation of the particles during application as SERS.26,34–36

The graphene base can effectively enhance the Raman signal and reduce the back action noise to allow the use as a graphene-SERS based biosensor.20,21,26 There are two key advantages of this system: (1) graphene is a favorable atomic surface test bed with a small-distance charge transfer between the graphene surface and the adsorbed molecules, which makes the Raman signal more reliable and efficient;20 (2) graphene with a large specific surface area of 2630 m² g⁻¹ can also work as a molecule enricher in SERS-active substrates, which can act as excellent adsorbsents toward organic molecules, particularly aromatic molecules.21

It is also well known that more efficient SERS effects can be yielded by 3D SERS substrates compared with planar substrates. The larger surface area improves the target molecule adsorption and pathway for light propagation. Denser “hot spots” can also be obtained by fabrication of 3D metal nanostructures, which are attractive areas for researchers recently. Jones reported that the SERS enhancement factor for 3D “hot spot”-based substrates is more than two orders of magnitude greater than that for two-dimensional (2D) substrates.26 Ultrasonic SERS performance in 3D “sunflower-like” nanoarrays decorated with Ag nanoparticles26 was also reported by Zhang et al. In our experiment, the obtained 3D AgNFs on graphene foams were used as SERS “hot spots” to improve the sensitivity of the stretchable biosensors.

2. Results and discussion

The three main stages (G/Ni foam formation, flexible Gr–NiP foam formation, stamp-transfer process) to form the stretchable Gr–NiP foam are illustrated in Fig. 1. Chemical vapor deposition (CVD) was used to precipitate carbon atoms on the nickel foam to fabricate the G/Ni foam at 1050 °C. An FeCl₃ and HF mixed solution was used to etch different amounts of metal nickel away by adjusting the immersion time to form the flexible Gr–NiP foam. Stamp-transfer, a simple, convenient, and highly efficient method, is proposed here to transfer such a Gr–NiP foam onto the elastomer substrate. After natural drying, the flexible and stretchable Gr–NiP foam, comprising a continuous and interconnected graphene 3D network wrapped around Ni nanoparticles, was obtained.

Graphene layers, which are controlled by the growth time of the CVD deposition, are crucial for the formation of flexible Gr–NiP peasecod foams. When the number of graphene layers is less than three (growth time was shortened than 15 min), all of the metal nickel materials are easily etched away, and the resulting as-prepared graphene foam is so thin and light that it collapses and is suspended in the FeCl₃ and HF mixed solution. The suspended graphene foam cannot be transferred by our proposed stamp-transfer processes due to the fact that the elastomer film cannot touch the suspended materials. On the other hand, when the number of graphene layers is more than 15 (growth time extended to 90 min), the obtained graphene foam is over-thick to prevent the intimal metallic Ni from dissolving, and hence the formed Gr–NiP foam is rigid, even though long-time etching has been carried out, which makes it unsuitable for flexible and stretchable devices. In our experiment, stretchable Gr–NiP foam could be formed with 6 to 10-layered graphene (shown in Fig. 2), obtained by 45 min CVD deposition.

The stamp-transfer method (shown in Fig. 1), which is appropriate for flexible, light, flimsy, and gummy elastomer substrates, is innovatively suggested here. The gummy elastomer substrate (3M4910 VHB), which was affixed to the edge of a plastic culture dish, is coated quickly and horizontally onto the floating flexible Gr–NiP foam for 10 s and then uplifted slowly at an oblique angle. By virtue of this transfer method, the as-prepared flexible Gr–NiP foam was attached on the elastomer substrates by the gummy of the elastomer and by the van der Waals interactions of Gr–NiP and the elastomer. Essentially, the stamp-transfer processes can also be used on other substrates (such as Si wafer, glass) without viscosity.

