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A simple methodology to predict the tunneling conductivity of polymer/CNT nanocomposites by the roles of tunneling distance, interphase and CNT waviness

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In this work, a simple methodology is presented that describes the main tunneling conductivity of polymer/CNT nanocomposites (PCNT) assuming the tunneling distance, interphase surrounding the CNT, and CNT waviness. The conductivity related to the tunneling distance is obtained by a simple equation, and its role is considered by using an extended CNT (including CNT and the tunneling space). Additionally, the effects of the interphase and CNT waviness on the percolation threshold, effective filler fraction, and percentages of percolated CNT are expressed by simple equations. The suggested model is evaluated by experimental results and the influences of CNTs and interphase parameters on the conductivity are plotted and justified. The predictions demonstrate good agreement with the experimental results, which allow the estimation of percolation threshold, interphase thickness, and tunneling distance. The conductivity changes from 0 to 350 S m^{-1} at different parameter ranges, where the best conductivity is obtained by the smallest waviness and the shortest tunneling distance. Generally, the high concentration of thin, long, straight, and super-conductive CNT, thick interphase, dense network, short tunneling distance, and poor percolation threshold present desirable conductivity.

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1 Introduction

Many promising applications have been suggested for polymer/carbon nanotube (PCNT) nanocomposites due to the exceptional properties of CNTs, including their electrical conductivity and mechanical performances; this has led to an increased level of research in this field.^{1–4} CNTs commonly form a three-dimensional (3D) continuous network in polymer matrices above a critical concentration, which indicates the percolation threshold.^{5,6} The value of the percolation threshold is heavily dependent on the aspect ratio of the CNTs (length divided by diameter) and their dispersion extent in the polymer matrix. Thus, a high CNT aspect ratio (about 500–1000) causes the development of a conductive nanocomposite when very low CNT loadings are used. However, it has been reported that the improvement in the conductivity at very low CNT fractions is limited, which is due to the deficient dispersion of CNT in the polymer matrix.^{7,8} The percolation level can be experimentally assessed by measuring the electrical conductivity at dissimilar CNT concentrations. The CNT concentration at which the electrical conductivity sharply increases denotes the percolation

threshold. The key mechanism for electrical conductivity in PCNT was determined to be electron tunneling, where electrons are transported between nanotubes by the tunneling effect.⁹ Although the nanotubes are not physically connected, neighboring CNT transfer charges by electron jumping. Therefore, the conductivity of PCNT mainly depends on the distance between nanotubes, which can promote electron tunneling.

From a modeling point of view, several models have been suggested to predict the electrical conductivity in polymer composites. The best-known model is a power-law equation based on conventional percolation theory, which depends on the conductivity-to-filler concentration, percolation threshold, and an exponent.¹⁰ This model also displays good agreement with the electrical conductivity of PCNT, as reported by (ref. 11–13). Although this model can follow the conductivity of PCNT, it cannot consider the physical properties of CNT, such as its nano-size or interphase. Some people have also developed micromechanics models that can predict the electrical conductivity of PCNT by assuming more parameters such as the waviness of CNT and the tunneling effect;^{14–16} however, these employed complicated equations that are not applicable for practical applications. Moreover, these previous models commonly did not reflect the influence of the interphase, which can change the percolation level and the percentages of percolated nanotubes.

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The formation of interphase regions in polymer nanocomposites has been described in many studies;^{17–19} this is related to the exceptional surface area of the nanofiller and the robust interfacial interaction between the polymer matrix and nanoparticles. It was also reported that the mechanical properties of polymer nanocomposites, such as the tensile modulus and strength, directly depend on the interphase level.^{20–23} Some simple models were established based on micromechanics models to predict the roles of the interphase dimensions and stiffness on the tensile properties.^{24,25} Interphase regions have also been shown to have a positive effect on the percolation level in some studies.^{26–28} Interphase regions create a continuous network and cause the percolation threshold to occur before the actual joining of nanoparticles. Although the role of interphase percolation on the mechanical properties of PCNT has been investigated,^{29,30} the impacts of the interphase on the electrical percolation and conductivity of nanocomposites have not been studied.

As mentioned, some authors have studied the tunneling conductivity of PCNT by assuming the interphase or waviness of CNT, but their complex equations cannot be applied in practice. Accordingly, a simple equation that accurately suggests the tunneling conductivity of PCNT based on the interphase and waviness does not exist. In addition, previous studies did not consider the effects of the interphase and CNT waviness on the percolation threshold, effective concentration of CNT, or the portion of percolated nanotubes. In this study, the tunneling conductivity of PCNT is modeled by a simple methodology that considers the impacts of the interphase surrounding CNT, CNT waviness, and tunneling distance. An extended nanotube is supposed by considering the effects of CNT and the tunneling distance, and its conductivity is obtained from simple equations. In addition, the roles of the interphase and waviness on the percolation threshold, effective filler fraction, and percentages of networked CNT are expressed. The predictions of the suggested approach are compared with many experimental results from the literature and the outputs are discussed. Finally, the present methodology is evaluated by plotting the conductivity at different CNT ranges and interphase parameters.

2 Theoretical approaches

The conductivity of a tunneling distance between CNT can be expressed³¹ by:

$$\sigma_d = B \exp(-Ad) \quad (1)$$

where “ d ” is distance between nanoparticles, “ A ” is a characteristic tunnel distance and “ B ” is a constant parameter. This approach was applied for the conductivity of nanocomposites in which the electron tunneling is the main mechanism.^{31,32} “ B ” parameter can be assumed as the conductivity of CNT (σ_N), because $d = 0$ is obtained for CNT which result in $\sigma = \sigma_N$. Also, the value of “ A ” was suggested as 2 which presents accurate results compared to experimental data. So, eqn (1) can be presented as:

$$\sigma_d = \sigma_N \exp(-2d) \quad (2)$$

which creates very poor conductivity at a high “ d ” as the separate distance between CNT.

The electrical resistance of the distance between CNT is also suggested¹⁵ as:

$$R_d = \frac{d}{a\sigma_d} \quad (3)$$

where a is contact area of CNT.

