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## Rapid spray-crosslinked assembly of a stable high-performance polyelectrolyte bipolar membrane

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Bipolar membrane processes have evolved as one of the most promising technologies in the field of acid and base production as well as many interesting separation applications. Herein, we report a rapid spray-crosslinked assembly for fabricating a high-performance polyelectrolyte bipolar membrane. Polyvinyl alcohol (PVA), glutaric dialdehyde (GA) and polyethylenimine (PEI) are alternatively and successively sprayed onto a supporting cation-exchange membrane. GA crosslinked PVA and PEI are responsible for the interlayer and anion-exchange layer, respectively. Under optimal conditions, at a current density of  $100 \text{ mA cm}^{-2}$ , the cell voltage of the BPM was as low as 1.79 V. Moreover, it has been demonstrated that the spray crosslinked membrane has good stability in acid and alkali harsh conditions. In contrast to the traditional casting method, spray assembly combined with chemical cross-linking can tune the membrane thickness at the nanoscale and microscale levels, as well as increase its charge density and ion-exchange capacity. This facile approach might open a new way to efficiently and flexibly produce various bipolar membranes with different polyelectrolytes.

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## 1. Introduction

Bipolar membranes (BPMs) are special layered ion-exchange composite membranes consisting of a cation-exchange membrane (CM) layer, an anion-exchange (AM) membrane layer, and an interlayer between them. In a direct electric field, water at the interlayer of a BPM can be split into hydroxide ions and protons, which can transfer to both sides of the membrane.<sup>1,2</sup> Making use of the feather, BPM and other AMs and CMs can be used in combination in electrodialysis, which is widely applied in acid and alkali production, pollutant control, and resource recovery, as well as in marine, chemical, food, and pharmaceutical industries.<sup>3–7</sup> Protons and hydroxide ions in the interlayers of the anion- and cation-exchanger layers of a BPM can migrate to the solution. A BPM must possess high rates of water dissociation, high permselectivity, and good mechanical stability.<sup>8,9</sup> Membrane materials that are most commonly used in studies on BPMs are polystyrene, fluoropolymers, and poly(2,6-dimethyl-1,4-phenylene oxide).<sup>10,11</sup> The anion- and cation-exchange layers of the BPM are modified or a medium that promotes water dissociation is added between the layers in order to improve and enhance its overall performance.<sup>12</sup> Polyelectrolytes, a kind of water-soluble polymeric material that can ionize into polyions and counterions, can be used as

membranes materials for the anion- and cation-exchange layers of BPMs.<sup>13</sup>

Currently, most of the BPMs are normally produced by direct adhering of commercial anion- and cation-exchange membranes together with hot-pressure and casting a cation (or an anion) exchange membrane onto the oppositely charged (anion or cation) membrane.<sup>14,15</sup> This process generally includes polymer dissolution, casting/coating onto substrate, solvent volatilization and post-crosslinking, which is a relatively complicate, time-consuming and highly inefficient.<sup>16</sup> More importantly, it is difficult to tune the intermediate layer on the nanometer scale. Therefore, the reported intermediate layer is relatively thick at the micrometer scale.<sup>17–19</sup> In recent years, spray assembly has attracted considerable attention in the field of membrane preparation, because it offers the advantages of mild membrane-forming conditions, controllability of thickness within nanometer scale. For example, Zhang<sup>20</sup> had reported that the simultaneous spray self-assembly for the fabrication of a well-dispersed ZIF-8-PDMS nanohybrid membrane with an extremely high loading. It was demonstrated that the thickness in this study was far thinner than that of other reported butanol-permselective composite membranes.<sup>21</sup> More recently, they also proposed to construct a super hydrophilic water uptake layer by spray-assisted biomimetic mineralization of calcium carbonate ( $\text{CaCO}_3$ ) onto a (poly(acrylic acid)/poly(ethylenimine))<sub>n</sub>/polyacrylonitrile ((PAA/PEI)<sub>n</sub>/PAN) membrane.<sup>22</sup> This work suggested that rapid spray strategy could not only tune the thickness but also could facilely tune the membrane surface morphology and wettability. However,

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these works particularly focused on the alcohol permselective membrane, none of work have dealt with the BPM using spray assembly.