It is critical to investigate the morphology and crystallization of the Gr–NiP foam for understanding its electrical and mechanical properties. Scanning electron microscopy (SEM, Zeiss Gemini Ultra-55) was used for the morphology characterization of such a Gr–NiP foam. Compared to that of the G/Ni foam (Fig. 2a), the graphene skeleton of the Gr–NiP foam (Fig. 2b) was oblate and the space between the layers decreased drastically. The frame structure of the foam possesses an irregular rectangle structure instead of the hexagonal structure, and a surface structure with more ridges was detected on the stretchable Gr–NiP foam. These ridges surfaces and shape changes of the frame structure, combined with the self-constricted structures, make the Gr–NiP foam suitable for flexible and stretchable sensors. Moreover, the fabricated Gr–NiP foam still maintains a monolith of a 3D network, providing a channel for charge carriers to move rapidly through the high-quality and continuous building blocks with low resistance. Therefore, extraordinary electrical and mechanical properties of Gr–NiP foam were expected.

Fig. 1 Schematic of the stretchable Gr–NiP foam fabrication.
Because the graphene layers were synthesized on the surface of the metallic Ni, most of the Ni particles are covered by the graphene layer. The TEM images of the obtained Gr–NiP foams are presented in Fig. 2c and d, which prove the existence of multilayer graphene (3 nm, ~10 layers) and Ni nanoparticles. As shown in Fig. 2c, the black areas represent the Ni particles aggregation bodies, which are covered by the graphene layers. The inset exhibits the TEM image under high magnification, in which there are still a mass of Ni particles scattered in the relative gray areas.

To investigate the electromechanical response of such a Gr–NiP foam, both ends of the as-prepared stretchable Gr–NiP foam were immobilized on a motorized moving controller, as shown in Fig. 3. Different strain/release cycles were carried out by virtue of the different strain levels and frequencies, while the resistance changes were measured using a Keithley 4200 device. Owing to the strong adhesive strength of the gummy acrylic acid substrates, the adhesion between the foams and the substrate was very strong, and the graphene foams follow the deformation of the stretched acrylic acid substrate. When the elastomer film was uniaxially or biaxially stretched and relaxed over multiple cycles (more than 1000 cycles in our experiment), the Gr–NiP foam still maintained its integrity and a perfect electromechanical performance, which can be attributed to its flexibility and high fracture toughness.

In order to investigate the influence of the size and number of Ni particles on the electrical resistance response of the Gr–NiP-based sensors, typical curves of the normalized resistance changes as a function of applied strain for the Gr–NiP-based sensors with different Ni element densities controlled by different etching time were obtained and are shown in Fig. 4. The normalized relative resistances of the Gr–NiP-based sensors all increased upon the application of strain. The change in the electrical conductance is the main reason for the Gr–NiP foam-based sensor to act as a type of resistance-strain sensor. Upon stretching, the graphene foam was elongated, such that some Ni particles may become separated within the graphene foam, which represents the reason for the electrical conductance reduction. Interestingly, the sensitivity, linearity, and stretchability of the strain sensors could be tuned by adjusting the etching time of the G/Ni foam.

Due to the gradual reduction of embedded Ni metal and the surface roughness of the gummy acrylic acid substrates, the stretchability of Gr–NiP increased gradually with an increase in the etching time. Fig. 4a shows the normalized relative resistance changes of Gr–NiP foams for 15 min etching time under different applied strains. Because relatively more Ni particles existed in the Gr–NiP foam undergoing 15 min etching, a failure strain of <50% and a relatively weak linearity ($R^2$) of 0.848 were obtained. When the etching time was increased from 15 min to 30 min, as shown in Fig. 4b and the inset of Fig. 4b, it exhibited excellent linear electromechanical performance in 0–80%, and a stretchability ($\varepsilon$) of up to 120% was achieved. Moreover, in the stretchability range of 80–120%, the Gr–NiP peasecod foam-based strain sensors still showed an excellent linear performance. As a demarcation point, when the foam substrate was stretched beyond 80%, the Gr–NiP peasecod foams transform from “homogeneous foam” to “inhomogeneous foam” with emerging bottleneck locations that critically limited the electrical current, which led to serious nonlinearity in the entire stretchability range.