Takeda *et al.*¹⁶ assumed extended nanotubes including CNT and inter-nanotube region in filler networks. They suggested two forms for the distance between nanotubes as shown in Fig. 1. For above form, it was suggested that contact area at overlapping position is $(2R)^2$ (R is CNT radius), while the contact area is about the cross-sectional area of nanotubes as πR^2 for another type. As a result, an average contact area can be approximated as $3R^2$ which results in:

$$R_d = \frac{d}{3R^2\sigma_d} \quad (4)$$

By substituting of eqn (2) into latter equation, the resistance of tunnel distance between CNT is calculated by:

$$R_d = \frac{d}{3R^2\sigma_N \exp(-2d)} \quad (5)$$

In addition, it was suggested that the electrical resistance of effective CNT involves the resistances of CNT and tunneling distance¹⁶ as:

$$R_{ND} = R_N + R_d \quad (6)$$

where “ R_N ” is the resistance of CNT defined as:

$$R_N = \frac{l}{\pi R^2 \sigma_N} \quad (7)$$

where “ l ” is CNT length. Assuming eqn. (5) and (7) into eqn (6) expresses the resistance of extended CNT including CNT and tunneling distance as:

$$R_{ND} = \frac{d}{3R^2\sigma_N \exp(-2d)} + \frac{l}{\pi R^2 \sigma_N} \quad (8)$$

The conductivity of extended CNT can be suggested by rewriting of eqn (7) as:

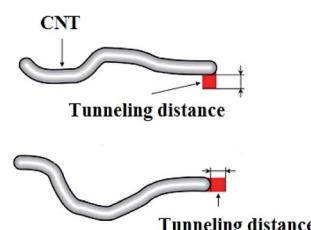


Fig. 1 Different forms of tunneling distance between nanotubes, where extended nanotube includes CNT and inter-nanotube region.¹⁶



$$\sigma_{\text{ND}} = \frac{l_{\text{ex}}}{\pi R_{\text{ex}}^2 R_{\text{ND}}} \quad (9)$$

where “ l_{ex} ” and “ R_{ex} ” are the length and radius of extended CNT, respectively. The length of CNT is much more than the tunneling distance. As a result, “ l_{ex} ” is considered as the length of CNT. Also, the radius of extended CNT does not change by tunneling distance. Accordingly, eqn (9) can be presented as:

$$\sigma_{\text{ND}} = \frac{l}{\pi R^2 R_{\text{ND}}} \quad (10)$$

By replacing of “ R_{ND} ” from eqn (8) into above equation, the electrical conductivity of extended CNT is estimated by:

$$\sigma_{\text{ND}} = \frac{l}{\pi R^2 \left[\frac{d}{\sigma_N 3 R^2 \exp(-2d)} + \frac{l}{\pi R^2 \sigma_N} \right]} \quad (11)$$

which presents the electrical conductivity of CNT and tunneling distance by a simple model. Now, the calculated conductivity for extended CNT can be applied in a developed model to estimate the conductivity of PCNT assuming tunneling mechanism.

Deng and Zheng¹⁴ proposed a model for electrical conductivity of PCNT reinforcing with randomly straight CNT after percolation threshold as:

$$\sigma = \sigma_0 + \frac{f \phi_f \sigma_N}{3} \quad (12)$$

where “ σ_0 ” is conductivity of polymer matrix, “ f ” is the percentages of networked CNT and “ ϕ_f ” is filler volume fraction. The very low level of “ σ_0 ” can be deleted from this model.

By substituting of “ σ_{ND} ” from eqn (11) into above equation, it is possible to calculate the conductivity of PCNT by tunneling effect as:

$$\sigma = \frac{f \phi_f l \sigma_N}{\frac{3d}{\exp(-2d)} + 3l} \quad (13)$$

which expresses the tunneling conductivity of PCNT as a function of CNT and network properties. However, this model does not regard the influences of interphase and CNT curvature on the conductivity, while these terms significantly change the percolation threshold and the percentages of networked filler.

The percolation threshold for CNT in PCNT containing random dispersion of nanoparticles was proposed³³ as:

$$\phi_p = \frac{V}{V_{\text{ex}}} \quad (14)$$

where “ V ” and “ V_{ex} ” denote the volume and excluded volume of CNT, respectively. The excluded volume includes the volume nearby nanotubes into which the center of a same particle cannot arrive.

“ V ” and “ V_{ex} ” in for random distribution of CNT in PCNT were expressed³³ as:

$$V = \pi R^2 l + (4/3)\pi R^3 \quad (15)$$

$$V_{\text{ex}} = \frac{32}{3}\pi R^3 \left[1 + \frac{3}{4} \left(\frac{l}{R} \right) + \frac{3}{32} \left(\frac{l}{R} \right)^2 \right] \quad (16)$$

However, the interphase layer surrounding CNT speeds up the development of a conductive network in PCNT which should be taken into account in percolation threshold. The interphase zones decrease the excluded volume³⁰ as:

$$V_{\text{ex}} = \frac{32}{3}\pi(R+t)^3 \left[1 + \frac{3}{4} \left(\frac{l}{R+t} \right) + \frac{3}{32} \left(\frac{l}{R+t} \right)^2 \right] \quad (17)$$

where “ t ” is interphase thickness.

Moreover, the enormous aspect ratio of CNT (ratio of length to diameter) produces waviness in CNT which decreases their effectiveness. An equivalent length as “ l_{eq} ” can be considered for curved nanotubes based on Fig. 2a. A waviness factor can be also defined as:

$$u = \frac{l}{l_{\text{eq}}} \quad (18)$$

where $u = 1$ shows the straight CNT, *i.e.* no waviness, but the higher levels of “ u ” indicate more waviness and less effective length.

When “ l_{eq} ” as the effective length of waved CNT is supposed in eqn (17) by $l_{\text{eq}} = l/u$, the excluded volume assuming interphase and CNT waviness is presented as:

$$V_{\text{ex}} = \frac{32}{3}\pi(R+t)^3 \left[1 + \frac{3}{4} \left(\frac{l/u}{R+t} \right) + \frac{3}{32} \left(\frac{l/u}{R+t} \right)^2 \right] \quad (19)$$

Also, the waviness does not affect the volume of CNT.

Now, the percolation threshold by the influences of interphase and waviness can be suggested as:

$$\phi_p = \frac{\pi R^2 l + (4/3)\pi R^3}{\frac{32}{3}\pi(R+t)^3 \left[1 + \frac{3}{4} \left(\frac{l/u}{R+t} \right) + \frac{3}{32} \left(\frac{l/u}{R+t} \right)^2 \right]} \quad (20)$$

It will be shown in the next section that this equation can suggest useful predictions for percolation threshold of nanoparticles in PCNT.

