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## Influence of molecular interplay on the HPAM/UR rheological properties in an aqueous solution

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Herein, the interaction between partially hydrolyzed polyacrylamide (HPAM) and urea (UR) in an aqueous solution was characterized *via* differential scanning calorimetry (DSC) and two-dimension correlation spectra (2DCOS). The rheological properties of the HPAM solution (2000 and 2500 mg L<sup>-1</sup>) were studied as a function of the addition of the UR content (50, 100, 200, 300, and 400 mg L<sup>-1</sup>). The results indicate that the HPAM/UR solution exhibits higher intrinsic viscosity, apparent viscosity, first normal stress difference, and modulus than the HPAM solution due to the larger hydraulic size of HPAM in the aqueous solution. From the DSC and 2DCOS results, a stronger hydrogen bonding interaction between carbonyl and amino groups was observed in the vicinity of 45 °C. Dynamic light scattering (DLS) was employed to directly analyze the hydrodynamic diameter, and it further confirmed that a certain amount of UR enabled the blending solution to increase the hydraulic size. Moreover, an interplay model was put forward based on the rheology and dynamic light scattering data.

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## Introduction

As a type of polymer flooding agent, partially hydrolyzed polyacrylamide (HPAM) has received significant interest due to its applications in tertiary oil recovery, especially in reducing liquid permeability, increasing sweep efficiency or microscopic oil-displacing efficiency, and some other aspects.<sup>1–3</sup> It is vital to the mechanism of polymer flooding for enhanced oil recovery that the polymer flooding agents exhibit a relatively higher viscoelasticity performance following injection.<sup>4–6</sup> However, viscoelasticity of the HPAM solution is strongly influenced by shear stress, electrolyte, temperature, and pH due to its weak polyelectrolyte structure.<sup>7–11</sup> HPAM exhibits weak polyelectrolyte behavior in the aqueous solution. Mamdouh T. Ghannam<sup>12</sup> have found that the addition of NaCl to the PAM solution decreases the apparent viscosity of the solution. Zhang Qing *et al.*<sup>13</sup> found that the shielding effect of inorganic salts enables the HPAM coil to transform into a more constructive conformation in a saline solution. However, this effect tended to decline at high salt concentrations ( $C > 0.2$  mol L<sup>-1</sup>).<sup>7</sup> On the other hand, the HPAM solution easily shows shear thinning and viscosity break properties once it suffers from shear stress and

heat treatment, respectively. Rheological properties of the solution refer to the polymer structure, component, conformation, and macromolecular interplay. Through molecular interplay, the alternation of polymer conformation and improvement of rheological behavior can be realized. Several research groups have developed approaches to solve these issues. As a widely investigated example, surfactants were extensively utilized for improving salt tolerance and temperature resistance.<sup>14–20</sup> Although these observations were particularly helpful for holding solution viscosity, the crude oil exploited through injecting polymer/surfactant flooding inevitably contained a certain amount of surfactant and presented difficulties during post-processing owing to the unique surface activity of the surfactant.<sup>21</sup> To enhance the oil recovery efficiency and lower the cost, inexpensive and well-separated modifiers can be employed.

Urea is a type of salt that consists of a carbonyl and two polar amino groups. It is also utilized as a fertilizer in agricultural production ascribing to its low-cost and favorable effect. More importantly, UR is easily separated from oil–water blend solutions. S. A. Frangou<sup>10</sup> have explored the effect of urea on the chain conformation of xanthan solution and found that the concentration of urea has a noticeable influence on the conformation transformation of xanthan. Moreover, several types of studies on the thermal cross-linking of carboxylate/amine groups have already been reported and suggested the potential for temperature resistance.<sup>22,23</sup> In this study, the rheological properties of HPAM/UR solutions were explored *via* viscosimetry and rheometry using different detection models and temperatures. Dynamic light scattering was employed to

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directly analyze the hydrodynamic diameter.<sup>24–32</sup> DSC and 2DCOS techniques were carried out to obtain further evidence of the interplay between HPAM segments and urea molecules under variable temperature conditions from a different perspective.<sup>33–38</sup>

## Experimental

### 1 Materials

HPAM (industrial grade) was supplied by the Shengli Oil Field, China. The weight-average molecular weight of HPAM,  $2.3 \times 10^7 \text{ g mol}^{-1}$ , was determined *via* static light scattering tests, and the hydrolysis degree (HD) was 27%. Samples were employed after further purification. Urea and NaCl were purchased from Chengdu Kelong Chemical Agents Company (AR grade). Homemade ultrapure water was used in the preparation of solutions.

The samples for rheological measurements were prepared by dissolving HPAM powder in ultrapure water and then precipitating with methanol. The precipitate was washed and placed in a vacuum drying box at 35 °C for 24 h, and the dried product was used for mother solution preparation. All the samples were obtained by the dilution method, and dilution solvents were sodium chloride solution and NaCl/UR solution. The concentration of the sodium chloride solution is 0.1 mol L<sup>-1</sup>. Samples for the DSL tests were diluted to 50 mg L<sup>-1</sup> and centrifuged (12 000 rpm) for about 10 min. Before being placed in the sample cell, the test solutions were filtered *via* a 0.22 μm microporous filter. For the FT-IR and DSC experiments, the concentration was fixed at 10 wt%. All the testing samples were aged for 12 hours at ambient temperature before use.