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**Fig. 2** SEM images of G/Ni foam (a) and Gr–NiP foam (b) with 45 min etching (inset is the photo of the corresponding G/Ni foam and Gr–NiP foam samples). (c) TEM image of Gr–NiP foams (inset: the TEM image at a higher magnification). (d) HRTEM image of the 10-layered graphene.
The limit of detection (LOD) of strain sensors is important to the development of effective ultra-low and subtle-strain sensors. A low LOD means that a subtle applied strain is able to arouse large normalized resistance change. With the etching time further increasing from 30 min to 45 min, as shown in Fig. 4c, Gr-NiP foams with a very low limit of detection were also present and the strain sensors responded to the applied strain with excellent linearity ($R^2 = 0.997$) for the range from 0% to

![Fig. 3 Photographs of the strain sensor before (a) and after stretching of (b) $\varepsilon = 50\%$, (c) $\varepsilon = 100\%$, (d) $\varepsilon = 150\%$.](image)

![Fig. 4 Typical curves of the normalized resistance changes as a function of applied strain for the Gr-NiP-based sensors with different Ni element densities controlled by different etching times: (a) 15 min, (b) 30 min, (c) 45 min, (d) 60 min.](image)
80%. Amazingly, as shown in the inset of Fig. 4c, the Gr–NiP foams showed outstanding stretchability, which increased from 120% to 160%, showing a 40% improvement. In particular, in a quite wide range of strains (from 0% to 160%), the linearity of the strain sensors just showed a negligible change, decreasing from 0.997 to 0.980.

As can be seen in Fig. 4d, when the etching time was further increased from 45 min to 60 min, because all or almost all the Ni skeleton was etched away, which leads to collapse of the 3D foam structure, the stretchability and linearity of the sample all declined.

The sensing ability of Gr–NiP foam was further investigated and is shown in Fig. 5. Fig. 5a depicts the relative resistance responses of stretching-releasing cycles of Gr–NiP foams undergoing 45 min etching under various applied strains. In the multiple stretching-releasing cycles loaded with different strains, the response signal still remained at a stable performance despite the return occurring in the stretching processes under large tensile stress loading. In addition, the recoverability of the Gr–NiP-based strain sensors was investigated. As shown in Fig. 5b, the stretching and releasing curves showed nearly reversible behavior, and hysteresis was negligible. Negligible hysteresis at lower applied strains ($\varepsilon \leq 10\%$) arises from strong interfacial binding between nanomaterials and elastic polymers.40-46

Durability and stability are extremely critical for the practical application of strain sensors. Electrical responses of the strain sensors based on Gr–NiP foams exhibited good stability with 50% strain at frequencies ranging from 1 to 5 Hz (Fig. 5c). The variations of the relative resistance signals were almost the same as the increase in frequency. The response of the strain sensors to cyclic loading from 0 to 10% strain for more than 100 cycles with good stability and reproducibility is illustrated in Fig. 5d, which could be attributed to strong adhesion between Gr–NiP foams and acrylic acid substrates.

Applications of the graphene-based biosensor (such as G-SERS) have drawn a tremendous amount of attention recently due to their flexibility, chemical absorption, and the reduction of the back action noise.47,48 To improve the performance of graphene toward high sensitive SERS applications, recent studies have focused on the hybrid nanostructures combined with metal nanostructure.48,49 Herein, we found that 3D AgNFs could be easily synthesized on such Gr–NiP foam to use as a stretchable graphene-SERS based biosensor.