CNT and surrounding interphase can be included in effective CNT (Fig. 2b) which change the general properties of PCNT. The effective volume fraction of effective CNT assuming the roles of interphase and curvature¹⁵ can be expressed as:

$$\phi_{\text{eff}} = \frac{(R+t)^2(l/u + 2t)}{R^2 l/u} \phi_f \quad (21)$$

Additionally, only a number of CNT are employed in the continuous network after percolation, while others are dispersed in PCNT. “ f ” parameter as the percentages of percolated CNT¹⁵ is calculated by:



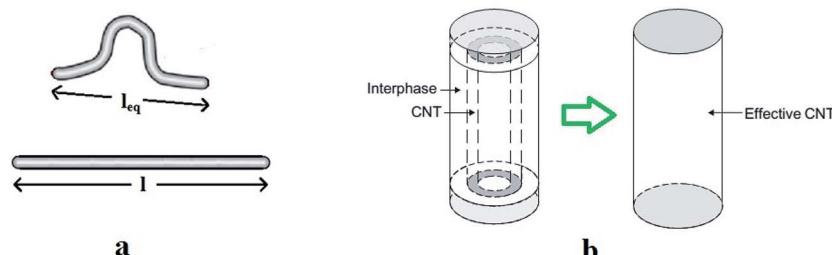


Fig. 2 (a) waved and straight CNT and (b) effective nanotube assuming interphase.¹⁵

$$f = \frac{\phi_{\text{eff}}^{1/3} - \phi_{\text{p}}^{1/3}}{1 - \phi_{\text{p}}^{1/3}} \quad (22)$$

It was also indicated that the curvature of CNT deteriorates its nature conductivity.¹⁴ The role of waviness in “ σ_{N} ” parameter is considered as:

$$\sigma_{\text{N}} = \frac{\sigma_{\text{N}}}{u} \quad (23)$$

The suggested equations for “ f ”, “ ϕ_{eff} ” and “ σ_{N} ” terms can be used in eqn (13) to predict the electrical conductivity of PCNT based on tunneling mechanism by the roles of interphase, waviness and tunneling distance.

3 Results and discussion

The suggested methodology for tunneling conductivity of PCNT can be examined by experimental results. Too, the efficiencies of parameters on the conductivity of PCNT can be revealed by the suggested equations.

Fig. 3 demonstrates the experimental results and predictions for epoxy/single walled CNT (SWCNT) ($R = 1 \text{ nm}$, $l = 2 \mu\text{m}$, $u = 1.6$),³⁴ epoxy/multi walled CNT (MWCNT) ($R = 8 \text{ nm}$, $l = 30 \mu\text{m}$, $u = 1.2$),³⁵ ultrahigh molecular weight polyethylene/MWCNT ($R = 8 \text{ nm}$, $l = 8 \mu\text{m}$, $u = 1.2$)³⁶ and polycarbonate/acrylonitrile butadiene styrene/MWCNT ($R = 5 \text{ nm}$, $l = 1.5 \mu\text{m}$, $u = 1.2$).¹⁰ The nature conductivity of both SWCNT and MWCNT are assumed as 10^6 S m^{-1} . A good agreement between the measurements of conductivity and the calculations are

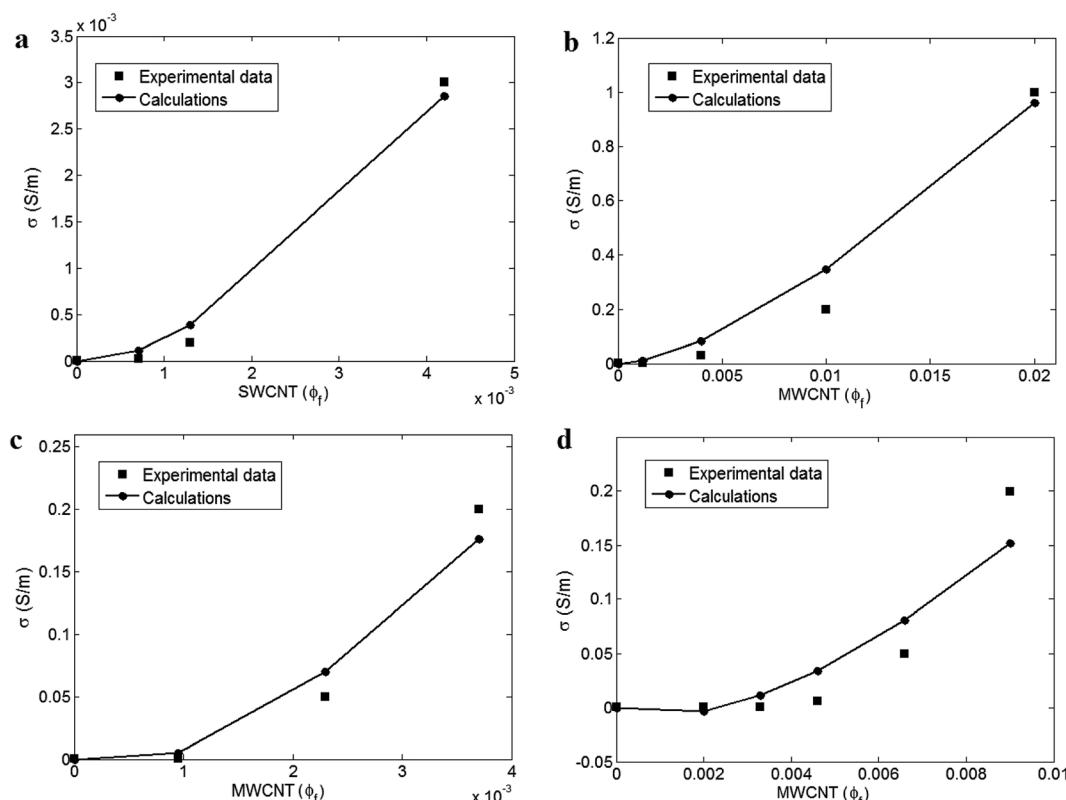


Fig. 3 Comparison between experimental results and predictions for (a) epoxy/SWCNT,³⁴ (b) epoxy/MWCNT,³⁵ (c) ultrahigh molecular weight polyethylene/MWCNT³⁶ and (d) polycarbonate/acrylonitrile butadiene styrene/MWCNT¹⁰ samples.



observed in all samples demonstrating the predictability of the suggested model for tunneling mechanism of electrical conductivity in PCNT. Therefore, the presented model can estimate the electrical conductivity of PCNT by tunneling mechanism assuming the influences of CNT curvature, interphase surrounding nanoparticles and tunneling distance.