In the present work, we proposed a rapid spray assembly coupled with chemical crosslinking to prepare a stable high-performance polyelectrolyte bipolar membrane. This technique was based on the ionization properties of the polyelectrolyte and the advantages of spraying assembly. In order to improve ion migration rate, promote water splitting, lower the IR drop, polyethyleneimine (PEI) was used to form the AM because PEI was a primary amine produced by polymerization of ethylene imine, branched polymer secondary and tertiary amines, in water to form a polycation, preparation of anion exchange membrane bipolar membrane layer materials was very good.<sup>23</sup> Hydrophilic polyvinyl alcohol (PVA) as the interlayer because of its highly hydrophilic,<sup>24</sup> and commercial CM as cation-exchange layer, PVA, glutaricdialdehyde (GA) (crosslinkers), a high-performance BPM could be rapidly fabricated. In this case, spraying glutaricdialdehyde between PVA and PEI can crosslink both PEI and PVA, which made the resulting bipolar membrane much more stable. The spray-crosslinked membranes were intensively characterized by scanning electron microscopy (SEM), Fourier-transform infrared (FTIR) spectroscopy, and thermo gravimetric analysis (TGA). The membranes were frozen in liquid nitrogen, broken, and then sputtered with gold before SEM analysis. The influences of assembly conditions on water-dissociation voltage were also investigated.

## 2. Experimental

### 2.1 Materials

The cation-exchange membrane (CM-ZHJ) were obtained from Hangzhou Grion Environmental Technology Co., Ltd. Zhejiang, China. The CM-ZHJ with strongly acid groups,  $R-SO_3^-$  were provided by Hangzhou Grion Environmental Technology Co., Ltd. The cation-exchange membrane had thickness 0.42 mm, water content 40–55%, exchange capacity 2.0 mol kg<sup>-1</sup>, area resistance 11  $\Omega$  cm<sup>-2</sup>, and selective penetration 93%. Respectively, PEI (50% aqueous solution) and PVA (PVA-1799) were purchased from Aladdin Corporation Ltd. Shanghai, China. Sodium sulfate, sodium chloride, sodium hydroxide, hydrochloric acid all of analytical grade were from Beijing Chemical Works, Beijing China. GA (GA, 25%) was purchased from Tianjin Fu chen Chemical Reagents Factory, Tianjin China. Nafion membranes was bought from DuPont Corporation.

### 2.2 Spray assembly system

In order to achieve automatic control of the BPM preparation process, we developed a spray system for membrane self-assembly based on a logic-control program (PLC system; Fig. 1). The device was mainly composed of gas supply systems, spray systems, a carrier membrane, and a PLC system.

The equipment consisted of three identical atomizing nozzles with a nozzle diameter of 0.5 mm, each connected to a pressure tank and a solenoid valve that controlled the opening

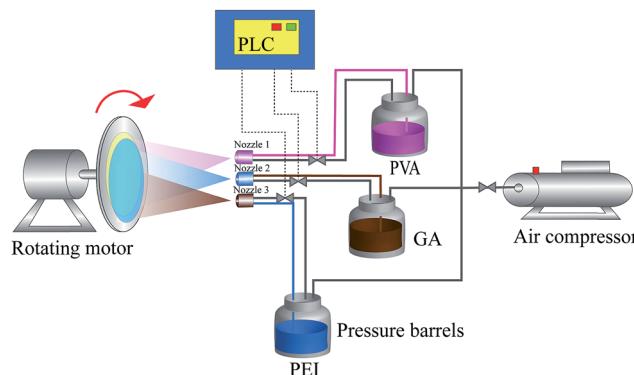


Fig. 1 Automatic spray system for the preparation of bipolar membranes.

and closing of the nozzles. A high volume air compressor was utilized to maintain a constant pressure of 2 bars inside the two pressure tanks while spraying. A metal substrate was fixed perpendicularly and rotated at 100 rpm, solely to accelerate the drainage of the solution from the surface of the membrane. The operating parameters, such as spraying time, standing interval, spray cycles, and on-off bunker, were controlled by a programmable logic controller (PLC) system. PLC also controlled sprayer and burner start and stop commands and allowed for fully automatic operation. The nozzles, the burner and the substrate were placed inside a Constant Temperature and Low Humidity Box (CTLH Box) which could be controlled at a constant temperature and humidity.

