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In situ synthesis and immobilization of a Cu(II)–pyridyl complex on silica microspheres as a novel Fenton-like catalyst for RhB degradation at near-neutral pH†

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A highly efficient Fenton-like catalyst was successfully developed by covalently immobilizing a Cu(II)–pyridine group complex onto silica microspheres. The catalyst was characterized by SEM, FTIR and XPS measurements. The catalytic activity was evaluated by heterogeneous degradation of Rhodamine B (RhB) with H₂O₂ in the dark. The effects of pH, catalyst loading, H₂O₂ concentration, initial dye concentration, and temperature on the degradation kinetics were investigated to optimize operational variables and find the potential mechanisms. It was found that the optimum pH of medium was near neutral, at which over 98% of RhB (5–7.5 mg L⁻¹) was efficiently decolorized in 6 hours with 2 g L⁻¹ catalyst and 200 mg L⁻¹ H₂O₂. The TOC removal of RhB (10 mg L⁻¹) also reached 72% after the reaction duration. Meanwhile, the acute toxicity of RhB to marine bacteria *Vibrio fischeri* was almost completely eliminated. The degradation of RhB could be well described with a pseudo-first order kinetic model. The reaction activation energy was approximately 38.60 kJ mol⁻¹. Fluorescence analysis and free radical scavenging experiments were performed, and revealed that the hydroxyl radical was the main active species for RhB degradation. The stability of the catalyst was confirmed by insignificant leaching of copper species and loss of activity after four cycles. Based on these results and the literature, a possible mechanism for RhB degradation was proposed.

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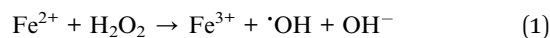
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1. Introduction

Recently, the presence of refractory organic species in wastewater streams has raised a severe challenge to the conventional biological treatment methods due to their high chemical stability and/or low biodegradability. Therefore, it is highly in demand to develop new technologies which are able to decontaminate biorefractory molecules in wastewater streams.^{1,2} Many studies up to now have revealed that the advanced oxidation process is a good alternative for treating a wide range and variety of recalcitrant and/or toxic pollutants in the environment.^{3,4} Advanced oxidation processes are defined as processes that *in situ* generate hydroxyl radicals (primarily but not exclusively) to oxidize the majority of the complex chemicals present in the effluent water. The ·OH radical is a powerful oxidizing reagent, which has a very high standard redox potential (1.9–2.8 V), bimolecular reaction rate constants (10⁸–

10¹¹ M⁻¹ s⁻¹) and non-selective reactivity, and thus could quickly decompose various organic compounds into smaller molecules and even into less harmful substances such as CO₂, H₂O and inorganic salts.⁴ Over the past decades, a variety of AOPs such as photocatalysis, radiation, sonolysis, and Fenton, ozone, and electrochemical oxidation have been established to destroy hazardous pollutants in the environment.⁴

Among various AOPs, Fenton's oxidation has received great attention because of its high efficiency, ease of operation and relatively low operating costs.^{5–7} The traditional Fenton oxidation process is based on soluble ferrous ion and hydrogen peroxide to generate highly oxidative species, *i.e.*, hydroxyl radicals, according to the Haber–Weiss mechanism following the reaction:^{6–8}



However, homogeneous Fenton process suffers from several drawbacks like difficult regeneration of catalyst, highly acidic environment required for the reaction (pH 2–4), and the necessity of dispose of iron-containing sludge before discharging to receiving waters.^{5,7} To address these problems, much effort has been devoted to developing the heterogeneous Fenton-like catalysts. A wide range of solid materials, such as

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iron-containing minerals,³ silica supported iron,⁹ iron-pillared clays,^{3,10} iron-exchanged zeolites and resins,^{11,12} iron oxides,¹³ Fe^{III}-containing phosphotungstate,¹⁴ and iron-based metal-organic framework¹⁵ have been tested as Fenton catalysts to accelerate the catalytic decomposition of H₂O₂.

Although those heterogeneous Fenton agents generally could be applied in a wide-working pH range (pH 3–7), many of them presented weak catalytic activity¹⁶ and the better catalytic performance were often need the help of ultrasonic and/or UV light irradiation to accelerate the electron transfer at the interface of catalyst and water.^{2,3,17} Therefore, searching for the new Fenton-like catalysts with the wider pH range, higher activity, better stability and reusability for decontaminating recalcitrant organic pollutants in water is still hot research topics and challenging tasks.

In addition to the ferrous ion (Fe²⁺), a number of other metal ions, including Cu⁺, Ti³⁺, Cr⁺, Co²⁺, were found to have the oxidative features of Fenton's reagent in the presence of hydrogen peroxide.^{2,18,19} Cu²⁺/H₂O₂ systems have been extensively used in organic synthesis.^{20,21} Cu²⁺/H₂O₂ systems were also employed to decompose atrazine, polycyclic aromatic hydrocarbons, and olive mill wastewater.^{22–24} In addition, Lim and Bali *et al.* reported that the H₂O₂/pyridine/Cu(II) systems were very effective in the decolorization of synthetic dyes.^{25,26} Moreover, copper and copper complexes supported on different supports were employed as potentially catalysts for H₂O₂ decomposition and the oxidative degradation of organic contaminants and dyes as well.^{27–30} Compared to the Fe²⁺/H₂O₂ system working only in the acidic condition, the Cu²⁺-based catalysts often work over a broader pH range.² Furthermore, copper complexes with organic degradation intermediates are easily decomposed by ·OH, whereas the corresponding Fe³⁺ complexes are highly stable.²

Inspired by the advantage of Cu-base Fenton-like catalysts, especially the high decolorization efficiency of H₂O₂/pyridine/Cu²⁺ system for dye wastewater and the non-enzymatic biological system consisting of Cu²⁺, pyridine, and inorganic or organic peroxides was able to depolymerise synthetic lignin,³¹ we expected to construct a new heterogeneous catalyst through anchoring pyridine groups onto silica microspheres followed by post-coordination with copper ions. Compared with the homogenous pyridine and Cu²⁺ system, the prepared catalyst would be easy recycled and could reduce the secondary pollution caused by copper ions and pyridine. The prepared catalyst was characterized by scanning electron microscopy (SEM), Fourier transform infrared (FTIR), X-ray photoelectron spectroscopy (XPS) analyses. The catalytic activity of the catalyst was evaluated by degradation of dye RhB in the presence of hydrogen peroxide. Rhodamine B (RhB) is chosen as a representative target pollutant based on the considerations as follows: (1) RhB is a widely used in industrial case and laboratory study. Its toxic and carcinogenic effects have been experimentally proven; (2) RhB is very stable under various pH with considerably high resistance to oxidative and photo degradation.^{9,32} The influences of catalyst loading, hydrogen peroxide and dye concentrations, solution pH, and reaction temperature on RhB degradation efficiency and kinetics were investigated in

detail. The mineralization and detoxification of RhB solution by the prepared catalyst/H₂O₂ system were also investigated. The stability of the catalyst was evaluated by repeating the catalytic degradation of RhB over the prepared catalyst/H₂O₂ system and determined the leached copper ions. The active species involved in the reaction were confirmed by the photoluminescence technique and the radical scavenging experiments. Moreover, a possible mechanism for RhB degradation over the prepared catalyst and H₂O₂ was discussed as well. To the best of our knowledge, no study so far has succeeded in designing a heterogeneous Fenton-like catalyst composed of copper and pyridine group for Fenton process.