### 2 Instruments and measurements

The intrinsic viscosity measurements were carried out using an Ubbelohde viscometer (globule volume was 4 mL and the average capillary diameter was 0.65 mm) in a water bath with automatic temperature control. The temperature was controlled at 25 ± 0.1 °C. In all the cases, the flow time of the solvent (NaCl solution) was less than 100 seconds such that kinetic energy corrections were made. The corresponding Ubbelohde viscometer was calibrated *via* calibration experiments. The corresponding parameters of the standard solutions employed are listed in Table 1.

All the reduced viscosities were calculated by eqn (1) as follows:

$$\eta_r = (At - Bt)/(At_s - Bt_s) \quad (1)$$

Table 1 Density and viscosity of the standard solutions

	Acetone; T = 25 °C	n-Butanol; T = 25 °C
$\rho \text{ (g mL}^{-1}\text{)}$	0.7851	0.8051
$\eta_r \text{ (Pa S)}$	$3.075 \times 10^{-3}$	$2.6390 \times 10^{-2}$

where  $\eta_r$  is the relative viscosity of the solution, which is the ratio of the viscosity of the polymer solution to that of neat solvent;  $t$  is the efflux time of the calibrating liquid; and  $t_s$  is the efflux time of the solvent. The calibration parameters are  $A = 0.00016010212$  and  $B = 0.01211235447$ . For rheological measurements, the AR-2000 rheometer (TA Instrument, America) was employed with a standard parallel plate (diameter = 40 mm). The gap was set at 200 μm, and the middle-temperature error was controlled at less than 0.1 °C. To cope with various test requirements, flow sweep and oscillation models were selected in the applicable shear rate or angular frequency. The first normal stress difference was measured by the Anton Paar MCR 302 rheometer (Anton Paar, America). Dynamic light scattering measurements were conducted using a Brookhaven Instrument (BI-200SM) at 25 °C. All time-resolved FTIR spectra were obtained using a resolution of 2 cm<sup>-1</sup> *via* a NICOLET-6700 infrared spectrometer equipped with an electronic cell. HPAM sample was sealed between two CaF<sub>2</sub> tables. In these tests, 64 scans were available for an acceptable signal-to-noise ratio. Manual method was used to control the temperature at the rate of *ca.* 0.5 °C min<sup>-1</sup> with an increment of 5 °C. The baseline correction process was performed by the software Omnic ver. 8.2.0.387. 2D correlation analysis was conducted by the software 2D shige ver. 1.3 (2D-shige (c) Shigeaki Morita, Kwansai-Gakuin University, Japan, 2004–2005) and further plotted into contour maps *via* the Origin 8.0. Calorimetric measurements were performed using a Mettler Toledo DSC823-TGA/SDTA85/e thermal analyzer at the rate of 1 °C min<sup>-1</sup> during the heating process.

## Results and discussion

### 1 Effect of UR on the viscosity of HPAM

It is known that hydrodynamic size is closely related to the rheological behavior of the polymer dilute solution, and according to the polymer solution theory, intrinsic viscosity ( $[\eta]$ ) can reflect the variation of hydrodynamic size and molecular conformation of a polymer. Thus, Fig. 1 shows the effect of UR addition on the intrinsic viscosity of the HPAM solution at  $T = 25$  °C. It is observed that the intrinsic viscosity increases with

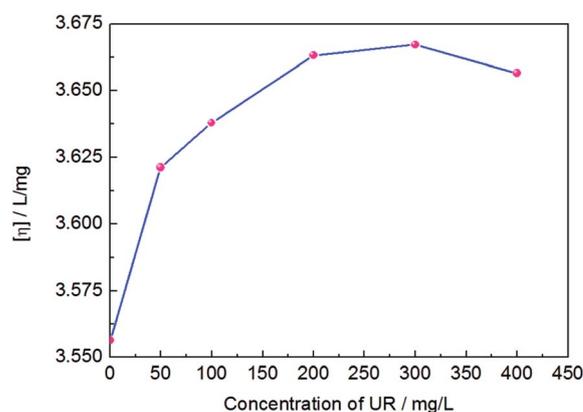


Fig. 1 Intrinsic viscosity versus the UR concentration for the HPAM solution ( $T = 25$  °C).



UR addition and reaches maximum at 300 mg L<sup>-1</sup> of the UR content. This behavior is a result of an interplay between HPAM segments and UR molecules as well as acylamino and amino interactions that are manifested by variation in the UR content. Moreover, changes in  $[\eta]$  suggest that the alternation of the HPAM coil conformation occurs in the aqueous solution. The UR molecules enable HPAM coils to be more extensive and increase the hydrodynamic radii to some degree. Therefore, a certain amount of UR is especially useful for the improvement of viscosity.

Fig. 2 shows the effects of UR addition on the apparent viscosity in 2000 mg L<sup>-1</sup> of the HPAM solutions at 25 °C. It was notable that in the low shear rate area (less than 0.3 S<sup>-1</sup>), similar trends were observed for the apparent viscosity of HPAM. In the HPAM/UR solutions, the viscosity increases in the order of UR concentration: 0 mg L<sup>-1</sup> < 50 mg L<sup>-1</sup> < 100 mg L<sup>-1</sup> < 400 mg L<sup>-1</sup> < 200 mg L<sup>-1</sup> < 300 mg L<sup>-1</sup>, and the maximum in these cases occurred at 300 mg L<sup>-1</sup>. However, the viscosities of the solutions, which are close to each other in the high shear rate area, are expected to result in the complete orientation of macromolecules in the aqueous solution. When a higher shear rate is imposed, the motion of the chain segment play as the main migration unit, which enables molecule conformation to vary and causes a decrease in the hydrodynamic volume. Moreover, shear stress can damage hydrogen bonding between HPAM and UR, especially at higher shear rates. Consequently, the viscosity of the solution reduces.