### 2.3 Preparation of BPM

The membrane preparation process was depicted in Fig. 2. PEI was dissolved in deionized water to form a 5 wt% PEI aqueous solution, which was stirred well to obtain a solution that formed a colorless transparent solution. A 3 wt% PVA aqueous solution prepared from PVA was stirred in a 90 °C water bath for 1 h and then allowed to cool. GA (3 wt%) was mixed and stirred well. The CM-ZHJ, was cut into 5 cm × 5 cm pieces, which were then soaked in distilled water for 24 h. Subsequently, they were removed and fixed to the membrane carrier. A PVA aqueous solution (3 wt%) was sprayed onto one topside of the CM-ZHJ and then 3 wt% GA and 5 wt% PEI solutions were sprayed onto the same side. The spraying time and standing interval

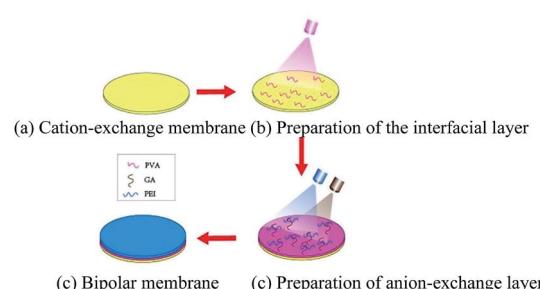
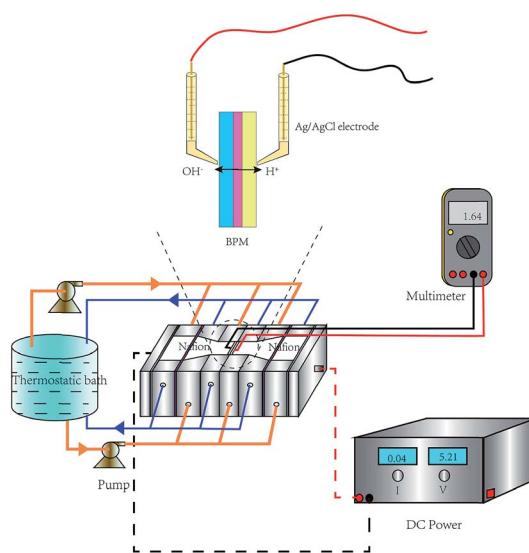


Fig. 2 Schematic of the preparation of the bipolar membrane.

**Table 1** The name abbreviations of the sample with different deposition condition

Abbreviations	Deposition condition
CM-ZHJ	A commercial cation-exchange membrane
CM-ZHJ-PVA	Spraying 3% PVA twice on CM-ZHJ
PEI/CM-ZHJ	Spraying 3% PVA twice, 3% GA three times, followed by 5% PEI three times
(PEI-CYC/CM-ZHJ) <sub>1</sub>	Spraying 3% PVA twice, 5% PEI and 3% GA alternately one cycle
(PEI-CYC/CM-ZHJ) <sub>3</sub>	Spraying 3% PVA twice, and then 5% PEI and 3% GA alternately three cycle
(PEI-CYC/CM-ZHJ) <sub>5</sub>	Spraying 3% PVA twice, and then 5% PEI and 3% GA alternately five cycle



**Fig. 3** Equipment for obtaining *I*–*V* curves of the bipolar membranes.

between two spraying cycles was 5 s and 10 min respectively. Finally, the membrane was dried at room temperature to obtain BPM. The membranes with different deposition condition were denoted as CM-ZHJ, CM-ZHJ-PVA, PEI/CM-ZHJ BPM separately, which was shown in Table 1.

#### 2.4 Water dissociation on the BPM

*I*–*V* curves of a BPM could be used to determine its water-dissociation voltage, limiting current density, and water-splitting efficiency.<sup>25</sup> The set used to obtain the *I*–*V* curves of the BPM was shown in Fig. 3. Cathode and anode chambers were separated from the BPM by Nafion membranes to prevent electrode products from coming into contact with the BPM and to maintain the environments of the two compartments near BPM. The BPM was placed in the middle of the cell, and the trans-membrane voltages were measured by two Ag/AgCl electrodes. The BPM specimen was immersed in the Na<sub>2</sub>SO<sub>4</sub> solution to keep it wet and then placed in the measuring cell. Before the experiment, each chamber was circulated for 30 min to eliminate visible bubbles.<sup>26</sup> The device was run for 20 min at

a current density of 20 mA cm<sup>−2</sup> to allow BPM to reach steady state. The applied current density was then increased from 0 to 120 mA cm<sup>−2</sup> at a rate of 10 mA cm<sup>−2</sup> while the voltage was recorded. The results were reported as the average of three runs.