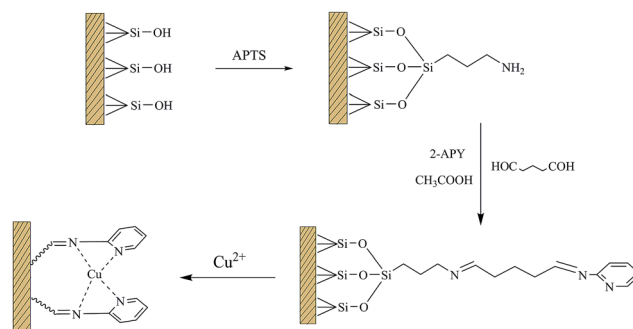
2. Experimental

2.1 Materials and reagents

All chemicals were used as received without further purification. 2-Aminopyridine (2-APY, >99.0%), and coumarin (>98.0%) were obtained from J&K Scientific Co. (China). Tetraethoxysilane (TEOS, >97.0%), glutaraldehyde (AR, 50% in H₂O), dye Rhodamine B (AR grade), hydrogen peroxide (30 wt% aqueous solution), cupric sulfate pentahydrate (>99.0%), 3-aminopropyltriethoxysilane (APTS, >98%), and other chemicals were procured from Sinopharm Chemical Reagent Co., Ltd. (China). Deionized water obtained from the Millipore Mill-Q system was used throughout the study. Before use, the concentration of hydrogen peroxide was standardized by iodimetric titration using sodium thiosulfate standard solution.

2.2 Catalyst preparation

2.2.1 Synthesis of silica microsphere and the surface modified with APTS. The procedure used for preparing the Cu(II)-pyridyl complex immobilized silica microsphere heterogeneous catalyst is illustrated in Scheme 1. Firstly, silica gel microsphere was synthesized *via* a sol-gel process according to the literature.³³ Tetraethoxysilane (TEOS, 10 mL) was added dropwise to a solution containing ethanol (100 mL), water (10 mL) and aqueous ammonia (30 mL) under stirring at 40 °C for 22 h. The product was washed thoroughly with water and dried at 60 °C. Amine group was grafted on the surface of silica particles followed the method described by Hernández-Morales *et al.*³⁴



Scheme 1 Schematic representation of preparing process for Cu(II)-pyridyl complex immobilized on silica microspheres.



2.0 g of silica gel product was dispersed in 15 mL absolute ethanol and then 5 mL APTS dissolved in 15 mL acetonitrile was added. After ultrasonic treatment for 20 min, the suspensions was introduced into a 100 mL three-neck flask, and refluxed at 60 °C for 5 hours under mechanical stirring. The products were separated by centrifugation, washed with ethanol three times, and dried at 60 °C. The final products were denoted as SiO₂-NH₂.

2.2.2 Synthesis of Cu(II)-pyridyl complex immobilized silica microspheres.³⁵ To this end, 2.0 g of 2-APY dissolved in 50 mL absolute ethanol was transferred to 250 mL round-bottom flask, which contained 1.0 g of SiO₂-NH₂. The glutaraldehyde (4.22 mL) and glacial acetic acid (0.5 mL) were added into the suspensions. The reaction mixture was refluxed at 60 °C for 6 hours under vigorous stirring. Afterwards, the solid products were filtered, washed with ethanol and water successively. The silica particles grafted with pyridine groups were further contacted with CuSO₄ aqueous solution (80 mL, 0.1 mol L⁻¹) at 60 °C for 5 hours under continuous stirring. The resulting catalysts were collected, washed with deionized water, and dried at 80 °C for one day. The loading of copper on the catalyst was determined, which was 3.75 mmol g⁻¹.

2.3 Characterization

Scanning electron microscopy (SEM) was taken on a Hitachi S-570 microscope (Hitachi, Japan). Fourier transform infrared spectra (FTIR) of samples were recorded on a Bruker TENSIR 27 spectrometer (Bruker, Germany) using the pressed KBr disks. The X-ray photoelectron spectroscopy (XPS) was measured on a Thermo Scientific K-Alpha X-ray photoelectron Spectrometer (Thermo Fisher Scientific Ltd, UK) using a monochromatic Al K α irradiation and low-energy electron flooding for charge compensation. The binding energies were referenced to the C 1s peak at 284.8 eV.

2.4 Heterogeneous Fenton-like degradation of RhB

All experiments were carried out in a glass cylindrical reactor (100 mL) which was equipped with a double jacket for circulation of external thermostatic water to keep temperature of the solution at the desired values. The reactor was covered with Al foil to prevent exposure to light. Mixing was achieved by vigorous magnetic stirring at about 500 rpm to avoid concentration gradients. To start each experiment, an appropriate volume of stock solution of RhB and a certain amount of the catalyst were placed into the reactor together, then diluted with deionized water to 50 mL. The pH values of the reaction solutions were adjusted to the desired levels using 1.0 mol L⁻¹ NaOH or HClO₄ solution. After the suspension was thoroughly mixed and reached temperature equilibrium, a required amount of H₂O₂ was added to initiate the reaction. At given time intervals, the samples were taken out from the reactor and centrifuged for separation of the suspended solids, and the supernatant solutions were used to measure the residual RhB concentrations after filtering through a 0.45 μ m PVDF membrane. Each experiment was carried out at least thrice to ensure reproducibility of the results, and the average value was reported.

During examination of the effects of various operating variables on RhB degradation, the concentration of dye was ranged

from 2.5 to 12.5 mg L⁻¹, which is based on the consideration that 5 mg L⁻¹ of RhB was used in several studies on its degradation using AOPs.^{10,17} It is well-known that the optimum pH for the traditional Fenton oxidation process is around 2.8. However, dye waste effluent is discharged at different pH. Consequently, the effect of pH value was explored in the range of 3 to 9. As for the effect of catalyst loading on RhB degradation, the catalysts concentration of 0.5–4 g L⁻¹ was chosen based on many studies on Fenton-like processes.⁵ The concentrations of hydrogen peroxide vary in a large range in the different Fenton or Fenton-like processes.^{5,36} Thus, we changed it from 50 to 300 mg L⁻¹ in this study. As the high reaction temperature means large energy consumption, thus only 20–40 °C reaction temperatures were tested.