The correct predictions of model indicate the formation of interphase in PCNT samples. The values of interphase thickness (t) can be obtained by comparison of experimental percolation threshold with the calculations of eqn (20). The epoxy/SWCNT, epoxy/MWCNT, ultrahigh molecular weight polyethylene/MWCNT and polycarbonate/acrylonitrile butadiene styrene/MWCNT samples show “ ϕ_p ” levels of 0.0003, 0.0002, 0.0007 and 0.002 by the experimental levels of conductivity, respectively. Applying eqn (20), the best values of “ t ” are obtained as 3, 7, 7 and 5 for these samples, correspondingly. So, it is concluded that eqn (20) is valid, because it can predict the percolation level of PCNT by logical interphase thickness. Moreover, it is possible to compare the thickness of interphase in the samples which depends on the interfacial properties,³⁷ *i.e.* a thicker interphase shows a stronger interaction/bonding between polymer matrix and nanoparticles.

By the properties of CNT and “ t ” values, the values of “ d ” can be calculated. The predictions suggest $d = 9.7, 8.5, 7.4$ and 7.4 nm for epoxy/SWCNT, epoxy/MWCNT, ultrahigh molecular weight polyethylene/MWCNT and polycarbonate/acrylonitrile butadiene styrene/MWCNT samples, respectively. The maximum allowed range for tunneling distance between nanotubes was reported as 10 nm.³⁸ As a result, the suggested model shows proper calculations of tunneling distance for the reported samples confirming its predictability. Conclusively, the suggested methodology can predict the percolation threshold, interphase thickness and tunneling distance by the measurements of electrical conductivity of PCNT.

The effects of different parameters on the electrical conductivity of PCNT can be investigated by the suggested model. In all calculations, the conductivity of CNT is considered as 10^6 S m⁻¹.

Fig. 4 illustrates the roles of “ ϕ_f ” and “ l ” parameters in the predicted conductivity at $R = 10$ nm, $t = 2$ nm, $u = 1.25$ and $d = 6$ nm. The best outputs are shown at the highest levels of “ ϕ_f ”

and “ l ” parameters, but the low ranges of these parameters decrease the conductivity. A poor conductivity around 0 is observed at $\phi_f < 0.01$ and $l < 10$ μm demonstrating the negative influences of low “ ϕ_f ” and “ l ” parameters on tunneling conductivity. On the other hand, the best conductivity as 25 S m⁻¹ is obtained at $\phi_f = 0.02$ and $l = 20$ μm . Therefore, the CNT concentration and length cause positive effects on the electrical conductivity of PCNT.

CNT commonly are much more conductive than polymer matrices. The conductivity of CNT commonly reaches to 10^6 S m⁻¹, while the conductivity of polymers is reported at about 10^{-14} S m⁻¹. So, the conductivity of PCNT significantly changes when a low amount of CNT is dispersed in polymer matrix, because a small number of CNT can form a percolated conductive network in polymer matrix which considerably improves the electrical conductivity of PCNT. Obviously, a higher loading of nanoparticles above percolation threshold enlarges the density of network which increases the charge transfer. Other models in literature also showed the similar effect of “ ϕ_f ” parameter on conductivity.^{16,32} In addition, long CNT raise the aspect ratio which decreases the needed number of CNT to form the conductive network. In fact, the longer CNT can be more easily interacted and connected in PCNT compared to short ones which ease their networking. Also, larger nanotubes can produce a bigger and denser network which quickly transports electrons whole of PCNT. The positive role of CNT length in the conductivity of PCNT has been reported in previous studies.³⁹ Accordingly, the suggested approach properly predicts the influences of “ ϕ_f ” and “ l ” parameters on the tunneling conductivity of PCNT.

The variations of conductivity at different levels of “ R ” and “ t ” parameters and average $\phi_f = 0.01$, $l = 10$ μm , $u = 1.25$ and $d = 6$ nm are observed in Fig. 5. The different roles of these parameters in conductivity are shown in this illustration, where low “ R ” and large “ t ” grow the conductivity. As observed, $\sigma = 7$ S m⁻¹ is achieved at $R = 10$ nm and $t = 4$ nm, while $R > 40$ nm and $t < 1$ nm significantly decrease the conductivity to about 0.6 S m⁻¹. As a result, a high tunneling conductivity is obtained by thin nanotubes and thick interphase, while thick CNT and absence or formation of thin interphase cause poor conductivity.

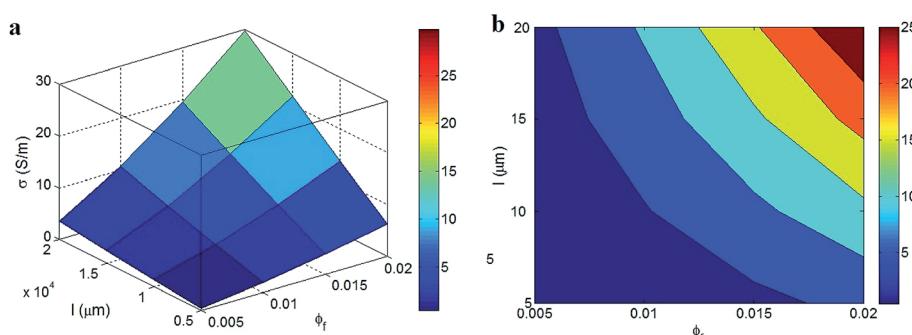


Fig. 4 (a) 3D and (b) contour plots to show the influences of “ ϕ_f ” and “ l ” parameters on tunneling conductivity of PCNT based on the suggested methodology at $R = 10$ nm, $t = 2$ nm, $u = 1.25$ and $d = 6$ nm.