#### 2.5 Membrane characterization

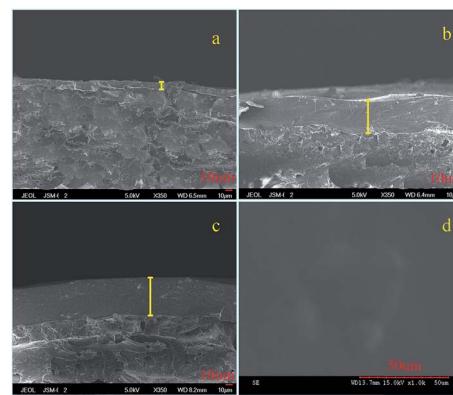
SEM was utilized to observe the cross-sections and surface of the BPMs.<sup>27</sup> A Nicolet-560 FTIR spectrometer was used to obtain the spectra for CM-ZHJ, CM-ZHJ-PVA, and PEI/CM-ZHJ BPM. TGA measurements on PEI/CM-ZHJ BPM were performed with a DT-40 thermal analyzer. The temperature was increased from 20 to 600 °C at a heating rate of 10 °C min<sup>−1</sup>.

### 3. Results and discussion

#### 3.1 SEM, FTIR analyses

SEM images of the cross-section and surface morphology of the BPM were displayed in Fig. 4. The cross-sectional morphology of the PEI/CM-ZHJ BPM, which had different composite layers of polyelectrolyte (Fig. 4), clearly had a boundary layer. The CM-ZHJ was sprayed PVA twice, followed by spraying the optimum concentration of 5% PEI and 3% GA alternately one cycle ((PEI-CYC/CM-ZHJ)<sub>1</sub>), three cycles ((PEI-CYC/CM-ZHJ)<sub>3</sub>) and five cycles ((PEI-CYC/CM-ZHJ)<sub>5</sub>) respectively. The upper anion-exchange layer was formed by cross-linking reaction among GA, PEI, and PVA. Its cross-section was smooth and dense. Its thickness increased with the increase in number of composite layers, indicating its dependence on the spraying assembly. The cross-section formed. The transition zone in which water dissociation occurs was the PVA interface. Since it was of nanometer thickness, it was not visible in Fig. 4. Although the cross-sectional morphology of BPM was distinct, its anion- and cation-exchange layers were in close contact, showing no bubbles in between them. The surfaces of the BPM anion- and cation-exchange layers (Fig. 4d) showed smooth morphology, with the former layer being smoother and tighter.

Fig. 5 shows the IR spectra of CM-ZHJ, CM-ZHJ-PVA, and PEI/CM-ZHJ membranes. The characteristic absorption of sulfonic acid group at 1190–1120 cm<sup>−1</sup> was present in the spectrum of



**Fig. 4** SEM images for: (a) cross-section (PEI-CYC/CM-ZHJ)<sub>1</sub>; (b) cross-section (PEI-CYC/CM-ZHJ)<sub>3</sub>; (c) cross-section (PEI-CYC/CM-ZHJ)<sub>5</sub>; (d) Surface of (PEI-CYC/CM-ZHJ)<sub>3</sub>.

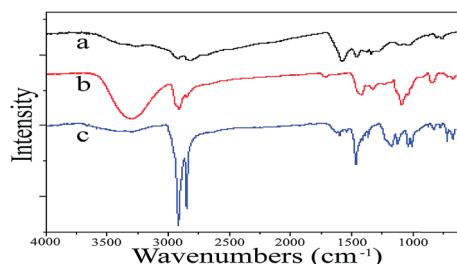


Fig. 5 FTIR spectra of the (a) PEI/CM-ZHJ bipolar membrane, (b) CM-ZHJ-PVA membrane, (c) CM-ZHJ membrane.