The apparent viscosities for variable HPAM concentrations were measured to explore the effect of HPAM concentration on the solution viscosity in the HPAM/UR system. Fig. 3 shows the apparent viscosity *versus* shear rate curves for different HPAM solutions involving blends formed from two compositions: HPAM and 300 mg L<sup>-1</sup> UR. The deviation of apparent viscosity for 2000 mg L<sup>-1</sup> and 2500 mg L<sup>-1</sup> HPAM solution in Fig. 3 is most likely a consequence of the effects of HPAM concentration and hydrodynamic volume at lower shear rates. For the 2000 mg L<sup>-1</sup> HPAM/300 mg L<sup>-1</sup> UR solution, the molar ratio of UR and HPAM is bigger than the ratio in the 2500 mg L<sup>-1</sup> HPAM/300 mg

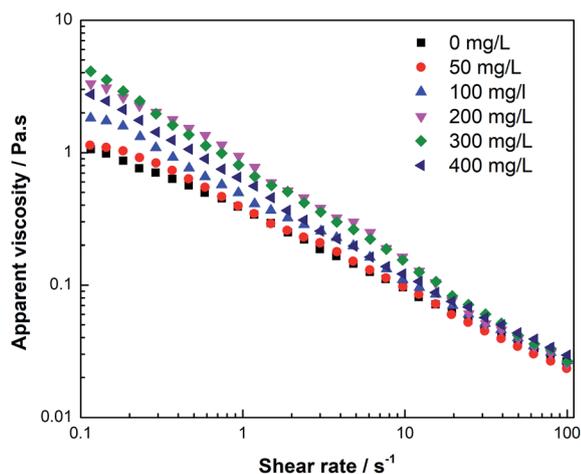


Fig. 2 Apparent viscosity of the 2000 mg L<sup>-1</sup> HPAM solutions *versus* the shear rate for various UR contents ( $T = 25\text{ }^{\circ}\text{C}$ ).

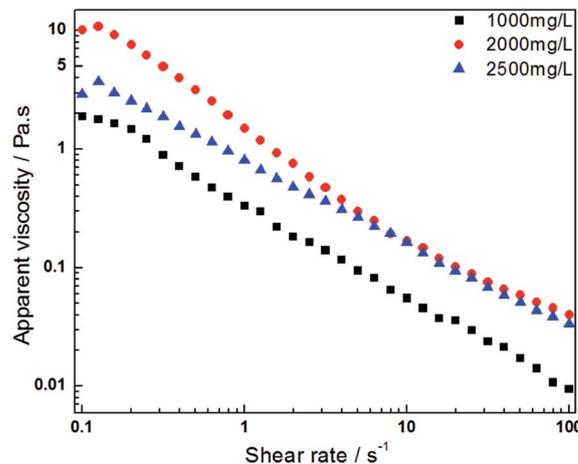


Fig. 3 Apparent viscosity of the HPAM/UR (300 mg L<sup>-1</sup> UR) blend solution *versus* the shear rate for various HPAM concentrations ( $T = 25\text{ }^{\circ}\text{C}$ ).

L<sup>-1</sup> UR solution. Therefore, the interplay between HPAM and UR is more prominent and forms a larger hydrodynamic volume in the former solution. To a certain degree, it confirms that there is an interaction between the UR and HPAM structural unit. It also provides evidence that UR has a significant influence on solution viscosity in this system. As abovementioned, the orientation of the HPAM molecule is completed when the HPAM/UR solution suffers from high shear rates. Thus, the hydrodynamic volume of polymer is no longer the decisive factor for viscosity. However, the concentration of the polymer has a greater effect in this case. As a result, the viscosities of the two abovementioned systems are almost the same when they suffer from high shear rates. The viscosity of the 1000 mg L<sup>-1</sup> HPAM/300 mg L<sup>-1</sup> UR solution, however, is lower than that of the remaining two solutions under the present experimental condition; this indicates that the variation of the HPAM concentration is the dominant factor for the apparent viscosity.

Based on the experimental results shown in Fig. 1–3, a proper amount of UR in the HPAM solution effectively enhances the apparent viscosity, but is less efficient when excess UR is added. The possible reason is that the HPAM molecular conformation transforms and possesses bigger hydrodynamic volume; this is caused by hydrogen bonds formed by the amino groups of UR and the HPAM structural unit, which involves molecular interaction in progress. The specific interplay is described as the adjacent carbonyls along the HPAM chain adsorbed by UR *via* hydrogen bonding. Thus, the HPAM chain segments become rigid and increase the hydraulic size. However, this influence is finite. At low UR contents, the specific interaction holds the dominated position, which has been manifested by the enhancement of the intrinsic viscosity of HAPM/UR. In contrast, a high UR content may cause a reduction in the intrinsic viscosity.

When the concentration of UR was lower than 300 ppm, the interaction between the side groups of HPAM and UR was weak owing to lesser number of UR molecules in the solution. However, when the UR content exceeded 300 ppm, the increase



in the interaction enabled the hydraulic size of the HPAM molecules to enlarge, causing the intrinsic viscosity to reach maximum. As the concentration of UR is further increased, the UR molecules might have interaction with two or more side groups in the HPAM molecules, which causes the decrease in intrinsic viscosity. Based on the abovementioned discussion, this interaction is more efficient for the enhancement of intrinsic viscosity under the present experimental conditions when the content of UR is 300 mg L<sup>-1</sup>. A schematic of the specific interaction in the aqueous solution is presented in Fig. 4.