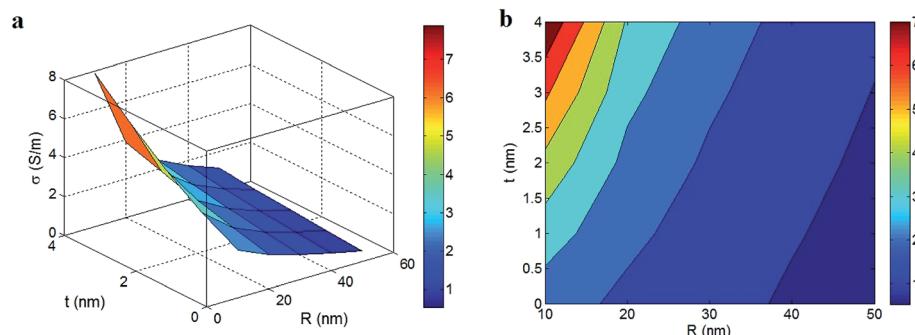


Fig. 5 The conductivity of PCNT as a function of “ R ” and “ t ” parameters at average $\phi_f = 0.01$, $l = 10 \mu\text{m}$, $u = 1.25$ and $d = 6 \text{ nm}$: (a) 3D and (b) contour patterns.

The effect of “ R ” parameter on the conductivity is attributed to its roles in percolation threshold (eqn (20)), effective filler fraction (eqn (21)) and the percentages of percolated filler (eqn (22)). In fact, thin nanotubes produce a low percolation level, more effective CNT and a high number of networked CNT. On the other hand, the conductivity of PCNT improves by poor percolation threshold and the high levels of effective and networked nanotubes. As a result, it is logical to obtain a strong conductivity by thin CNT. The previous articles have related the effect of CNT radius on percolation level and conductivity of PCNT by aspect ratio.²⁴ They reported a similar trend between percolation effect and CNT radius which confirms the suggested model.

The interphase thickness also plays a positive role in percolation threshold, effective CNT and the percentages of networked CNT. The interphase creates a layer around nanotubes which approaches the nanotubes and produces a conductive network at low filler fraction. In addition, a thick interphase thickens the effective CNT (Fig. 2b) which enlarges “ ϕ_{eff} ” parameter. Since the interphase employs many nanotubes for networking, it effectively increases the level of percolated CNT in the network. Accordingly, a high level of interphase thickness undoubtedly raises the conductivity of PCNT. The effects of interphase on percolation threshold and effective CNT were indicated in the literature,¹⁵ but its role in tunneling conductivity was not shown in the preceding works. Conclusively, the roles of “ R ” and “ t ” parameters in tunneling

conductivity of PCNT are well justified which show the correctness of the presented approach.

Fig. 6 exhibits the influences of “ u ” and “ d ” parameters on the tunneling conductivity of PCNT at $\phi_f = 0.01$, $R = 10 \text{ nm}$, $l = 10 \mu\text{m}$ and $t = 2 \text{ nm}$. As observed, the high levels of “ u ” and “ d ” cannot improve the conductivity of PCNT, but the least values of these parameters significantly improve the conductivity. As shown, $u > 2.5$ and $d < 5.2 \text{ nm}$ cannot promote the conductivity of PCNT, while $\sigma = 350 \text{ S m}^{-1}$ is achieved at $u = 1$ and $d = 4 \text{ nm}$. As a result, “ u ” and “ d ” parameters show direct effects on tunneling conductivity revealing that the conductivity is negatively related to the high levels of waviness and tunneling distance. It means that the small levels of these parameters are necessary in practice to obtain a high level of conductivity in PCNT.

“ u ” parameter determines the effective length of nanotubes in PCNT. A low level of “ u ” shows a poor waviness, but a high “ u ” demonstrates the more curvature of CNT in PCNT which decreases the effectiveness of CNT. A high level of waviness negatively affects the percolation threshold, effective nanoparticles and the number of CNT in the conductive network, due to the reduced length of an equivalent nanotube. Moreover, it was mentioned that the waviness reduces the conductivity of CNT according to eqn (23). Therefore, the waviness of CNT weakens the effects of CNT on the network levels which results in an insulate network. The detrimental effects of waviness on the electrical and mechanical properties of PCNT were also

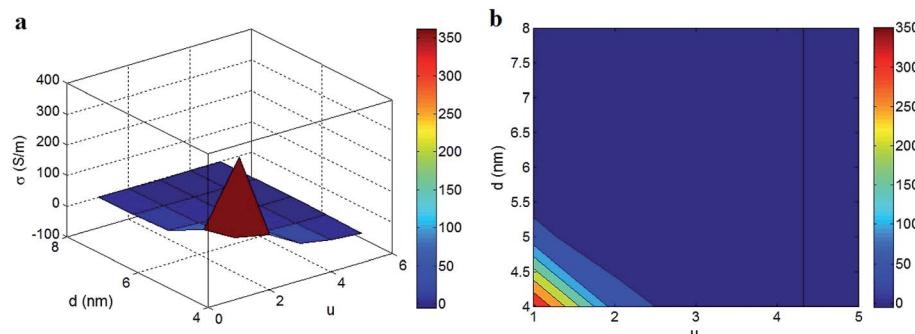


Fig. 6 (a) 3D and (b) contour plans for the roles of “ u ” and “ d ” parameters in the conductivity of PCNT at $\phi_f = 0.01$, $R = 10 \text{ nm}$, $l = 10 \mu\text{m}$ and $t = 2 \text{ nm}$.



reported in different papers.^{40,41} So, the suggested model properly shows the negative effect of waviness on the tunneling conductivity of PCNT.

The electron tunneling in PCNT extremely depends on the separation distance between CNT. When the separation distance is larger than a critical level, the nanotubes cannot cause tunneling and PCNT is insulated. However, the separate distance between CNT decreases when CNT volume fraction growths, where CNT can form conductive networks even by a distance of 2 nm.¹⁵ Moreover, the percolated CNT are still in electrical contact rather than physical attachments, due to van der Waals attractions among CNT. Therefore, the separation distance between nanotubes is an important parameter which manages the electrical conductivity, because the high distance cannot cause tunneling effect. In fact, “*d*” parameter is a border of conductivity and insulating in PCNT, as well observed by the suggested model. Some authors studied the tunneling distance, but they did not explicitly show the effect of this parameter on conductivity. However, the presented methodology reasonably reveals the role of tunneling distance in electrical conductivity of PCNT.