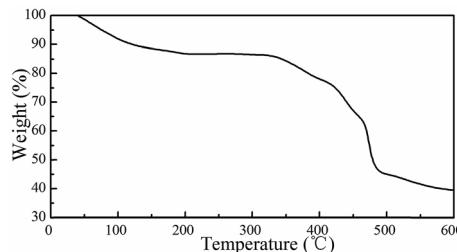


Fig. 6 TG profiles of the (PEI-CYC/CM-ZHJ)<sub>3</sub> bipolar membrane.

the CM-ZHJ membrane (Fig. 5c). The IR spectrum of the CM-ZHJ-PVA membrane, which was prepared by spraying an intermediate layer of PVA on the CM-ZHJ membrane (curve b is), had a broad band at 3600–3200 cm<sup>-1</sup> due to O–H stretching vibration. The absorption at 1091 cm<sup>-1</sup> was due to C–O stretching vibration.<sup>28</sup> The O–H absorption peak in the FTIR spectrum of the BPM (curve a) was markedly weaker than that in curve b. The absorption peak at 1575 cm<sup>-1</sup>, which arised from C=N stretching vibration, indicated that GA underwent cross-linking reaction with amide of PEI, generating imino groups and formed a dense membrane, thereby improving the mechanical properties of the membrane.

### 3.2 Stability of spray-crosslinked membrane

The thermal stability of the spray-crosslinked bipolar membrane was investigated by thermogravimetry (TG). The thermo gram of the PEI/CM-ZHJ BPM (Fig. 6) roughly had three sloping sections. The first section (30–120 °C), which showed a relatively small loss (~10%), corresponded to loss of water absorbed on the polymer membrane. The second section (100–350 °C), which had a lower slope and loss (~5%), indicated the good thermal stability of the BPM within this temperature range. The slope of the third section was large and had a steep peak for the weight loss due to structural collapse of the sample, which caused CO<sub>2</sub> release.

### 3.3 Effects of assembly conditions on *I*–*V* curves of the BPM

**3.3.1 Effect of PEI concentration.** The effect of PEI concentration on the water-dissociation performance of the BPM was shown in Fig. 7. When the PEI concentration was low, the formative anion exchange layer was thin but relatively

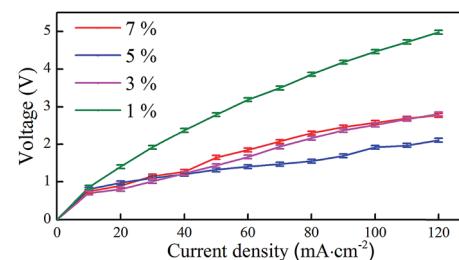


Fig. 7 *I*–*V* curves of the bipolar membranes with anion-exchange layers prepared with different PEI concentrations.

homogenous. It possessed few fixed groups, thus impeding the transfer of OH<sup>-</sup> and causing a large water-dissociation voltage. With the increase in PEI concentration, the concentration of fixed groups increased and thereby enhanced the transfer of OH<sup>-</sup>. Because of the hydrophilicity of PVA, water migrated to the intermediate layer and splits. This reaction lowered the voltage across the BPM to a relatively stable level. Since its concentration of exchangeable groups was too high, the cross-linking reaction between layers was inhomogeneous. The electrostatic repulsion between layers was strong, the extension of hyper branched polymer chain segments was irregular, and the surface structure of the membrane gradually loosened when the PEI concentration was too high. Consequently, the voltage drop across the BPM rebounded during the testing process, and delamination or ballooning between layers easily occurred, thereby increasing the water-dissociation voltage and decreasing the mechanical stability of the membrane. When PVA 3 wt% solutions were sprayed twice and 2 wt% GA were sprayed three times, then, the appropriate concentration of PEI with molecular mass of 70 000 sprayed three times was found to be 5 wt%. The voltage across the BPM was 1.92 V (error  $\pm$  0.05) at 100 mA cm<sup>-2</sup> current density. The voltage drop was small.