From another perspective, the HPAM hydraulic size and how closely migration matches angular frequency have a significant influence on the macromolecular motion behavior in blend solution when oscillation stress is imposed. The related parameters obtained from the oscillation measurement model can reflect information about the molecular motion. The data corresponding to the storage modulus and loss modulus for the HPAM and HPAM/UR solutions are plotted in Fig. 5 as a function of angular frequency. Values of  $G'$  for HPAM/UR, which are expressed by the solid pattern, are higher than those for HPAM. Similar trends for  $G''$  were observed. The improvement of  $G'$  and  $G''$  is due to the enhancement of the deformation resistance caused by an increase of coil size. Hydrodynamic volume, however, has been further discussed hereinafter. Herein, it is notable that the addition of UR can improve the viscoelasticity of the HPAM solution; on the other hand, this also indicates that the interaction between UR and HPAM occurred in the aqueous solution.

DLS was employed to analyze the distribution of the hydrodynamic diameter ( $D_h$ ) when the HPAM concentration was diluted to 50 mg L<sup>-1</sup>. Although the HPAM concentration was diluted, the UR content was maintained at 300 mg L<sup>-1</sup>. The results shown in Fig. 6 are consistent with the previously proposed rheological properties discussion. The distribution of the hydrodynamic diameter for the HPAM solution mainly concentrated at 110–300 nm, whereas the distribution for the HPAM/UR solution was at 200–700 nm. This is probably

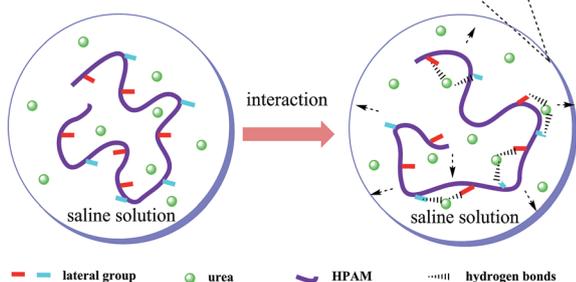
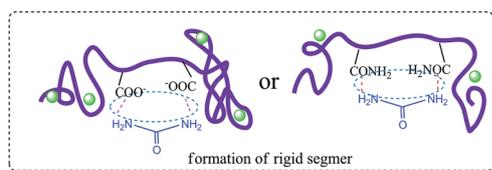


Fig. 4 Schematic for the short-range and long-range interactions.

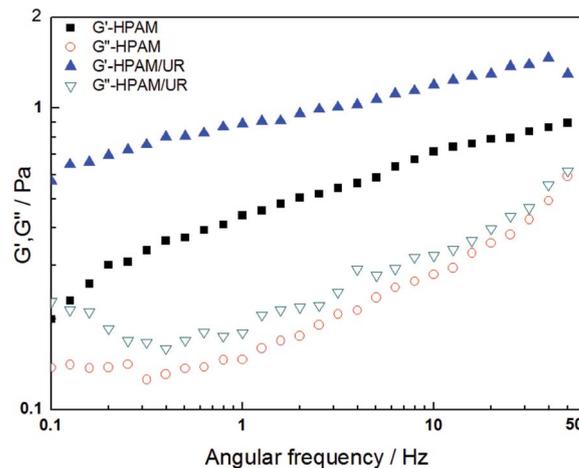


Fig. 5  $G'$  and  $G''$  as a function of frequency for the 2000 mg L<sup>-1</sup> HPAM and HPAM/UR (300 mg L<sup>-1</sup>) solutions ( $T = 25\text{ }^{\circ}\text{C}$ ).

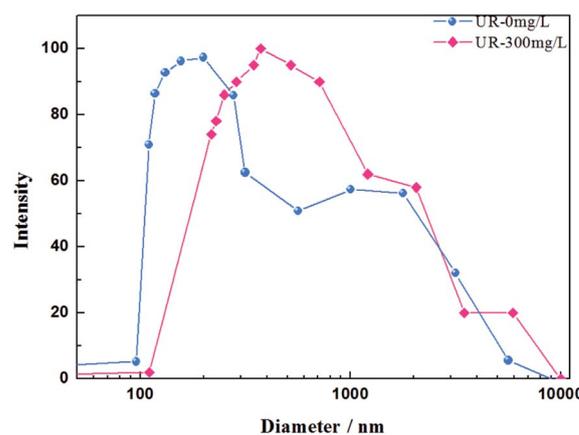


Fig. 6 DLS measurements of the HPAM and HPAM/UR solutions at 25 °C.

a consequence of the interplay between HPAM and UR. Acylamino, which is on the HPAM lateral chain, can bond to UR *via* hydrogen bonding. According to the analysis of Fig. 4, an extensive conformation and increase of  $D_h$  are benefited from the formation of hydrogen bonding when UR was added under the present experimental condition. Thus, the larger the  $D_h$ , the higher the viscosity of the dilute solution.<sup>39,40</sup>