The as-prepared AgNFs, synthesized under the molar ratio of ascorbic acid (AA) to Ag⁺ of 0.5, were large scale and uniform with spherical structures in a high yield (shown in Fig. 6a). Such closely arranged AgNFs were quasi-spherical, consisting of a solid core with a large amount of small, ellipsoidal surface protuberances. The average overall dimension of these quasi-
R6G as well as the linear a 3D-oriented attachment, began to act as the sites for further Ag precipitation. Following of the Ni skeleton, the skeleton of Gr substrates with a smooth graphene skeleton, due to the etching able sites for the deposition and aggregation of Sn+.A layers are closer and even stick together, which provide favor-
kles, imperfections, and edges. Moreover, adjacent skeleton appeared to collapse to some extent, causing numerous wrin-

tions of the MB with a good linear relationship ($R^2 = 0.971$, $0.902$, and $0.905$, respectively). The intensities of the SERS spectra of R6G are proportional to the logarithm of the concentrations of the R6G. The good line correlation indicates a great potential application of such a stretchable foam to detect analytes in real biological systems. Fig. 7c exhibits the SERS spectra of $10^{-6}$ M R6G adsorbed on the four randomly chosen AgNFs aggregates. The detected Raman peaks show similar SERS responses, which indicate a high reproducibility.58–54

The hybrid substrate exhibited excellent SERS properties and malleability, which could be bent back and forth without any breakdown. To demonstrate the wide suitability of SERS substrates under different states, such as tension and bending, we further studied the SERS performance of AgNF-decorated Gr–NiP foam in the state of stretching by applying different stretching forces to it. Fig. 7d shows the SERS performance of such substrates under stretching. The SERS performance was consistent when undergoing different deformation, indicating that such substrates can be used as cut-and-paste SERS substrates to cover the surface of arbitrary configurations for highly sensitive in situ detection.

To further investigate the practical application of the AgNF-decorated Gr–NiP foams as stretchable biosensors, a type of food additive was examined. Methylene blue (MB), an aromatic heterocyclic compound, is often illegally added into water bodies to increase the fish livability in the process of fish breeding by some vendors.52 Fish tidlers were immersed in the new-prepared MB solution with different concentrations from 0.01 mM to 10 nM for half an hour and then covered by the stretchable AgNF-decorated Gr–NiP substrate to directly absorb MB solution from the fish surface. The collected SERS spectra of MB are demonstrated in Fig. 8a. Several vibrational peaks located at about 449, 505, 678, 1036, 1072, 1387, 1440 and 1622 cm$^{-1}$ can be observed, which belong to MB according to the normal Raman spectrum of MB powder. The lowest detected concentration of MB was 10 nM in our experiment. This fact indicates that the stretchable biosensor possessed excellent adsorption abilities and SERS properties. To prove the capability of the stretchable substrate products in the quantitative detection of MB, the linear fit calibration curve is illustrated in Fig. 8b. The intensities of the SERS spectra of MB at 678 and 1440 cm$^{-1}$ are proportional to the logarithm of the concentrations of the MB with a good linear relationship ($R^2 = 0.9$, 0.88 respectively) ranging from 0.01 mM to 10 nM.
COMSOL simulation based on such AgNFs and Ag hemispheres is shown in Fig. 9, where the size of the AgNFs was settled according to the actual shape, as shown in Fig. 6. The electromagnetic enhancement (EM) is well known as the main mechanism of SERS for metallic nanostructures (such as AgNPs). Local surface plasmon resonances (LSPRs) existing in the gaps between the metal particles enhance the local electric field near the metallic nanostructure significantly, which produces an enhancement highly localized to the metal surface. Fig. 9a and b show the y–z views of the electric field distribution on the AgNFs and Ag hemisphere by a plane wave of 532 nm. It can be seen clearly that, compared with that of a smooth Ag hemisphere, more and denser hotspots are widely spread across the surface of AgNFs, and the local electric field of the incident light is magnified strongly. Fig. 9c–f show the x–y views of the electric field distribution on the AgNFs at different heights ($h = 0, 90, 100, 110$ nm), respectively. A large number of strong and high-density hotspots are scattered across the entire surface of the AgNFs, which is well consistent with the SERS experimental results. Based on the theoretical results, the 3D AgNF-decorated
Gr–NiP substrate is a truly outstanding candidate for a higher sensitivity stretchable SERS substrate.