The stability of catalyst was evaluated by a sequential cycle experiment. After completion of the reaction, the catalysts were filtered, washed with water, and dried at 70 °C. The recovered catalysts were used in the next reaction under the identical experimental conditions.

2.5 Sample analysis

The concentration of RhB was detected using an ultraviolet-visible spectrophotometer (754 PC, Shanghai Spectrum) at wavelength of 553 nm. Total organic carbon (TOC) was measured with a Shimadzu TOC-L CPN CN200 analyzer. The leached copper ions in the reaction solution after the catalytic degradation of RhB were measured by atomic absorption spectroscopy (Shimadzu AARM-6 spectrophotometer). Hydroxyl radical ([•]OH) was detected by the coumarin luminescence probing technique that is based on the reaction of a poor fluorescent molecule coumarin with [•]OH to generate a highly fluorescent 7-hydroxycoumarin.³⁷ The experimental procedure was similar to that used in evaluating catalytic activity of the catalyst except that a certain amount of coumarin (1 \times 10⁻³ mol L⁻¹) instead of RhB was added into reaction solution. 7-Hydroxycoumarin was monitored using a HITACHI F-4500 fluorescence spectrophotometer at the excitation wavelength of 335 nm. H₂O₂ concentration was measured by DPD method.³⁸

2.6 Toxicity test

The toxicity analysis was carried out on DeltaTox toxicity analyzer (Strategic Diagnostics Inc., US) using luminescent marine bacterium *Vibrio fischeri* as the test species, and the 81.9% test protocol was followed. Prior to toxicity analysis, the sample was pre-prepared according to the standard operating procedure as described in the Microtox manual. The residual hydrogen peroxide was removed from the solution using catalase. After 5 min incubation of the samples and luminescent bacteria at 15 °C, the photobacteria light emission was determined. At the same time, the control samples were carried out in parallel. The toxicity is quantified as the relative decrease of the photobacteria light emission with respect to the sample control that only contained MicroTox diluent.



3. Results and discussion

3.1 Characterization of the catalyst

The prepared silica particles were nearly spherical in shape with a mean diameter of 0.82 μm (Fig. S1 and S2 in the ESI[†]). After silica particles reacted with APTS, amine groups were anchored on their surface through a silylation reaction between the surface hydroxyl groups and APTS. This is confirmed by appearance of N–H deformation peak at 1556 cm^{-1} and C–H ($-\text{CH}_2\text{CH}_2\text{CH}_2\text{NH}_2$ groups) stretching peak at 2941 cm^{-1} in aminosilane treatment silica particles (Fig. 1b).^{34,39,40} It is well-known that amino groups can easily react with aldehyde to form Schiff-base, as shown in Scheme 1. FT-IR spectrum of 2-APY modified silica particles in Fig. 1c displays a C=N (Schiff base) absorption peak at 1654 cm^{-1} , and C=N and C=C stretching vibration peaks at 1477 cm^{-1} .^{41–43} The C=N stretching vibration in pyridine ring was reported locating in the range 1569–1571 cm^{-1} .^{35,41} Comparing absorption bands of 2-APY modified silica particles with its precursor in this region, the stronger absorption can be seen for 2-APY modified silica particles. This finding may suggest that C=N vibration of pyridine exists. Moreover, the disappearance of the N–H deformation peak at 1556 cm^{-1} in 2-APY modified silica particles also implies that the pyridine ring has successfully grafted on silica particles through condensation reaction between amine groups and aldehyde groups of glutaraldehyde. After 2-APY modified silica particles were contacted with CuSO_4 aqueous solution, the silica particles turned from colorless to pale blue. The FT-IR spectra of 2-APY modified silica particles before and after loading copper ions are shown in Fig. 1c and d. It can be seen that the 2-APY modified silica particles lost the peaks at 1654 cm^{-1} and at same time appeared a new peak at 1578 cm^{-1} after loading of copper ions (Fig. 1d). In addition, an absorption peak in 2-APY modified silica particles shifts from 1477 cm^{-1} to 1483 cm^{-1} after reaction with copper ions. These results may indicate that N atoms in pyridine ring and in Schiff base took part in coordination with copper ions.

Fig. 2 shows the typical results of XPS spectra for 2-APY modified silica before and after loading copper ions. The peaks

at bond energy (BE) of 103 eV, 285 eV, 400 eV, and 534 eV correspond to the Si 2p, C 1s, N 1s, and O 1s spectra, respectively, which exist in all samples (Fig. 2a). It is observed that after loading Cu(II) , a new peak with a binding energy of 934.5 eV appeared, which could be assigned to the Cu 2p_{3/2} orbital. The high resolution XPS spectra of N 1s and Cu 2d regions were used to further clarify the surface functional groups and chemical state of copper element. Fig. 2b shows that the strong Cu 2p_{1/2} and Cu 2p_{3/2} peaks occurred at 955.7 and 935.9 eV. The BE of 935.9 eV for Cu 2p_{3/2} is in agreement with its oxidation states +2, which is further confirmed by two additional satellite bands in the 941–946 eV and 961–965 eV regions.^{44,45} N 1s core-level spectra are larger bands. The fitting of these peaks shows the presence of various contributions with BEs of 398.8 eV and 400.3 eV in 2-APY modified silica particles (Fig. 2c). The peak with BE of 398.8 eV can be assigned to nitrogen in pyridine groups while the peak with BE of 400.3 eV can be ascribed to nitrogen in primary amines or imines.^{45–47} After loading copper ions, BEs of N 1s in 2-APY modified silica particles shifted to 399.3 eV and 401.2 eV, respectively (Fig. 2d). The increase in BEs of N 1s indicates that the lone pair electrons in the nitrogen atoms were donated to form a shared bond between Cu(II) ions.⁴⁵

3.2 Evaluation of the catalytic activity of the prepared catalyst

The catalytic activity of the prepared catalyst was evaluated by the oxidative degradation of RhB with hydrogen peroxide. The control experiments, which consisted of RhB/catalyst or RhB/ H_2O_2 , were also carried out under the otherwise identical conditions. Fig. 3a displays the experimental results. It is seen that RhB was hardly decomposed in catalyst/RhB and RhB/ H_2O_2 reaction systems. These results suggest that neither the adsorption of RhB on the catalyst nor the direct oxidation by H_2O_2 was important. However, RhB was significantly degraded in the RhB/ H_2O_2 /catalyst system. After 6 hours reaction, 94.6% RhB was decolorized. Meanwhile, 0.38 mg L^{-1} of copper ions were detected in the reaction solution, accounting for 0.08% of copper loaded on the catalyst. The lower leaching degree of copper ions, on the other hand, indicates that the prepared catalyst was stable. To exclude the catalytic activity was not due to the leached copper ions, 0.4 mg L^{-1} of copper ions were used to catalyze H_2O_2 for RhB degradation under otherwise identical conditions. But no significant degradation of RhB was observed during 6 h reaction (the data not shown). Accordingly, the degradation of RhB with H_2O_2 was mainly dominated by the heterogeneous reaction catalyzed by the prepared catalyst. It should be pointed out that the leached copper ions in the reaction solution were also lower than the discharge standard ($\sim 1 \text{ mg L}^{-1}$) suggested by the Environmental Protection Agency.²⁹ This means the treated contaminants could be directly discharged into the sewage system.