## 2 Effect of temperature on the HPAM/UR interplay and rheological properties

Temperature has significant effects on the intermolecular interaction and migration. In our previous study,<sup>41</sup> hydrogen bonding interaction in an aqueous solution explored by DSC differential spectrum was reported, and it was found that in the low shear rate region, the maximum apparent viscosity value occurred near 40 °C in the temperature-rise period. Fig. 7 shows the apparent viscosity *versus* the shear rate curves for the HPAM solutions involving blends formed from two different compositions: 2000 mg L<sup>-1</sup> HPAM and UR.<sup>41</sup> In the low shear rate area,



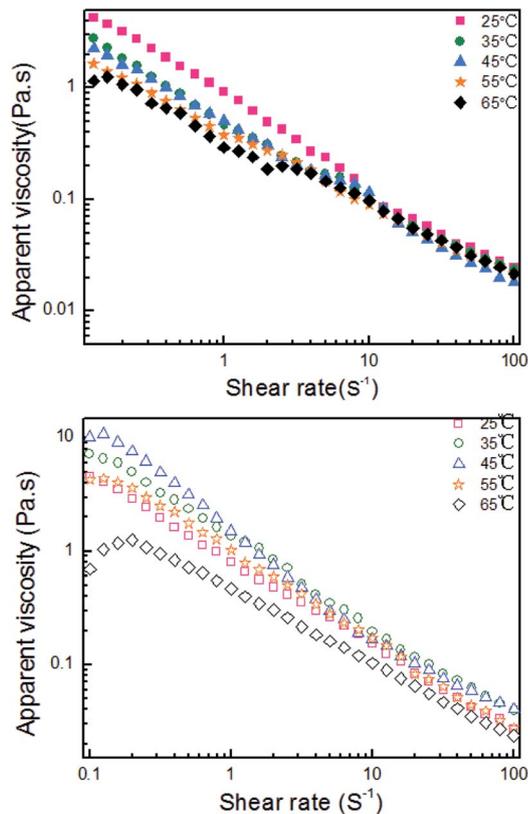


Fig. 7 (a) Apparent viscosity of 2000 mg L<sup>-1</sup> HPAM with the 0 mg L<sup>-1</sup> UR content versus shear rate at various temperatures. (b) Apparent viscosity of 2000 mg L<sup>-1</sup> HPAM with 300 mg L<sup>-1</sup> UR content versus shear rate at various temperatures.

the apparent viscosity reduces with the increasing temperature when the UR content is 0 mg L<sup>-1</sup>, as shown in Fig. 7(a). While in Fig. 7(b), the viscosity initially increases and then decreases with the increasing temperature in the same shear rate region when the UR content in the blends is 300 mg L<sup>-1</sup>. In the HPAM solutions, the active ability of the molecular motion unit was improved and manifested *via* a reduction in the viscosity. However, for various temperature series, the viscosity of the blend solution increases in the order: 65 °C < 25 °C < 55 °C < 35 °C < 45 °C. It was considered that the addition of UR causes an increase in the viscosity, and this may involve hydrogen bond damage and restructuring, conformation variation, and thermal effect.<sup>41</sup> This behavior has been discussed further in the following section.

As discussed above, intrinsic viscosity can directly reflect interplay in a dilute solution. The effect of the temperature on  $[\eta]$  is shown in Fig. 8. In these tests, two types of solutions were employed to measure the  $[\eta]$ : one is the HPAM solution and the other is a blend of HPAM and UR. The UR concentration was maintained at 300 mg L<sup>-1</sup> in the blends. The results show that the viscosity of the HPAM/UR solution first increases and then decreases with the increasing temperature, which is in accordance with the changes of the apparent viscosity shown in Fig. 7(b). At  $T < 30$  °C and  $T > 45$  °C,  $[\eta]$  for the HPAM solution is relatively lower than the  $[\eta]$  of the blend solution, whereas it is

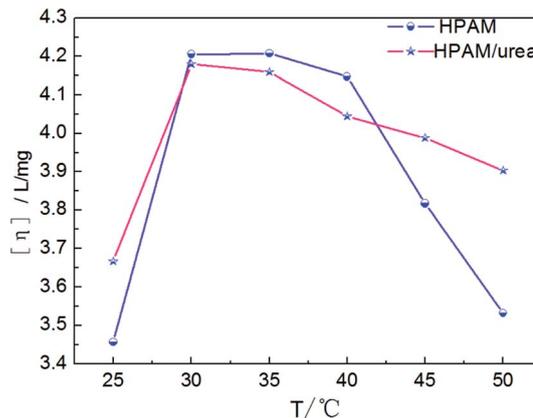


Fig. 8 Temperature dependence of the intrinsic viscosity for the HPAM and HPAM/UR (300 mg L<sup>-1</sup>) solutions.

contrary in the situation where the temperature ranges from 30 °C to 45 °C. When the temperature is higher than 40 °C, the downtrend of  $[\eta]$  observed in the HPAM/UR solution is gentler than that in the HPAM solution. Partly, the addition of UR can improve the temperature resistance of the HPAM solution. The possible reason may be stated as follows: HPAM exhibits weak polyelectrolyte behavior in an aqueous solution; electrostatic repulsion and solvation have significant effect on its conformation and hydraulic size. For electrostatic repulsion, the higher the polyelectrolyte solution ionization degree, the stronger the repulsive interaction. Thus, the solution has a higher intrinsic viscosity. From another perspective, the effect of solvation in this system is manifested by the hydrogen bonding interaction. At lower temperatures, short-range interplay holds the dominated position, which has been discussed in Fig. 4. Once the temperature increases, the migration ability of the counter-ion becomes stronger, and the ionization intensity increases. Thus, electrostatic repulsion is enhanced, and a higher intrinsic viscosity is observed.