**3.3.2 Effect of GA concentration.** Since both PEI and PVA are water-soluble, GA was often cross-linked with them in order to increase the mechanical stability of membranes. The effect of the GA concentration on the water-dissociation voltage of the BPM was shown in Fig. 8. When the GA concentration was very low, both PVA and PEI gradually dissolved in water, since the cross-linking degree was not enough, resulting in less fixed groups in the layer and lower ion-exchange capacity. The cross-linking reaction was enhanced at higher GA concentration. Both PEI and PVA fixed on CM-ZHJ formed a dense anion-

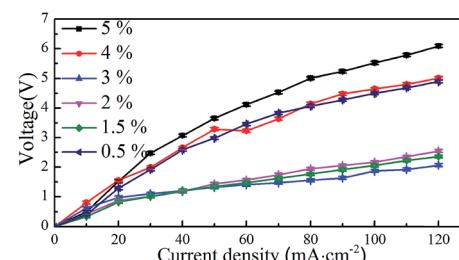


Fig. 8 *I*–*V* curves of the bipolar membranes with anion-exchange layers prepared with different concentrations of GA solutions.

exchange layer *via* cross-linking with GA, thus increasing the membrane stability. When PVA 3 wt% solutions were sprayed twice, the GA was sprayed three times, followed by the optimum concentration of PEI with molecular mass of 70 000 sprayed three times, the membrane voltage increased because of excessive cross-linking, changing the membrane structure and affecting the water-dissociation voltage when the GA (spraying 3 times) concentration more than 3 wt%. Thus, the PVA 3 wt% solutions were sprayed twice, 3 wt% GA were sprayed three times, and 5 wt% PEI with molecular mass of 70 000 were sprayed three times, the optimum water-dissociation voltage of the BPM decreased from 1.92 V (error  $\pm$  0.05) above result to 1.87 V (error  $\pm$  0.05) at a current density of  $100 \text{ mA cm}^{-2}$ .

**3.3.3 Effect of PVA concentration.** The effect of the PVA intermediate layer on the water dissociation on BPMs modified with 1, 2, 3, 4, and 5 wt% PVA solutions was examined from their *I*-*V* curves (Fig. 9). The membranes were prepared with spraying PVA twice, the optimum concentration of 3% GA three times and 5% PEI with molecular mass of 70 000 three times. The curves showed that PVA at low concentration catalyzes water dissociation on the BPM. In contrast, PVA at high concentration was disadvantageous to the performance of the membranes. Thus, the water-dissociation voltage of the BPM decreased and then increased with the increase in PVA concentration. When the PVA concentration was low, the intermediate layer that formed was so thin that the surface of the anion- and cation-exchange layers came in and contacted with each other, resulting in failure of the BPM. Furthermore, hydrophilic groups in the intermediate layer were few and water dissociation was slow under this condition. The adsorbed amount also increased with the increase in PVA concentration. Therefore, the intermediate layer possessed more catalytic and hydrophilic sites, resulting in the observed water dissociation performance of the BPM. When the PVA concentration was too high, PVA molecules had many hydroxyl groups, which lead to strong interactions between PVA and water molecules and between PVA molecules. The intermolecular interaction greatly increased the thickness of the interfacial layer and formed a dense PVA film. An excessive increase in the junction thickness, however, increased both the membrane resistance and the working voltage. When the BPM was alternately sprayed three times with 3 wt% PVA, 5 wt% PEI, and 3 wt% GA solutions, its water splitting-voltage reached the minimum. The membrane voltage was 1.87 V (error  $\pm$  0.05) at a current density of  $100 \text{ mA cm}^{-2}$ .

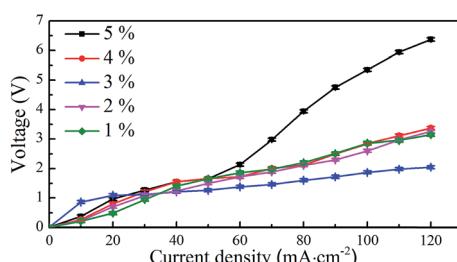


Fig. 9 *I*-*V* curves of the bipolar membranes with anion-exchange layers prepared with different concentrations of PVA solutions.

$\text{cm}^{-2}$ . Acid and alkali detected on both sides of the BPM suggested facile ion migration on the membrane.