Fig. 3b displays the temporal change of UV-vis spectra of RhB in the heterogeneous catalyst/ H_2O_2 /RhB system. It is seen that the characteristic band of RhB centered at 553 nm decreased continuously with the reaction time prolonged but did not shift

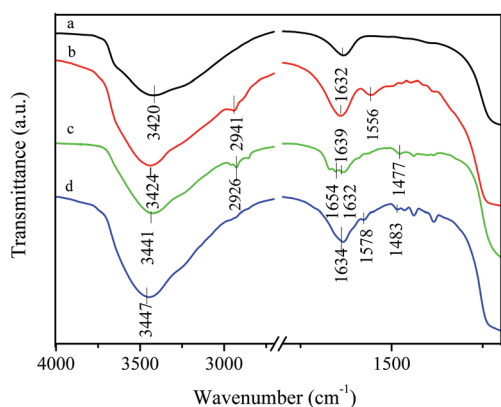


Fig. 1 FT-IR spectra of (a) SiO_2 , (b) APS modified SiO_2 , (c) 2-APY modified SiO_2 , and (d) 2-APY modified SiO_2 after loading Cu(II) .



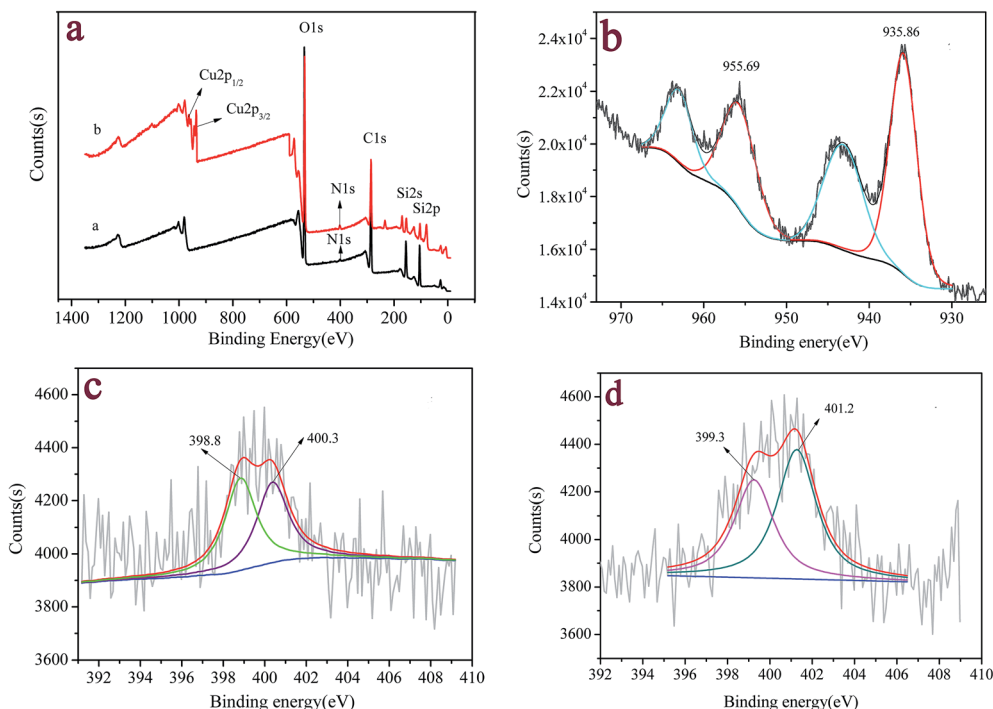


Fig. 2 (a) XPS survey spectra of 2-APY modified SiO_2 before (curve a) and after loading Cu(II) (curve b), and the corresponding high-resolution XP spectra for (b) Cu 2p, and N 1s (c) before and (d) after loading Cu(II) .

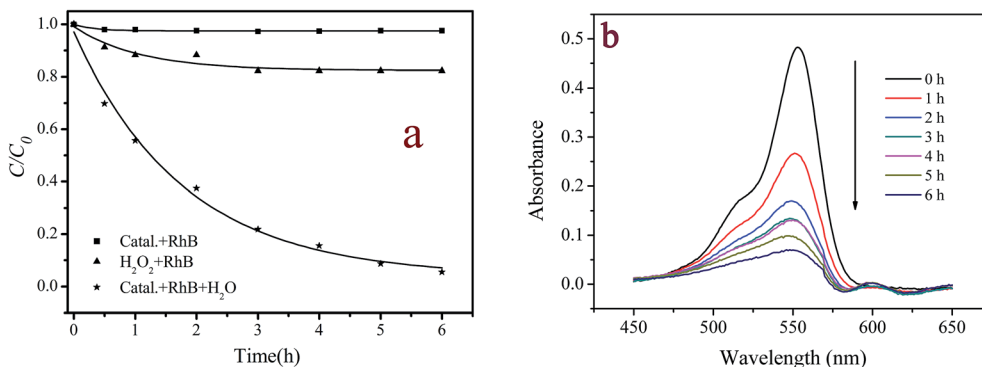


Fig. 3 (a) Degradation of RhB and H_2O_2 under the different conditions and (b) changes in UV-vis spectral of RhB during the catalytic degradation process. ($[\text{RhB}] = 5 \text{ mg L}^{-1}$; $[\text{catalyst}] = 2 \text{ g L}^{-1}$; $[\text{H}_2\text{O}_2] = 200 \text{ mg L}^{-1}$; $\text{pH} = 7.1$; $T = 20 \text{ }^\circ\text{C}$).

to shorter wavelengths. This finding indicates that the chromophore group in RhB molecule structure was destroyed during the reaction.^{48,49} As the decolorization of dyes did not mean their complete degradation, the mineralization degree and the toxicity evolution of RhB during the treatment were also monitored by measurement of the changes in TOC and *Vibrio fischeri* light inhibition for 10 mg L^{-1} RhB solution. The TOC values of the reaction solution were observed gradual decrease from 7.52 to 2.14 mg L^{-1} during an 11 hour reaction, *i.e.*, TOC removal achieved 72% (see Fig. S3, ESI†). The original 10 mg L^{-1} RhB solution was found to be extremely ecotoxic to *Vibrio fischeri* since bioluminescence was fully inhibited. However, after 8 h of oxidation, the toxicity was almost completely eliminated, as indicated by 8.6% light inhibition (Fig. S3, ESI†).

These results demonstrate that the prepared catalyst/ H_2O_2 system not only could fade RhB solution but also could decompose the reaction products completely for the greater part to reduce their toxicity.