3. Conclusion

Novel and high-performance stretchable sensors based on the new 3D Gr–NiP are proposed by virtue of an imaginative stamp-transfer process. By controlling the thickness of the graphene layers and by optimizing the etching time, such a strain sensor exhibited perfect sensitivity, stretchability, a low limit of detection, and excellent linearity. AgNFs, profiting from the sunken ravines, could be easily synthesized on such a Gr–NiP substrate to form a stretchable SERS substrate. The combined advantages of electromagnetic enhancement from the AgNFs and the chemical absorption of graphene could be used to obtain an ultrasensitive biosensor to detect molecules on the surfaces of any shape.

4. Experimental

Flexible Gr–NiP peasecod foam formation

To fabricate the G/Ni foam, a scaffold of porous nickel foam was used as a template for the deposition of carbon atoms. The large-area multilayer graphene was grown by CVD technology as described in previous work. Briefly, after the pressure of a quartz tube was pumped to under $10^{-3}$ Pa by a double-pump system, H$_2$ with the flow of 50 sccm was piped into the tube to remove the remaining nickel oxide when the temperature reached 300 °C. The growth process of graphene was carried out at 1050 °C with a mixed flow of H$_2$ (50 sccm) and CH$_4$ (50 sccm). The nickel scaffold was then partly removed using chemical etching by a hot HCl (or FeCl$_3$) solution. Ferric chloride (FeCl$_3$) and hydrochloric acid (HCl) were purchased from the Shanghai Chemical Reagent Company.

Characterization of the stretchable Gr–NiP foam strain sensors

Both ends of the as-prepared stretchable Gr–NiP foam were immobilized on a motorized moving controller to investigate the electromechanical performance of the Gr–NiP foams, as shown in Fig. 3. The Keithley 4200 instrument was used to measure the resistance changes of Gr–NiP foam when the tensile strain of different strain levels and frequencies was applied.

AgNF-decorated Gr–NiP foam formation

Silver nitrate (AgNO$_3$) and l-ascorbic acid were purchased from the Shanghai Chemical Reagent Company. In order to further explore the application of the Gr–NiP peasecod foams as biosensors, silver microspheres were formed on the sunken ravines of graphene branches, which required two steps, including silver seed deposition and the in situ growth of silver nanostructures. Silver seeds were immobilized inside Gr–NiP peasecod foams by electroless deposition. The Gr–NiP peasecod foam was immersed in an acidic aqueous solution of SnCl$_2$ (0.1 M) and H$_2$O$_2$ (0.1 M).
by immersing in the mixed solution of AgNO₃ and ascorbic acid out. The AgNF-decorated Gr
Local electric
distributions of silver seed on the surface of Gr–NiP peasecod foam, which was necessary for the final in situ growth of silver nanostructures. Subsequently, the in situ growth of silver seeds on the Gr–NiP peasecod foam substrate was carried out. The AgNF-decorated Gr–NiP peasecod foam was obtained by immersing in the mixed solution of AgNO₃ and ascorbic acid for 2 min growth.

Characterization of AgNF-decorated Gr–NiP foam biosensors
To elucidate the nanostructured morphologies, we conducted scanning electron microscopy (SEM, Zeiss Gemini Ultra-55) detection to show the size and degree of aggregation of the Ag. The Raman instrument used in this study was Horiba HR Evolution 800 with excitation by an Ar laser (532 nm). The laser beam was focused on a sample of about 1 µm in size. For each sample, the SERS spectra on display were the average values of the spectra of three different positions of the substrate.

Theoretical modeling
Local electric field properties of the proposed 3D AgNFs were obtained using the finite element method (commercial COMSOL software) to analyze and clarify the enhancement mechanisms of SERS. A plane wave (532 nm) was irradiated down to the AgNFs in the z direction. The electric field was parallel to the x direction. For simplicity, a series of Ag ellipsoids, with the radius of 10 nm and 30 nm, respectively, were designed on a 200 nm-diameter hemisphere to study the underlying physics of the proposed structure. The refractive index of the Ag was ε = −12.373 + i0.40392.

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