The variations of conductivity by different values of “ ϕ_p ” and “ ϕ_{eff} ” at $u = 1.25$, $l = 10 \mu\text{m}$ and $d = 6 \text{ nm}$ are also shown in Fig. 7. A low “ ϕ_{eff} ” mainly decreases the conductivity, but the small level of “ ϕ_p ” and the great value of “ ϕ_{eff} ” increase the conductivity. As a result, the lowest $\phi_{eff} < 0.014$ produces the slightest conductivity as about 0, while the best conductivity as 30 S m^{-1} is observed at $\phi_p = 0.001$ and $\phi_{eff} = 0.05$. Generally, it can be stated that “ ϕ_p ” and “ ϕ_{eff} ” parameters inversely and directly affect the conductivity, respectively.

“ ϕ_p ” is a critical fraction of nanoparticles which causes the conductivity in PCNT. Also, a low level of “ ϕ_p ” induces good effect on the fraction of percolated CNT demonstrating that a poor percolation threshold causes positive influences on the properties of network in PCNT. Accordingly, a slight percolation threshold clearly leads to a high level of conductivity in PCNT. The literature reports have extensively calculated the percolation threshold by a conventional power-law model,^{32,34} but they rarely evaluated the effect of percolation threshold on the network extent and electrical conductivity of PCNT. Generally, the suggested methodology shows an inverse relation between “ ϕ_p ” parameter and electrical conductivity which shows a good

agreement with other suggested models.³⁴ In addition, a high level of “ ϕ_{eff} ” is calculated by thin and long CNT as well as thick interphase based on eqn (21) and Fig. 2b. It is clear a better level of conductivity is achieved by a greater “ ϕ_{eff} ”, because it indicates the optimistic contributions of CNT and interphase in performances of PCNT. As a result, “ ϕ_{eff} ” parameter is a sign of effective CNT in PCNT which directly changes the conductivity of PCNT.

Fig. 8 also reveals the influences of “*f*” and “ σ_N ” parameters on the conductivity of PCNT at average levels of other factors. The best conductivity is obtained by the highest levels of these parameters. The maximum levels of $f = 0.5$ and $\sigma_N = 10^6 \text{ S m}^{-1}$ result in the best conductivity of 14 S m^{-1} . However, the little levels of these parameters as $f < 0.2$ and $\sigma_N < 3 \times 10^5 \text{ S m}^{-1}$ decrease the conductivity to about 0. Therefore, the conductivity of PCNT directly depends on the fraction of percolated network and the conductivity of CNT. These evidences indicate that the researchers should attempt to provide a high level of networked fraction and use super-conductive CNT to promote the conductivity of nanocomposites.

The electron transportation in PCNT is performed by the network of CNT. Clearly, a large and dense network can effectively transfer the electrons, while a poor network decreases the level of electron current in PCNT. As a result, the conductivity of PCNT highly depends on the network level, because it manages the electron transportation. A higher level of “*f*” shows the presence of more nanotubes in network phase which produces high conductivity, while a low “*f*” demonstrates the formation of a small network which negatively affects the conductivity. Some authors have reported the direct effects of network properties on the electrical conductivity of polymer nanocomposites.⁹

On the other hand, the electrical conductivity of PCNT reasonably depends on the nature conduction of CNT, because CNT conduction lonely determines the conductivity of filler networks and PCNT and polymer matrices are insulate. Accordingly, the higher-conductive CNT more improve the conductivity of PCNT, whereas a less filler conductivity cannot change the conductivity of produced composite. However, it was reported that the conductivity of CNT depends on their size, curvature and defects,⁴² where thin, straight and less-defective CNT show the best conduction. Therefore, it is important to provide thin, straight and perfective CNT to use the full

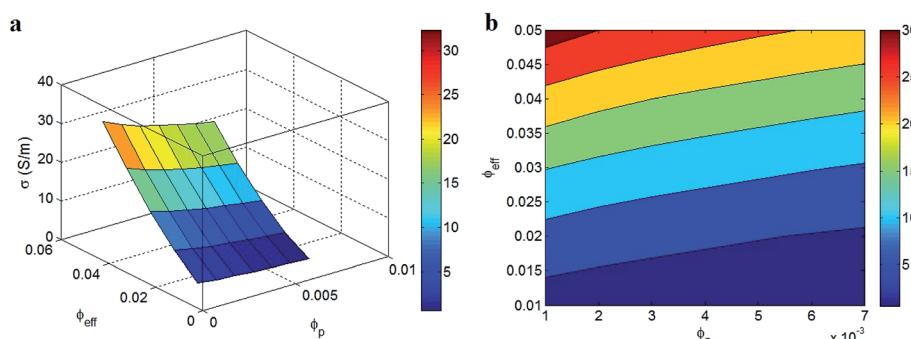


Fig. 7 The tunneling conductivity of PCNT as a function of “ ϕ_p ” and “ ϕ_{eff} ” parameters at $u = 1.25$, $l = 10 \mu\text{m}$ and $d = 6 \text{ nm}$ by (a) 3D and (b) contour plots.



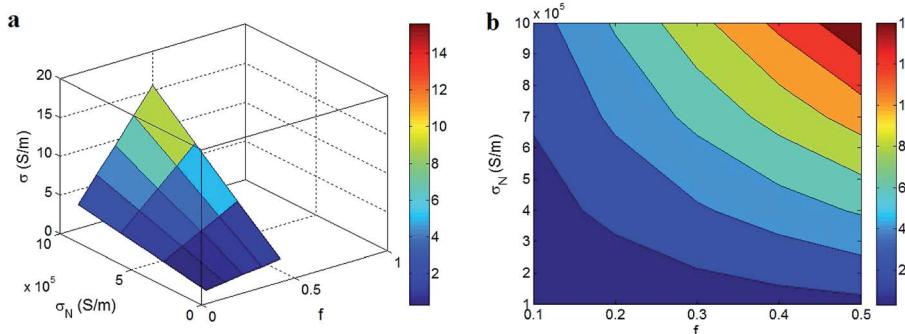


Fig. 8 The conductivity of PCNT at different levels of "f" and " σ_N " parameters at $\phi_f = 0.01$, $R = 10$ nm, $l = 10$ μ m, $t = 2$ nm, $u = 1.25$ and $d = 6$ nm.

advantages of nanoparticles such as big surface area and conductivity in PCNT. Generally, the influences of "f" and " σ_N " parameters on tunneling conductivity of PCNT are acceptable which confirm the predictions of the suggested approach.