3.3 Affecting factors and kinetics

3.3.1 Effect of pH. pH is considered as the most influential variables regarding the effectiveness of Fenton process. Therefore, the effect of solution pH on RhB degradation in the prepared catalyst/ H_2O_2 system was first studied. Fig. 4 shows that the degradation of RhB was strongly dependent on the initial pH of the solution. When the initial pH value of the solution increased from 3.1 to 6.2, the degradation efficiency of RhB within 6 hours sharply increased from 37.4% to 82.2%.



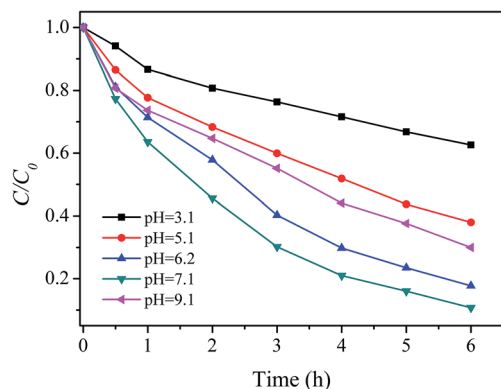


Fig. 4 Effect of pH on RhB degradation ($[\text{RhB}] = 5 \text{ mg L}^{-1}$; $[\text{catalyst}] = 2 \text{ g L}^{-1}$; $[\text{H}_2\text{O}_2] = 150 \text{ mg L}^{-1}$; $T = 20^\circ \text{C}$).

Subsequently, this trend slowed down; at pH 7.1, 89.9% of RhB was removed within 6 hours of reaction. However, the further increase of pH (>7.1) caused the degradation efficiency to decrease to 70.0% at pH 9.1. Therefore, the optimum pH range 6–7 was found to degrade RhB by the prepared catalyst and H_2O_2 . Most studies concerning Fe-based Fenton or Fenton-like catalytic systems claimed that the optimum working pH was situated in the range 3–4.^{4,50} Out of this interval the efficiency of the treatment experiences strong reduction.^{4,29} In this regard, the prepared catalyst/ H_2O_2 system is superior to the conventional Fenton and Fenton-like systems in the practical application.

The higher or lower pH resulted in reducing degradation efficiency of RhB in this study could be explained as following: the decrease in rate with increasing proton concentration may be ascribed to the lower deprotonation constant of H_2O_2 in acid medium as well as to protonation of the dye amino groups. The former effect will lead to a decrease in the possibility of formation of the peroxy-complex by eqn (4) (see below), whereas the latter effect will decrease the possibility of dye molecules accessing catalyst due to the electrostatic repulsion. As a result, the degradation rate of RhB decreased with increasing proton concentration. As for the lower removal rate and efficiency at pH 9.1, several reasons may be contributed to this result together, such as auto-decomposition of H_2O_2 at alkaline condition, the

decrease in the oxidation potential of hydroxyl radical with increasing pH as well as the electrostatic repulsion between the negatively charged the catalyst and dye anionic at alkaline condition.⁵¹

3.3.2 Effect of catalyst loading. Fig. 5a presents the influence of catalyst loading on the catalytic degradation of 5 mg L^{-1} RhB. It is seen that the degradation of RhB over the heterogeneous catalyst/ H_2O_2 systems followed pseudo-first order kinetics. The first-order kinetic equation can be written as

$$\ln\left(\frac{C_t}{C_0}\right) = -kt \quad (2)$$

where k is the pseudo-first-order rate constant, C_t and C_0 are the initial concentration and the concentration at time t , of RhB, respectively.

The fitted results are listed in Table S1 (ESI[†]). Fig. 5b displays the pseudo-first order rate constant (k) as function of catalyst concentration. As seen from Fig. 5b, k increased near linearly with the increase in the catalyst loading up to 3 g L^{-1} . Above this loading, k almost was independent on the concentration of catalyst reaching a maximum. The initial concentration of H_2O_2 and the available catalyst surface may be responsible for the finding experimental results. Generally, the number of active site increases with increasing catalyst amount. Therefore, the faster degradation of RhB was obtained at the higher concentration of the catalyst. Nevertheless, when catalyst concentration was larger than a certain value, the catalytic performance might be restrained either by the limited H_2O_2 concentration in the reaction system or by loss of surface active sites available for H_2O_2 due to agglomeration of catalyst, which could be further corroborated by the decomposition of H_2O_2 with varying amount of the catalyst in Fig. S4.[†] Consequently, the addition of higher concentration of catalyst did not obviously improve the degradation rate of RhB. The similar phenomena have been extensively reported in the heterogeneous catalytic processes.^{9,12,52}

3.3.3 Effect of H_2O_2 concentration. H_2O_2 concentration is a key parameter in Fenton or Fenton-like oxidation process. The effect of H_2O_2 concentration on RhB degradation is shown in Fig. 6a. It can be seen that the pseudo-first-order kinetic model fitted RhB degradation well, and the fitted results are presented

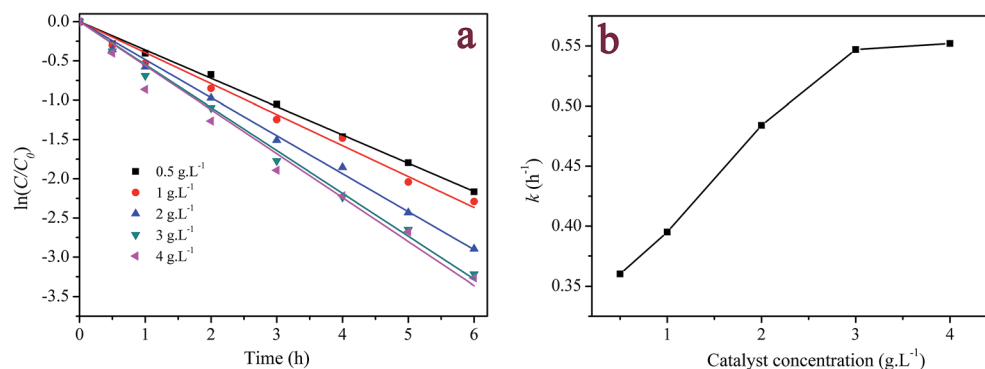


Fig. 5 Effect of catalyst loading on RhB degradation: (a) first-order plot for dye degradation; (b) dependency of the measured first-order constant on catalyst concentration. ($[\text{RhB}] = 5 \text{ mg L}^{-1}$; $[\text{H}_2\text{O}_2] = 200 \text{ mg L}^{-1}$; $\text{pH} = 7.1$; $T = 20^\circ \text{C}$).



in Table S1† as well. When H_2O_2 concentration increased from 0 to 150 mg L^{-1} , the pseudo-first order rate constants for RhB degradation increased from 5.40×10^{-3} to 0.453 h^{-1} . Meanwhile, the degradation efficiency in 6 hour reaction increased from 2.4% to 89.9%. A further increase in H_2O_2 concentration from 200 to 300 mg L^{-1} led to the smaller increase in rate constant (0.484 h^{-1} to 0.665 h^{-1}) and degradation efficiency (94.6% to 96.4%).