**3.3.4 Effect of spraying cycles.** The effect of spraying cycles on the water-dissociation performance of the BPM was depicted in Fig. 10. The CM-ZHJ was sprayed PVA twice, followed by spraying the optimum concentration of 5% PEI and 3% GA alternately. When GA and PEI were sprayed alternately once on the CM-ZHJ surface, the AM thus formed was so thin that few functional groups formed, resulting in very weak ion transport. With the increase in number of composite membrane layers, the thickness and density of the membrane also increased, thus increasing the concentration of functional groups and the water dissociation voltage. When the layer was too thick, the rate at which the outer solution diffused into the intermediate layer was low, facilitating the formation of a depletion region. When the number of spraying cycles was excessive, the layers interact electrostatically, thus also affecting ion transfer and the water-splitting of the BPM. The above experimental results therefore indicated that the number of assembled layers could determine the water-dissociation performance of the BPM. When the concentrations of PEI, GA, and PVA were 5, 3, and 3 wt% respectively, the optimum number of alternate spraying cycles of GA and PEI was three. This corresponded to a water-splitting voltage of 1.82 V (error  $\pm$  0.05) across the BPM at a current density of  $100 \text{ mA cm}^{-2}$ .

**3.3.5 Effect of molecular weight of PEI.** Since PEI with low molecular weight possessed few branched chains, it cross-links with GA, forming an anion-exchange layer with few functional groups and weak ability to transfer  $\text{OH}^-$ . Conversely, a higher molecular weight implied more segments in the polymer. High degree of cross-linking of the material could impede hydrolysis of large polymers and thus prevented degradation of the polymer. With its flexible chain segments, PEI with high molecular weight could easily form a dense and smooth anion-exchange layer with abundant dissociating groups and strong ability for ion transfer. When the concentrations of PEI, GA, and PVA were 5, 3, and 3 wt% respectively, the spraying number of PVA was twice and the alternate spraying of PEI and GA was three times. The decrease in voltage across the BPM showed an improvement of the BPM's water-dissociation performance (Fig. 11). Although the water-splitting voltage of BPM prepared using low-molecular-weight PEI was low, the acid and alkali on both sides of membrane produced by water dissociation were weak. By contrast, BPM prepared using PEI-7000 showed better

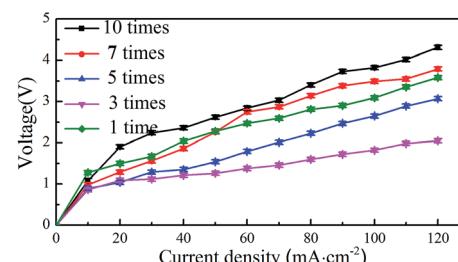


Fig. 10 *I*-*V* curves of bipolar membranes with anion-exchange layers prepared with different spray times.



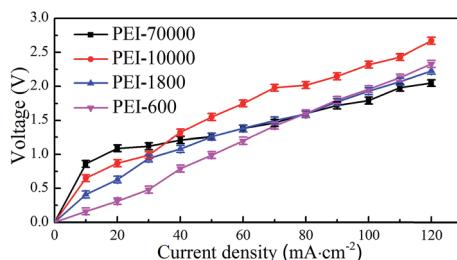


Fig. 11  $I$ - $V$  curves of the bipolar membranes with anion-exchange layers prepared with different molecular weights PEI.

performance; its membrane voltage was only 1.79 V (error  $\pm$  0.05) at current density of 100  $\text{mA cm}^{-2}$ .

## 4. Conclusions

In the present study, the combination of spray assembly with chemical cross-linking technology was successfully used to rapidly fabricate stable high-performance bipolar membranes. The resulting PEI/CM-ZHJ BPM possessed low membrane voltage and shows facile ion migration, which were desirable characteristics of a BPM. The effects of assembly conditions such as polyelectrolyte concentration, cross-linker concentration, composite layers, polyelectrolyte molecular weight, and PVA concentration on the performance of the membrane had been intensively investigated. Under the optimal conditions, the water-splitting voltage of the BPM was 1.79 V (error  $\pm$  0.05) at a current density of 100  $\text{mA cm}^{-2}$ . Spray cross-linking improved the charge density and ion-exchange capacity of the membrane, as well as enhanced the adhesion between the interfacial layer and anion- and cation-exchange layers. They also modified the BPM microstructure according to the membrane-forming conditions and spraying process parameters. Spray crosslinked assembly was a fast process; it only took several seconds to complete, thus greatly shortening the membrane-forming time and improving the membrane efficiency.

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