4 Conclusions

A simple model was presented to predict the tunneling conductivity of polymer/CNT nanocomposites by assuming the effects of the tunneling distance, interphase, and CNT waviness. The conductivity of CNT and tunneling distance were considered by using an extended CNT. Moreover, the roles of interphase thickness and CNT waviness on the percolation threshold, effective filler fraction, and percentages of percolated CNT were considered in the suggested model.

The predictions of the suggested methodology agree with the experimental conductivity results. Also, it is possible to calculate some parameters, such as the percolation threshold, interphase thickness, and tunneling distance, by applying the experimental results to the suggested model. A poor conductivity near 0 is observed at $\phi_f < 0.01$ and $l < 10$ μ m, while the best conductivity (25 $S\ m^{-1}$) is obtained at the highest $\phi_f = 0.02$ and $l = 20$ μ m. Also, $\sigma = 7$ $S\ m^{-1}$ is obtained at $R = 10$ nm and $t = 4$ nm, whereas $R > 40$ nm and $t < 1$ nm result in $\sigma = 0.6$ $S\ m^{-1}$. Moreover, $u > 2.5$ and $d < 5.2$ nm cannot increase the conductivity of PCNT, while $\sigma = 350$ $S\ m^{-1}$ is attained at $u = 1$ and $d = 4$ nm. A low $\phi_{eff} < 0.014$ produces $\sigma = 0$, but the best conductivity (30 $S\ m^{-1}$) is observed at $\phi_p = 0.001$ and $\phi_{eff} = 0.05$. The best conductivity (14 $S\ m^{-1}$) is also obtained with the highest levels of $f = 0.5$ and $\sigma_N = 10^6$ $S\ m^{-1}$. However, small values of $f < 0.2$ and $\sigma_N < 3 \times 10^5$ $S\ m^{-1}$ result in $\sigma = 0$. Conclusively, the concentration, length, waviness, and conductivity of CNT, interphase thickness, effective filler fraction, and network density play direct roles in the tunneling conductivity of PCNT. Moreover, a high conductivity is obtained with thin CNT, a low tunneling distance, and a slight percolation threshold.

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References

- 1 E. N. Zare, M. M. Lakouraj, S. Ghasemi and E. Moosavi, Emulsion polymerization for the fabrication of poly(*o*-phenylenediamine)@ multi-walled carbon nanotubes nanocomposites: characterization and their application in the corrosion protection of 316L SS, *RSC Adv.*, 2015, **5**, 68788–68795.
- 2 S. V. Ebadi, A. Fakhrali, S. O. Ranaei-Siadat, A. A. Gharehaghaji, S. Mazinani, M. Dinari and J. Harati, Immobilization of acetylcholinesterase on electrospun poly(acrylic acid)/multi-walled carbon nanotube nanofibrous membranes, *RSC Adv.*, 2015, **5**, 42572–42579.
- 3 J. Yang, Y. Zhang, Z. Wang and P. Chen, Influences of high aspect ratio carbon nanotube network on normal stress difference measurements and extrusion behaviors for isotactic polypropylene nanocomposite melts, *RSC Adv.*, 2014, **4**, 1246–1255.
- 4 A. Rostami, M. Masoomi, M. J. Fayazi and M. Vahdati, Role of multiwalled carbon nanotubes (MWCNTs) on rheological, thermal and electrical properties of PC/ABS blend, *RSC Adv.*, 2015, **5**, 32880–32890.
- 5 M. M. Shokrieh and R. Rafiee, On the tensile behavior of an embedded carbon nanotube in polymer matrix with non-bonded interphase region, *Compos. Struct.*, 2010, **92**, 647–652.
- 6 Q.-Q. Ni, C.-s. Zhang, Y. Fu, G. Dai and T. Kimura, Shape memory effect and mechanical properties of carbon nanotube/shape memory polymer nanocomposites, *Compos. Struct.*, 2007, **81**, 176–184.
- 7 A. Abdolmaleki, S. Mallakpour and S. Borandeh, Amino acid-functionalized multi-walled carbon nanotubes for improving compatibility with chiral poly(amide-ester-imide) containing L-phenylalanine and L-tyrosine linkages, *Appl. Surf. Sci.*, 2013, **287**, 117–123.
- 8 C. Choi, S. Park and H. Choi, Carbon nanotube/polyaniline nanocomposites and their electrorheological characteristics under an applied electric field, *Curr. Appl. Phys.*, 2007, **7**, 352–355.
- 9 F. Du, R. C. Scogna, W. Zhou, S. Brand, J. E. Fischer and K. I. Winey, Nanotube networks in polymer nanocomposites: rheology and electrical conductivity, *Macromolecules*, 2004, **37**, 9048–9055.



10 S. Maiti, N. K. Shrivastava and B. Khatua, Reduction of percolation threshold through double percolation in melt-blended polycarbonate/acrylonitrile butadiene styrene/multiwall carbon nanotubes elastomer nanocomposites, *Polym. Compos.*, 2013, **34**, 570–579.

11 M. L. Clingerman, J. A. King, K. H. Schulz and J. D. Meyers, Evaluation of electrical conductivity models for conductive polymer composites, *J. Appl. Polym. Sci.*, 2002, **83**, 1341–1356.

12 L. Chang, K. Friedrich, L. Ye and P. Toro, Evaluation and visualization of the percolating networks in multi-wall carbon nanotube/epoxy composites, *J. Mater. Sci.*, 2009, **44**, 4003–4012.

13 S. Kara, E. Arda, F. Dolastir and Ö. Pekcan, Electrical and optical percolations of polystyrene latex-multiwalled carbon nanotube composites, *J. Colloid Interface Sci.*, 2010, **344**, 395–401.

14 F. Deng and Q.-S. Zheng, An analytical model of effective electrical conductivity of carbon nanotube composites, *Appl. Phys. Lett.*, 2008, **92**, 071902.

15 C. Feng and L. Jiang, Micromechanics modeling of the electrical conductivity of carbon nanotube (CNT)–polymer nanocomposites, *Composites, Part A*, 2013, **47**, 143–149.