On the other hand, high temperature does not favor the formation of hydrogen bonds and solvation. As a result, the intrinsic viscosity decreases. When solutions are exposed to lower temperatures ( $T < 30$  °C in the present tests), the former holds the dominated position, which was manifested by the enhancement of  $[\eta]$  with the increasing temperature, whereas the latter has greater influence when the solutions suffer from higher temperatures ( $t > 35$  °C) and the  $[\eta]$  decreases with the increasing temperature. It is notable that the  $[\eta]$  of the HPAM/UR system is higher than the  $[\eta]$  of the HPAM solution when  $45$  °C <  $T$  <  $50$  °C, as shown in Fig. 8. This is probably a consequence of large numbers of the short-range interplay between HPAM and UR within this temperature range. The corresponding evidence has been given in the following section.

The  $G'$  and  $G''$  data for the HPAM and HPAM/UR solution are plotted in Fig. 9 as a function of angular frequency. For the temperature influence series, the  $G'$  and  $G''$  of the HPAM solution increase in the order 60 °C < 45 °C < 35 °C, whereas for the HPAM/UR blend solution, the order is 35 °C < 60 °C < 45 °C. As per the previous discussion on modulus, the enhancement of  $G'$



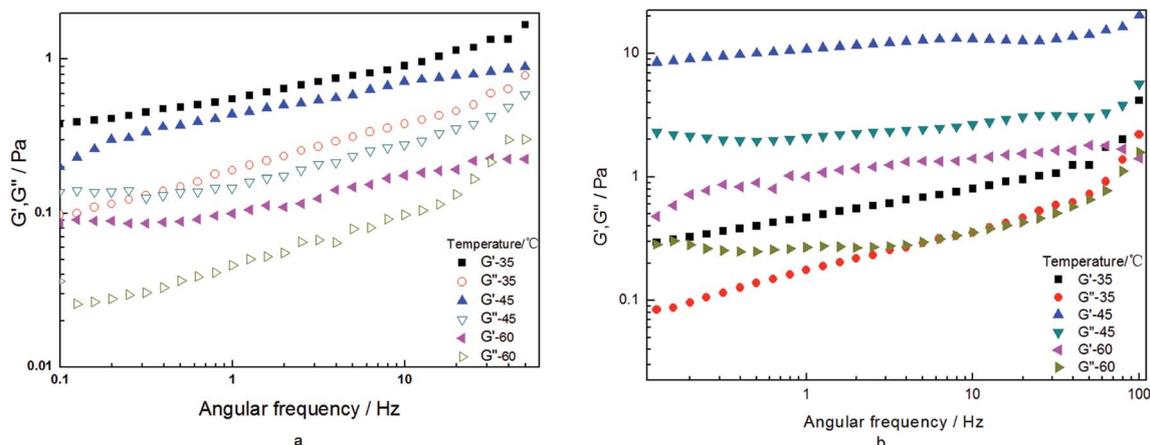


Fig. 9 (a) Modulus of 2000 mg L<sup>-1</sup> HPAM. (b) Modulus of 2000 mg L<sup>-1</sup> HPAM/300 mg L<sup>-1</sup> urea solution.

and  $G''$  is probably due to the strong, short-range interaction between HPAM and UR at  $T = 45$  °C. Moreover, the hydraulic size has great influence on the elastic properties of the polymer in an aqueous solution. As is known, the first normal stress difference can reflect elastic performance. Compared with a small hydraulic size polymer, a bigger hydraulic size polymer would suffer from greater motion resistance. Therefore, it is easy to yield elastic deformation when shear stress is imposed on a bigger coil-sized macromolecule. The effect of temperature on first normal stress difference for HPAM and HPAM/UR (300 mg L<sup>-1</sup>) solution is shown in Fig. 10. Contrary to the HPAM solution, higher values of the first normal stress difference were observed in the HPAM/UR system under the experimental condition, especially in high shear rate area. This indicates that the latter exhibited excellent performance when shear stress was imposed. Thus, the results shown in Fig. 10 are consistent with the previous discussion, that is, a larger coil size is formed in the HPAM/UR system due to the short-range interaction.

To further explore the molecular interplay, the calorimetric measurements were carried out to explore the temperature effect on the interaction involving HPAM and UR. First, the TG

test was performed to explore whether degradation reactions existed with the increasing temperature. The TG and DTG curves for the 40 wt% HPAM solution are shown in Fig. 11. An apparent weight loss only occurred at  $T = 155$  °C in the entire test temperature range. Moreover, a peak appears at the same position in the corresponding DTG curve. This evidence indicated that no degradation reactions occurred when the temperature was less than 155 °C. In a way, in the lower temperature range, the variations of rheological behavior with the increasing temperature are expected to be related to the change in the strength of the molecular interaction. On the basis of abovementioned discussion, DSC differential spectrum was employed to explore the abovementioned interplay in an aqueous solution.<sup>41–43</sup> The difference of heat flows (DHF) between HPAM/UR and HPAM solutions and the corresponding DSC curves are shown in Fig. 12. Through the difference of heat flows of two types of polymer solutions, thermal effect of the molecular interaction between UR and HPAM stood out, and the energy variations under the increasing temperature conditions were obtained. The red curve in Fig. 12 is the heat flow curve for the HPAM/UR solution, and the blue curve is the heat flow curve for the HPAM solution. The green curve is the