When $1/k$ was plotted against $1/[\text{H}_2\text{O}_2]_0$, a linear relationship was found between both of them (see Fig. 6b), that is, $k = 6.97 \times 10^{-3} [\text{H}_2\text{O}_2]_0 / (1 + 8.23 \times 10^{-3} [\text{H}_2\text{O}_2]_0)$. This result indicates that the degradation rate of RhB increased with increasing initial concentration of H_2O_2 but reached saturation at a high concentration of H_2O_2 . According to this saturation kinetics, we speculated that similar to the enzyme catalytic reaction, H_2O_2 bound to the catalyst before oxidizing dye. The effect of H_2O_2 concentration on RhB degradation could be explained as following: the more H_2O_2 was used, the larger amount of $\cdot\text{OH}$ would be produced. Therefore, the degradation efficiency and rate increased with the increase in H_2O_2 concentration. However, when the excessive H_2O_2 was used, the catalytic active sites on the catalyst might be saturated by H_2O_2 or $\cdot\text{OH}$ radicals might be scavenged by excess H_2O_2 according to eqn (10) forming a less reactive hydroperoxyl radicals. Consequently, the dye removal was less influenced by varying H_2O_2 concentration at high levels.

3.3.4 Effect of initial RhB concentration. The effect of the initial concentration of dye on RhB degradation was performed by varying the initial concentration of RhB between 2.5 and 12.5 mg L^{-1} . The results are shown in Fig. 7a. Once again, the degradation of RhB was well described by the pseudo-first order kinetic model ($R^2 > 0.992$) (see Table S1 in ESI†). When the concentration of RhB increased from 2.5 mg L^{-1} to 12.5 mg L^{-1} , the degradation efficiency and pseudo-first order rate constants reduced from 99.2% to 81.2%, and 0.574 h^{-1} to 0.306 h^{-1} , respectively. The first-order rate constant depended on the initial concentration of RhB, suggesting that it is not a true, but rather a pseudo-first order reaction with respect to dye concentration. The negative effect of the initial concentration of RhB on its decolorization efficiency and pseudo-first-order rate constant could be explained as follows: since the amount of

hydrogen peroxide molecules initially present in the reactor was the same, the generated active species were almost constant. When the initial concentration of dye was increased, more dye molecules and intermediates would compete for the oxidative species.⁵³ As a result, the intact dye molecules increased. Considering this result, it is speculated that the oxidation reaction was rate limiting-step; otherwise the zero-order reaction should be observed.

Although decolorization efficiencies decreased with increasing the initial concentration of RhB, the amounts of the degraded RhB increased with the increase in the concentration of RhB. Thus a further analysis was carried out on the initial degradation rate (r_0) and the initial dye concentration (C_0), where the initial rate was determined from the linear fit of the first three experimental points. Plotting $1/r_0$ versus $1/C_0$ gives a straight-line in Fig. 7b, that could expressed as

$$\frac{1}{r_0} = 1.72 + \frac{5.89}{C_0} \quad (3)$$

Eqn (3) is analogous to the Langmuir–Hinshelwood kinetic model. That is, the initial dye concentration has a first-order dependence on RhB concentration at lower concentration. However, with increases of RhB concentration the order of reaction decreases and almost attains a limiting rate at higher concentrations. As shown in Section 3.2, the adsorption of RhB on the catalyst was negligible. This result could be alternatively explained by the competition among dye and other reactants for a certain amount of the reactive species such as hydroxyl radicals.

3.4 Stability of the catalyst

The stability of the prepared catalyst was evaluated by four consecutive experiments at the same reaction conditions, and the results are shown in Fig. S5.† It is seen that after 4-time recycles the degradation rate of RhB was slightly slowed down. The first-order rate constants changed from 0.484 h^{-1} (1st cycle), 0.468 h^{-1} (2nd cycle), 0.387 h^{-1} (3rd cycle), to 0.378 h^{-1} (4th cycle). Meanwhile, the degradation efficiency of RhB in the 4th cycle was still larger than 90%. These findings, on the other hand, are consistent with the result obtained in Section 3.2,

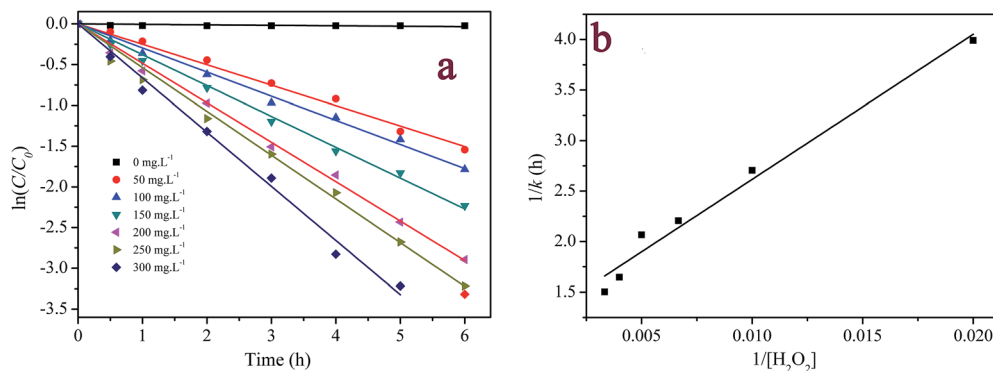


Fig. 6 Effect of H_2O_2 concentration on RhB degradation: (a) first-order plot for dye degradation; (b) a plot of $1/k$ versus $1/[\text{H}_2\text{O}_2]_0$. ($[\text{RhB}] = 5 \text{ mg L}^{-1}$; $[\text{catalyst}] = 2 \text{ g L}^{-1}$; $\text{pH} = 7.1$; $T = 20 \text{ }^\circ\text{C}$).