16 T. Takeda, Y. Shindo, Y. Kuronuma and F. Narita, Modeling and characterization of the electrical conductivity of carbon nanotube-based polymer composites, *Polymer*, 2011, **52**, 3852–3856.

17 Y. Zare, Development of Nicolais–Narkis model for yield strength of polymer nanocomposites reinforced with spherical nanoparticles, *Int. J. Adhes. Adhes.*, 2016, **70**, 191–195.

18 Y. Zare, Effects of imperfect interfacial adhesion between polymer and nanoparticles on the tensile modulus of clay/polymer nanocomposites, *Appl. Clay Sci.*, 2016, **129**, 65–70.

19 P. Jahanmard and A. Shojaei, Mechanical properties and structure of solvent processed novolac resin/layered silicate: development of interphase region, *RSC Adv.*, 2015, **5**, 80875–80883.

20 Y. Zare, “*a*” interfacial parameter in Nicolais–Narkis model for yield strength of polymer particulate nanocomposites as a function of material and interphase properties, *J. Colloid Interface Sci.*, 2016, **470**, 245–249.

21 Y. Zare, Modeling approach for tensile strength of interphase layers in polymer nanocomposites, *J. Colloid Interface Sci.*, 2016, **471**, 89–93.

22 Y. Zare, A Two-Step Method Based on Micromechanical Models to Predict the Young's Modulus of Polymer Nanocomposites, *Macromol. Mater. Eng.*, 2016, **301**, 846–852.

23 B. Mortazavi, J. Bardon and S. Ahzi, Interphase effect on the elastic and thermal conductivity response of polymer nanocomposite materials: 3D finite element study, *Comput. Mater. Sci.*, 2013, **69**, 100–106.

24 Y. Zare, An approach to study the roles of percolation threshold and interphase in tensile modulus of polymer/clay nanocomposites, *J. Colloid Interface Sci.*, 2017, **486**, 249–254.

25 Y. Zare, The roles of nanoparticles accumulation and interphase properties in properties of polymer particulate nanocomposites by a multi-step methodology, *Composites, Part A*, 2016, **91**, 127–132.

26 Y. Zare and K. Y. Rhee, Accounting the reinforcing efficiency and percolating role of interphase regions in the tensile modulus of polymer/CNT nanocomposites, *Eur. Polym. J.*, 2017, 389–397.

27 Y. Zare and K. Y. Rhee, The mechanical behavior of CNT reinforced nanocomposites assuming imperfect interfacial bonding between matrix and nanoparticles and percolation of interphase regions, *Compos. Sci. Technol.*, 2017, **144**, 18–25.

28 Y. Zare and K. Y. Rhee, Development of a conventional model to predict the electrical conductivity of polymer/carbon nanotubes nanocomposites by interphase, waviness and contact effects, *Composites, Part A*, 2017, 305–312.

29 R. Qiao and L. C. Brinson, Simulation of interphase percolation and gradients in polymer nanocomposites, *Compos. Sci. Technol.*, 2009, **69**, 491–499.

30 S. C. Baxter and C. T. Robinson, Pseudo-percolation: Critical volume fractions and mechanical percolation in polymer nanocomposites, *Compos. Sci. Technol.*, 2011, **71**, 1273–1279.

31 N. Ryvkina, I. Tchmutin, J. Vilčáková, M. Pelíšková and P. Sáha, The deformation behavior of conductivity in composites where charge carrier transport is by tunneling: theoretical modeling and experimental results, *Synth. Met.*, 2005, **148**, 141–146.

32 S. Maiti, S. Suin, N. K. Shrivastava and B. Khatua, Low percolation threshold in polycarbonate/multiwalled carbon nanotubes nanocomposites through melt blending with poly (butylene terephthalate), *J. Appl. Polym. Sci.*, 2013, **130**, 543–553.

33 L. Berhan and A. Sastry, Modeling percolation in high-aspect-ratio fiber systems. I. Soft-core *versus* hard-core models, *Phys. Rev. E*, 2007, **75**, 041120.

34 F. H. Gojny, M. H. Wichmann, B. Fiedler, I. A. Kinloch, W. Bauhofer, A. H. Windle and K. Schulte, Evaluation and identification of electrical and thermal conduction mechanisms in carbon nanotube/epoxy composites, *Polymer*, 2006, **47**, 2036–2045.

35 Y. J. Kim, T. S. Shin, H. Do Choi, J. H. Kwon, Y.-C. Chung and H. G. Yoon, Electrical conductivity of chemically modified multiwalled carbon nanotube/epoxy composites, *Carbon*, 2005, **43**, 23–30.

36 M. Lisunova, Y. P. Mamunya, N. Lebovka and A. Melezhyk, Percolation behaviour of ultrahigh molecular weight polyethylene/multi-walled carbon nanotubes composites, *Eur. Polym. J.*, 2007, **43**, 949–958.

37 Y. Zare, Development of Halpin–Tsai model for polymer nanocomposites assuming interphase properties and nanofiller size, *Polym. Test.*, 2016, **51**, 69–73.

38 J. Li, P. C. Ma, W. S. Chow, C. K. To, B. Z. Tang and J. K. Kim, Correlations between percolation threshold, dispersion state, and aspect ratio of carbon nanotubes, *Adv. Funct. Mater.*, 2007, **17**, 3207–3215.



39 R. Arenhart, G. Barra and C. Fernandes, Simulation of percolation threshold and electrical conductivity in composites filled with conductive particles: Effect of polydisperse particle size distribution, *Polym. Compos.*, 2016, **37**, 61–69.

40 D.-L. Shi, X.-Q. Feng, Y. Y. Huang, K.-C. Hwang and H. Gao, The effect of nanotube waviness and agglomeration on the elastic property of carbon nanotube-reinforced composites, *J. Eng. Mater. Technol.*, 2004, **126**, 250–257.

41 R. Rafiee, Influence of carbon nanotube waviness on the stiffness reduction of CNT/polymer composites, *Compos. Struct.*, 2013, **97**, 304–309.

42 C. J. Lee, R. Salehiyan, D. S. Ham, S. K. Cho, S.-J. Lee, K. J. Kim, Y. Yoo, K. Hyun, J. H. Lee and W. J. Choi, Influence of carbon nanotubes localization and transfer on electrical conductivity in PA66/(PS/PPE)/CNTs nanocomposites, *Polymer*, 2016, **84**, 198–208.