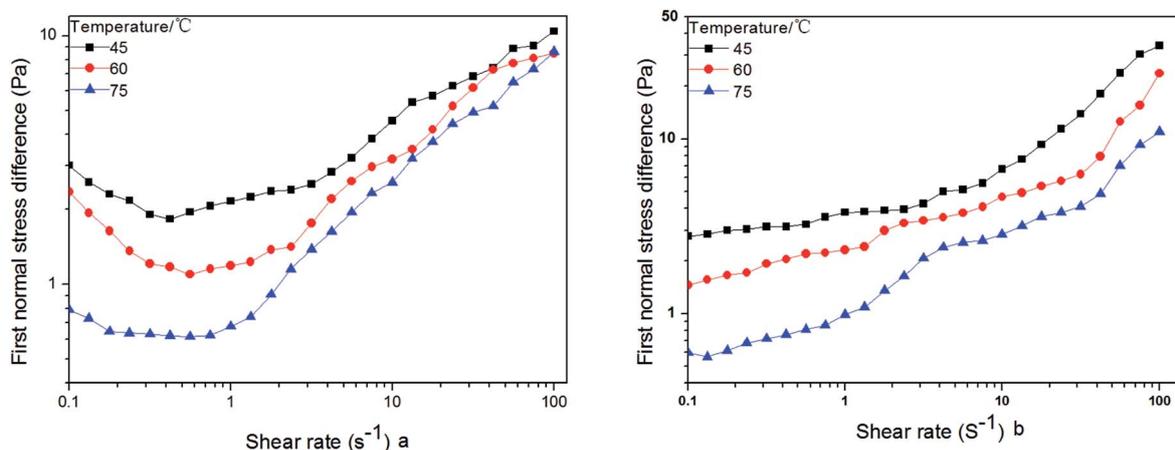


Fig. 10 First normal stress difference for the 2000 mg L<sup>-1</sup> HPAM (a) and HPAM/UR solution versus shear rate (b).



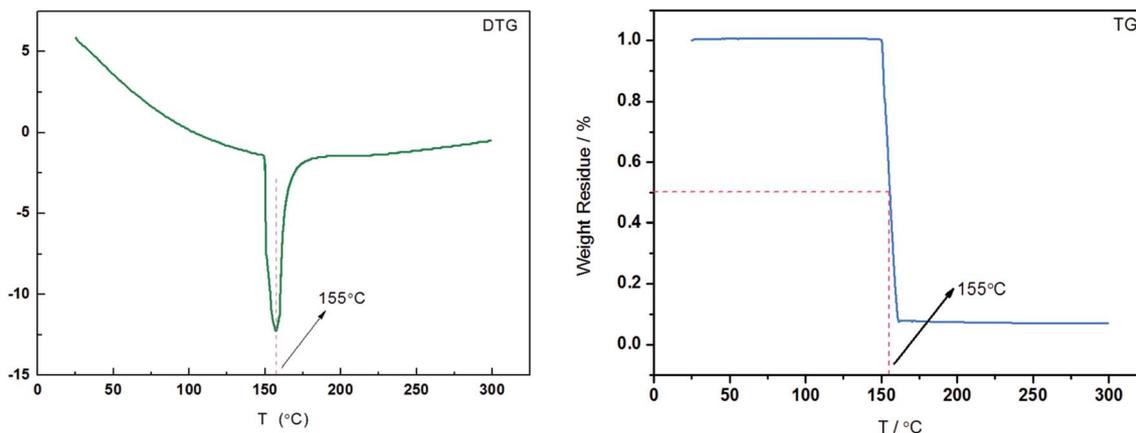


Fig. 11 TG and DTG curves for the 40 wt% HPAM solution.

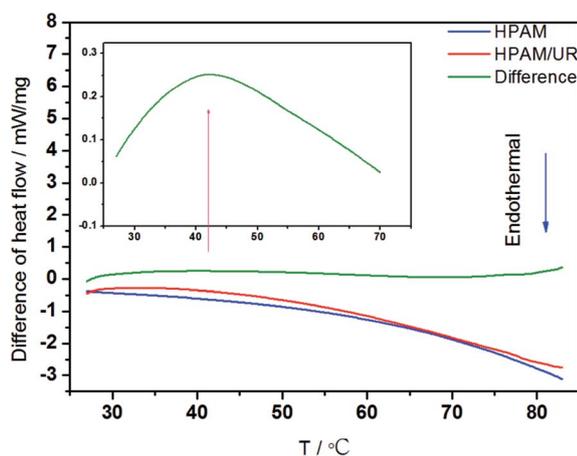


Fig. 12 The difference of heat flow between HPAM/UR and HPAM solutions versus temperature.

abovementioned DHF curve. The inset is a local amplification of the original curve in the temperature range: 27–70 °C. In the entire temperature-rise period, the variations of heat flow for

both HPAM and HPAM/UR are not visible. However, a visible exothermic process is observed in the local amplifying figure, and the strongest exothermic process appears near 40 °C. Based on the previous analysis of rheological behavior, it is possible that more hydrogen bonds form between the construction unit of HPAM and UR in this temperature range, and the exothermic process corresponds to the process of hydrogen bond formation.