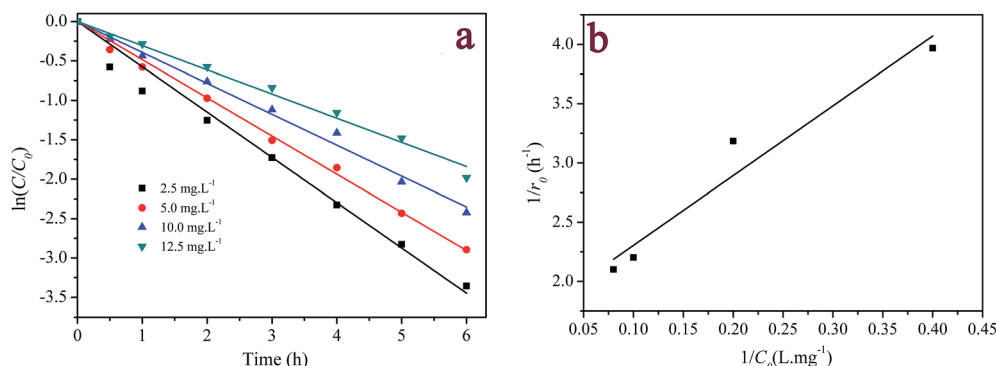


Fig. 7 Effect of initial dye concentration on RhB degradation: (a) first-order plot for dye degradation; (b) the relationship between the initial rate and dye concentration, ($[\text{catalyst}] = 2 \text{ g L}^{-1}$; $[\text{H}_2\text{O}_2] = 200 \text{ mg L}^{-1}$; $\text{pH} = 7.1$; $T = 20 \text{ }^\circ\text{C}$).

where the leaching of copper ions was found to be insignificant (about 0.38 mg L^{-1}). Accordingly, it can be concluded that Cu(II)-pyridyl complex immobilized on silica particle is a stable and effective catalyst for destroying organic contaminants with H_2O_2 at neutral pH conditions. Moreover, the developed catalyst could be easily recycled from the reaction solution by a simple filtration and could reduce the potential pollution caused by copper ions and pyridine in the homogenous Cu(II)/pyridine/ H_2O_2 process.

3.5 Reaction mechanisms

3.5.1 Estimating activation energy of the reaction. The effect of the reaction temperature on RhB degradation using the prepared catalyst and H_2O_2 at pH 7.1 are depicted in Fig. 8. As seen from Fig. 8, the degradation of RhB was accelerated with the increase of the reaction temperature. In order to calculate the activation parameters, the first 2 hour reaction data were fitted with pseudo-first order kinetic model to extract the rate constants (k) and the results are listed in Table S2 (ESI[†]). The inset in Fig. 8 shows a plot of $\ln k$ versus $1/T$, from which the activation energy (E_a) of the reaction was calculated according to the Arrhenius law. Other activation parameters, such as enthalpy (ΔH^\ddagger) and entropy (ΔS^\ddagger) of activation were also

determined from Eyring's equation and presented in Table S2.[†] The activation energy of $38.60 \text{ kJ mol}^{-1}$ is smaller than $82.53 \text{ kJ mol}^{-1}$ reported by Gan and Li for the degradation of RhB using rice hull-based silica supported iron as Fenton-like catalyst,⁹ but larger than 21.8 kJ mol^{-1} for degradation of Orange II by the photo-assisted Fenton process using Cu/MCM-41 catalyst.²⁹ The negative entropy of activation suggests that an ordered transition state was achieved.

3.5.2 Hydroxyl radical's detection and inhibition. $\cdot\text{OH}$ radical is known as a key active species in the Fenton processes. Therefore, the formation of $\cdot\text{OH}$ in the prepared catalyst/ H_2O_2 system was detected using coumarin fluorescence probing technique. This method has been widely used in detection of $\cdot\text{OH}$ radicals in various AOPs.^{37,54} Fig. 9 shows the variation of fluorescence intensity with the reaction time in coumarin/ H_2O_2 solution catalyzed by the prepared catalyst. It is clear to see that the fluorescence spectra of 7-hydroxycoumarin emerged with a maximum emission at 460 nm and the intensity steadily increased within an 80 minute incubation time. In contrast, no fluorescence was observed in the coumarin/ H_2O_2 system under the otherwise identical conditions. These results suggest that Cu(II)-pyridyl complex immobilized on silica particles could catalyze H_2O_2 to generate $\cdot\text{OH}$ radicals, and thus can be used to eliminate organic pollutants in water.

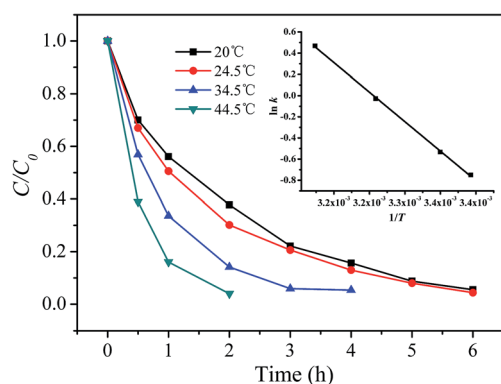


Fig. 8 Effect of temperature on the degradation of RhB. Inset shows a plot of $\ln k$ versus $1/T$. ($[\text{RhB}] = 5 \text{ mg L}^{-1}$; $[\text{catalyst}] = 2 \text{ g L}^{-1}$; $[\text{H}_2\text{O}_2] = 200 \text{ mg L}^{-1}$; $\text{pH} = 7.09$; $T = 20 \text{ }^\circ\text{C}$).

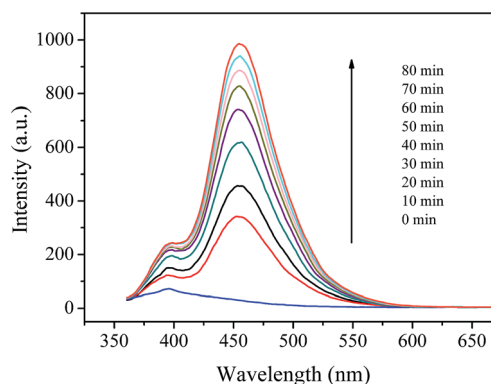


Fig. 9 Fluorescence spectral changes of the coumarin solution ($1 \times 10^{-3} \text{ mol L}^{-1}$) in the presence of 2 g L^{-1} catalyst and $200 \text{ mg L}^{-1} \text{H}_2\text{O}_2$ at pH 7.1.



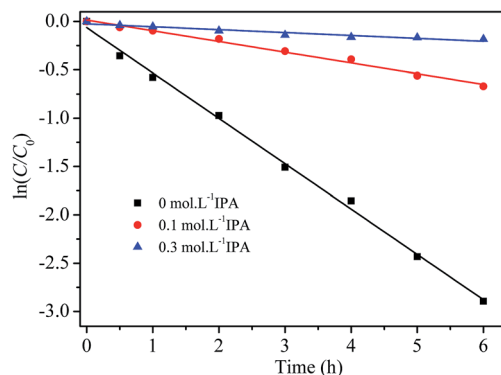
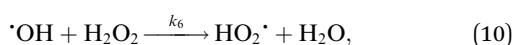
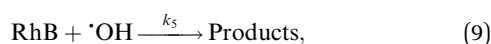
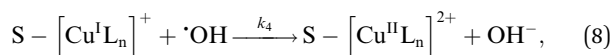
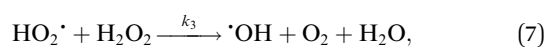
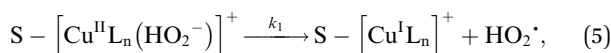
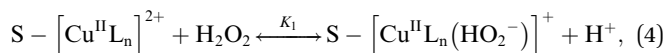


Fig. 10 Effect of free radical scavenger on RhB degradation by the prepared catalyst and H₂O₂ at 20 °C and pH 7.1.