Two-dimensional correlation spectra (2DCOS) is a mathematical method whose basic principles were first proposed by Noda in 1986. Due to the various responses of different species to external variables, helpful information about molecular interaction or conformation changes can be extracted, which cannot be directly obtained from a conventional 1D spectrum. On the basis of the temperature effect on the rheological properties and temperature region obtained from the DSC and apparent viscosity tests, infrared spectra obtained in the range from 30 °C to 50 °C were chosen to perform the 2DCOS analysis, and the results are shown in Fig. 13. 2DCOS can discern the specific order taking place under external perturbation. In this

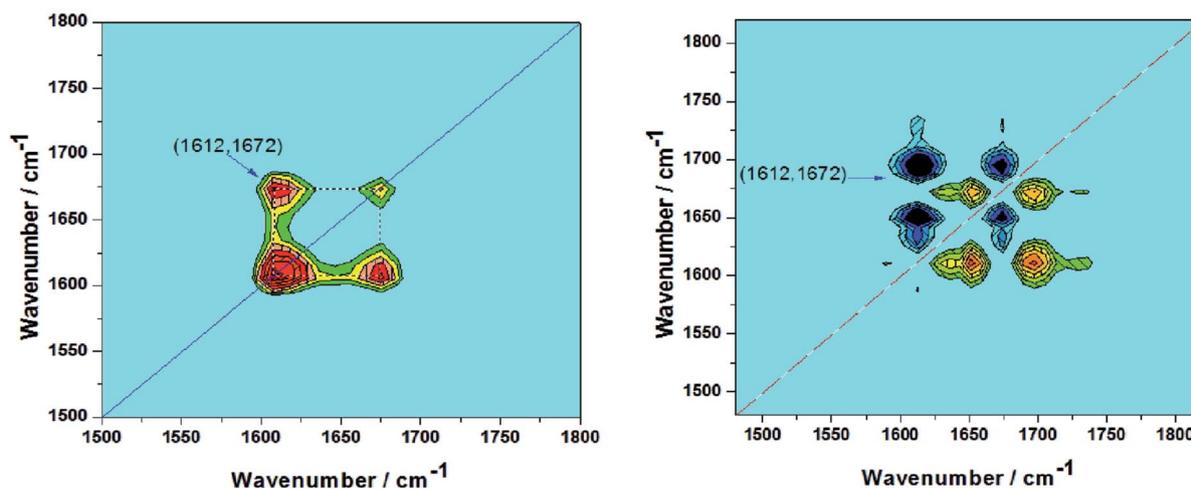


Fig. 13 Synchronous (left) and asynchronous (right) spectra of 2DCOS for carbonyl of the HPAM/UR composite solution. In the contour maps, warm colors are defined as positive intensities, whereas the cool colors are defined as negative intensities.



measurement, temperature served as a perturbation to explore the effect on the infrared absorption peak in the HPAM/UR system. The synchronous and asynchronous spectra, which are located at the 1500–1800 wavenumber, for carbonyl absorption of the HPAM/UR blend solution are obtained by the 2D shige. The determining rule can be simply summarized as Noda's rule, that is, the cross-peaks  $\nu_1$  and  $\nu_2$  (assuming  $\nu_2$  is less than  $\nu_1$ ) in the synchronous and asynchronous spectra have the same sign, and it indicates that the variation of  $\nu_1$  may occur before that of  $\nu_2$ , and *vice versa*. If the sign is zero or blank, an exact judgment cannot be made. In the synchronous spectra, two self-correlation peaks are located at the diagonal line with the wavenumber  $1612\text{ cm}^{-1}$  and  $1672\text{ cm}^{-1}$  corresponding to the absorbance of the carbonyl functional group, affected by UR and water through molecular hydrogen bonding, respectively. A positive cross-peak appears at  $(1612, 1672)\text{ cm}^{-1}$  in the synchronous spectra, whereas in the asynchronous spectra, the sign of the cross-peak  $(1612, 1672)\text{ cm}^{-1}$  is negative. According to the Noda's rule, the positive cross-peak in the synchronous spectra and negative cross-peak in the asynchronous spectra demonstrate that the larger wavenumber will respond to external perturbation earlier than the smaller wavenumber. In other words, hydrogen bonding between carbonyl group on the HPAM lateral chain and water is damaged initially and then the segmental free carbonyl group forms hydrogen bonding with UR. This result confirms the conclusions shown in Fig. 12.

## Conclusions

In this study, the rheological properties, in combination with the DLS, DSC, and 2DCOS technique, were employed to elucidate the shear rheological behavior of HPAM/UR in an aqueous solution and the interplay between HPAM and UR influenced by the temperature. The main conclusions are summarized as follows.

Due to the addition of UR, visible improvements in the viscoelastic properties of the HPAM aqueous solution were observed. Its intrinsic viscosity, hydraulic size, apparent viscosity, modulus, and first normal stress difference increase under the present measurement conditions. The UR content and temperature have great influence on the interaction mode and strength. The maximum value of the intrinsic viscosity occurred at the UR content of  $300\text{ mg L}^{-1}$ . The highest modulus and apparent viscosity for the HPAM/UR solution were observed when the temperature was in the vicinity of  $45\text{ }^\circ\text{C}$ . Based on the rheological data, it is found that HPAM/UR has better viscoelasticity performance that can be ascribed to a larger hydraulic size of HPAM in the aqueous solution. The DLS measurements indicate that the  $2000\text{ mg L}^{-1}$  HPAM/UR solution has a distribution of the hydraulic diameter in the range 200–700 nm, which is larger than that of the HPAM solution. The stronger hydrogen bonding interaction exists between the carbonyl and amino groups in this system in the vicinity of  $45\text{ }^\circ\text{C}$ , which is confirmed by DSC and 2DCOS techniques from a different perspective.

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