To further verify the oxidative species involved in RhB degradation with H₂O₂ catalyzed by the prepared catalyst, isopropyl alcohol (IPA), a hydroxyl radical scavenger,¹⁷ was added into the reaction solutions, which contained 5 mg L⁻¹ of RhB, 2 g L⁻¹ of catalyst and 200 mg L⁻¹ of H₂O₂. Fig. 10 displays the experimental results. The degradation of RhB was obviously depressed by the addition of IPA. When 0.1 mol L⁻¹ and 0.3 mol L⁻¹ of IPA were added in RhB/H₂O₂/catalyst solutions, the pseudo-first order rate constants of RhB degradation were reduced by 77.1% to 0.111 h⁻¹, and by 93.8% to 0.030 h⁻¹, respectively. So it is inferred that ·OH radicals are main active species for the oxidative degradation of RhB in the prepared catalyst/H₂O₂ process.

3.5.3 Degradation mechanisms. On the basis of all the above experimental results and the previous reports in the literature,^{27,28,36,55-57} a possible mechanism for the degradation of RhB catalyzed by the prepared catalyst in the presence of H₂O₂ was thought as follows:



where S-[Cu^{II}L_n]²⁺ denotes catalyst.

From eqn (4) the concentration of the peroxo complex is given by

$$[S - [Cu^{II}L_n(HO_2^-)]^+] = K_1[S - [Cu^{II}L_n]^{2+}][H_2O_2]/[H^+], \quad (11)$$

Applying the steady-state approximation for the rate of free radicals and cuprous complex,

$$\begin{aligned} \frac{d[\cdot OH]}{dt} &= k_2[S - [Cu^IL_n]^+][H_2O_2] + k_3[HO_2^{\cdot}][H_2O_2] \\ &\quad - k_5[\cdot OH][RhB] - k_4[S - [Cu^IL_n]^+][\cdot OH] \\ &\quad - k_6[H_2O_2][\cdot OH] = 0, \end{aligned} \quad (12)$$

$$\begin{aligned} \frac{d[S - [Cu^IL_n]^+]}{dt} &= k_1[S - [Cu^{II}L_n(HO_2^-)]^+] \\ &\quad - k_2[S - [Cu^IL_n]^+][H_2O_2] \\ &\quad - k_4[S - [Cu^IL_n]^+][\cdot OH] = 0, \end{aligned} \quad (13)$$

and

$$\begin{aligned} \frac{d[HO_2^{\cdot}]}{dt} &= k_1[S - [Cu^{II}L_n(HO_2^-)]^+] \\ &\quad + k_6[\cdot OH][H_2O_2] - k_3[HO_2^{\cdot}][H_2O_2] = 0, \end{aligned} \quad (14)$$

Substituting eqn (11) into (13) and meanwhile assuming that $k_2[H_2O_2] \gg k_4[\cdot OH]$, we get

$$[S - [Cu^IL_n]^+] = \frac{k_1}{k_2} K_1 [S - [Cu^{II}L_n]^{2+}] / [H^+], \quad (15)$$

In addition, substituting eqn (11) into (14), and assuming that $K_1[S - [Cu^{II}L_n]^{2+}]/[H^+] \gg k_6[\cdot OH]$, we can get

$$[HO_2^{\cdot}] = \frac{K_1}{k_3} \frac{[S - [Cu^{II}L_n]^{2+}]}{[H^+]}, \quad (16)$$

From eqn (11), (12) and, (16) the concentration of hydroxyl radical is expressed as

$$\begin{aligned} [\cdot OH] &= \frac{K_1(k_1 + 1)}{k_2} \\ &\quad \times \frac{[S - [Cu^{II}L_n]^{2+}][H_2O_2]}{k_5[RhB][H^+] + k_6[H_2O_2][H^+] + \frac{k_1 k_4 K_1}{k_2} [S - [Cu^{II}L_n]^{2+}]}, \end{aligned} \quad (17)$$

The rate-determining step, eqn (9), expresses the rate equation and is given by

$$-\frac{d[RhB]}{dt} = k_4[RhB][\cdot OH] \quad (18)$$

Thus, by replacement of hydroxyl radical concentration in eqn (18) with (17), the degradation rate of dye can be given as



$$-\frac{d[\text{RhB}]}{dt} = K_1 k_4 (k_1 + 1) \times \frac{[S - [\text{Cu}^{\text{II}}\text{L}_n]^{2+}][\text{H}_2\text{O}_2][\text{RhB}]}{k_5[\text{RhB}][\text{H}^+] + k_6[\text{H}_2\text{O}_2][\text{H}^+] + \frac{k_1 k_4 K_1}{k_2} [S - [\text{Cu}^{\text{II}}\text{L}_n]^{2+}]}$$
(19)

Reaction (4) produces the proton while the reaction (6) generates the hydroxyl. Thus, the pH value of reaction solution was little affected by the reaction, which was in accord with less than 0.2 pH unit change observed in each experimental run. Hence, the concentration of the proton in a given experimental condition is approximately constant. From eqn (19), it is expected that when H_2O_2 concentration is far larger than that of dye the degradation of dye will follow pseudo-first-order kinetics. The apparent first-order rate constant increases with increase of the initial concentration of H_2O_2 or catalyst and reaches saturation at the larger concentration. However, the increase in dye concentration will reduce the pseudo-first-order constant. In addition, an expression similar to Langmuir-Hinshelwood model could be found between the initial rate and the initial dye concentration. All these predicated results are consistent with the experimental findings. Therefore, the proposed mechanism in some extent is reasonable for explaining degradation of RhB by H_2O_2 in the presence of the prepared catalyst.

4. Conclusion

In summary, a $\text{Cu}(\text{II})$ -pyridyl complex was successfully immobilized on silica particle through chemical bonding. The prepared catalyst was stable and efficient for degradation of RhB with H_2O_2 at near-neutral pH. The degradation of RhB in the prepared catalyst/ H_2O_2 heterogeneous system depended on solution pH, H_2O_2 concentration, catalyst loading, initial dye concentration and the reaction temperature. The optimum condition for RhB degradation was found to be: 200 mg L^{-1} H_2O_2 , 2 g L^{-1} catalyst, and pH 7.1. Under this condition, the degradation efficiencies of RhB (5–7.5 mg L^{-1}) were more than 98% within 6 hours reaction. The mineralization of RhB also achieved to a large extent. The degradation of RhB could be well described with pseudo-first order kinetic model. The reaction activation energy was about 38.60 kJ mol^{-1} . Hydroxyl radical was the primary active species for RhB degradation. This study further indicates that immobilizing $\text{Cu}(\text{II})$ -pyridyl complexes on silica particles would be a good strategy to fabricate the new Fenton-like catalyst for eliminating the refractory organic pollutants in aqueous solution under near-natural condition.

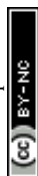
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